

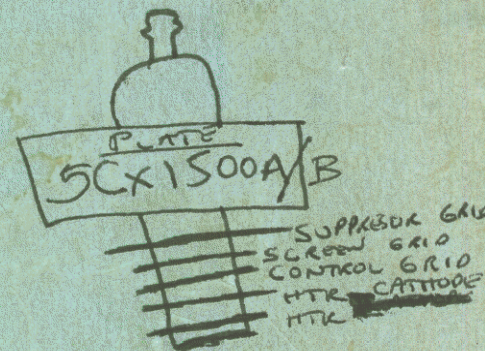


INSTALLATION AND MAINTENANCE MANUAL

FOR

FM-12KD & FM-25KD

FM BROADCAST TRANSMITTERS



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AERICAN **E**LECTRONIC **L**ABORATORIES

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AMERICAN ELECTRONIC LABORATORIES, INC.

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TELEPHONE - 215-822-2929

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SECTION I
GENERAL INFORMATION

1-1 Introduction

This manual contains information required to install, operate and maintain the American Electronic Laboratories FM Transmitters, Model FM-25KD and Model FM-12KD. These transmitters are rated at 25KW and 12KW output respectively. The circuitry, operation, and maintenance of these two models are so similar that this one manual will be used to detail all information necessary for proper utilization of the units. Where specific differences exist between the transmitters, these will be pointed out in the descriptive text. Where there is identity between units, general references will be made to "the transmitter" or to "the driver stage", etc.

Section I describes the transmitters and their respective specifications, Section II provides installation instructions, Section III contains operating procedures and Section IV describes the principles of operation. Maintenance procedures and trouble shooting diagrams are contained in Section V, and replaceable parts are identified and listed in Section VI. A complete operating and servicing manual covering the Model 2202A FM Exciter is included as a part of this manual

1-2 General Description

The Model FM-25KD FM Transmitter, also typical of the Model FM-12KD, see frontispiece photographs, consists of an AEL Model 2202A FM Exciter, two-stage RF amplifier and power supply, low-pass harmonic filter, and RF directional couplers. One coupler monitors forward or reflected power between the FM exciter and



Frontispiece. FM-25KD FM Transmitter, Front View

the driver grid input circuit. The second performs a similar function at the output of the harmonic filter into the transmission line. The FM-25KD transmitter provides an output of 10 to 25 kilowatts and the FM-12KD an output of 5 to 12 kilowatts in the frequency range of 88 to 108 MHz, they are type accepted by the Federal Communication Commission for use under Part 73, Broadcast Services.

The Model 2202A FM Exciter is a solid-state unit that provides monaural FM and, with an AEL Model 2213 Stereo Generator, full stereo modulation. Subsidiary Communication Authorization (SCA) mode of operation is also available with the use of a Mosely SCG-4T SCA Generator. The exciter modulation method is "direct FM" at the assigned carrier frequency and employs automatic frequency control by comparing the modulated oscillator frequency to a temperature stabilized crystal oscillator.

1-2.1 Physical Characteristics

Physical characteristics of the transmitters, excluding the Model 2202A FM Exciter and Model 2203 Stereo Generator, are given in Table 1-1.

Table 1-1. Physical Characteristics

Cabinet Dimensions	→ 77½"H x 48"W x 36"D (overall) 77½"H x 48"W x 33"D (trim & doors removed)
Weight	2000 lbs. approx., 1800 lbs. approx. (FM-25KD) (FM-12KD)
Floor Loading	162 lbs./sq. ft. approx.
Cabinet Style	Enclosed steel cabinet; access through front doors & quickly removable panels, swing-down centrally-located meter and control panel, rear doors.

Input/Output Connections

a. RF Output	3-1/8 inch coaxial line flange
b. Sampled RF Output to Station Monitor	Type BNC coaxial
c. Audio Inputs (to FM Exciter)	
Composite Stereo	Type BNC coaxial
SCA	Type BNC coaxial
Monaural	Barrier terminal strip
Ambient Temperature	Storage: -20°F to +120°F Operating: 20°F to +113°F
Altitude	7,500 ft. maximum
Harmonic Filter/ Coupler	58-5/8" long with 3-1/8" EIA flanges each end. Mounts externally. Coupler has two pairs of BNC output connectors. One pair for forward & reflected power at a 30 KW level--the other pair for a 15 KW level.
Cooling Provisions	Self-contained blowers plus a rear door filtered air intake fan for positive cabinet pressure.

1-2.2 Functional Characteristics

Functional characteristics of the transmitters, including the Model 2202A FM Exciter, are given in Table 1-2.

Table 1-2. Functional Characteristics

Frequency Range	88 to 108 MHz
Modulation	F3, F9
Power Output	10 to 25 KW capability - FM-25KD 5 to 12 KW capability - FM-12KD
Load Impedance	50 ohms (nominal)
VSWR	2:1 maximum
FM Noise	-63 db (max.)
AM Noise	-55 db (max.)

Table 1-2. Functional Characteristics (cont'd)

Harmonic & Spurious Output	Exceeds FCC requirements
Power Source	200 to 240 volts, 60 Hz, 3 phase, 90% power factor, $\pm 5\%$ regulation.
Power Consumption	42 KVA (at 90% power factor), 200 Amp Service (for 25 KW output) 26 KVA - for FM-12KD, 100 Amp Service
Tube Types	3CX15000A7 (PA) - FM-25KD 3CX10000A7 (PA) - FM-12KD 4CX1000K (Driver)
Deviation Capability	± 100 KHz
Frequency Stability	± 1 KHz
Monaural Input	600 ohms balanced +10 dbm ± 2 db for ± 75 KHz deviation
Monaural Response	50-15,000 Hz, ± 1 db
Monaural Pre-emphasis	75 μ sec. standard
Monaural Distortion	0.5% THD max. (50-15,000 Hz)
Controls and Indicators	See Table 3-1

1-3 Accessories

Each transmitter is supplied with the following accessories:

- a. One Printed Circuit Card Extender
AEL Part No. 3152853-1
- b. Two Insertion/Extraction Levers for PA Tube
AEL Part No. 2155500-1

The card extender permits measurement of printed circuit operating parameters. The tube installation levers permit easily controlled insertion and seating of the PA tube in its socket as well as convenient, gradual extraction for replacement purposes.

1-4

Optional Equipment

Available optional equipment consists of the following items:

- a. Stereo Generator, AEL Model 2213
- b. SCA Generator, Moseley Model SCG-4T
- c. FM-12KD option - Remote Power Control
- d. FM-12KD option - Automatic VSWR Protection

SECTION II

INSTALLATION

2-1 Installation Planning

Dimensions required for proper installation of the Model FM-25KD FM Transmitter are shown in Figure 2-1.

2-1.1 Environmental Requirements

Location of the Model FM-25KD must be within an environment that satisfies the following limits:

- a. Maximum altitude 7,500 ft.
- b. Maximum temperature +113°F
- c. Minimum temperature +20°F

2-1.2 Space Requirements

When installing the Model FM-25KD, it is important that sufficient space be left at the front and rear to permit full opening of all access doors and swing-down control panel. As shown in Figure 2-1, at least 25 inches of space must be provided in front of the cabinet and the unit should be placed with the rear surface no closer than 25 inches from the wall.

Adequate overhead space must also be provided to permit installation of the harmonic filter and to allow for adequate dispersal of air discharged through the cabinet top. A minimum distance of two feet from the cabinet top to the ceiling is recommended.

2-1.3 Power Requirements

Requirements for input power and power consumption are provided in Table 1-2, functional characteristics, in Section I.

2-1.4

Cooling Requirements

The external cooling requirements for the FM-12KD and FM-25KD must be such so as to prevent the ambient temperature from rising above the maximum specified in paragraph 1-2.1 (113°F). This would most likely occur during hot summer weather in a small closed transmitter building.

Under these conditions the user must be prepared to circulate external air through the transmitter room at a rate of at least 1000 cubic feet per minute for the FM-12KD and a rate of at least 1500 CFM for the FM-25KD. Inlets for cool air should be provided so that natural flow into the transmitter input air filters is possible. An output wall fan or hot air duct should carry off the exhausted hot air at the required rate.

During the cooler winter months, the transmitter exhaust may be utilized to heat the transmitter building. It is suggested that a thermostat element be used to turn on the building exhaust fan when the room temperature rises above 80°.

The FM-12KD at full output exhausts air at a rate of 900 CFM with a heat rise of 75°F above ambient temperature.

The FM-25KD heat rise is 95° F above ambient at a volume of 1500 CFM when operated at 25KW output.

If air conditioning is to be used for transmitter room temperature control it is suggested that a qualified air conditioning engineer be consulted to ensure that sufficient cooling capacity is provided.

A minimum clearance of 2 feet is suggested above the top of the transmitter as being sufficient space so as not to create any back pressure on the cooling system and causing reduction of air flow rate.

2-2 Unpacking and Inspection

Inspect the equipment for shipping damage as soon as it is unpacked. Check for broken knobs, tubes, meter faces, and connectors. Inspect surfaces for dents and scratches. If the equipment is damaged in any way, notify the carrier immediately and report the damage.

2-3 Input and Output Connections

The PA RF output will come out of the cabinet via a 3-1/8" EIA flange and a 90° elbow to the Harmonic Filter/Coupler. RF output to the station monitor will be brought out from BNC style connector, identified as 2J2 on P.A. cavity wall. Audio inputs and control lines will be brought in by means of grommets holes in the lower left side of the cabinet rear.

2-3.1 RF Input/Output Connections

The RF input and output connections are made to the transmitter as follows:

- a. A short length of RG-58/U coaxial cable with BNC connectors at each end is connected between the exciter RF OUTPUT jack and the exciter directional coupler, 1DC1, mounted on the right wall of the transmitter cabinet just to the rear of the exciter.
NOTE:- A 50 ohm attenuator box may also be used between the exciter and the directional coupler. The attenuation is usually 2 db or 3 db. This is used to stabilize tuning VSWR variations on the FM

exciter. The output of the directional coupler should be connected to the DRIVER RF INPUT jack, 2J1 located at the upper rear of the driver cavity. Ensure that these connectors are firmly in place.

- b. Using a 3-1/8 inch 90° coaxial elbow, connect the PA RF output coaxial line to the Harmonic Filter/Coupler.
 - c. Using RG-58/U coaxial cable and BNC coaxial connectors, connect station monitor to jack 2J2 located on rear of P.A. enclosure.
 - d. RF output for ALC circuits is obtained at 2J3.
- A large chassis ground terminal is provided for connecting the transmitter main frame to system or building ground.

NOTE

It is essential that the exact primary voltage be determined before connecting the primary windings of the PA filament transformer (1T), the bias transformer (2T3) and the plate transformer (1T4). See appropriate photos with parts call-outs for location. Typically, taps are provided at each end of transformers 1T1, 1T4, and 2T3 and are arranged as shown below in Figure 2-2. The 3-phase transformer, 1T4, of course, has each winding tapped in this manner. A primary voltage range of 180 to 260 volts can be accommodated. Refer to Tables 2-2 and 2-3 for the proper plate potentials to be used for specific legal power levels. Adjust the taps of 1T4 to provide the indicated plate voltages.

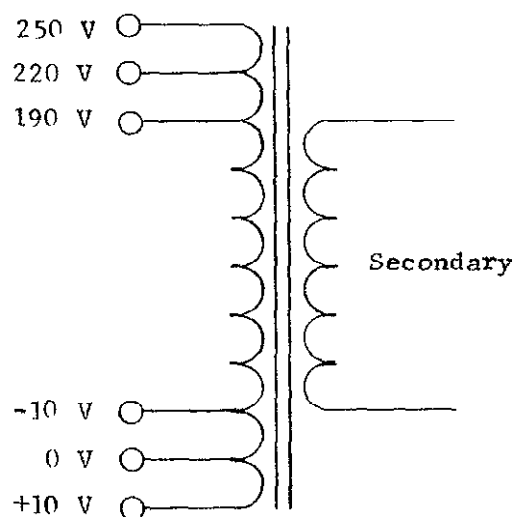


FIGURE 2-2

TABLE 2-1

REMOTE CONTROL FUNCTIONS

<u>TERM</u>	<u>FUNCTION</u>
1.	Pre-Heat/After-Cool Line
2.	+24 Volts Control Voltage
3.	START/STOP Line
4.	STOP & Interlock Line Return
5.	Interlock
6.	Reset Line (Momentary return to #2)
7.	Plate ON/OFF Interlock or Plate Voltage Remote Control
8.	" " " " " " " "
9.	PA Plate Voltage - remote read (+)
10.	PA Plate Current - remote read (-)
11.	Power Output - Ground
12.	Power Output - Remote Read (-)
13.	Remote Raise Power
14.	Remote Lower Power
15.	Ground

TABLE 2-2

FM-25KD OPERATING DATA

Frequency = 98 MHz

	25 KW	20 KW	15 KW	12 KW	10KW
PA Plate Current	4.4 Amp	3.5 Amp	2.8 Amp	2.2 Amp	2.0 Amp
PA Cathode Current	5.3 A	4.1 A	3.2 A	2.5 A	2.5 A
PA Plate Voltage	7.6 KV	7.6 KV	7.2 KV	7.2 KV	6.8 KV
Efficiency	75%	75.2%	74.5%	75.8%	73.5%
Driver Cath. Current	0.70 Amp	0.54 A	0.46 A	0.40 A	430 MA
Driver Plate Voltage	3.35 KV	3.4 KV	3.3 KV	3.4 KV	3.1 KV
PA Cathode Resistance	12.5 ohms	17 ohms	25 ohms	50 ohms	50 ohms

TABLE 2-3

FM-12KD OPERATING DATA

Frequency = 98 MHz

	12 KW	10 KW	8 KW	6 KW	5 KW
PA Plate Current	2.45 A	2.0 A	1.85 A	1.4 A	1.25 A
PA Cathode Current	2.85 A	2.35 A	2.2 A	1.6 A	1.4 A
PA Plate Voltage	6.4 KV	6.5 KV	5.7 KV	5.8 KV	5.8 KV
Efficiency	76.5 %	76.8 %	75.7 %	74 %	69 %
Driver Cath. Current	0.54 A	0.39 A	0.40 A	0.31 A	0.27 A
Driver Plate Voltage	2.9 KV	3.0 KV	2.6 KV	2.7 KV	2.75 KV
PA Cath. Resistance	50 ohms	50 ohms	50 ohms	100 ohms	100 ohms
Pi Loading Cap. (2C44 & 2C45)	125 pf	125 pf	150 pf	150 pf	150 pf

2-3.2 Primary Power and Grounding Connections

Primary power connections are made through the floor of the transmitter cabinet to a heavy duty terminal block 1TB3. Minimum cable size shall be No. 2. The safety disconnect switch supply, the primary power to the transmitter should be rated at 200 amperes for the FM-25KD and 100 amperes for the FM-12KD. A separate terminal is provided on 1TB3 for the three-phase neutral lead. CAUTION Consult your local power company's engineering department to determine if the "neutral" is a true symmetrical neutral line or as in some power systems is an artificial center-tap connection between two of the three phases. If the later is the case, carefully measure to determine which phases the artificial neutral is related to and connect these two phases to terminals #1 and #2 of 1TB3. Connect the remaining 3-phase wire to terminal #3. The internal single phase neutral return line is brought out to a separate terminal 1TB4-4 and identified as "NEUTRAL RETURN". Connect a jumper wire (#16) between this terminal and the incoming "neutral" for the power system. This will insure that the single phase circuits (fan 1B1, blower 2B2, and relays 3K18 and 3K19) are provided proper operating voltages.

The local electrical code will specify whether it is permissible to connect the neutral of the power system to ground or to let it "float". Consult your local power company or electrical contractor before proceeding.

2-3.3

Exciter Input Connections - See Model 2202A Manual

Refer to Figure 3 "FM Exciter - Rear View" and the transmitter schematic diagram which show the location of input connectors and patching circuits. Going from left to right, the following connectors and controls are located on the lower rear deck of the FM Exciter chassis.

- a. A three-wire AC connector with the center conductor connected to chassis ground.
- b. A three-terminal barrier strip (TB2) makes provision for local AC power control from a front panel switch by placing a jumper from terminal 1 to 2.
- c. The SCA input is injected into the AF input circuits via a BNC connector. There is no level control for this input. The level must be adjusted at the SCA generator.
- d. The RF output from the 10-watt solid-state amplifier of the exciter unit is also obtained from a BNC connector to be patched via an RG-58/U coaxial cable to the driver RF input connector at the upper rear portion of the driver RF compartment (2J1).

e. A six-terminal barrier strip (TB1) provides a patching capability for either the monaural or stereo mode of operation.

- (1) Monaural Operation. Place a jumper wire between terminals 4 and 5 and apply the AF signal to the balanced 600-ohm input terminals 1 and 3 with the ground connected to terminal 2. The modulation level can be adjusted by varying control R97.
- (2) Stereo Operation. Place a jumper wire between terminals 5 and 6 instead of 4 and 5. Apply the composite stereo signal to the BNC connector captioned STEREO INPUT. The modulation level can be adjusted by varying control R98.

2-4 Transmitter Remote Control

2-4.1 Both the FM-25KD and the FM12-KD may be operated remotely by using a local short run of control cable to a nearby operator's console. Remote operation via telephone line or microwave Studio-Transmitter Link is possible if an appropriate remote control unit is used.

2-4.2 Short Run Remote Control

Connections to the transmitter control circuits, power, voltage, and current monitoring points and power level control circuits are brought out on terminal board, 1TB2. Figure 2-3 shows the necessary connections that must be made to terminal board 1TB2 in order to functionally

remote control the transmitter. It must be understood that the remote meters must be calibrated to agree with the transmitter indicating panel instruments.

2-4.3 Remote Control via Telephone Line or STL

Selection of a remote control unit should include the facilities desired by the user and whose input and output characteristics are compatible with the remote control functions as shown in Figure 2-3. Note the polarities of the various metering signals available at 1TB2. The remote control unit selected must be capable of accepting either a positive or negative voltage for its conversion from voltage to audio frequency circuitry. The systems usually encountered have strapping terminals available so as to accept either polarity of metering signal. The operational functions on the remote control terminal represent "dry contact" relay closures and should be so connected.

Note that the "remote STOP" function is operated by the normally closed "back contacts" of a relay. The remaining functions are served by normally open relay contacts.

CAUTION: The Pre-Heat/After-Cool contacts must be closed momentarily on both START and STOP commands to insure proper time delayed operation. This will normally require two DPDT relays properly connected--one relay for remote START and one for remote STOP.

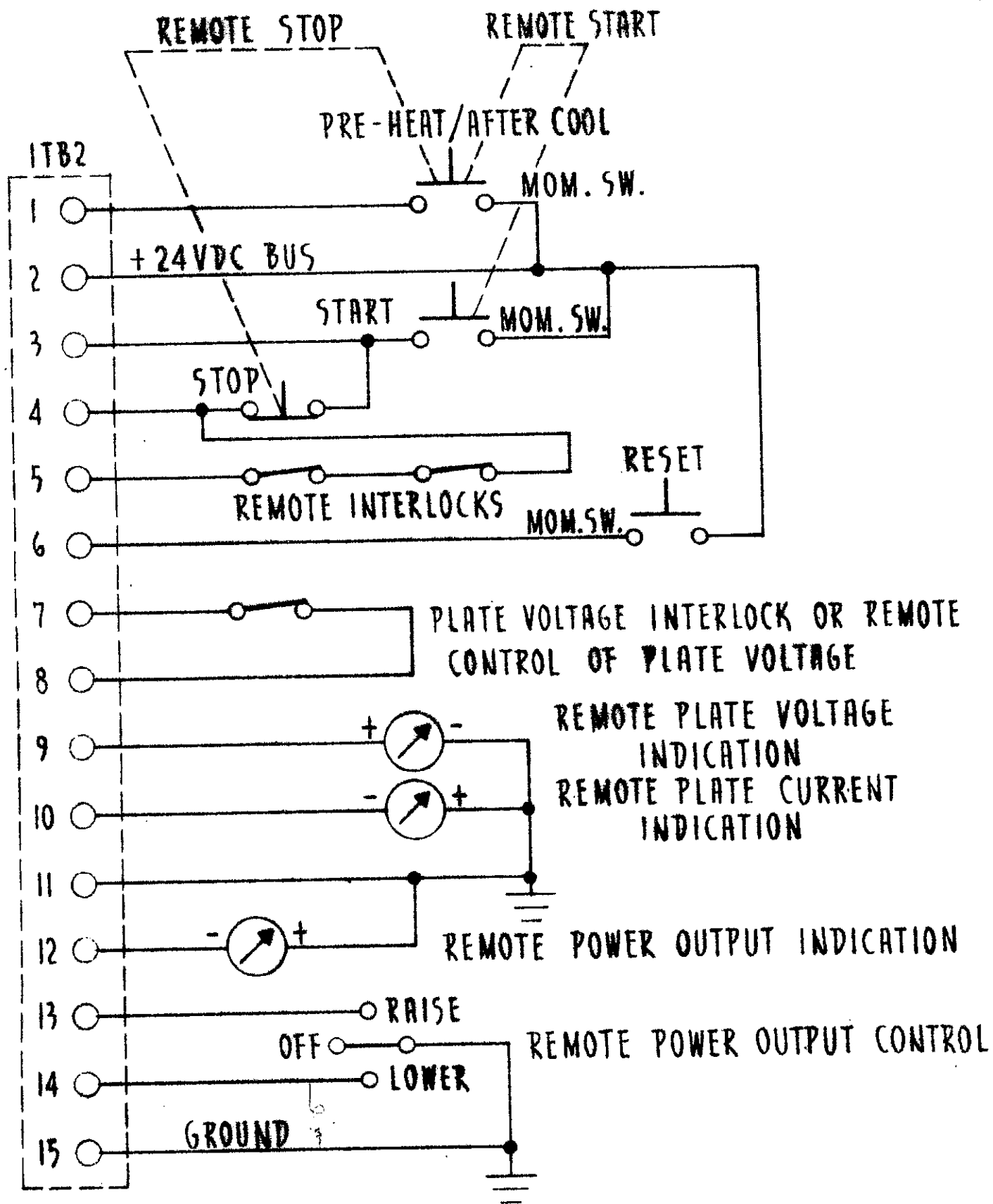


FIGURE 2-3. Remote Control Connection Diagram.

2-5 Initial Turn-On Procedures

2-5.1 Exciter Initial Turn-On

- a. Check the exciter front panel fuse (F1) and the fuse located behind the removable front panel near the power supply regulator (F2) to determine that they are of the proper value (1 ampere). When the fuses are properly installed and the power line safety switch for the transmitter is closed, power is applied to the crystal oscillator oven and FM oscillator chassis heater strips regardless of the position of the LINE switch on the exciter front panel. This feature provides an instant "on-frequency" condition, when the transmitter is turned on, since the heated areas are always at thermal equilibrium.
- b. While the exciter unit is properly tuned to the assigned operating frequency; it would still be wise to get acquainted with the RF tuning procedure. It would also ensure that nothing has happened in shipment that would impair performance.
 - (1) Set the RF OUTPUT LEVEL control to the maximum clockwise position.
 - (2) Operate the exciter LINE switch to the ON position.
 - (3) Set the meter selector switch to the B+ position and observe an indication of approximately 25 on the multimeter.
 - (4) Set the meter selector switch to the DRIVER position.
 - (5) Adjust the DRIVER TUNING for a minimum on the multimeter.

- (6) Set the meter selector switch to the OUTPUT position.
 - (7) Adjust the POWER AMP TUNING control for a maximum indication on the multimeter.
 - (8) Alternately adjust the DRIVER TUNING, DRIVER LOADING and POWER AMP TUNING for a maximum indication on the multimeter.
 - (9) Set the RF OUTPUT LEVEL control for the desired output power.
 - (10) Repeat Step 8.
- c. For maximum initial frequency accuracy and stability, the crystal and FM oscillator chassis should be allowed to warm up thoroughly before setting frequency. (One hour minimum.)
- d. Rotate the function switch to the LO position. With a small insulated tuning stick, adjust the LO coil (see Figure 2 of Model 2202A Manual). While adjusting the coil, a slowly rising reading will be indicated on the multimeter. The reading will rise to approximately 26 and then a sharp drop will occur. (This is the resonance characteristic of the crystal.) Reverse the tuning adjustment until the meter reading is on the slowly changing side of the crystal slope. Adjust for a reading of approximately 20.
- e. Rotate the function switch to the AFC position and operate the AFC disable switch to the disable position (switch toggle pointing toward the feedback adjust potentiometer).

- f. With an insulated tuning tool, adjust the FM oscillator tuning capacitor (located through front chassis cover) in a clockwise direction until the capacitor is fully meshed, and mechanical resistance is felt. Reverse the tuning direction, turning the capacitor in a counterclockwise direction, until a full null is observed on the multimeter. Continue counterclockwise again until a meter indication of approximately 28 is obtained.
- g. Operate the AFC disable switch into the AFC position (toggle away from feedback potentiometer).
- h. Set front panel FREQ. ADJ. potentiometer for a dial scale reading of 5.
- i. Adjust the feedback potentiometer until the exciter output frequency is within 1 KHz of the assigned frequency, as observed on a frequency counter or the deviation meter of the station monitor. Fine adjustment to the exact frequency is then accomplished by means of the FREQ. ADJ. control.

NOTE: The feedback adjust potentiometer is a 500 ohm multiturn potentiometer, and a frequency change may not be noted until after it is adjusted in a clockwise direction and then reversed in a counterclockwise direction to bring the AFC circuit within lock-in range. OVEN TEMP controls the temperature within the exciter FM oscillator chassis.

2-5.2

RF Amplifier Initial Turn-On

Protective devices and circuits are incorporated into the transmitter to provide maximum safety to operating personnel and minimize the occurrence of component damage during operation. High voltage circuits cannot be energized unless all access door interlocks are closed. A 180-second time delay circuit prevents screen and plate voltages from being applied to the driver and PA tubes until the filaments have achieved their proper operating temperature. The same delay circuit provides after-cooling for the tubes after the STOP button is pushed. At the end of the 180-second period, the blowers will turn off.

To energize the transmitter proceed as follows:

WARNING

This unit contains high-voltage and high-current power supplies. Potentials up to 7500 volts are present and exposed to maintenance personnel working with power on and interlocks defeated. Keep hands and metallic tools out of all high voltage areas. The principal purpose of defeatable interlock switches is to permit viewing areas where arcing may occur to determine the nature of a fault. Have another person standing by at all times.

- a. Check that rear doors, swing-down control panel, and the two RF compartment access covers are all in position and tightly secured. Open lower cabinet doors.

- b. Make certain that all circuit breakers are in the OFF position before turning on the 3-phase line safety switch.
- c. Operate the LINE circuit breaker to the ON position.
- d. Check the LINE voltage on all three phases by sequentially operating the three push-button switches located under the LINE meter.
- e. If the voltages are normal for the tap positions selected on the transformer primary windings, operate the BLOWER circuit breaker to the ON position.

The control circuit power supply is now energized.

- f. Operate the FILAMENT circuit breaker to the ON position.
- g. If the PLATE ON-OFF push-button switch is in the ON position, the built-in lamp will be lit. Push the switch to transfer it to the OFF condition and extinguish the lamp before proceeding to the next step. This switch has a push-ON, push-OFF type action.
- h. Press the START push-button switch. If the air interlocks pull in when the blowers function, the filament transformers and grid bias circuits will be energized by the closure of contacts on relay 3K18. The 180-second pre-heat timing cycle will also be initiated.
- i. Check the PA filament voltage by pressing the PA push-button below the FILAMENT meter. The meter

should read 6.3 volts for the FM-25KD and 7.5 volts for the FM-12KD. If it does not, rotate the PA FIL ADJUST control to obtain the proper reading.

- j. Check the driver filament voltage by pressing the DR push-button. The FILAMENT meter should again read 6.3 volts, or, very close to it. There is no adjustment for this voltage since it is obtained from a Sola constant-voltage transformer.
- k. With the OUTPUT POWER control rotated to its counterclockwise (CCW) extreme, the control grid bias on the tetrode driver tube should be approximately 250 volts as read on the DRIVER meter. The GRID push-button switch should be pressed. Leave the OUTPUT POWER control in the extreme CCW position. The driver screen voltage cannot be measured at this time since it is not applied until the high voltage power supply is energized.
- l. Operate the PLATE VOLTAGE switch (on lower panel) to the LOW position. (This applies to the FM-25KD only.)
- m. If the 180-second pre-heat cycle (referred to in Step h) has been completed, pressing the PLATE ON-OFF switch should close the contactors in the primary circuit of the high-voltage power supply. The lamp in the PLATE ON-OFF switch will be energized.

n. Readings on the PLATE voltmeter (approximately)

FM-25KD:-	DR (driver)	1.8	KV
	PA (amplifier)	4.0	KV
FM-12KD:-	DR (driver)	3.0	KV
	PA (amplifier)	6.7	KV

o. Press the SCRN push button under the DRIVER meter.
A reading of 300 volts should be obtained.

p. Press the PLATE ON-OFF switch to the OFF position.

This completes the initial turn-on sequence for the FM-12KD. If operating the FM-25KD, proceed with the following two steps.

q. Operate the plate voltage switch to the HIGH position.

r. Check to ascertain that the OUTPUT POWER control is still in the CCW position, press the PLATE ON-OFF switch to the ON position. Again measure the DR and PA plate voltages for the FM-25KD. They should read approximately 3.5KV and 7.5KV respectively.

This completes the FM-25KD initial turn-on sequence.

SECTION III

OPERATION

3-1 Front Panel Controls and Indications

As shown in Figures 3-1 through 3-4, all operational controls and indicators for the Model FM-25KD are located on the front of the unit. Table 3-1 lists these operating controls and indicators and gives their reference designators and a brief functional description of each. Photos for the FM-25KD are shown because the only visible difference is the absence of the Low-High Power Switch on the FM-12KD panel just underneath the elapsed time meter.

3-2 Tune Up Procedure

The transmitter is normally supplied tuned and tested at the factory on the customer's assigned operating frequency. The procedure used at the factory for initial tuning and final check out is as follows. (Assumes proper installation and connection of AC line, audio, monitors, filter, directional coupler and load, and a knowledge of operating control functions and location.)

- a. The exciter should be allowed 10 minutes to reach temperature stabilization. It is wired so that the crystal heater and circuit heater are on continuously if the line cord is connected to a 120 V. AC source. The exciter is otherwise turned on by operating its own On-Off switch. A 3db resistive 50-ohm pad should always be used in the coaxial line between the exciter and input to the driver stage, and initially the exciter power output control (screwdriver front panel adjustment) should be set to its full CCW direction.

b. Operate the following circuit breakers to the "ON" position.

(1) Blower

(2) Filament

(3) High Voltage (Note that control panel plate On/Off push button switch should be off at this point.)

c. Press the "START" button. Blowers and fans will start.

Observe that the following indicator lamps light.

(1) Bias Indicator

(2) Interlock Indicator

(3) Ready Indicator-lights after 3 minutes filament heating time.

Observe filament voltages. Adjust if necessary for proper voltage.

d. Operate the "POWER OUTPUT" control to maximum CCW position.

e. Operate the High-Low Power switch to the Low position.

(FM-25KD only.)

f. Observe Forward Power from the exciter. Adjust exciter power output control for about 1/3 scale reading. Adjust exciter driver and output tuning for maximum output power. If necessary reduce power output for a 1/3 scale forward indication.

g. Observe Reflected Power on the exciter output line. Carefully adjust DRIVER INPUT TUNING and DRIVER GRID TUNING for minimum reflected power.

After initial adjustment for minimum reflected, increase exciter power output to maximum and re-peak exciter tuning for maximum output.

Readjust DRIVER INPUT TUNING and DRIVER GRID TUNING for minimum reflected power. It is important that care be taken to optimize these input circuit adjustments to assure maximum transfer of power to the driver grid.

- h. Operate plate voltage switch. This is a "push-on/push-off" push button switch. It is illuminated red any time the plate circuit is "On".
- i. Observe plate voltage on both the PA and the Driver for proper values. Plate current at this point should be approximately 0 ma for the Driver (cut off) and 300 ma for the PA (normal zero bias idling current).
- j. Operate the POWER OUTPUT control for a small increase in Driver Plate Current. Adjust DRIVER PLATE TUNING for maximum PA plate current.
- k. Adjust PA PLATE TUNING and PA PLATE LOADING for maximum Power Output as indicated on the Power Output Meter. Readjust DRIVER PLATE TUNING and PA TUNING and PA LOADING for maximum Power Output.
- l. Operate Plate Voltage Switch to turn off high voltage.
- m. Operate the High-Low Power Switch to the High Position (FM-25KD only). Return Power Output Control to maximum CCW position.
- n. Operate Plate Voltage Switch to turn on high voltage. Driver and PA plate voltages should be approximately 3.5 KV and 7.6 KV respectively (FM-25KD). The FM-12KD voltages should be correspondingly 3KV and 6.7 KV.
- o. Increase Power Output to 10 KW by operating the Power Output Control.

- p. Adjust DRIVER PLATE TUNING and PA PLATE TUNING and PA PLATE LOADING for maximum Power Output.
- q. Check to see that reflected power in the exciter output line is minimum. Carefully adjust DRIVER INPUT and GRID TUNING as required for minimum reflected power.
- r. Operate Power Output Control to increase output to 25 KW (FM-25KD) or 12 KW for the FM-12KD or lower power as required.
- s. Allow at least 1/2 hour operation and then make final trimming adjustments of DRIVER PLATE TUNING and PA PLATE TUNING and PA PLATE LOADING to maximize power output. Readjust Power Output control for required Power Output.

NOTE: For all modes of operation, driver screen current should be maintained between +25 ma and -25 ma. This is a function of driver level and driver output loading. The latter is adjusted by the driver output loading capacitor, 2C64. Decreasing the value of this capacitor decreases loading, causing an increase in positive screen current, while increasing the value of capacitor increases loading and decreases screen current. Screen current will vary for varying power levels and from tube to tube. Any value between the limits indicated is satisfactory providing operation is otherwise satisfactory.

3-3 Automatic Power Control (ALC)

After completing the tune-up procedure shown in Section 3-2, the automatic level control may be set to maintain constant power output against varying line voltage of up to +5%. Use the following procedure:-

- a. Turn the manual OUTPUT POWER control (3R10) full clockwise.
- b. Turn the screwdriver automatic level control, ALC ADJ, (3R13), full clockwise.
- c. Load and retune the PA for one to two kilowatts over the authorized station transmitter output power. Under this condition the PA "apparent" plate circuit efficiency will often exceed 80%.
- d. Under condition of c. (above) note the Driver Screen current. It should read +20 to +35 ma for "full bore". This is satisfactory for this temporary condition.
- e. Turn the ALC ADJ screwdrive control counterwise to reduce the output power to the authorized output power level. Set the power output carefully by observing the OUTPUT FWD meter reading.
- f. Again observe the Driver Screen current. The reduced power setting should bring the screen meter to the mid-scale position with the preferred range for normal line voltage conditions being between -10 ma and 0 ma.
- g. Check the PA plate circuit efficiency at the authorized output power. It will be found that the efficiency has decreased to a value between 70% and 75%. This efficiency will vary with the amount of ALC reserve power allowed and the AC line voltage. The power output will, however, be held relatively constant

for line variations. Experience will show the operator how much "ALC reserve" is necessary to maintain authorized power output for the prevailing power line voltage variations.

3-4 Automatic VSWR Protection

Refer to Figure 3-5, which shows the relationship between reflected power on the output line and scale indications on the SWR protection meter relay. For any given transmitter operating power, select a reflected power limit which corresponds with a VSWR of 2:1 or less. The meter relay when set to this limit will provide an overload signal to the recycling control circuit if the reflected power exceeds the preset level.

NOTE:- For reference, a VSWR of 2:1 represents a reflected power of approximately 11% of the forward power in the 50 ohm line.

3-5 Driver Neutralizing

The 4CX1000K driver stage contains a capacitive bridge neutralizing arrangement with the variable capacitor coupled to the driver plate. It normally will not require attention. However, if necessary, any standard neutralizing procedure may be used. When properly neutralized, there should be little or no influence on the driver reflected power as the driver plate circuit is tuned through resonance and/or power is increased or decreased.

3-5.1 Neutralization Procedure

If reneutralization is necessary, the method employing a grid-dip oscillator operating as a diode absorption meter is recommended. NOTE:- No plate or screen voltages should be applied to the Driver stage. Remove the Driver cavity front-panel cover and mount the absorption meter in a stable position so that the pick-up coil is loosely coupled to the Driver plate tank line. Apply drive from the FM exciter and resonate grid and plate circuits for a maximum indication on the grid-dip meter. Without disturbing the coupling of the grid-dip meter to the plate tank circuit adjust the neutralizing capacitor a turn or two at a time-retuning the driver plate tuning each time for a maximum indication. A broad minimum indication in the output will be noted as the neutralizing capacitor is run through its tuning range. The most accurate setting will be obtained if the rotational turns of the capacitor are counted from a convenient reference and several passes are made through the minimum indication. NOTE:- A complete null will not be obtained. When satisfied that a minimum has been obtained, replace the Driver front panel cover and proceed with the tuning procedure described elsewhere. NOTE:- As an option an air pressure interlock system is sometimes used. For this system, the interlock must be bypassed with a jumper to operate the filament of the tube when the front panel cover is removed.

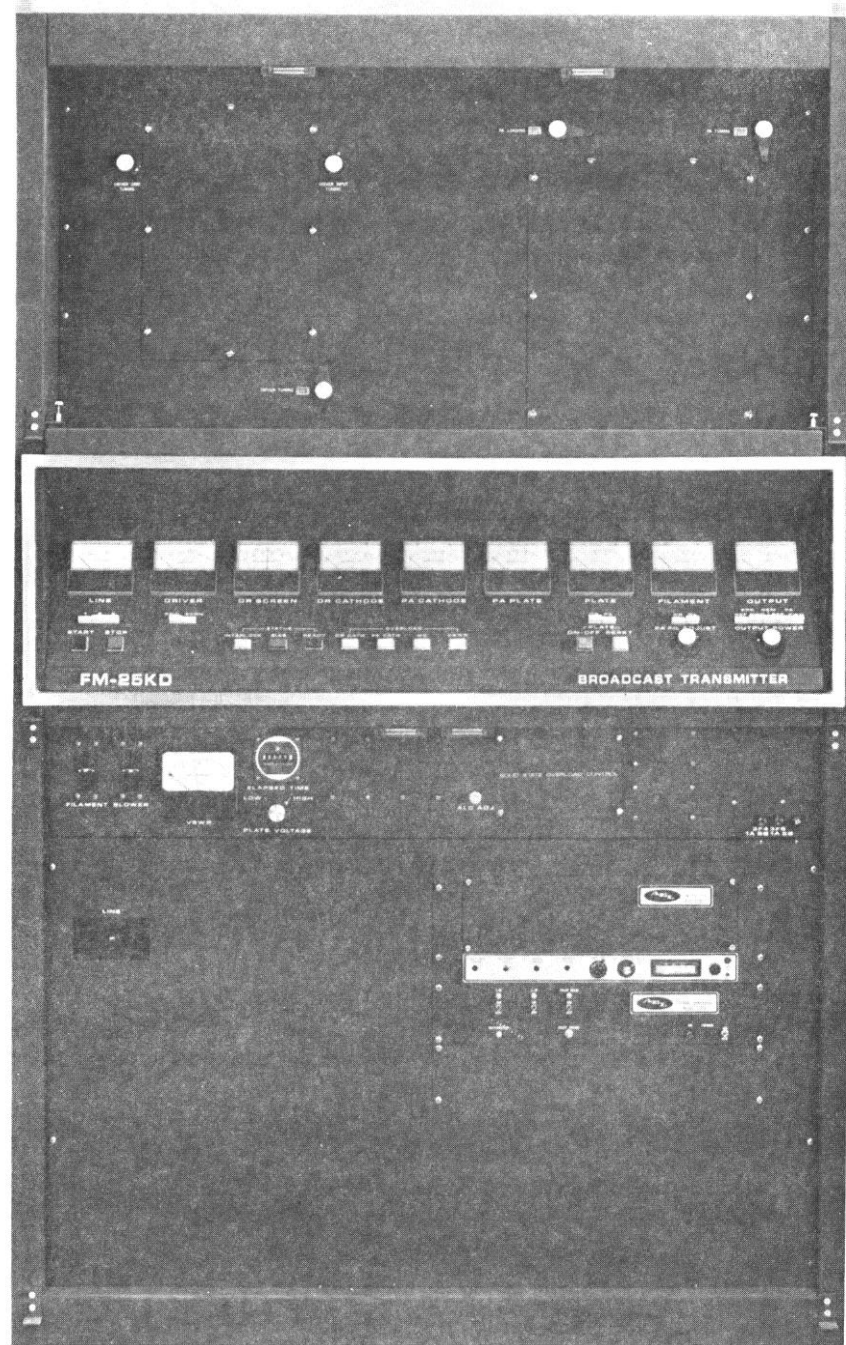


Figure 3-1. FM-25KD Front View, Doors Removed

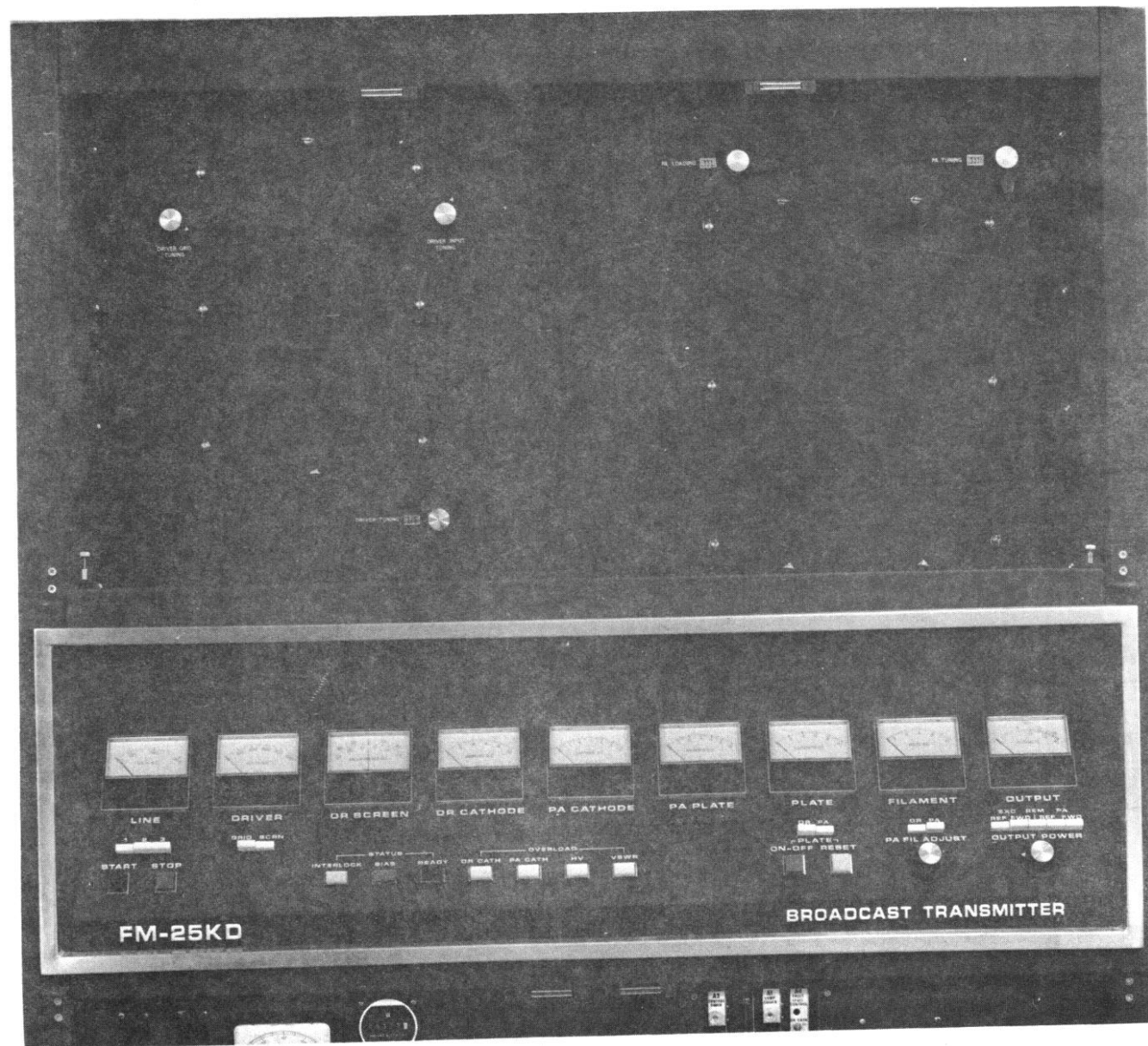
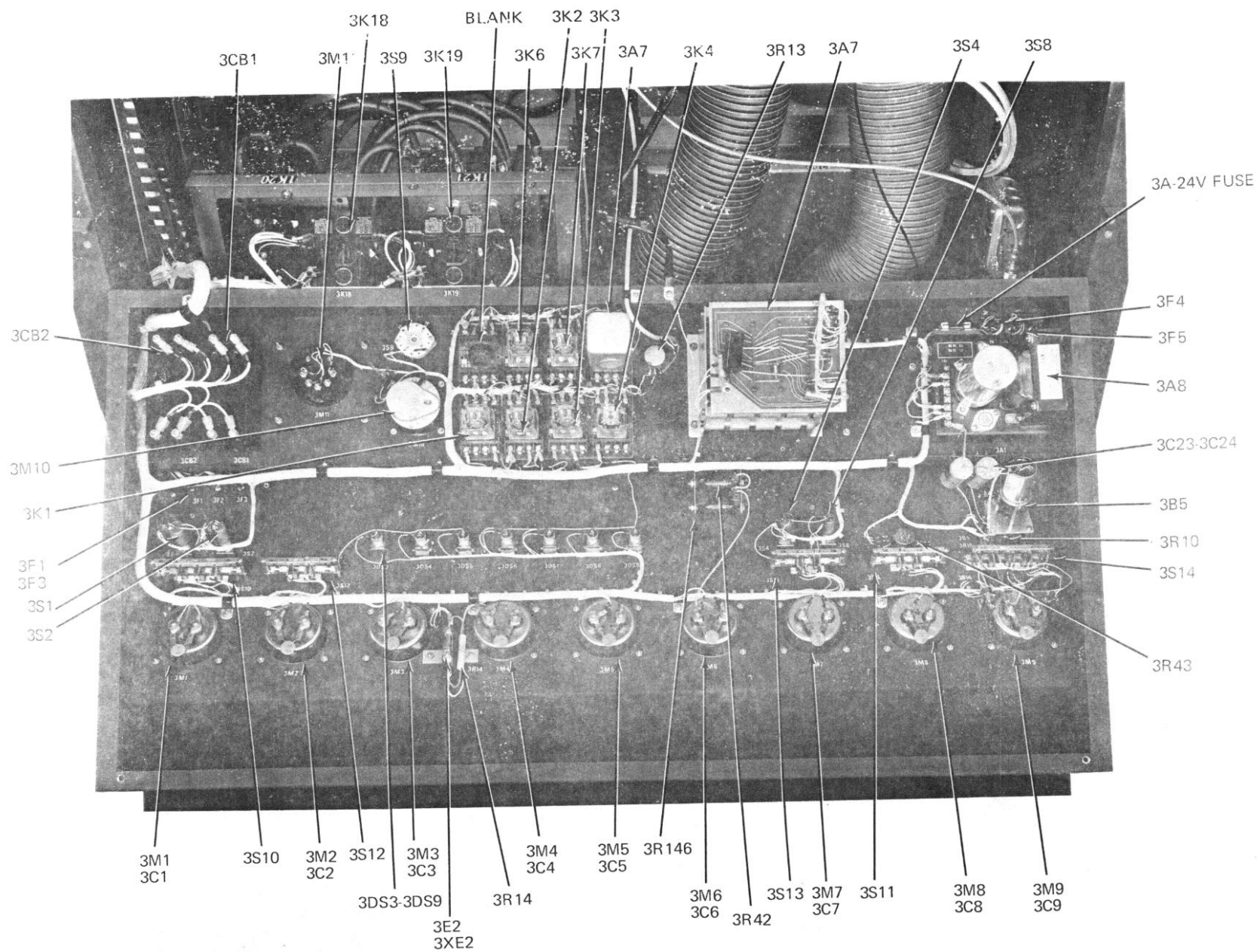


Figure 3-2. FM-25KD Control Panel Close-up



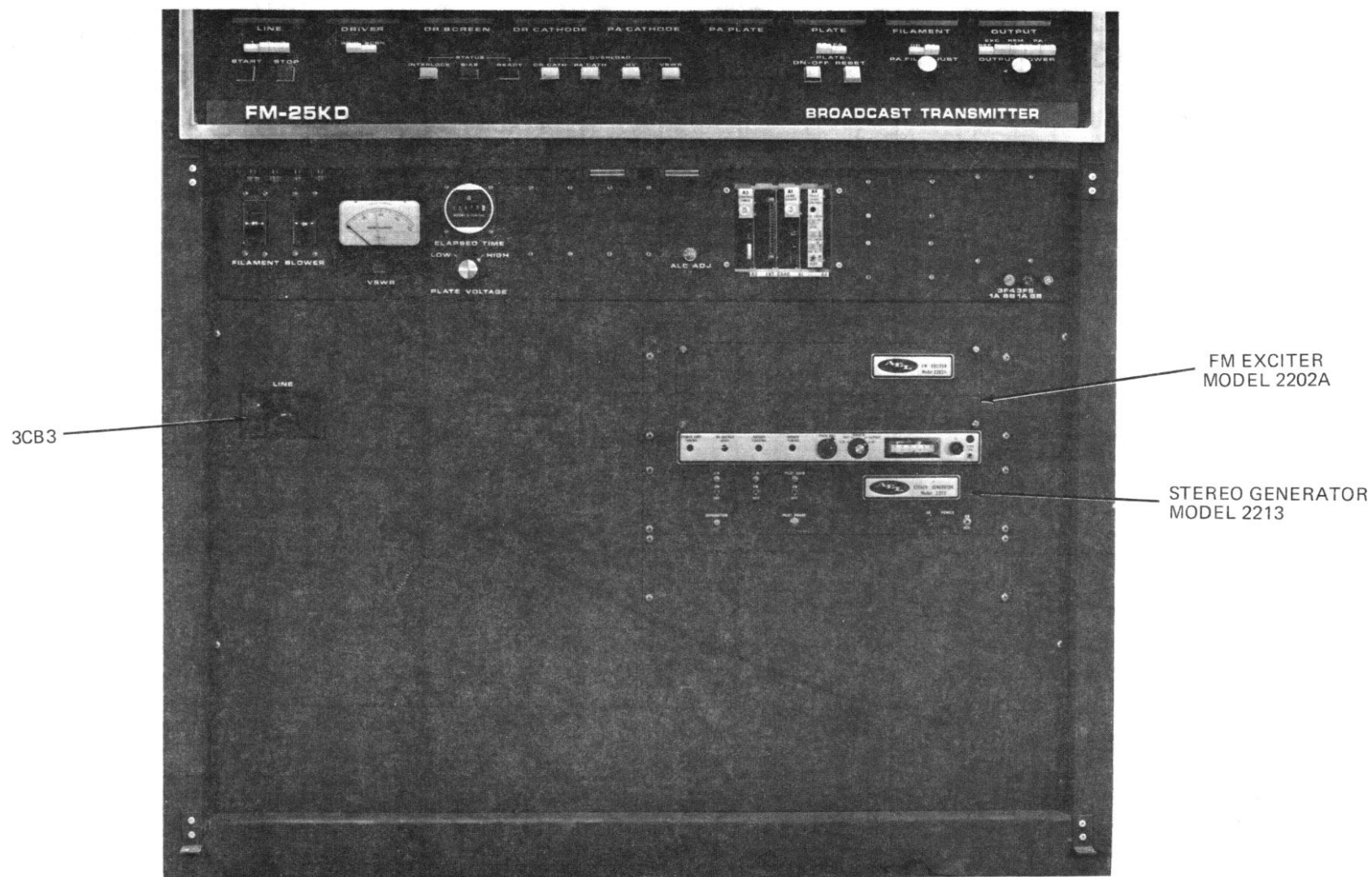


Figure 3-4. FM-25KD Lower Cover Panel Close-up

3-12

CURRENT IN VSWR METER RELAY IN μ A

200

150

100

50

0

0

0.25

0.5

0.75

1.0

1.25

1.5

(FM-12KD)

0.5

1.0

1.5

2.0

2.5

3.0

(FM 25KD)

REFLECTED POWER (KW)

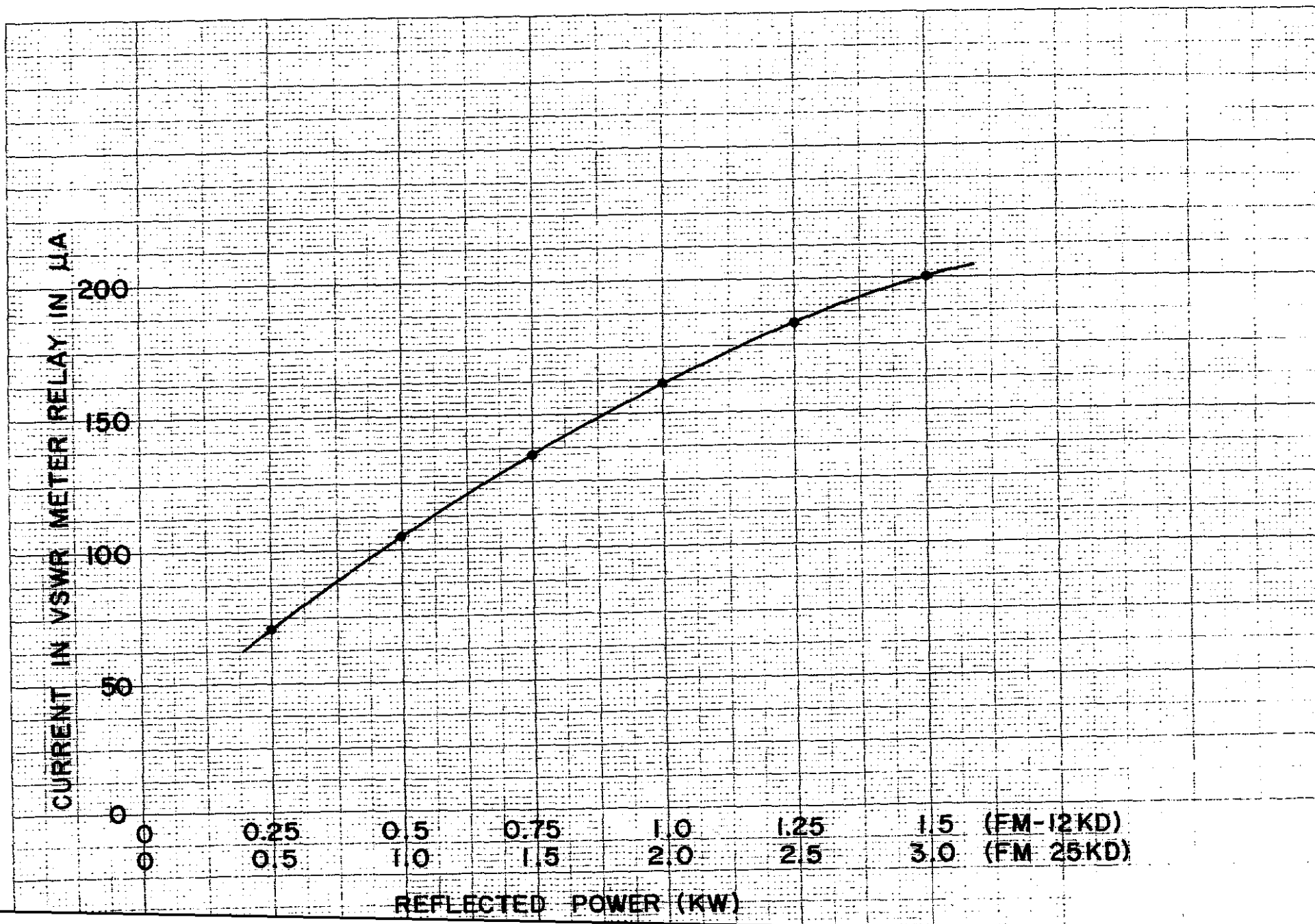


Table 3-1. Operating Controls and Indicators

Ref. Des.	Nomenclature	Function
MODEL 2202-A FM EXCITER (Front Panel)		
S2	Line On	Applies AC power to exciter power supply.
DS1	Line On	Lamp indicates when AC power is applied.
S1	(None)	Meter switch for multimeter.
	L.O.	Monitors voltage drop across the emitter resistor of the crystal oscillator transistor.
	AFC	Measures level of voltage derived from integration of the AFC IF frequency.
	Driver	Measures relative collector current of driver transistor.
	Output	Measures level of a rectified sample of the RF output.
	B+	Measures the output of the 15 volt power supply.
M1	(None)	Performs multimeter function as determined by the position of S1, described above.
C50	Driver Tuning	Tunes resonant frequency of driver tank circuit.
C52	Driver Loading	Adjusts loading on driver collector circuit and matches it to the base of the power amplifier Q18.
R30	RF Output Level	Adjusts the collector voltage applied to the driver transistor.
C55	Power Amp Tuning	Tunes resonant frequency of power amplifier collector tank circuit.
R25	Freq. Adjust	Adjusts the conduction period of a monostable multivibrator in the AFC loop.
F1	Fuse - 1 A	Provides overload protection for exciter power transformer.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
MODEL 2202-A FM EXCITER (Behind Removable Panel)		
S3	AFC-Lock	Closes AFC loop to establish FM oscillator frequency control by comparing it to a crystal controlled reference frequency.
S3	AFC-Disable	In this position, the AFC loop is opened and the FM oscillator operating frequency can be readily adjusted.
R106	Temp Adjust	Controls level of regulated temperature within the FMO chassis.
R8	R8	Establishes a reference voltage against which the integrated AFC IF frequency is compared.
L5	L.O. Tune	Tunes resonant frequency of crystal oscillator tank circuit.
C77	FMO Tune	Capacitor tunes the free-running frequency of the FM oscillator.
F2	F2 - 1A	Protects against damage from possible short circuits in the FMO chassis heater circuits.
R87	(None)	This control, mounted on the power supply regulator PC card, adjusts the +15 volt regulated output used by the FMO chassis circuits.
MODEL 2202-A FM EXCITER (Rear of Chassis)		
TB2	115 VAC Input TB2	Three wire (one grounded) input power connector. AC terminal board. With LINE ON switch (S2) closed and jumper removed from terminals 1 and 2, the exciter can be remotely controlled by placing a closure across these terminals. Ancillary equipment power (Stereo Generator, SCA) can be obtained from terminals 2 and 3.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
MODEL 2202-A FM EXCITER (Rear of Chassis)		
TB1	SCA	A modulated SCA carrier can be introduced at this connector to be combined with either a monaural or composite stereo signal to modulate the FM exciter.
	RF Output	High level output (10 watts nominal) from solid-state power amplifier.
	TB1	Audio terminal board. For monaural operation, the audio signal would be applied to terminals 1, 2, and 3 at a 600 ohm impedance level, balanced to ground. Terminal 2 is ground. A jumper is also placed across terminals 4 and 5. For stereo operation, the jumper would be placed across terminals 5 and 6. The composite stereo signal would be introduced via an unbalanced line to the connector captioned STEREO INPUT.
	Stereo Input	Accepts a composite stereo signal to modulate the exciter. A jumper should be placed across terminals 5 and 6 on terminal board TB1.
R97	R97	Adjusts the level of the monaural AF signal applied to the FM oscillator.
R98	R98	Adjusts the level of the composite stereo signal applied to the FM oscillator.
FM-12KD OR FM-25KD TRANSMITTER (Main Control Panel)		
3M1	Line (Meter)	AC Voltmeter (0-300 VAC) Measures input power line voltages.
3S10	Line (Switch)	Selects each of the three phases to measure line voltage.
3M2	Driver (Meter)	DC voltmeter (0-500 V) to measure driver grid bias and screen voltages.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
FM-12KD OR FM-25KD TRANSMITTER (Main Control Panel)		
3S12	Driver (Switch)	Selects either grid bias (GRID) screen voltage (SCRN) to be measured on meter 3M2.
3M3	DR Screen	DC Milliammeter (50-0-50 ma) to measure driver screen current.
3M4	DR Cathode	DC Ammeter (0-1 amp DC) measures driver cathode current.
3M5	PA CATHODE	DC Ammeter (0-6 amp DC) measures power amplifier cathode current.
3M6	PA Plate	DC Ammeter (0-6 amp DC) measures power amplifier plate current.
3M7	Plate (Meter)	DC Voltmeter (0-10 KVDC) measures either driver or PA plate voltages.
3S13	Plate (Switch)	Selects either driver (DR) or power amplifier (PA) plate voltages to be measured on meter 3M7.
3M8	Filament (Meter)	AC Voltmeter (0-10 VAC) measures either driver or PA filament voltages.
3S11	Filament (Switch)	Selects either driver (DR) or PA filament voltages to be measured on meter 3M8.
3R43	PA Fil Adjust	Controls operation of SCR regulator in primary of the PA filament transformer.
3M9	Output (Meter)	Measures forward and reflected power between the FM exciter and the driver grid and also between the output of the harmonic filter and the antenna transmission line. The various functions are selected by means of a push-button switch 3S14. In the REMOTE position the PA forward power reading can be monitored at a remote point.
3S14	Output (Switch)	Selects the various functions described in the preceding paragraphs.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
FM-12KD OR FM-25KD TRANSMITTER (Main Control Panel) (cont'd)		
3R10	Output Power	Controls transmitter output power by varying the grid bias on the driver and as a consequence, the RF drive to the PA stage. It is also motorized so it can be operated from a remote point.
3S1	Start (Switch)	Initiates the turn-on sequence of the transmitter after the LINE, BLOWER, and FILAMENT CIRCUIT breakers are turned on.
3DS1	Start (Lamp)	P/O START switch assembly. It will light when the START switch is actuated and is latched in by contacts on relay 3K1.
3S2	Stop	Opens up the coil circuit of relay 3K1, causing the START switch latching contacts to open. This shuts down the transmitter except for a 180-second after-cooling period initiated by operation of the STOP switch. The blowers will automatically shut down after this period.
3DS3	Interlock Status	If all door interlocks are closed the INTERLOCK STATUS lamp will be energized upon closure of the START switch.
3DS4	Bias Status	If the bias supply is functioning properly contacts on relay 3K4 will close to energize this indicator.
3DS5	Ready Status	Contacts of relay 3K3, that had opened at the instant the START switch was closed will again close, after the 180-second pre-heat period has been completed, and energize the READY STATUS indicator lamp.
3DS6	DR Cath Overload	If a malfunction occurs that increases the driver cathode current beyond a preset value, this indicator will light and remain lit until reset.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
FM-12KD OR FM-25KD TRANSMITTER (Main Control Panel) (cont'd)		
3DS7	PA Cath Overload	If a malfunction occurs that increases the PA cathode current beyond a preset value, this indicator will light and remain lit until reset.
3DS8	HV Overload	If a malfunction occurs that causes an increase in current, in high voltage circuits external to the power supply, beyond a preset value, this indicator will light until reset.
3DS9	VSWR	A meter relay, located on the lower front panel, monitors reflected power sampled at the output of the harmonic filter. When the current reading reaches a preset value due to excessive VSWR an impulse is sent to the fault cycling circuit and the VSWR lamp will light.
3DS11	Reset (P/O Plate Reset Switch)	With 3K7 energized at the time the +24 volt control power supply is activated, normally closed contacts in series with the RESET indicator (3DS11) will be opened preventing it from lighting. It will stay unlit until three faults occur and the HV supply control circuits are locked out when it will light to indicate a need for a manual reset of plate voltage and overload indicators.
3S4	Plate On-Off	If all previous steps have functioned normally and the fault-cycling control relay 3K7 is energized, pressing the PLATE ON-OFF switch will cause the high voltage plate transformer contactors to close to provide plate voltage for driver and PA plate circuits and via a Zener regulator circuit to the screen of the driver. Pressing the SCRN push-button under the DRIVER meter should obtain a reading of +300 volts.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
FM-12KD OR FM-25KD TRANSMITTER (Main Control Panel) (cont'd)		
3S8	Plate Reset	Reset the fault counter, in the fault-cycling circuit, to its original state and high voltage circuits are re-activated.
(Lower Control Panel)		
3F1	Line Filament Blower VSWR Elapsed Time Plate Voltage (FM-25KD Only)	Fuse in #1 section of 3S10 LINE switch. Protects against wiring harness damage in case of a short in the switch.
3F2		Fuse in #2 section of 3S10 LINE switch. Same function as above.
3F3		Fuse in #3 section of 3S10 LINE switch. Same function as above.
3CB3		Main power line circuit breaker. Rated at 225 amp max.
3CB2		Filament circuit breaker. Rated at 20 amp max.
3CB1		Blower circuit breaker. Rated at 20 amp max.
3M11		Meter relay provided for protection against excessive VSWR. Can be set to provide a contact closure at any preset value. Closure would activate the fault re-cycling circuit.
3M10		Elapsed time meter. Indicates accumulated operating time.
3S9		Provides a capability for reducing the high voltage during initial tuning procedures by connecting the 3-phase primary power source to the transformer primary windings connected in a WYE configuration (LOW). In the (HIGH) position, a DELTA primary circuit arrangement is used and full voltage is obtained.

Table 3-1. Operating Controls and Indicators
(continued)

Ref. Des.	Nomenclature	Function
FM-12KD OR FM-25KD TRANSMITTER (Lower Control Panel) (cont'd)		
3R13	ALC Adjust (Optional)	Establishes RF output power level that will be maintained constant regardless of normal tube aging and power line variations.
3F4	3F4	Primary circuit fuse for 24-volt control circuit power supply.
3F5	3F5	Same as above.
A4 (PC Board)	Overload Threshold Controls	Located behind an easily removable cover plate are three overload threshold adjustment controls. From top to bottom their functions are: DRIVER OL, PA OL & PLATE. Lower control is fault system test switch.
(Upper Front Panel)		
2C11	Driver Input Tuning	Tunes the primary of the input coupling transformer between the exciter and driver control grid.
2C12	Driver Grid Tuning	Tunes the secondary of the input coupling transformer.
2I4	Driver Tuning	Varies the effective length of the driver-to-PA coupling transformer.
2L9	PA Tuning	Tunes the input to the pi output matching network.
2L10	PA Loading	Tunes the series inductance of the network to control loading of the PA by the antenna circuits.

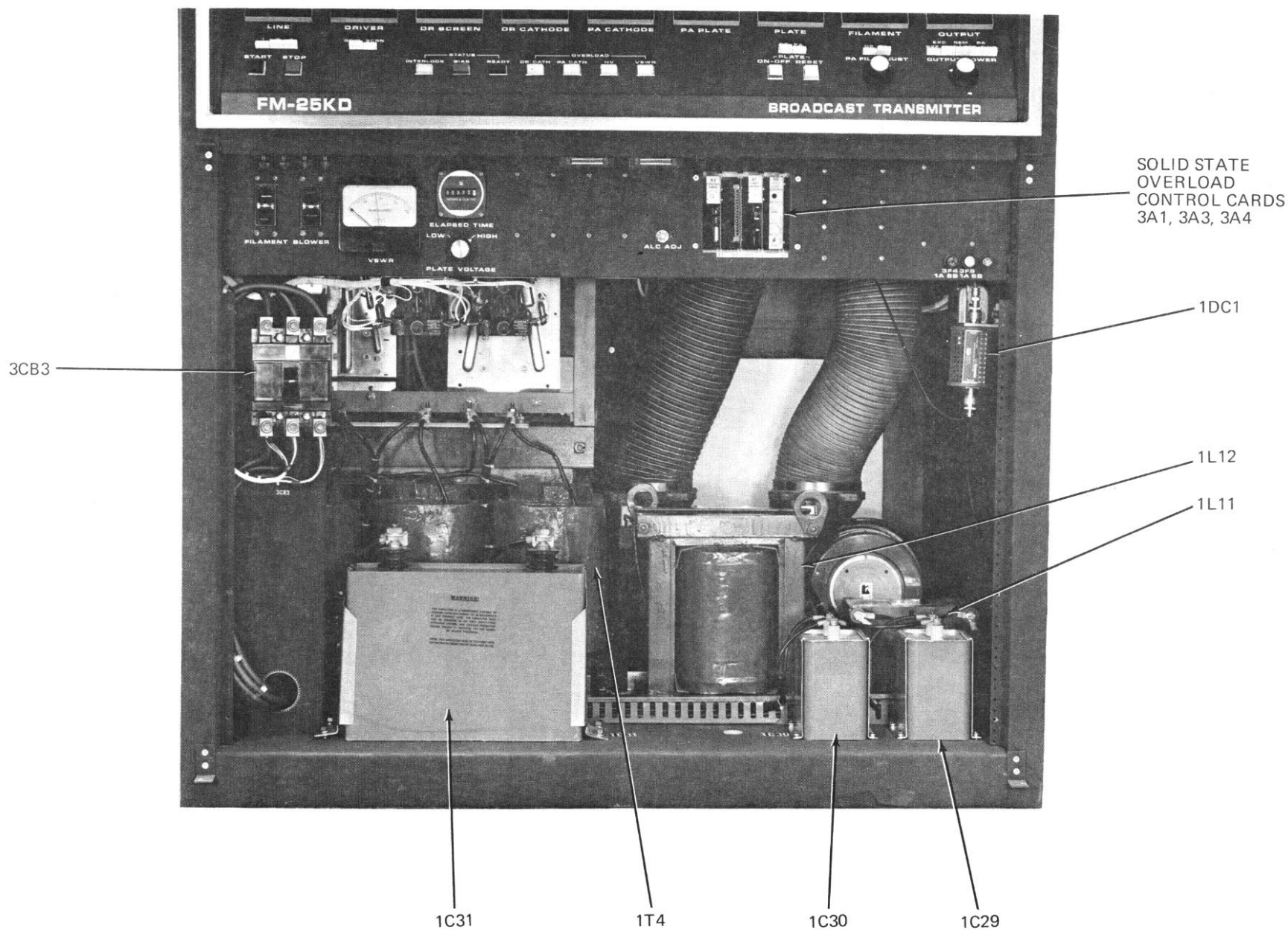


Figure 3-6. FM-25KD Front Lower Panel Removed

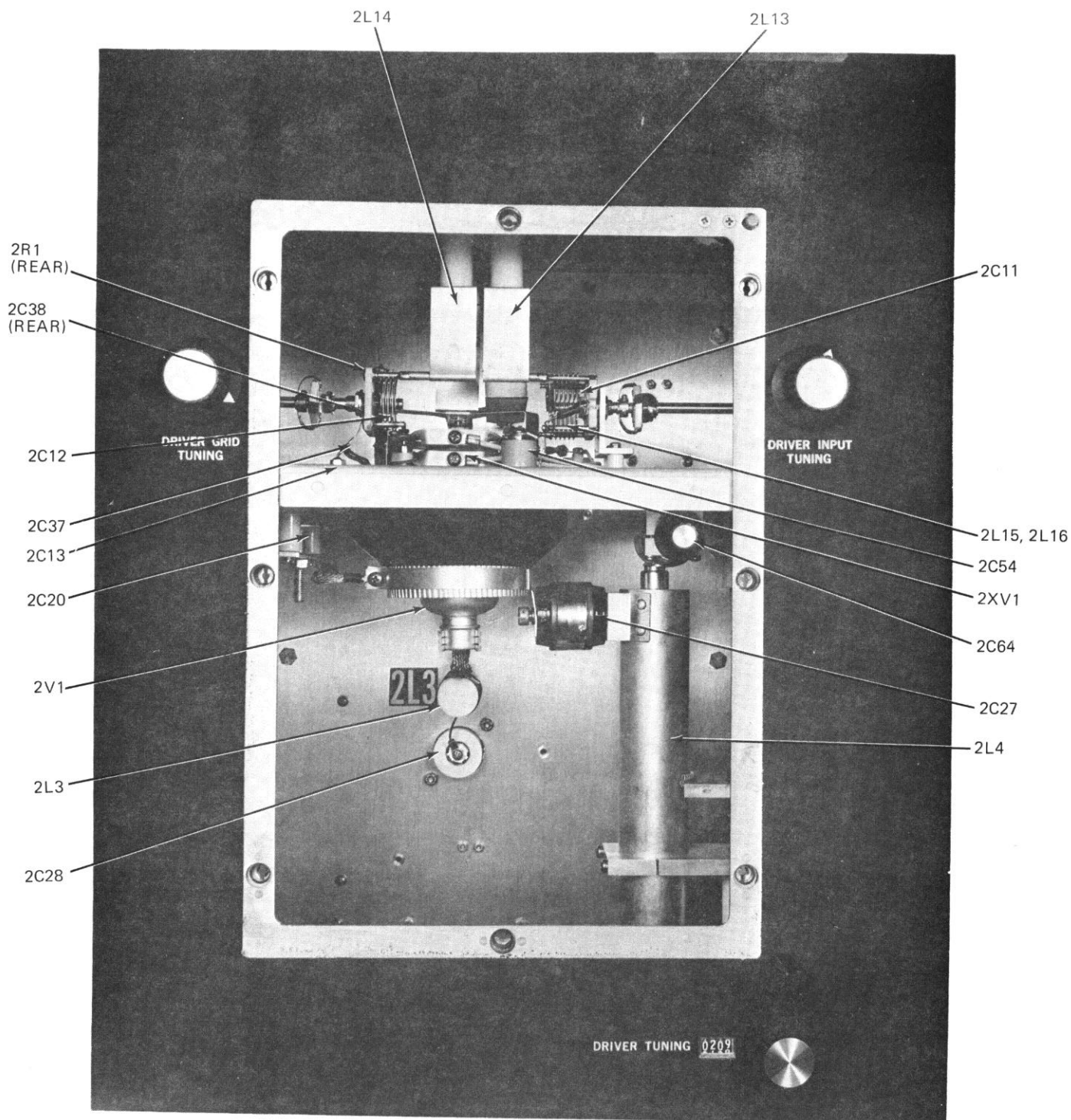


Figure 3-7. Driver Compartment, Cover Removed

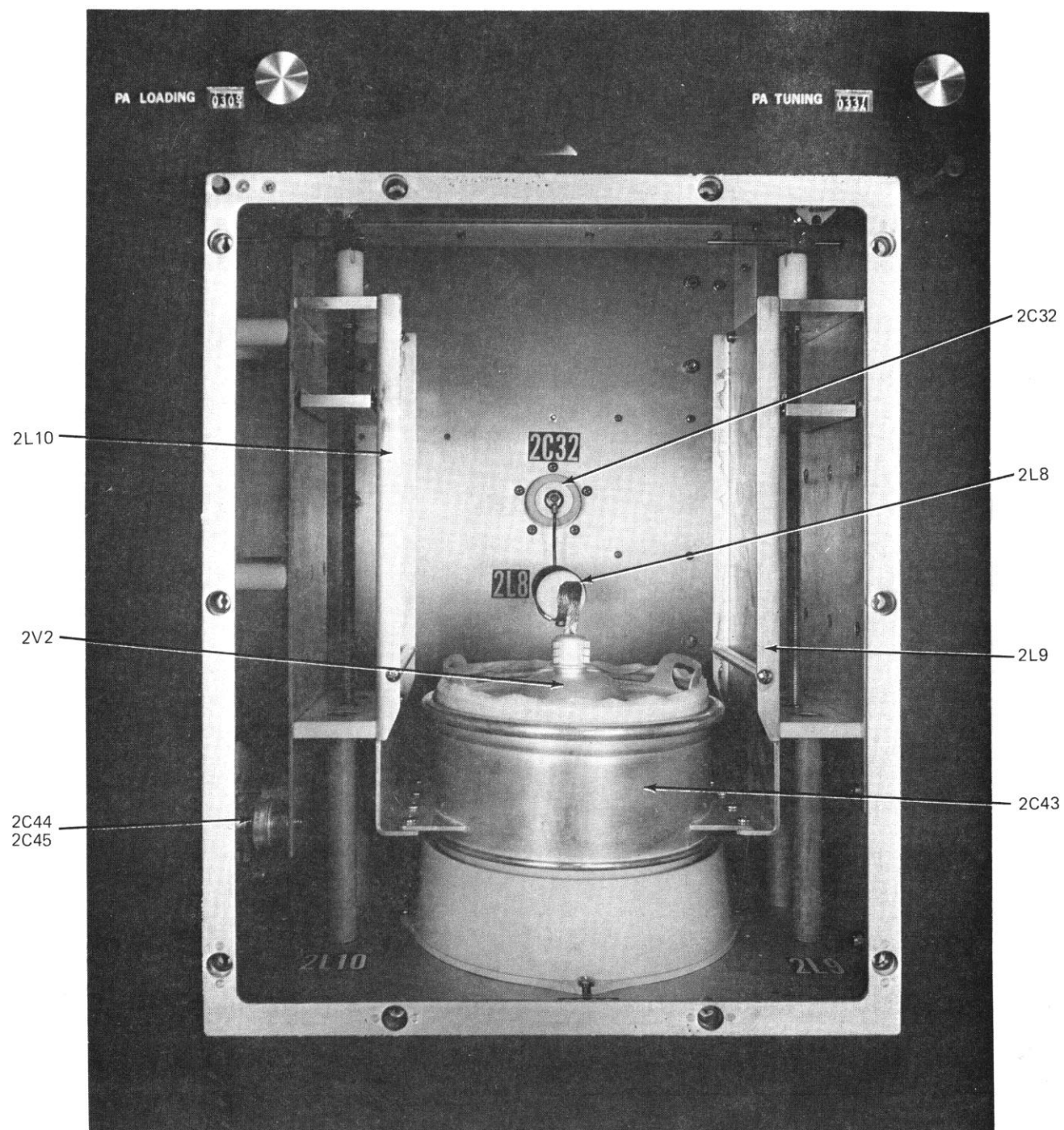


Figure 3-8. Power Amplifier Compartment, Top Cover Removed

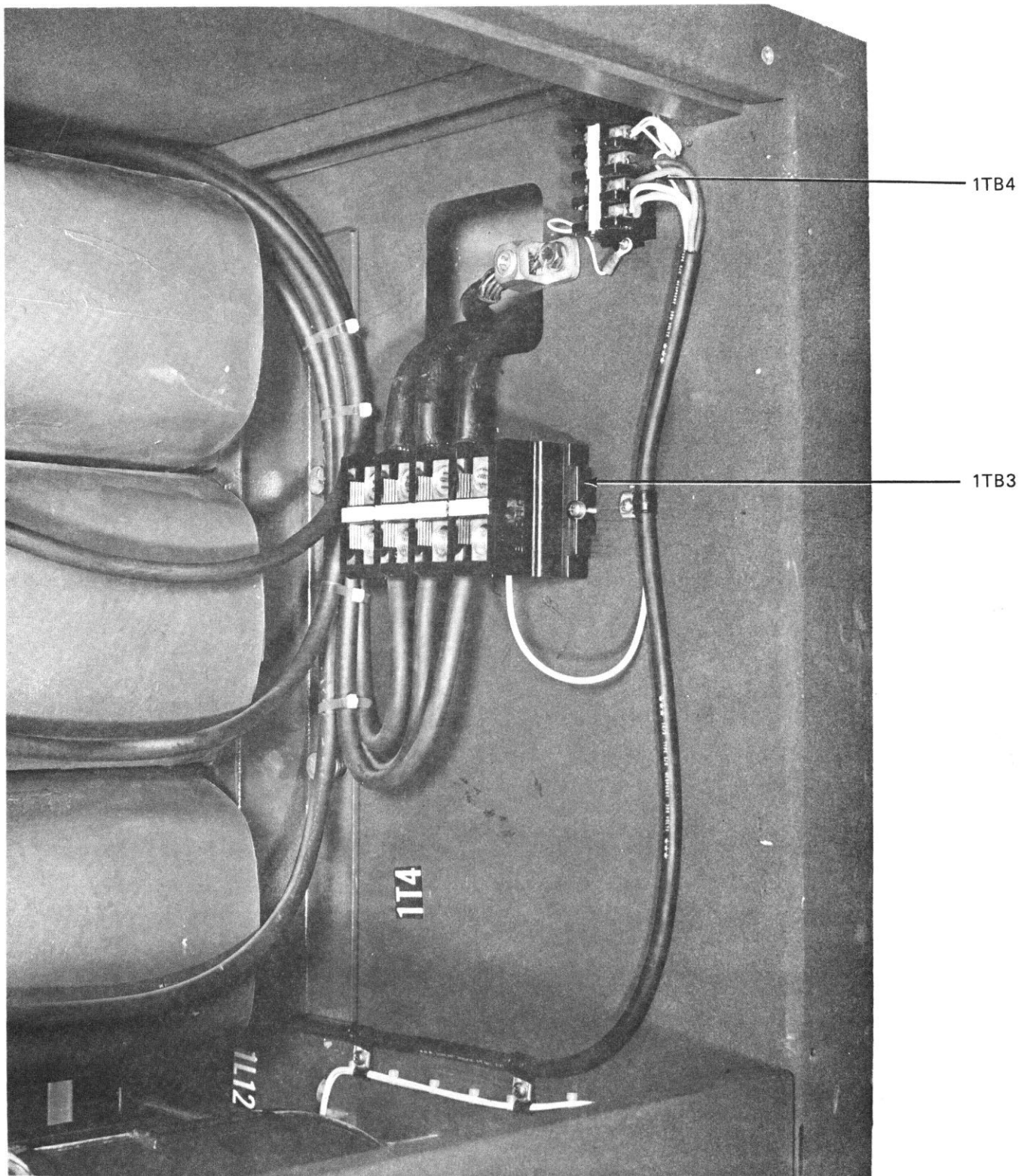


Figure 3-10. AC Power Input Connections

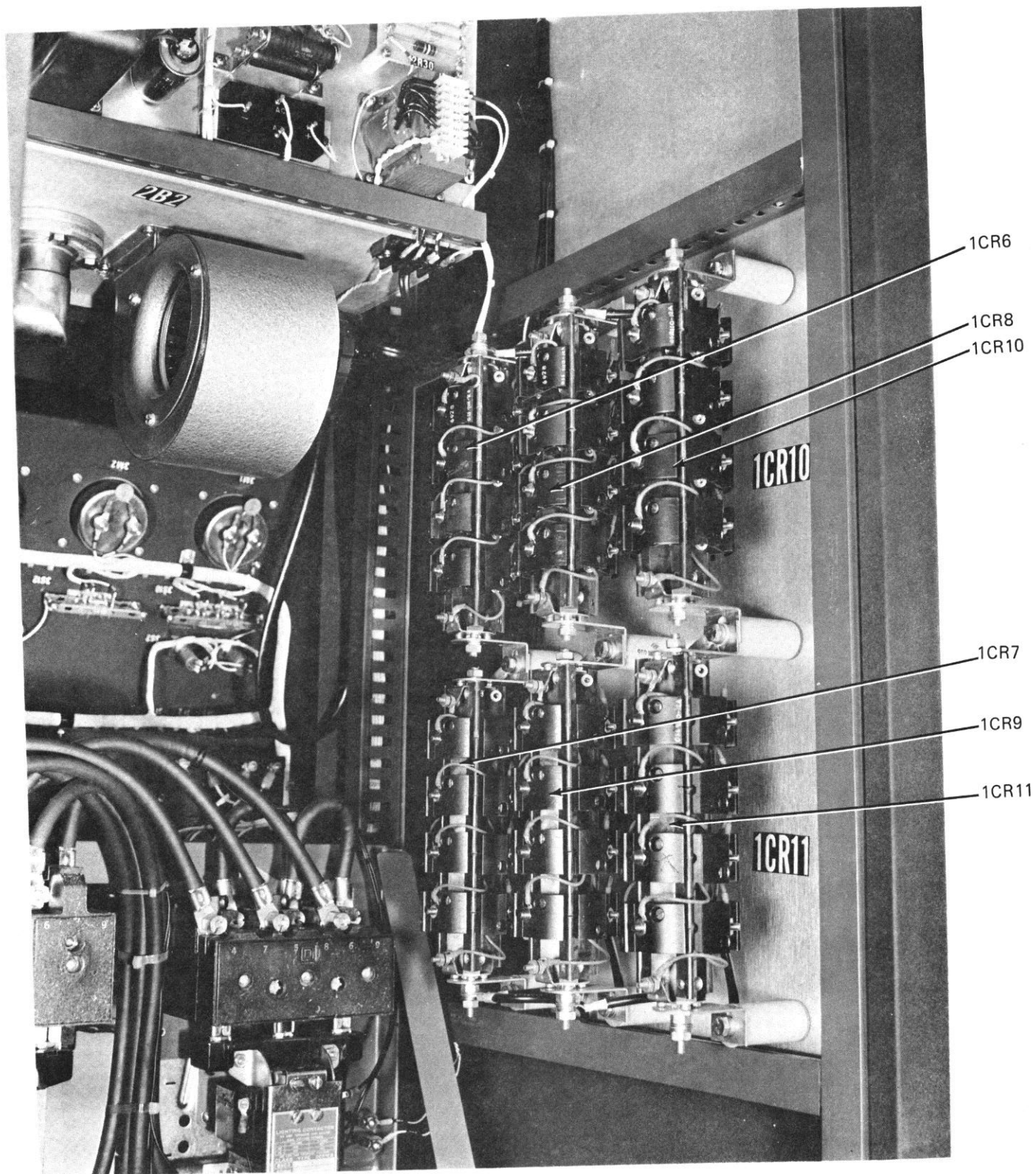


Figure 3-11. HV Rectifier Assembly

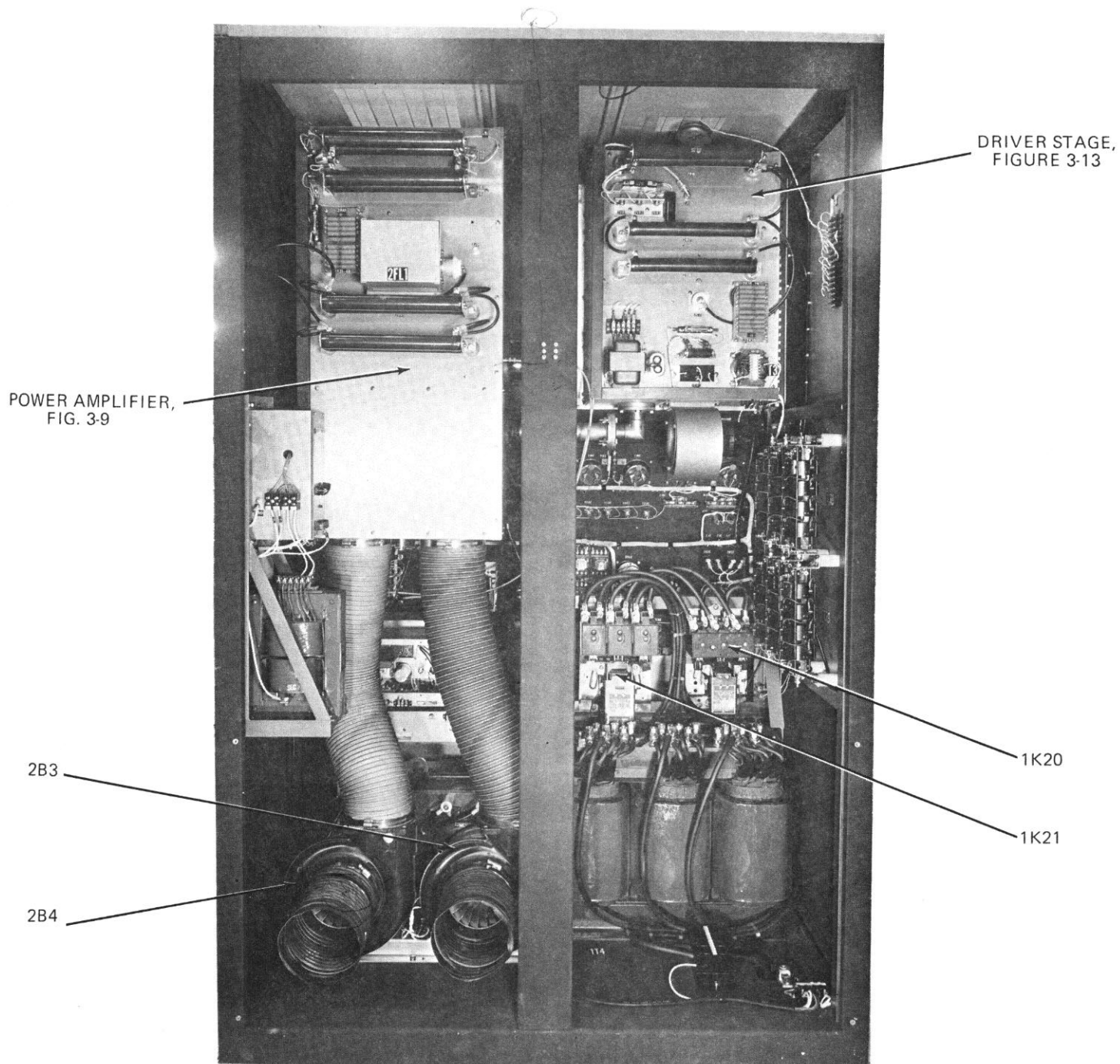


Figure 3-12. FM-25KD, Rear View, Doors Removed

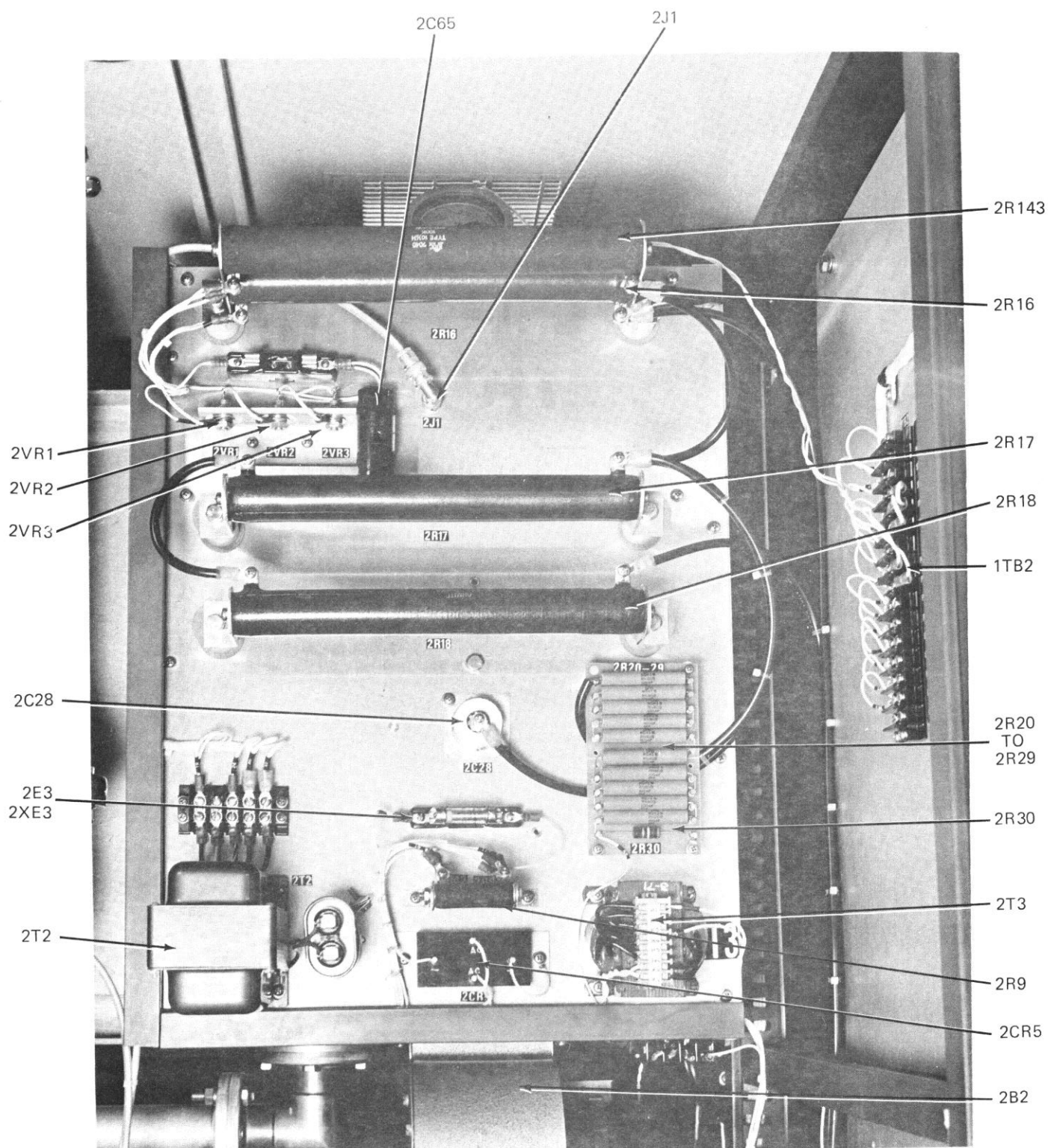


Figure 3-13. Driver Compartment, Rear View

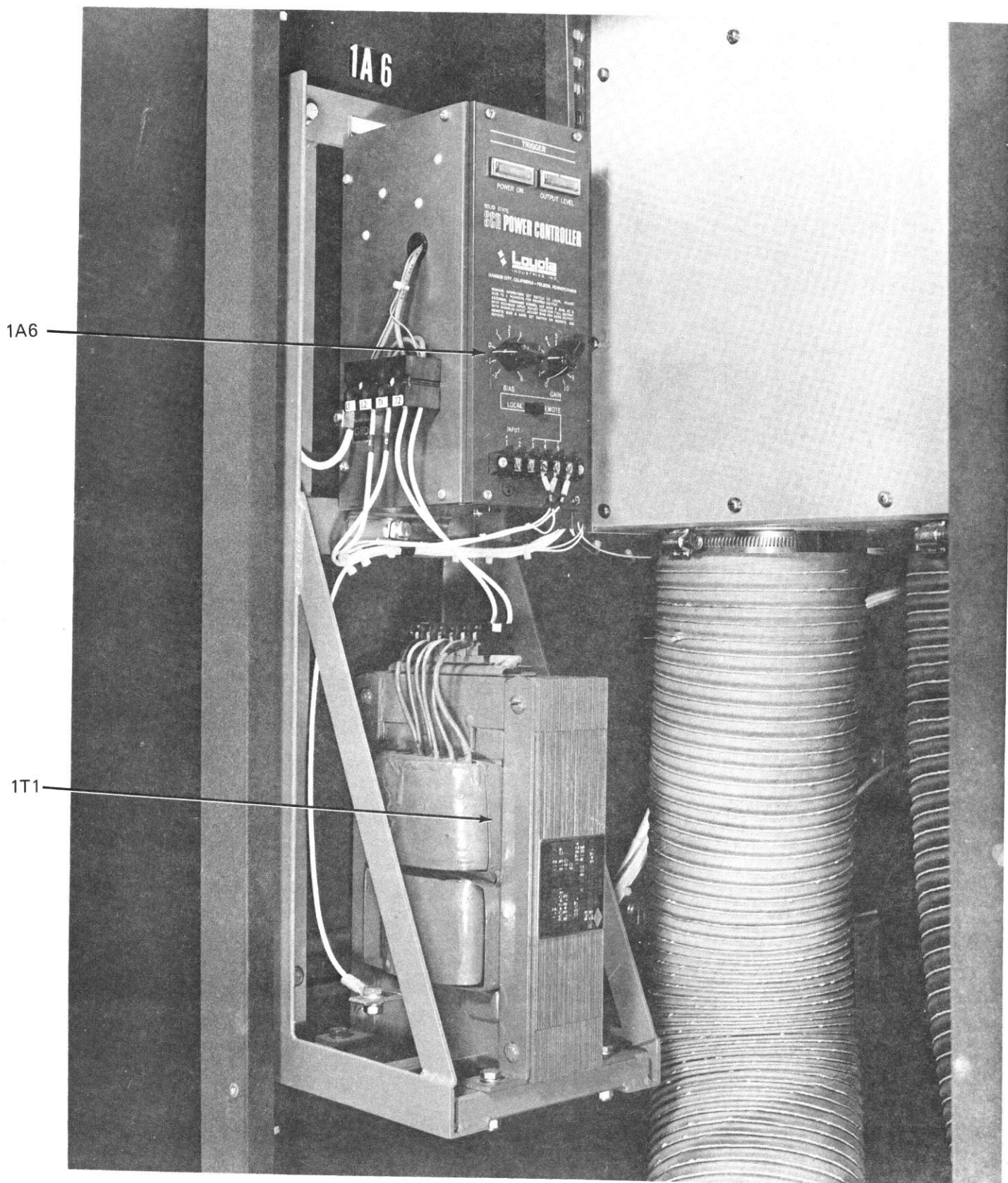


Figure 3-14. FM-25KD PA Filament Regulator and Transformer

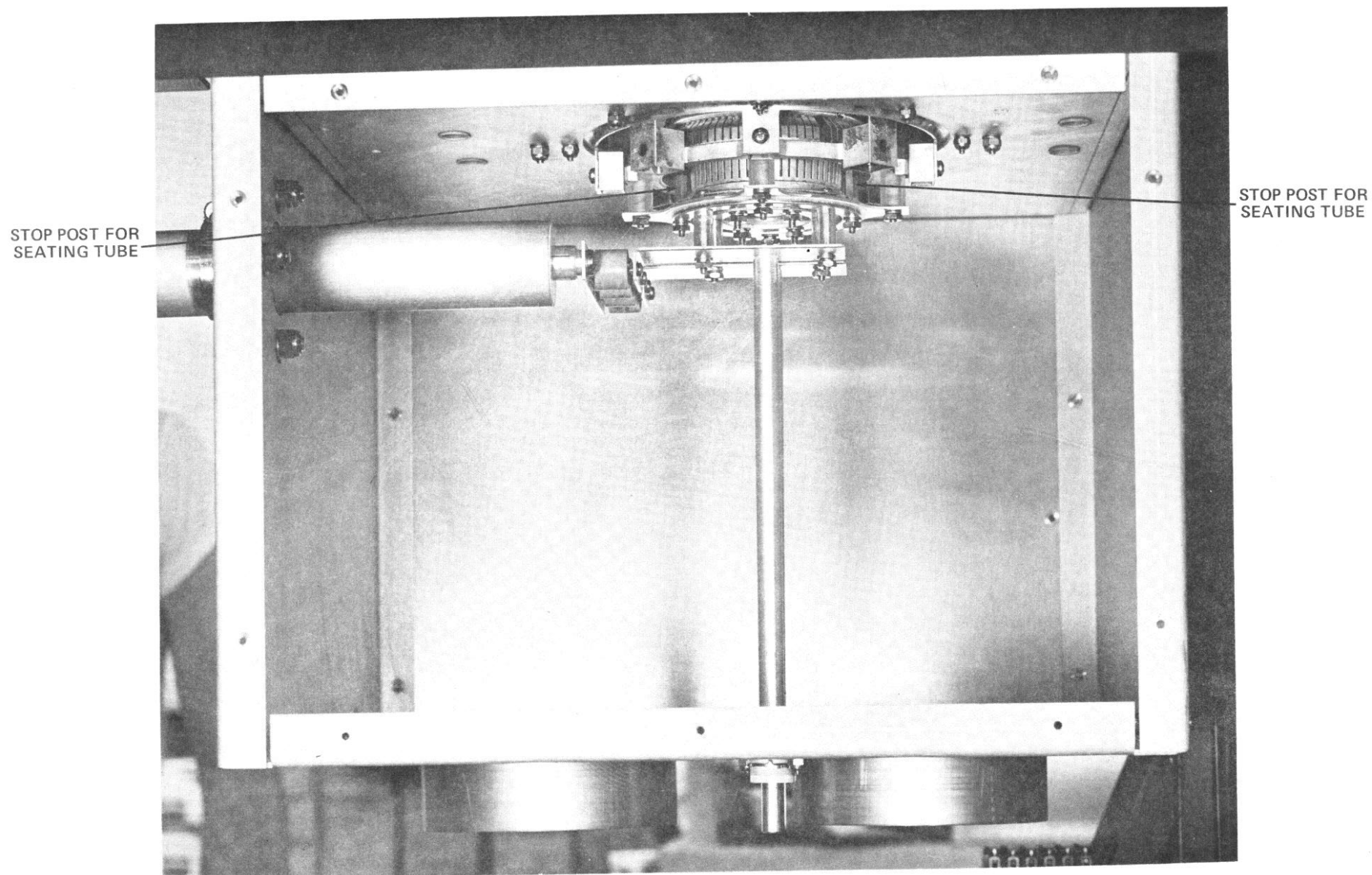


Figure 3-15. Power Amplifier Compartment, Lower Cover Removed

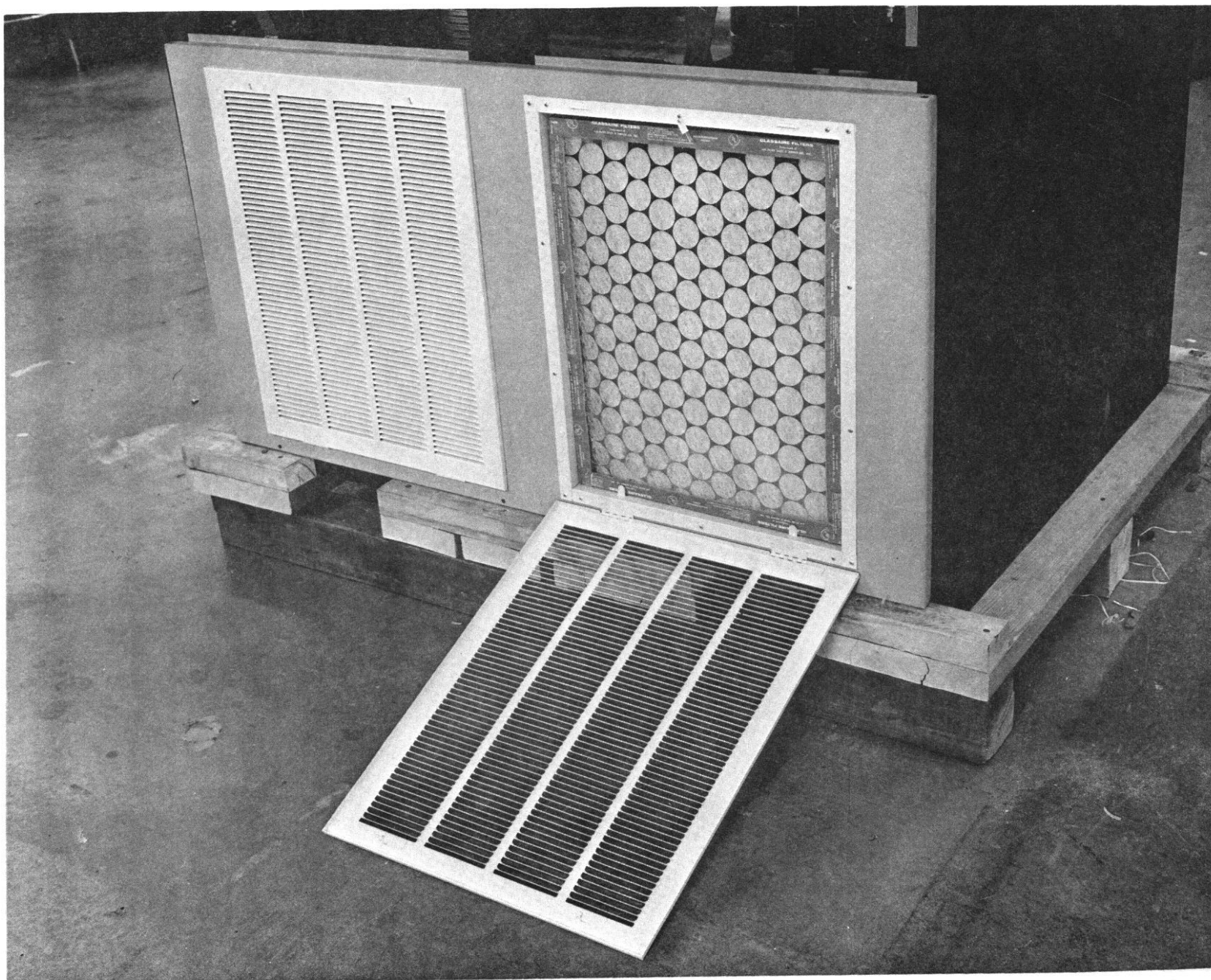


Figure 3-16. Rear Filter Panel

SECTION IV
PRINCIPLES OF OPERATION

4-1 General

The transmitter is divided functionally into the following:

(1) Interlock and Control Circuits, (2) Power Supplies, (3) RF Amplifier Section, (4) Automatic Power Level Control, and (5) Overload Protection and Automatic Recycling Circuits. The Model 2202A FM Exciter will be discussed in detail in its operating and maintenance manual.

4-2 Interlock and Control Circuit Analysis

The interlock and control circuits are concentrated at the left side and lower edge of the schematic diagram for the applicable transmitter. Refer to schematics, Fig. 4-1 or Fig. 4-2.

Power is first applied by operating the LINE circuit breaker (3CB3) to the ON position. The voltage available at each of the three phases can be measured on LINE meter (3M1) by sequentially pushing the three push-buttons of LINE switch (3S10). Fuses (3F1), (3F2) and (3F3) are used to prevent damage to the wiring harness if a short circuit occurs in the switches. Capacitor (1C1) serves as an RF by-pass for LINE meter (3M1).

The blower and filament circuits are made ready for subsequent application of power by closing the BLOWER circuit breaker (3CB1) and the FILAMENT circuit breaker (3CB2). Closure of the BLOWERS breaker energizes the 24-volt power supply used for the control circuits. This insures that the cooling blowers will be energized before control circuits can be activated to apply filament and high voltage to the driver and PA tubes.

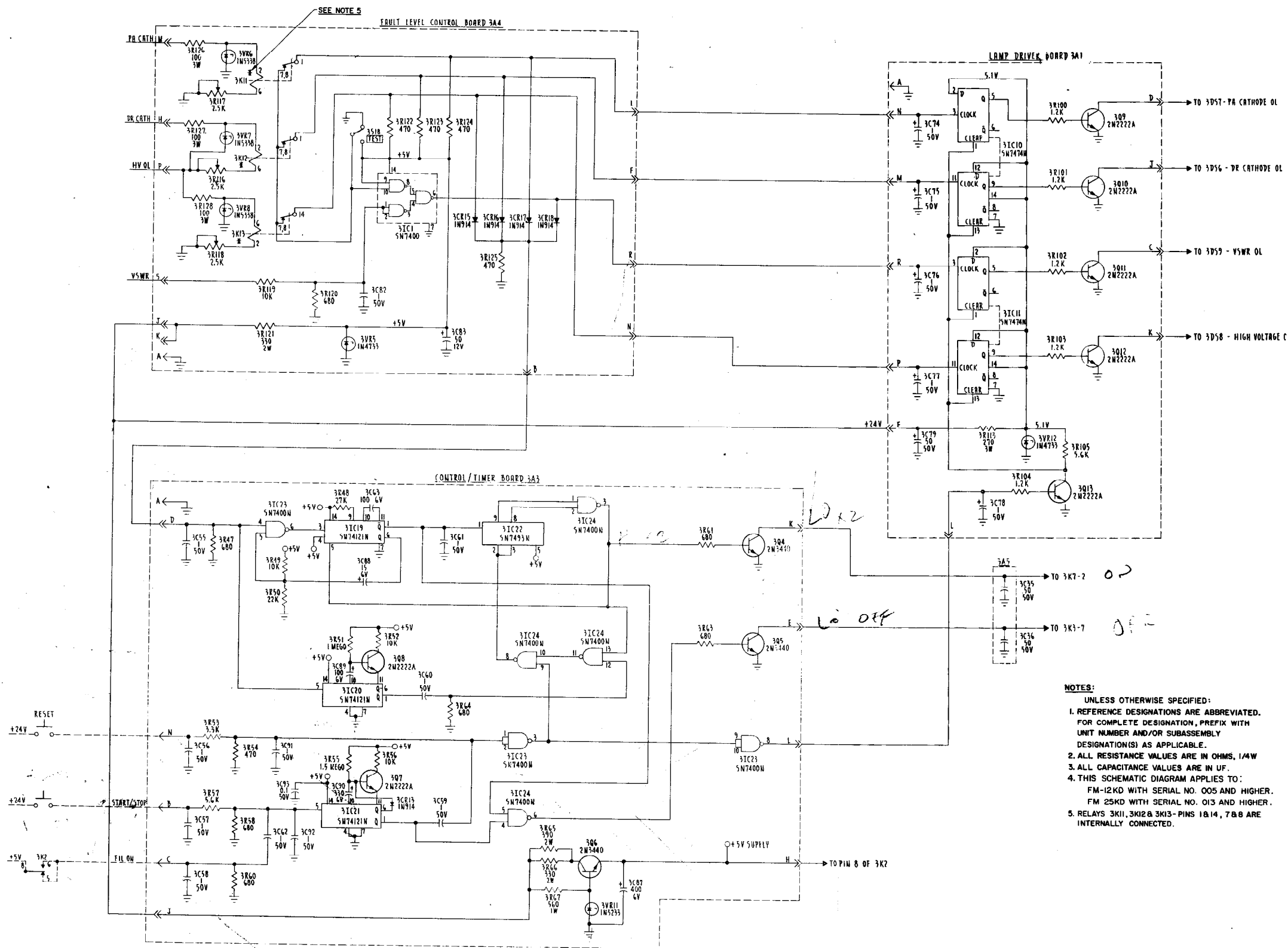


Figure 4-4. Schematic Diagram Control Circuit
Logic with Rev. G of 3A4 Fault Board

When the START push-button switch (3S1) is closed, a number of simultaneous events take place as described below:

- a. Relay 3K1 is energized, closing latching contacts across the START switch (3S1), and also closes another set of contacts to apply power to the cabinet fan (1B1), driver blower (2B2), and relay (3K19) whose contact closure energizes PA blowers (2B3) and (2B4).
- b. Power is applied to a 180-second monostable multivibrator timer that instantly applies power to relay (3K3) opening normally-closed contacts (5-8) to keep the READY light (3DS5) from operating and normally-open contacts (1-3) are closed. Contacts (1-3) appear to represent a redundancy since contacts (6-8) of relay (3K1) already perform a similar function. However, contacts (1-3) play a role in an after-cooling function when the STOP switch (3S2) is pressed).
- c. If all the air interlocks are closed, power is applied to relay (3K2) whose contacts (1-3) energize relay (3K18). Power is thereby applied to the PA filaments, the primary of the driver Sola filament transformer (2T2) and the elapsed-time meter (3M10).
- d. If all the door and access hatch interlock switches are closed, the INTERLOCK indicator (3DS3) will illuminate and relay 3K5 will be energized applying power to the Bias transformer, 2T3.
- e. At the moment the bias supply delivers voltage, relay (3K4) will close contacts (1-3) to apply power to the

BIAS indicator (3DS4). It will also apply voltage to 3K3 contact 5.

- f. After the 180-second pre-heat time interval has elapsed, relay (3K3) contacts (1-3) will open again and contacts (5-8) will close to energize the READY indicator (3DS5).

NOTE:- Opening of relay (3K3) contacts (1-3) will not shut down the blowers since they are still being supplied power via relay (3K1) contacts (6-8) and contacts of relay (3K19).

The PLATE VOLTAGE switch (3S9) should be rotated to the LOW position (FM-25KD only). This utilizes contactor, 1K20. When the PLATE ON/OFF latching switch (3S4) is pressed into the ON position, the PLATE indicator (3DS10) will light and relay (1K20) will be energized. Its contacts will connect the high voltage transformer primary windings to the three-phase power source in a WYE configuration. This will provide a reduced secondary output voltage. Rotating the PLATE VOLTAGE switch (3S9) from LOW to HIGH can be done without operating the PLATE ON/OFF switch (3S4) to the OFF position. No damage can occur since the switch has a 90° index and the WYE connection contactor (1K20) will drop out before the DELTA connection contactor (1K21) pulls in and provides the increased secondary voltage.

4-3 Power Supplies

4-3.1 Bias Power Supply (See photo, Figure 3-13)

The bias power supply consists of transformer (2T3) whose secondary winding is connected to a full-wave bridge rectifier quad (2CR5). An R/C filter is used, consisting of

a 3,000 ohm, 25 watt resistor (2R4) and a 100 MFD capacitor (3C24). The coil winding of relay (3K4) is connected across the output of the power supply. A serious malfunction in the power supply that reduces the bias voltage below the hold-in voltage of the relay will cause it to drop out and open up the plate voltage contactor control circuit. The output of the power supply is also connected to one end of OUTPUT POWER control potentiometer (3R10). The arm of this control is connected to the control grid circuit of the driver amplifier. The remaining end of the control is tied into the automatic level control circuits which will be described separately. The automatic level control circuit is optionally available on the FM-12KD transmitter.

4-3.2 High Voltage Power Supplies

The high voltage power supply provides power for several circuits. It utilizes a 3-phase power transformer (1T4). The secondary is connected to a full-wave bridge rectifier (diodes 1CR6 through 1CR11) and then through a filter reactor (1L12) to the output filter capacitor (1C31) to provide the high voltage output for the PA tube. The bleeder system consists of resistors (2R44, 2R45, 2R144 and 2R145).

A second power supply configuration utilizes rectifiers (1CR7, 1CR9 and 1CR11) in a half-wave arrangement to provide half the high voltage output for the driver amplifier. The filtering consists of filter reactor (1L11), capacitor (1C30), series resistors (2R17) and (2R18) and the output capacitor (1C29). Resistor (2R143)

performs a bleeder function at the output of the power supply.

In addition to supply the driver plate, this half-voltage power supply also supplies the driver screen via dropping resistor (2R16) and series connected Zener regulators (2VR1, 2VR2 and 2VR3). Capacitor (2C65) serves as a by-pass. The driver screen is supplied a regulated 300 volts from this circuit.

4-3.3 24-Volt Control Circuitry Power Supply

A commercially available 24-volt power supply is used for the control circuits. Its capacity is 2.5 amperes steady state and is regulated at the 24-volt output level. This power supply has its own self-contained fuse (3 amp) mounted on the power supply sub-chassis. The manufacturer's data sheet and schematic is provided as a part of the appendix of this manual.

A failure of the 24-volt power supply primary fuses (3F4 or 3F5) or its own D.C. output fuse will disable the control circuits and it will be impossible to start the transmitter. A failure of this sort will be obvious since none of the panel lights will be illuminated.

4-4 RF Amplifiers

4-4.1 Driver Amplifier (See Figure 3-7)

The driver amplifier employs a 4CX1000K tetrode (2V1) operated in a neutralized grounded cathode circuit. It uses the Bruene method of neutralization by sampling plate RF voltage and applying it via a capacitance divider consisting of a variable capacitor (2C20) and

the feedthrough by-pass capacitor (2C13). This latter capacitor presents an "imperfect" by-pass in that its value is deliberately selected to allow a small amount of controllable "out-of-phase" RF voltage to be fed back into the grid circuit, thereby stabilizing its operation.

The input of the driver control grid circuit is double tuned by means of inductance/capacitance combinations (2L14-2C12) (DR GRID TUNING) and (2L13-2C11) (DR INPUT TUNING). Inductive coupling is used between the two tuned circuits. Bias voltage is shunt fed to the driver control grid by means of RF choke (2RL1).

A directional coupler (1DC1) is installed between the exciter RF output and the driver input coaxial connector (2J1). This permits monitoring the reflected and the forward power on meter (3M9) via switch (2S14) to optimize the impedance match and transfer of power.

Capacitors (2C15 through 2C18) and (2C66 through 2C69) provide low-inductance RF by-passing of both sets of filament wiring is further decoupled by feed-through by-pass capacitors (2C21 and 2C22) prior to being connected to metering circuits and the Sola filament transformer (2T2).

The cathode side of the filament is wired through the DR CATHODE meter (3M4) and an overload sampling resistor (3R14) back to the ground circuit of the high voltage power supply. Capacitor (3C4) provides an RF by-pass for the meter (3M4).

Resistor (2R15), directly at the screen of the driver, minimizes any tendency toward parasitic oscillations. It is followed by by-pass capacitor (2C54) and then goes through DR SCRN current meter (3M3) to the regulated 300 volt supply. RF by-passing of the meter is provided by capacitor (3C5). RF by-passing of the 300 volts to the DRIVER SCRN voltage metering circuit is accomplished by capacitor (2C65). Metering of DRIVER GRID and SCRN voltages is provided by meter (3M2) and push-button selector switch (3S12).

The plate of the tetrode driver amplifier (2V1) is shunt-fed through RF choke (2L3). Capacitor (2C27) serves as a plate-voltage blocking and coupling capacitor to a coaxial quarter-wave coupling transformer that serves to match the driver plate impedance to the input impedance of the grounded-grid PA stage. The effective length of the "quarter-wave" line and its impedance transformation characteristics are controlled by variable capacitor (2C64) and the variable shunt inductance DRIVER TUNING (2L4).

4-4.2 Power Amplifier (See Figures 3-8 and 3-15)

The power amplifier is a 3CX15,000A7 in the FM-25KD and a 3CX10,000A7 for the FM-12KD arranged in a grounded-grid circuit configuration. RF driving power is coupled into the filament circuit by means of a moderately balanced physical layout through ceramic coupling capacitors (2C70 through 2C73). The filament is maintained above RF ground by RF chokes (2L6 and 2L7).

NOTE:- Physically, these chokes are straight silver-plated rods. However, at the frequency of operation, they exhibit sufficient inductive reactance to prevent short-circuiting the driving power to ground.

The rods pass through the floor of the lower RF shield compartment by means of feed-through capacitors (2C33 and 2C34) wherein the rods themselves serve as one surface of each capacitor. At the bottom end of each rod, heavy gauge wiring is used to connect the rods to a high-reactance filament transformer (1T1). The primary winding of the transformer in the FM-25KD is provided a regulated input voltage obtained from the SCR regulator (1A6). The regulated output can be manually controlled over a limited range by the front panel control PA FIL ADJUST (3R43). The FM-12KD filament voltage is adjusted by means of a transformer primary manually-adjusted filament power rheostat identified as 3R43 in the FM-12KD schematic. Wiring is run from points B-B on the schematic diagram to the filament metering circuit consisting of FILAMENT meter (3M8) and the push-button selector switch (3S11). Four resistors (2R5 through 2R8) are wired in series parallel combination and are connected in series with the PA filament transformer secondary winding center tap through the PA CATH meter (3M6) to ground. Capacitor (3C6) serves as an RF by-pass for the meter. The PA cathode current passes through resistor 2R4 creating a voltage drop which is monitored by the PA CATH overload protection circuits.

DC power is shunt fed to the plate of the power amplifier through a single L-section filter (2FL1), feed-through by-pass capacitor (2C32) and RF choke (2L8). Capacitor (2C43), built into the PA tube socket assembly, serves as a DC blocking and coupling capacitor to the output RF tuned circuits.

While the PA output tuned circuit does not look like a pi-section filter, schematically, it actually is. The input capacitance of the pi-network is actually the plate-to-filament capacity of the output PA tube (2V2). However, it very obviously cannot be varied.

If a variable inductor, such as (2L9), is placed in shunt with this capacitance to be tunable at some frequency below the operating frequency, it can provide a variation in the effective negative reactance. This would appear as a variable capacitor at the input to the pi-network to tune its overall resonant frequency. The value of the loading capacitors (2C43 and 2C44) are determined at the factory for the specific operating frequency. Control of the degree of loading is accomplished by variation of the pi-network series inductance (2L10).

The output of the pi-network is coupled to a harmonic filter (1FL2). Two pairs of directional couplers are installed at the load end of the filter. One pair is used to sample reflected and forward power up to a 30 kilowatt level. The other pair performs a similar function for the FM-12KD transmitter in which power can be measured up to a 15 kilowatt level.

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The output of the directional couplers is connected via two sections of OUTPUT switch (3S14) to meter (3M9), which is calibrated to read output power directly. If the switch section, associated with PA FWD, is depressed the reflected power is then monitored on the VSWR meter relay (3M11) (located on lower front panel). The contacts on this meter can be set to provide a pulse to the overload cycling circuit when the VSWR exceeds some preset value. When switch (3S14) is in the REM position, the forward power level can be monitored at some remote location from terminals 1TB2-11 and 1TB2-12 by one of many remote monitoring methods.

A small wire probe in a BNC coaxial connector (2J2) on the rear of the PA upper shield compartment samples the PA RF power to be applied to station monitoring equipment. Output to the automatic level control is obtained from coaxial connector (2J3).

4-5 Automatic Power Level Control (ALC)

The transmitter ALC system maintains the transmitter output power constant for varying conditions of line voltage, RF drive, and tube aging. It is essentially a feedback scheme in which the system gain is controlled by varying the bias level on the driver

stage. The PA output signal is sampled by an envelope detector, filtered and used as a feedback control signal in a transistor DC amplifier. The desired output power level is set by adjusting the ALC ADJ potentiometer, 2R13.

The sampled RF energy is detected and converted to a filtered DC voltage by Automatic Detector level module 2A2 mounted on the side of the PA chamber. This DC signal which is proportional to the amplitude of the RF carrier is fed via a coax cable to the Automatic Level Control module, 3A7, mounted in the control panel. ALC control potentiometer, 3R13, adjusts the amount of negative DC feedback voltage applied to the two-stage DC coupled amplifiers, 3Q1 and 3Q2, of 3A7 module.

Transistor (3Q1) is biased to draw a reasonable amount of current to cause a voltage drop across the OUTPUT POWER control (3R10). The controlling action is such that an increase in the sampled RF, perhaps due to an increase in line voltage acts to increase the base bias on transistor (3Q2) causing it to draw more collector current resulting in an increased voltage drop across resistor (3R141). This increased voltage drop produces a reduction in forward bias on the base of transistor (3Q1). The reduced bias decreases (3Q1) collector current flow permitting the bias voltage on the driver to increase.

The increased bias reduces the RF output of the driver and tends to compensate for the initial rise in the power amplifier RF output. The action is practically instantaneous and is very much the same as an automatic gain control in a receiver.

Resistor (3R140) is a voltage dropping resistor for the Zener regulator (3VR4).

4-6 Overload Protection and Automatic Recycling Circuits

4-6.1 Basic Overload Protection

Protection against serious damage in the event of a component failure is provided at many points in the transmitter and is done in many ways.

The following paragraphs will describe the various forms:

<u>Component</u>	<u>Symbol</u>	<u>Rating</u>
Line Breaker	3CB3	225 Amp
Blower Breaker	3CB1	20 Amp
Filament Breaker	3CB2	20 Amp
Fuse (for 220 VAC-Phase 1) Meter Ckt.	3F1	1/2 Amp
Fuse (for 220 VAC-Phase 2) Meter Ckt.	3F2	1/2 Amp
Fuse (for 220 VAC-Phase 3) Meter Ckt.	3F3	1/2 Amp
Fuse (24V Power Supply)	3F4	1 Amp
Fuse (24V Power Supply)	3F5	1 Amp
Fuse (24V Supply Output)	-	3 Amp

4-6.2 Automatic Re-cycling System - General

Other forms of protection are provided by the overload re-cycling system. The following four parameters are monitored and the system will react to any change in excess of a preset threshold:

Driver Cathode Current

Power Amplifier Cathode Current

High Voltage (Excess current drain external to
power supply).

VSWR at output of harmonic filter. (Optional in FM-12KD)

In the event of an excess in any of the four parameters, an overload re-cycling system is brought into action. An overload will shut down the high-voltage circuits for a 2-second period and also start a 60-second timing interval. After the 2-second interval, the high-voltage will again be applied. If the fault is still present the process will be automatically repeated. This can take place three times within the 60-second period after which the system will lock out the high voltage circuits. Fault indicator lights will show the location of the fault. Re-setting of the system must be done manually by pushing the PLATE RESET switch (3S8) after the fault has been cleared.

If the fault occurs only once, the 2-second timer will automatically re-cycle the system to its initial state. The fault light associated with the circuit trouble will remain lit until manually extinguished by the RESET button. This is to provide a memory function for the major faults causing shut-down.

The first overload will shut down the high voltage circuits for a 2-second interval and also start a 60-second timing interval. After the 2-second interval the circuits are again enabled, however, if the fault has not cleared, the circuit will disable the high voltage before the voltage is applied. If, as in a power overload, the fault disappears when the high voltage is down, then the high voltage will again be applied. If the fault should appear again when the high voltage is applied the

process will repeat itself. If the process occurs 3 times within a 60-second time interval the system will lock out the high voltage circuits. The system may be cleared by depressing the Plate Reset Switch (3S8) after the fault has been corrected.

4-6.3 Automatic Recycling System - Detailed Analysis

- 4-6.3.1 The Automatic Recycling System utilizes computer type integrated circuits to perform control logic functions. The system is designed to:
1. Detect a fault on one of four lines
 2. Light and maintain a lamp indicating the specific fault
 3. Remove the high voltage for a period of 2 secs.
 4. Return the transmitter to operation only if the fault has cleared.
 5. If three faults occur in 60 seconds remove the transmitter from operation (locks out the high voltage).
 6. If 60 seconds elapse with 2 or less faults, clear the count.
 7. Clear the count and indication when a start command occurs (Note:- When power is applied to the unit one or more fault indications occur due to the random order in which the logic is energized. This clears the meaningless indication automatically.)

4-6.3.2 Introduction to logic

Since use of logic devices in broadcast transmitters is relatively new, the basic functions will be described here. The devices used on Transistor-Transistor-logic (TTL) 7400 series which operates at voltage levels of about 5 Volts. It is mostly Medium Scale Integration (MSI) manufactured in Dual in-line Plastic (DIP) packages rather than discrete circuits.

These circuits operate at levels called 0 and 1. A "0" level is 0 to .8 Volts and a "1" is 2.0 to 5.0 Volts. The region from .8 to 2.0 is usually a "1", but cannot be depended upon.

Devices Used:

(A) Nand Gate

Symbol:



Types: SN7400N quad dual input nand gate

SN7430N eight input nand gate

The Truth Table to describe a 2 input nand gate is:

Case	Inputs		Output
	A	B	C
#1	0	0	1
#2	0	1	1
#3	1	0	1
#4	1	1	0

It can thus be seen that the output is a "1" for all cases except when both inputs are high or it can be said the output is low only when all inputs are high.

For an eight input gate the same is true - the output is low only when all inputs are high.

(B) The Inverter or Not Gate

Symbol:



Type: SN7404N

Truth table:

<u>Input</u>	<u>Output</u>
A	B
0	1
1	0

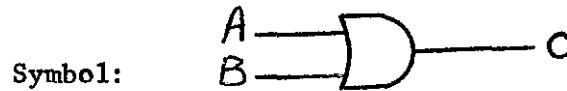
Thus the output is always the opposite of the input.

An inverter may also be created by using a nand gate.

This done by tying both inputs together as shown below. Operation may be verified from the truth

table of 4-6.3.2-A

(C) Or Gate:



Type: No individual or gates used, but used in other devices.

Truth table:

<u>Inputs</u>		<u>Output</u>
A	B	C
0	0	0
0	1	1
1	0	1
1	1	1

Thus the output is high whenever any input is high.

It may also be said to have a 0 output only if all inputs are Zero.

(D) Schmitt Triggers

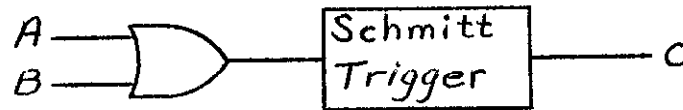
Symbol: No Special Symbol

Types: MC9809P - Quad Dual Input Schmitt Trigger

SN7413N - Dual Quad Input Schmitt Trigger

Description: The Schmitt trigger is a device which remains off until a specified voltage level is reached (called threshold level). It then turns on (output = 1) and remains on until the voltage decreases to another specified level. This turn off level usually is less than the turn on level.

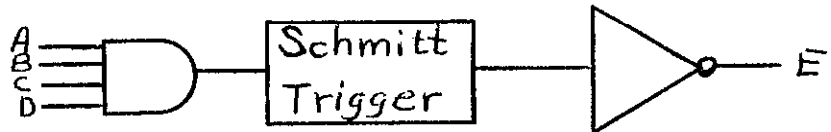
MC9809P: Each Schmitt Trigger is preceded by a dual input OR gate. The symbol circuitry may appear as follows:



The device MC9809P contains four of these circuits.

V On = 1.40 V V Off = .70 V

SN7413N: Each Schmitt Trigger is preceded by a four input AND gate. The output is followed by an inverter. The symbol circuits appears as follows:



This may be simplified to appear as a four input Nand Gate as shown below:



(E) Monostable Multivibrator or one shot.

Symbol: No symbol

Type: SN74121N

Description: This is a typical one shot with 3 inputs, 2 outputs and external timing circuits.

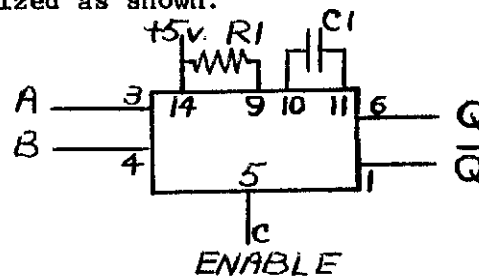
When fired the Q output goes high, $\bar{Q}$ goes low.

When reset Q is low and $\bar{Q}$ is high.

The device may be fired in two ways.

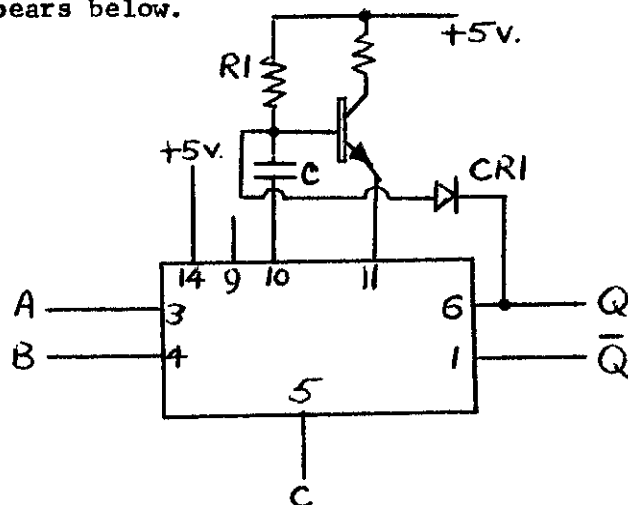
1. If C is high, it will fire when either A or B goes low.
2. If either A or B is low it will fire when C goes high.

The one shot does require a transition to trigger. Once fired the inputs are locked out for future transitions until the cycle has completed itself. Normally the one shot is utilized as shown:



With R_1 and C_1 being timing components the 2-second timer utilized is constructed in this manner.

For longer periods a transistor is used to multiply the capacity. The circuit configuration appears below.



CR₁ provides a rapid discharge for the capacitor to insure proper termination of the cycle.

Both the 60-second and 180-second timer use the capacitor multiplier. Only the 180-second timer uses the discharge diode.

(F) Counter - 4 Bit Resettable Up Counter

Symbol: No special symbol

Type: SN7493N

Description: This device contains 2 sections A & B. The A section contains a single bit flip-flop and is not used. The B section contains a 3 Bit Counter which counts negative transitions. Only the first 2 bits are actually used. There are 2 inputs to reset and both must operate together thus they are tied together. The reset inputs reset the count to zero when high. They must be held at 0 to count.

(G) Flip-Flop

Symbol: No special symbol is used for a Flip-Flop

Type: SN7474N Dual D-Type Edge-Triggered Flip-Flop

This device has one input (D) and two outputs (Q and $\bar{Q}$). When the clock input is pulsed, the D input is transferred to the output. The clear input must be held at a "1" in order to clock an input, and when set at Logic 0 will reset the Q output to Logic 0. The device has a preset input which automatically sets the Q output to a Logic 1.

The circuit which is used in the Lamp Driver Circuit ties the input D to Logic 1. The fault signal from the fault detector board goes to the clock input. Thus when a fault occurs the Logic 1 is clocked to the Q output. The Q output remains at Logic 1 until a clear signal is received.

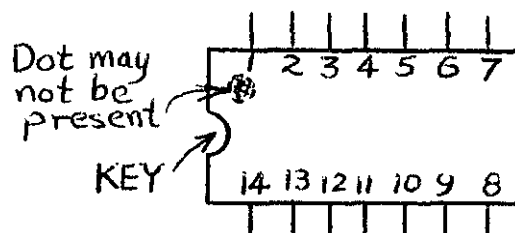
All the devices are 14 lead DIP.

Vcc (+5) and Gnd are supplied on the following pins:

<u>Device</u>	<u>Vcc</u>	<u>Gnd</u>
SN7400N	14	7
SN7404N	14	7
SN74121N	14	7
SN7413	14	7
SN7474	14	7
SN7493N	5	10
MC9809D	11	4

The devices appear as below:

Bottom View



The following reproductions from the Texas Instrument manual are shown for the reader's convenience.

CIRCUIT TYPES SN5413, SN7413 DUAL NAND SCHMITT TRIGGERS

recommended operating conditions

		SN5413			SN7413			UNIT
		MIN	NOM	MAX	MIN	NOM	MAX	
Supply voltage V_{CC}		4.5	5	5.5	4.75	5	5.25	V
Fan-out from each output, N	High logic level			20			20	
	Low logic level			10			10	
Operating free-air temperature range, T_A		-55	0	125	0	25	70	°C
Maximum input rise and fall times		No restriction			No restriction			

electrical characteristics over recommended operating free-air temperature range (unless otherwise noted)

PARAMETER	TEST FIGURE	TEST CONDITIONS†	MIN	TYP‡	MAX	UNIT
V_{T+} Positive-going threshold voltage	94	$V_{CC} = 5\text{ V}$	1.5	1.7	2	V
V_{T-} Negative-going threshold voltage	95	$V_{CC} = 5\text{ V}$	0.6	0.9	1.1	V
$V_{T+} - V_{T-}$ Hysteresis	94 & 95	$V_{CC} = 5\text{ V}$	0.4	0.8		V
V_I Input clamp voltage	97	$V_{CC} = \text{MIN}$, $I_I = -12\text{ mA}$			-1.5	V
V_{OH} High-level output voltage	95	$V_{CC} = \text{MIN}$, $V_I = 0.6\text{ V}$, $I_{OH} = -800\text{ }\mu\text{A}$	2.4	3.3		V
V_{OL} Low-level output voltage	94	$V_{CC} = \text{MIN}$, $V_I = 2\text{ V}$, $I_{OL} = 16\text{ mA}$		0.22	0.4	V
I_{T+} Input current at positive-going threshold	94	$V_{CC} = 5\text{ V}$, $V_I = V_{T+}$	-0.65			mA
I_{T-} Input current at negative-going threshold	95	$V_{CC} = 5\text{ V}$, $V_I = V_{T-}$	-0.85			mA
I_I Input current at maximum input voltage	96	$V_{CC} = \text{MAX}$, $V_I = 5.5\text{ V}$			1	mA
I_{IH} High-level input current	96	$V_{CC} = \text{MAX}$, $V_I = 2.4\text{ V}$			40	μA
I_{IL} Low-level input current	97	$V_{CC} = \text{MAX}$, $V_I = 0.4\text{ V}$		-1	-1.6	mA
I_{OS} Short-circuit output current§	98	$V_{CC} = \text{MAX}$	-18		-55	mA
I_{CCH} Supply current, high-level output	99	$V_{CC} = \text{MAX}$, $V_I = 0$		14	23	mA
I_{CCL} Supply current, low-level output	99	$V_{CC} = \text{MAX}$, $V_I = 4.5\text{ V}$		20	32	mA

† For conditions shown as MIN or MAX, use the appropriate value specified under recommended operating conditions for the applicable device type.

‡ All typical values are at $V_{CC} = 5\text{ V}$, $T_A = 25^\circ\text{C}$.

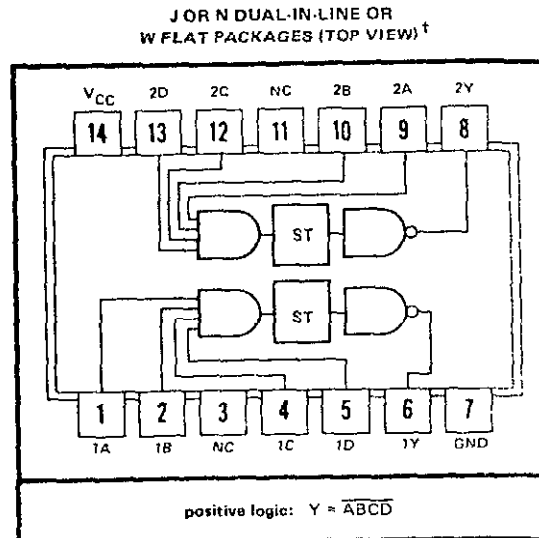
§ Not more than one output should be shorted at a time.

switching characteristics, $V_{CC} = 5\text{ V}$, $T_A = 25^\circ\text{C}$, $N = 10$

PARAMETER	TEST FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{PLH} Propagation delay time, low-to-high-level output	100	$C_L = 15\text{ pF}$, $R_L = 400\text{ }\Omega$		18	27	ns
t_{PHL} Propagation delay time, high-to-low-level output	100	$C_L = 15\text{ pF}$, $R_L = 400\text{ }\Omega$		15	22	ns

CIRCUIT TYPES SN5413, SN7413 DUAL NAND SCHMITT TRIGGERS

- Operation from Very Slow Edges
- Temperature-Compensated Threshold Levels
- Temperature-Compensated Hysteresis, Typically 0.8 V
- High Noise Immunity



NC—No internal connection.

†Pin assignments for these circuits are the same for all packages.

description

The SN5413 and SN7413 dual Schmitt triggers consist of two identical Schmitt-trigger circuits in monolithic integrated circuit form. Logically, each circuit functions as a four-input NAND gate, but because of the Schmitt action, the gate has different input threshold levels for positive- and negative-going signals. The hysteresis, or backlash, which is the difference between the two threshold levels, is typically 800 mV.

An important design feature is the built-in temperature compensation which ensures very high stability of the threshold levels and the hysteresis over a very wide temperature range. Typically, the hysteresis changes by 3% over the temperature range of -55°C to 125°C and the upper threshold changes by 1% over the same range. The SN5413/SN7413 can be triggered from the slowest of input ramps and still give clean, jitter-free output signals. It can also be triggered from straight d-c levels.

These circuits are fully compatible with most other TTL, DTL, or MSI circuits. The SN5413 is characterized for operation over the full military temperature range of -65°C to 125°C ; the SN7413 is characterized for operation from 0°C to 70°C .

absolute maximum ratings over operating free-air temperature range (unless otherwise noted)

Supply voltage V_{CC} (see Note 1)	7 V
Input voltage (see Note 1)	5.5 V
Interemitter voltage (see Note 2)	5.5 V
Operating free-air temperature range: SN5413 Circuits	-55°C to 125°C
SN7413 Circuits	0°C to 70°C
Storage temperature range	-65°C to 150°C

NOTES: 1. Voltage values, except interemitter voltage, are with respect to network ground terminal.
2. This is the voltage between two emitters of a multiple-emitter transistor.

CIRCUIT TYPES SN54121, SN74121 MONOSTABLE MULTIVIBRATORS

logic

TRUTH TABLE (See Notes 1 thru 3)

I _n INPUT			I _{n+1} INPUT			OUTPUT
A1	A2	B	A1	A2	B	
1	1	0	1	1	1	Inhibit
0	X	1	0	X	0	Inhibit
X	0	1	X	0	0	Inhibit
0	X	0	0	X	1	One Shot
X	0	0	X	0	1	One Shot
1	1	1	X	0	1	One Shot
1	1	1	0	X	1	One Shot
X	0	0	X	1	0	Inhibit
0	X	0	1	X	0	Inhibit
X	0	1	1	1	1	Inhibit
0	X	1	1	1	1	Inhibit
1	1	0	X	0	0	Inhibit
1	1	0	0	X	0	Inhibit

$$1 = V_{in(1)} \geq 2V$$

$$0 = V_{in(0)} \leq 0.8V$$

- NOTES:
1. t_n = time before input transition.
 2. t_{n+1} = time after input transition.
 3. X indicates that either a logical 0 or 1 may be present.
 4. NC = No Internal Connection.

description

This monolithic TTL monostable multivibrator features d-c triggering from positive or gated negative-going inputs with inhibit facility. Both positive and negative-going output pulses are provided with full fan-out to 10 normalized loads.

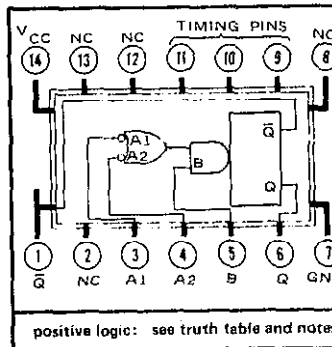
Pulse triggering occurs at a particular voltage level and is not directly related to the transition time of the input pulse. Schmitt-trigger input circuitry (TTL compatible and featuring temperature-independent backlash, See Figure L) for the B input allows jitter-free triggering from inputs with transition times as slow as 1 volt/second, providing the circuit with an excellent noise immunity of typically 1.2 volts. A high immunity to V_{CC} noise of typically 1.5 volts is also provided by internal latching circuitry.

Once fired, the outputs are independent of further transitions on the inputs and are a function only of the timing components. Input pulses may be of any duration relative to the output pulse. Output pulse lengths may be varied from 40 nanoseconds to 40 seconds by choosing appropriate timing components. With no external timing components (i.e., pin 9 connected to pin 14, pins 10, 11 open) an output pulse of typically 30 nanoseconds is achieved which may be used as a d-c triggered reset signal. Output rise and fall times are TTL compatible and independent of pulse length.

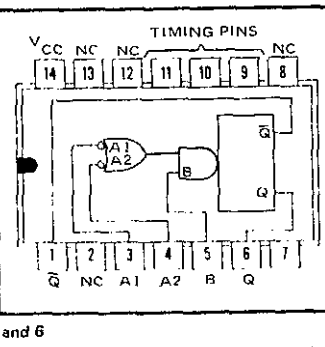
Pulse width is achieved through internal compensation and is virtually independent of V_{CC} and temperature. In most applications, pulse stability will only be limited by the accuracy of external timing components.

—SEE ORDERING INSTRUCTIONS PAGE 1-1—

S FLAT PACKAGE
(TOP VIEW)
(SEE NOTES 6 THRU 9)

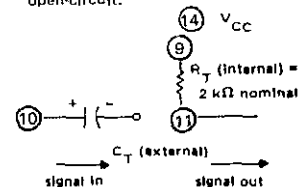


J OR N DUAL-IN-LINE PACKAGE
(TOP VIEW)
(SEE NOTES 6 THRU 9)



positive logic: see truth table and notes 5 and 6

5. A1 and A2 are negative edge triggered logic inputs, and will trigger the one shot when either or both go to logical 0 with B at logical 1.
6. B is a positive Schmitt-trigger input for slow edges or level detection, and will trigger the one shot when B goes to logical 1 with either A1 or A2 at logical 0. (See Truth Table)
7. External timing capacitor may be connected between pin 10 (positive) and pin 11. With no external capacitance, an output pulse width of typically 30 ns is obtained.
8. To use the internal timing resistor (2 kΩ nominal), connect pin 9 to pin 14.
9. To obtain variable pulse width connect external variable resistance between pin 9 and pin 14. No external current limiting is needed.
10. For accurate repeatable pulse widths connect an external resistor between pin 11 and pin 14 with pin 9 open-circuit.



CIRCUIT TYPES SN5474, SN7474

DUAL D-TYPE EDGE-TRIGGERED FLIP-FLOPS

logic

TRUTH TABLE (Each Flip-Flop)

t_n	t_{n+1}	
INPUT	OUTPUT	OUTPUT
D	Q	$\bar{Q}$
0	0	1
1	1	0

NOTES: 1. t_n = bit time before clock pulse.
2. t_{n+1} = bit time after clock pulse

description

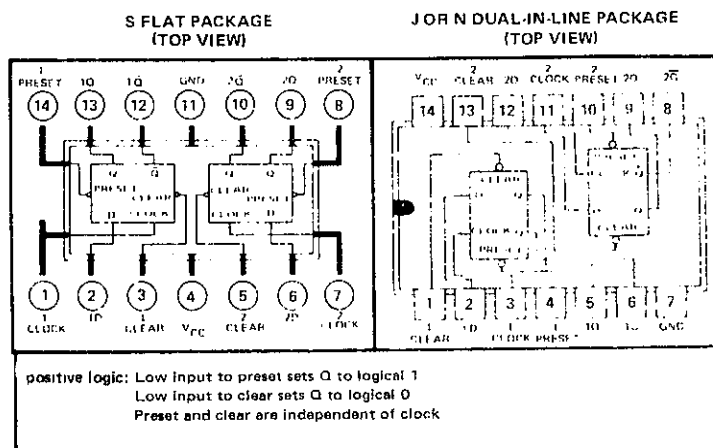
These monolithic, dual, D-type, edge-triggered flip-flops feature direct clear and preset inputs and complementary Q and $\bar{Q}$ outputs. Input information is transferred to the outputs on the positive edge of the clock pulse.

Clock triggering occurs at a voltage level of the clock pulse and is not directly related to the transition time of the positive going pulse. After the clock input threshold voltage has been passed, the data input (D) is locked out.

These dual flip-flops have the same clocking characteristics as the SN5470/SN7470 gated (edge-triggered) flip-flop circuits, and both are ideally suited for medium- to-high-speed applications. They can result in a significant saving in system power dissipation and package count in applications where input gating is not required.

recommended operating conditions

	MIN	NOM	MAX	UNIT
Supply Voltage V_{CC} : SN5474 Circuits	4.5	5	5.5	V
SN7474 Circuits	4.75	5	5.25	V
Operating Free-Air Temperature Range, T_A : SN5474 Circuits	55	25	125	$^{\circ}\text{C}$
SN7474 Circuits	0	25	70	$^{\circ}\text{C}$
Normalized Fan-Out From Each Output, N			10	
Width of Clock Pulse, $t_{p(\text{clock})}$ (See figure 71)	30			ns
Width of Preset Pulse, $t_{p(\text{preset})}$ (See figure 67)	30			ns
Width of Clear Pulse, $t_{p(\text{clear})}$ (See figure 67)	30			ns



—SEE ORDERING INSTRUCTIONS PAGE 1-1—

MSI TTL HIGH-SPEED RIPPLE-THROUGH COUNTERS

for applications in

• Digital Computer Systems

• Data-Handling Systems

• Control Systems

logic

TRUTH TABLE (See Notes 1, 2, and 3)

COUNT	Q	D	C	B	A
0	0	0	0	0	0
1	0	0	0	1	1
2	0	0	1	0	0
3	0	0	1	0	1
4	0	1	0	0	0
5	0	1	0	0	1
6	0	1	1	0	0
7	0	1	1	0	1
8	1	0	0	0	0
9	1	0	0	0	1
10	1	0	1	0	0
11	1	0	1	0	1
12	1	1	0	0	0
13	1	1	0	0	1
14	1	1	1	0	0
15	1	1	1	0	1

- NOTES: 1. Output A connected to input B.
 2. To reset all outputs to logical 0 both $R_0(1)$ and $R_0(2)$ inputs must be at logical 1.
 3. Either (or both) reset inputs $R_0(1)$ and $R_0(2)$ must be at a logical 0 to count.

description

These high-speed, monolithic 4 bit binary counters consist of four master-slave flip-flops which are internally interconnected to provide a divide-by-two counter and a divide-by-eight counter. A gated direct reset line is provided which inhibits the count inputs and simultaneously returns the four flip-flop outputs to a logical 0. As the output from flip-flop A is not internally connected to the succeeding flip-flops the counter may be operated in two independent modes:

1. When used as a 4-bit ripple-through counter, output A must be externally connected to input B. The input count pulses are applied to input A. Simultaneous divisions of 2, 4, 8, and 16 are performed at the A, B, C, and D outputs as shown in the truth table above.
2. When used as a 3-bit ripple-through counter, the input count pulses are applied to input B. Simultaneous frequency divisions of 2, 4, and 8 are available at the B, C, and D outputs. Independent use of flip-flop A is available if the reset function coincides with reset of the 3-bit ripple-through counter.

These circuits are completely compatible with Series 54/74 TTL and DTL logic families. Average power dissipation is 32 mW per flip-flop (128 mW total).

absolute maximum ratings (over operating temperature range unless otherwise noted)

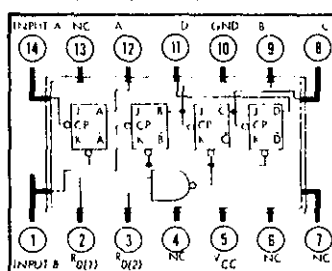
Supply Voltage V_{CC} (See Note 4)	7 V
Input Voltage, V_{in} (See Notes 4 and 5)	5.5 V
Operating Case Temperature Range: SN5493S	-55°C to 125°C
Operating Free-Air Temperature Range: SN5493J, SN5493N	-55°C to 125°C
SN7493 Circuits	0°C to 70°C
Storage Temperature Range	-65°C to 150°C

- NOTES: 4. These voltage values are with respect to network ground terminal.
 5. Input signals must be zero or positive with respect to network ground terminal.

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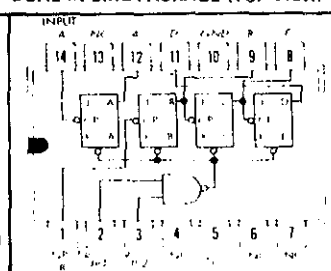
FLAT PACKAGE (TOP VIEW)



positive logic: see truth table

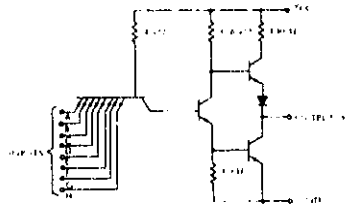
NC: No Internal Connection

DUAL-IN-LINE PACKAGE (TOP VIEW)



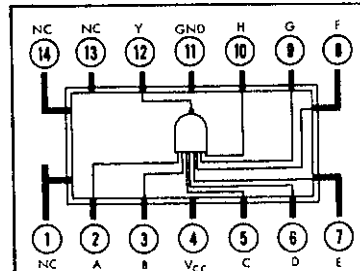
CIRCUIT TYPES SN5430, SN7430 8-INPUT POSITIVE NAND GATES

schematic

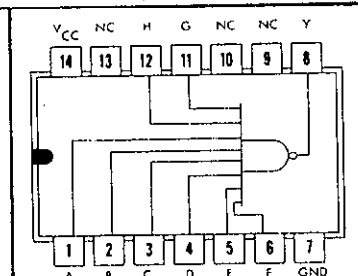


Component values shown are nominal.
NC = No Internal Connection

S FLAT PACKAGE
(TOP VIEW)



J OR N DUAL-IN-LINE PACKAGE
(TOP VIEW)



positive logic: $Y = ABCDEFGH$

recommended operating conditions

Supply Voltage V_{CC} :	SN5430 Circuits	
	SN7430 Circuits	
Normalized Fan-Out From Output, N		
Operating Free-Air Temperature Range, T_A :	SN5430 Circuits	
	SN7430 Circuits	

MIN	NOM	MAX	UNIT
4.5	5	5.5	V
4.75	5	5.25	V
	10		
-55	25	125	°C
0	25	70	°C

electrical characteristics (over recommended operating free-air temperature range unless otherwise noted)

PARAMETER	TEST FIGURE	TEST CONDITIONS†	MIN	TYP‡	MAX	UNIT
$V_{in(1)}$ Logical 1 input voltage required at all input terminals to ensure logical 0 level at output	1	V_{CC} MIN	2			V
$V_{in(0)}$ Logical 0 input voltage required at any input terminal to ensure logical 1 level at output	2	V_{CC} MIN			0.8	V
$V_{out(1)}$ Logical 1 output voltage	2	V_{CC} MIN, $V_{in} = 0.8$ V, $I_{load} = -400 \mu A$	2.4	3.3		V
$V_{out(0)}$ Logical 0 output voltage	1	V_{CC} MIN, $V_{in} = 2$ V, $I_{sink} = 16$ mA	0.22	0.4		V
$I_{in(0)}$ Logical 0 level input current (each input)	3	V_{CC} MAX, $V_{in} = 0.4$ V			-1.6	mA
$I_{in(1)}$ Logical 1 level input current (each input)	4	$V_{CC} = MAX$, $V_{in} = 2.4$ V $V_{CC} = MAX$, $V_{in} = 5.5$ V			40 1	μA mA
I_{OS} Short-circuit output current	5	$V_{CC} = MAX$	SN5430 -20 SN7430 -18		-55 -55	mA
$I_{CC(0)}$ Logical 0 level supply current	6	$V_{CC} = MAX$, $V_{in} = 5$ V		3	6	mA
$I_{CC(1)}$ Logical 1 level supply current	6	$V_{CC} = MAX$, $V_{in} = 0$		1	2	mA

switching characteristics, $V_{CC} = 5$ V, $T_A = 25^\circ C$, $N = 10$

PARAMETER	TEST FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{pd0} Propagation delay time to logical 0 level	65	$C_L = 15$ pF, $R_L = 400 \Omega$		8	15	ns
t_{pd1} Propagation delay time to logical 1 level	65	$C_L = 15$ pF, $R_L = 400 \Omega$		13	22	ns

† For conditions shown as MIN or MAX, use the appropriate value specified under recommended operating conditions for the applicable device type.

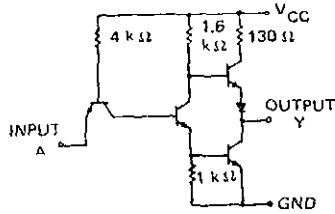
‡ All typical values are at $V_{CC} = 5$ V, $T_A = 25^\circ C$.

§ Not more than one output should be shorted at a time.

—SEE ORDERING INSTRUCTIONS PAGE 1-1—

CIRCUIT TYPES SN5404, SN7404 HEX INVERTERS

schematic (each inverter)



NOTE: Component values shown are nominal

recommended operating conditions

Supply Voltage V_{CC} : SN5404 Circuits
SN7404 Circuits
Normalized Fan-Out From Each Output, N
Operating Free-Air Temperature Range, T_A : SN5404 Circuits
SN7404 Circuits

MIN	NOM	MAX	UNIT
4.5	5	5.5	V
4.75	5	5.25	V
	10		
-55	25	125	°C
0	25	70	°C

electrical characteristics (over recommended operating free-air temperature range unless otherwise noted)

PARAMETER	TEST FIGURE	TEST CONDITIONS†	MIN	TYP‡	MAX	UNIT
$V_{in(1)}$ Logical 1 input voltage required at input terminal to ensure logical 0 level at output	15	$V_{CC} = \text{MIN}$	2			V
$V_{in(0)}$ Logical 0 input voltage required at any input terminal to ensure logical 1 level at output	16	$V_{CC} = \text{MIN}$			0.8	V
$V_{out(1)}$ Logical 1 output voltage	16	$V_{CC} = \text{MIN}$, $V_{in} = 0.8 \text{ V}$, $I_{load} = -400 \mu\text{A}$	2.4	3.3		V
$V_{out(0)}$ Logical 0 output voltage	15	$V_{CC} = \text{MIN}$, $V_{in} = 2 \text{ V}$, $I_{sink} = 16 \text{ mA}$		0.22	0.4	V
$I_{in(0)}$ Logical 0 level input current (each Logical 0 level input current)	17	$V_{CC} = \text{MAX}$, $V_{in} = 0.4 \text{ V}$			-1.6	mA
$I_{in(1)}$ Logical 1 level input current	18	$V_{CC} = \text{MAX}$, $V_{in} = 2.4 \text{ V}$ $V_{CC} = \text{MAX}$, $V_{in} = 5.5 \text{ V}$			40 1	μA mA
I_{OS} Short-circuit output current§	19	$V_{CC} = \text{MAX}$			-20 -18	mA
$I_{CC(0)}$ Logical 0 level supply current	20	$V_{CC} = \text{MAX}$, $V_{in} = 5 \text{ V}$		18	33	mA
$I_{CC(1)}$ Logical 1 level supply current	20	$V_{CC} = \text{MAX}$, $V_{in} = 0$		6	12	mA

switching characteristics, $V_{CC} = 5 \text{ V}$, $T_A = 25^\circ\text{C}$, $N = 10$

PARAMETER	TEST FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{pd0} Propagation delay time to logical 0 level	65	$C_L = 15 \text{ pF}$, $R_L = 400 \Omega$		8	15	ns
t_{pd1} Propagation delay time to logical 1 level	65	$C_L = 15 \text{ pF}$, $R_L = 400 \Omega$		12	22	ns

† For conditions shown as MIN or MAX, use the appropriate value specified under recommended operating conditions for the applicable device type.

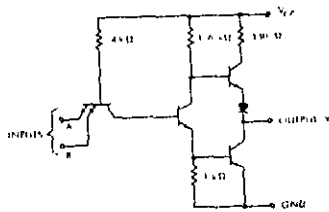
‡ All typical values are at $V_{CC} = 5 \text{ V}$, $T_A = 25^\circ\text{C}$.

§ Not more than one output should be shorted at a time.

—SEE ORDERING INSTRUCTIONS PAGE 1-1—

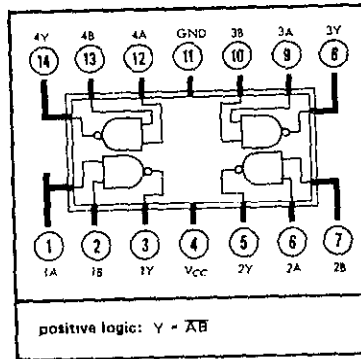
CIRCUIT TYPES SN5400, SN7400 QUADRUPLE 2-INPUT POSITIVE NAND GATES

schematic (each gate)

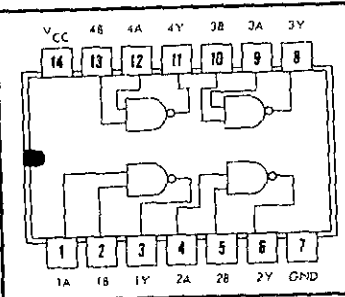


NOTE: Component values shown are nominal.

F FLAT PACKAGE
(TOP VIEW)



J OR N DUAL-IN-LINE PACKAGE
(TOP VIEW)



positive logic: $Y = AB$

recommended operating conditions

Supply Voltage V_{CC} : SN5400 Circuits
SN7400 Circuits

Normalized Fan-Out From Each Output, N

Operating Free-Air Temperature Range, T_A : SN5400 Circuits
SN7400 Circuits

MIN	NOM	MAX	UNIT
4.5	5	5.5	V
4.75	5	5.25	V
	10		
-55	25	125	°C
0	25	70	°C

electrical characteristics (over recommended operating free-air temperature range unless otherwise noted)

PARAMETER	TEST FIGURE	TEST CONDITIONS†	MIN	TYP‡	MAX	UNIT
$V_{in(1)}$ Logical 1 input voltage required at both input terminals to ensure logical 0 level at output	1	$V_{CC} = \text{MIN}$	2			V
$V_{in(0)}$ Logical 0 input voltage required at either input terminal to ensure logical 1 level at output	2	$V_{CC} = \text{MIN}$			0.8	V
$V_{out(1)}$ Logical 1 output voltage	2	$V_{CC} = \text{MIN}$, $V_{in} = 0.8 \text{ V}$, $I_{load} = -400 \mu\text{A}$	2.4	3.3		V
$V_{out(0)}$ Logical 0 output voltage	1	$V_{CC} = \text{MIN}$, $V_{in} = 2 \text{ V}$, $I_{sink} = 16 \text{ mA}$	0.22	0.4		V
$I_{in(0)}$ Logical 0 level input current (each input)	3	$V_{CC} = \text{MAX}$, $V_{in} = 0.4 \text{ V}$			-1.6	mA
$I_{in(1)}$ Logical 1 level input current (each input)	4	$V_{CC} = \text{MAX}$, $V_{in} = 2.4 \text{ V}$ $V_{CC} = \text{MAX}$, $V_{in} = 5.5 \text{ V}$			40 1	μA mA
I_{OS} Short-circuit output current§	5	$V_{CC} = \text{MAX}$			-20 -18	mA
$I_{CC(0)}$ Logical 0 level supply current	6	$V_{CC} = \text{MAX}$, $V_{in} = 5 \text{ V}$			12 22	mA
$I_{CC(1)}$ Logical 1 level supply current	6	$V_{CC} = \text{MAX}$, $V_{in} = 0$			4 8	mA

switching characteristics, $V_{CC} = 5 \text{ V}$, $T_A = 25^\circ\text{C}$, $N = 10$

PARAMETER	TEST FIGURE	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_{pd0} Propagation delay time to logical 0 level	65	$C_L = 15 \text{ pF}$, $R_L = 400 \Omega$		7	15	ns
t_{pd1} Propagation delay time to logical 1 level	65	$C_L = 15 \text{ pF}$, $R_L = 400 \Omega$		11	22	ns

† For conditions shown as MIN or MAX, use the appropriate value specified under recommended operating conditions for the applicable device type.

‡ All typical values are at $V_{CC} = 5 \text{ V}$, $T_A = 25^\circ\text{C}$.

§ Not more than one output should be shorted at a time.

—SEE ORDERING INSTRUCTIONS PAGE 1-1—

4-6.3.3.1 Fault Level Control Board (3A4), Rev. D

Basically the fault level control board operates by detecting a threshold voltage level and then sending parallel fault signals to the control timer board (3A3) and the lamp driver board (3A1).

- (a) The VSWR fault level is detected by the closing of meter contacts on the VSWR meter (3M11). Contact closure applies 24 V to the fault level detector board. This signal is scaled by 3R122 and 3R123 and then inverted by 3IC1. (Note: The no fault output of 3IC1, Pin 6, is a Logic 1). Information on setting the VSWR meter contacts may be found in Para. 3-4.
- (b) The PA cathode fault level is sensed by 2R4 in the cathode circuit of the PA. The signal level is sent to the fault level control board, scaled by 3R117, and sent to the Schmitt trigger. The Schmitt trigger detects the fault level and inverts the signal. (Note: The no fault signal at 3IC1, Pin 8, is a Logic 1).
- (c) The High Voltage overload fault level (HVOL)
The HVOL fault level is a negative voltage sensed by 3R42. Since the Schmitt trigger is capable of dealing with positive voltages only and we are only interested in the magnitude of the voltage, the HVOL input is treated as follows:

1. The HVOL becomes the Reference or "Ground".
2. Ground becomes the signal input.
3. Power to supply the device is developed through 3R133 and 3VR6.
4. Fault level input may be measured from TP1 to ground.
5. This input is scaled by 3R118, detected and inverted by 3IC2, converted to a normal logic level by 3Q14. 3Q14 inverts the signal so 3IC3 again inverts it to restore it to the required form.

Normal no fault logic levels are:

3IC2 Pin 6 - Logic 1 Reference TP1
 3Q14 Collector - Logic 0 Reference Gnd.
 3IC3 Pin 10 - Logic 1 Reference Gnd.

- (d) The driver Cathode fault level is sensed by 3R14, but is referenced from the HVOL input. The same technique for fault detection as that of the HVOL is used, but the level input is the top of 3R14. The signal is scaled by 3R116, detected and inverted by 3IC2, converted and inverted by 3Q3.

The normal no fault levels and references are:

3IC2 Pin 8 - Logic 1 Reference TP1
 3Q3 Collector - Logic 0 Reference Gnd.
 3IC Pin 12 - Logic 1 Reference TP1

- (e) Test Switch (3S18), diodes 3CR14 to 3CR17 and resistors 3R126 to 3R129 force "low" inputs to 3IC4 and the four inverters which drive the lamp drivers. Operating this switch creates an artificial fault to test the operation of the lamp driver board (3A1) and the control timer board (3A3). This switch will test the entire fault system but will not test the actual input to the Schmitt trigger. It should be used as a system test but not as a fault test.
- (f) The normal no fault outputs from the board are Logic 0.
- (g) Zener Diodes 3VR7, 3VR8 and 3VR9 with resistors 3R119, 3R120, and 3R121 provide protection from large excursions of the fault levels. They provide protection in the order of several hundred volts. Externally mounted surge protectors limit these voltages to 230 V. 2E1 protects the PA Cathode Circuit and is located adjacent to 2R4. 3E2 protects the Driver Cathode Circuit and is located adjacent to 3R14. 2E3 protects the HVOL input and is located adjacent to 2R9.

4-6.3.3.2 Fault Level Control Board (3A4), Rev. F

Fault Level Control Boards 3A4 revisions D and F are similar in function and are interchangeable. Refer to the schematic diagrams Fig. 4-1 and Fig. 4-4 for the following explanation.

- (a) The VSWR fault level is detected by the closing of meter relay contacts in the VSWR meter, 3M11. Contact closure applies 24 volts to the fault level detector board. This signal is scaled by voltage-divider 3R119 and 3R120 and inverted by 3IC1. The fault test signal from 3S18 is also inverted by 3IC1, thus the two signals are combined and inverted. The net operation is the OR function of a fault signal or a test signal.
- (b) The PA cathode fault level is sensed by the voltage drop across resistor 2R4 in the cathode circuit of the PA. The signal level is sent to the fault level control board. Variable resistance 3R117 and the relay coil resistance form a voltage divider. The fault level voltage is about 4 volts and 3R117 is used to set the fault threshold level at a convenient point below this level.

- (c) The High Voltage Overload fault level (HVOL) is a negative voltage (with respect to chassis ground) sensed across 3R42. Variable resistor 3R118 and relay 3K13 are the sensing elements. Operation is similar to that described above.
- (d) The Driver Cathode fault level is sensed across 3R14 but is referenced to the HVOL fault signal input (this is the "B-off ground point-not chassis ground). The relay trigger level is controlled by 3R116.
- (e) Each fault signal circuit is held to ground by the back contact (N.C.) of its respective reed relay. When one of the relays is energized the individual line is pulled to logic level "1" by a pull-up resistor connected to A+. This sends a logic "1" to the lamp driver board and to a diode OR gate composed of 3CR15 to 3CR18.
- (f) The TEST switch provides a logic "0" condition to all relays and the test input of 3IC1. When 3S18 is operated its output is switched to a logic "1" and the output of all relays and 3IC1 switch to a logic "1".
- (g) Externally mounted surge suppressors limit overload voltages to 230 volts in the event that large overload currents are drawn due to arc-overs or lightning strikes. Suppressor 2E1 protects the PA circuit and is located

adjacent to 2R4. 3E2 protects the Driver cathode circuit and is located adjacent to 3R14. 2E3 protects the HVOL input circuit and limits the B- signal to 230 volts. 2E3 is located adjacent to 2R9.

4-6.3.4 Control Timer (3A3)

The control timer board A-3 contains two subsystems:

1. Preheat/after cool 180-second timer.
2. Fault counter and recycling system.

180-Second Timer

The timer utilizes a long period monostable multi-vibrator described in Section 4-6.3.2E.

- Inputs: (1) When either the start switch (3S1) or the stop switch (3S2) is operated, 24 V is applied to the voltage divider 3R57 and 3R55. The output of this is about 2.6 V when 24 volts is applied. This voltage is applied to the input of 3IC21.
- (2) Whenever the filament circuit is energized +5 volts is applied by means of contacts 6 and 8 of 3K2 to a capacitor to the "one shot". The capacitor causes only a pulse to be applied thus making the one shot available for a stop command. The primary purpose of this input is to prevent the plate voltage from being applied should the filament relay drop out momentarily.

An interruption to the air flow could cause this.

- Outputs: (1) The 180-second timer provides a steady drive to 3IC23 which in turn operates 3K3 whenever the 180-second timer operates. Further explanation of 3K3 appears in Section 4-2-b and 4-2-f.
- (2) A pulse is coupled through 3C59 into the manual reset bus. If power failure occurs to the entire transmitter the system often energizes to a full fault count. This pulse insures that the counter and memory are cleared prior to resumption of normal operation.

Note: The function of relay 3K3 is to:

1. Prevent application of plate voltage during "preheat" period and during 2-second fault recycling period.
2. To insure blower operation during 180-second "cool-down" period.

4-6.3.5 Fault Counter and Recycling System

Refer to Fig. 4-1. When a fault occurs the output of the fault level control board (3IC14 Pin 8) goes high. This signal is fed to one input of a nand gate (3IC23 Pin 4) the remaining input is held high by voltage divider 3R49 and 3R50. At this time both inputs are high and the output goes low which triggers the 2-second timer (3IC19). The Q output goes to "1", the $\bar{Q}$ output to "0". The $\bar{Q}$ output is fed to one

input of a nand gate (3EC24 Pin 5). The other input is from the 180-second timer. During a no fault condition both inputs of this nand gate (3IC23 Pin 5 and Pin 4) are high. When 3IC23 Pin 5 goes low and its output (3IC23 Pin 6) goes high it turns on 3Q6 which operates relay 3K3. This removes the plate voltage. This same "0" level increments the counter. For a count of 1, 3IC22 Pin 9 is "1", Pin 8 is "0". At the end of 2 seconds the Q output goes low, the $\bar{Q}$ output goes high. When the $\bar{Q}$ output goes high both inputs of the 3IC24 Gate are high and the Plate Voltage is subsequently restored.

When the fault occurred the Q output of the 2-second one shot (3IC19 Pin 6) went high, which "pushed" the output of the voltage divider higher until the capacitor discharged. This point was already high, thus there was no change of logic state. When the Q output goes low it forces this point low. This is a change in logic state. When the 2-second shut-down occurs most faults or overloads will disappear and the fault signal will go low. The input to the 2-second timer will go high and remain so. The "0" pulse fed back from the Q output will normally have no effect. If, for some reason such as the VSWR meter contacts sticking, the fault condition stays, this pulse fed back to the gate (3IC23 Pin 5) insures that the input to the 2-second timer goes high and low again triggering off a second fault and so on until a count of 3 is reached.

The third change that happens when a fault occurs is the starting of the sixty-second timer. Capacitor 3C60 feeds a "0" pulse to an input which is already "0" thus affecting no logic state change.

When a second fault occurs, the process repeats itself. The sixty-second timer has already started and its inputs are locked out. The counter increments to a count of 2. 3IC22 Pin 9 becomes "0" and Pin 8 become "1".

When a third fault occurs the 2-second process again repeats itself. The counter outputs 3IC22 Pin 9 and Pin 8 both become "1". These points feed the inputs of a nand gate, 3IC24. Since both inputs are now high, the output now goes low. Thus with a count of 0, 1, or 2 this output is high and is used to enable the 2-second timer. When the count reaches 3, this output goes low and inhibits the 2-second timer and also turns off 3Q4 which in turn drops out 3K7. The back contacts of 3K7 Pins 5 & 8 close, lighting the reset light. The front contacts 1 and 3 prevent 1 plate voltage from being applied.

The nand gate of 3IC24 Pins 11, 12 & 13 act as a gate. The input from the counter circuit (3IC24 Pin 13) is normally a "1" thus enabling the gate. Any time a "1" is applied to Pin 12 by the sixty-second timer both inputs will be high and the output will go to zero. If the count goes to 3 the input to the nand gate goes low and the gate is inhibited. No

reset pulse can be transmitted from sixty-second timer.

A manual reset signal, or an automatic signal from the 180-second timer (3IC21 Pin 1) coupled through 3IC23 Pin 1-2 produces a "0" level which is coupled through 3IC24 Pin 9, the output is inverted and is applied to the reset input of the counter and to the reset input of the lamp Driver Board.

The Relay Drivers are simply 5 watt transistors which complete the ground connection for the relay.

4-6.3.6 Lamp Driver Board (3A1)

The lamp driver board consists of 2 dual edge triggered flip-flops. The Q output of the flip-flop drive transistors which complete the ground path of the individual fault lamps.

The D input of the flip-flop is continuously connected to Logic 1 and the fault signals are fed to the clock input. A fault signal will clock a Logic 1 into the output.

The reset is accomplished by inverting the reset signal with 3Q13. The normal no reset condition of the collector of 3Q13 is a Logic 1.

4-6.3.7 Alignment Procedure for Fault Level Control Board
(3A4 Rev. D)

Tools: Accurate VOM

Screw Driver

5/16" Wrench

Extender Board (3A9)

Transmitter:

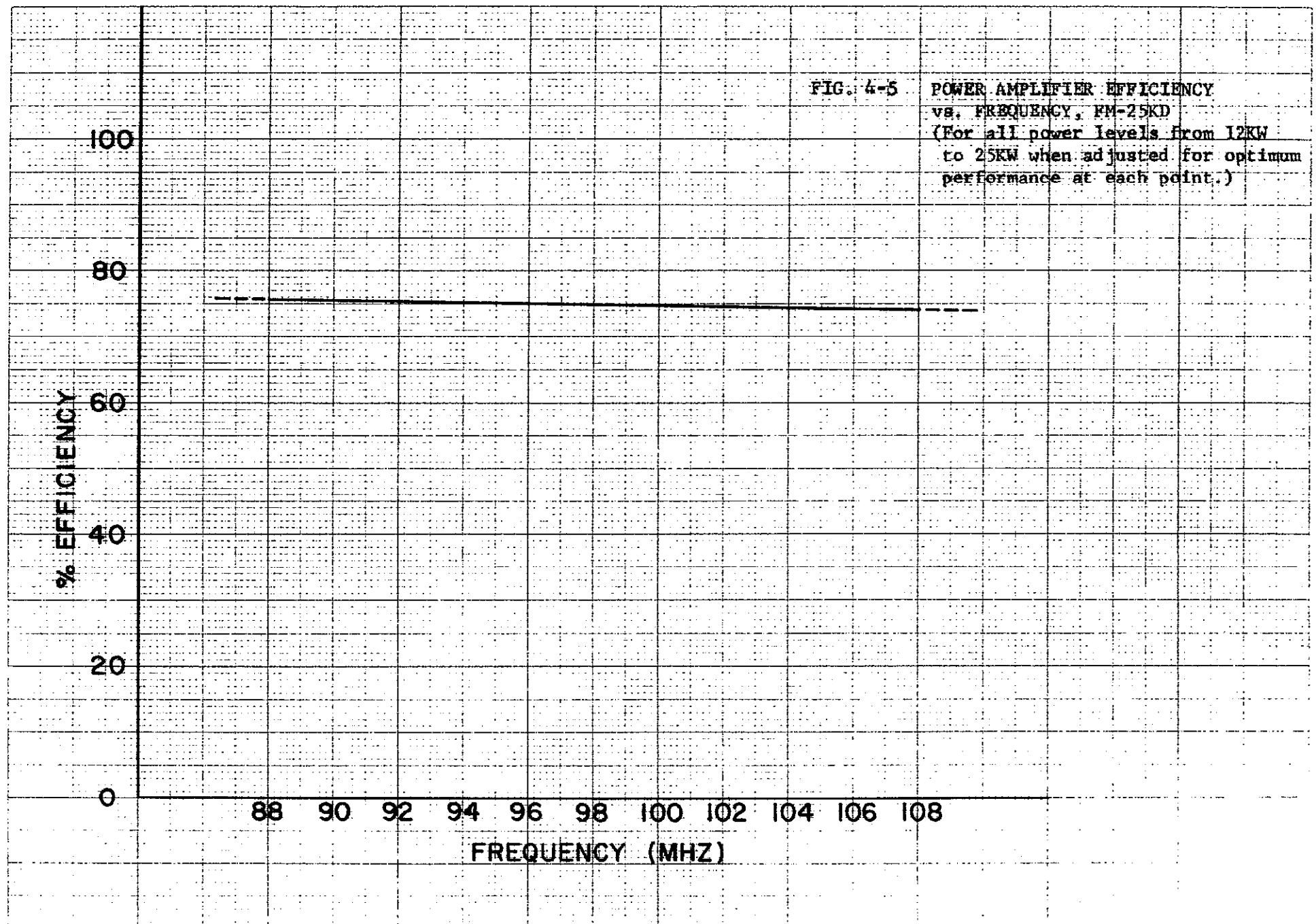
1. Stop transmitter.
2. Attach dummy load and bring transmitter to normal operational power.
3. Remove A-4 board, remove locknuts from 3R116, 3R117 and 3R118. Tighten retainer nut. Replace locknut loosely.
4. Plug A-4 into extender board and then plug both boards into A-4 slot.
5. Set driver cathode control (3R116), PA cathode control 3R117, and H. V. O/L control (3R118) to full CCW position.
6. Depress reset switch (3S8), then plate switch (3S4) to ON.
7. With the meter on the 2.5 V scale (or equivalent) measure the voltage on Pin 9 of IC-1. Advance (cw) PA cathode control (3R117) until the transmitter trips off and the PA cathode lamp lights. This voltage should be $1.7 \text{ V} \pm .2$.
8. Turn control to full CCW. Depress plate to OFF, depress reset switch, depress plate to ON.

9. Adjust metering Pin 9 of IC-1. Adjust the voltage for 1.0 V.
10. Attach the negative lead of the meter to TP-1.
11. Meter Pin of IC-2 (to TP-1). Repeat steps 6 to 9 adjusting the driver cathode control (3R116). The driver cathode lamp (3DS6) should light.
12. Meter Pin 5 of IC-2 (to TP-1). Repeat steps 6 to 9 adjusting the H.V. O/L control 3R118. The HV OL lamp 3DS8 should light.
13. Reset meter Pin 6 of 3IC-1 to ground using 10 V scale. Adjust the contact of the VSWR meter until the contact touches the meter needle. Pin 6 should go low, the transmitter should trip off and the VSWR lamp should light. Return the contact to the previous setting. (See Para. 3-4).
14. Depress and release test switch 3S18. Transmitter should trip off for 2 sec. (± 1 sec.). All four should extinguish for 2 seconds and relight. Repeat 2 more times. On 3rd time reset light should come on and stay on. Transmitter should not come on.
15. Wait 75 seconds after all previous faults then depress and release 3S18 for 2 faults. Wait 75 seconds and repeat Step 14. The number of faults should be 3.

16. Let transmitter operate at normal operating power for 10 minutes. Readjust each level to 1.0 volts. Tighten lock nuts, recheck, adjust if necessary.
17. Shut down transmitter, remove extender board, and replace A-4.

Note: The above procedure establishes a fault level as 140% of normal operating levels.

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SECTION V

MAINTENANCE

CAUTION: Disconnect safety switch before starting any maintenance procedures. This will insure that there will be no voltage of any level present within the cabinet.

Use a grounding stick and ascertain that all filter capacitors are discharged. There are redundant discharge paths on both high-voltage supplies to minimize the possibility of any charge remaining but it is always wise to be safe.

All blower and fan motors are permanently lubricated and require no periodic maintenance except the occasional cleaning of the squirrel cage and fan blades. There should be very little entry of dust into the cabinet since the fan at the cabinet rear maintains a positive internal air pressure.

Lead screws for the adjustable shorting bars are combined with Oilite mating threads and also do not require lubrication. The right-angle gears for the driver input and grid tuning are lubricated with Lubriplate. Because of the very limited usage, these gear pairs should only require an occasional inspection.

The replacement interval for the air filters at the cabinet rear will, of course, depend upon the environment and the local dust conditions. Periodic visual inspection will make it obvious when replacement becomes necessary.

Air filters can easily be inspected by turning counter-clockwise (2) 1/4 turn latches located at top of the louvered grille. This allows the hinged grille to drop down exposing the filter. See Figure 3-16. Filters are 16" x 20" x 1" thick fiberglass type used in heating and air conditioning systems.

Blow-out the driver and PA tube anode heat sinks with an air hose.

Examine the condition of the screen mesh in the lower sections of the driver and PA RF compartments. Clean, if necessary.

Check the conditions of the flexible air ducts and their associated clamps.

Look for discoloration or charring of resistor surfaces that would indicate excessive dissipation.

Also check for signs of overheating at finger stock contacts on the shorting bars for the driver and PA RF tuned circuits.

Operation of overload cycling circuits can be tested by manipulating the individual threshold controls, while the transmitter is operating, to deliberately simulate the repeated overload 2-second shutdowns until three have occurred and the system locks out. Reset all controls to original settings.

SECTION VI

REPLACEABLE PARTS

6-1 Ordering Information

If replacement or spare parts are required for any AEL transmitting equipment write or call:-

American Electronic Laboratories, Inc.
P. O. Box 552
Lansdale, Penna., 19446

Phone:- (215) 822-2929
Ask for Broadcast Sales or if not available, ask for
Broadcast Engineering

Information required:-

- (1) Station Call
- (2) Transmitter in use:- Model and Serial No.
- (3) Circuit symbol of part needed.
- (4) AEL Part Number or Manufacturer's part number.
- (5) Desired method of shipment including pick-up information for emergency shipments.

Every effort will be made to expedite shipment of urgently needed parts. The station operator should make an effort to keep on hand spare parts for transmitting components which experience indicates might be needed. AEL engineering personnel will be glad to confer with station personnel in making recommendations for a reasonable list of running spare parts.

6-2 Parts Location

All major parts are identified by component labels attached either on the component or on the chassis or cabinet surface near the component.

Many of the photographs included in this manual have part call-outs indicated by arrow and part number. Reference to the schematics will allow identification of components that are impossible to label.

It is to be noted that the components have prefix numbers to indicate general location areas as follows:-

- (a) No prefix, i.e., R19-FM Exciter chassis
- (b) "1" prefix, i.e., 1T4 - Main Cabinet mounted component
- (c) "2" prefix, i.e., 2C12 - Driver or Power Amplifier component
- (d) "3" prefix, i.e., 3S8 - Control Panel component

6-3 Replaceable Parts List

The following tabulated list of parts is to be used by the station personnel in ordering spare or replacement parts for the FM-25KD or FM-12KD transmitters.

PARTS LIST FM-25KD

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3A1	PC Board - Complete Listing At End		10001
2A2	PC Board - Complete Listing At End		10001
3A3	PC Board - Complete Listing At End		10001
3A4	PC Board - Complete Listing At End		10001
3A5	PC Board - Complete Listing At End		10001
1A6	SCR Filament Control	LPAC-J-240-2	20121
3A7	ALC Module - Complete Listing At End		10001
3A8	Power Supply - 24 VDC	C-214	20221
3A9	PC Board - Complete Listing At End		10001
2A10	B + Filter Ass'y - Complete Listing At End		10001
1B1	Filter Fan	KB1000S	20112
2B2	Blower	KBB35	20112
2B3	Blower	CXH33A3G	20172
2B4	Blower	CXH33A3G	20172
3B5	Drive Motor - Remote Output	BK4452-875406-250117	10304
3C1	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C2	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C3	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C4	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C5	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C6	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C7	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C8	Capacitor - Disk - .01 @ 1KV	DD-103	10301

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C9	Capacitor - Disk - .01 @ 1KV	DD-103	10301
3C10	Capacitor - Disk - .01 @ 1KV	DD-103	10301
2C11	Capacitor - Air Variable	167-22	10903
2C12	Capacitor - Air Variable	HFA-25-B	10700
2C13	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C14	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C15	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C16	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C17	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C18	Capacitor - Disk - .001 @ 1KV	DD-102	10301
3C19	Capacitor - Disk - .01 @ 1KV	DD-103	10301
2C20	Capacitor - Neutralizing Disk	3252764-501	10001
2C21	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C22	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
3C23	Capacitor - Paper - 100uF @ 250V	TVA-1522	20188
3C24	Capacitor - Paper - 100uF @ 250V	TVA-1522	20188
3C25	Capacitor - Part of 3A7		
3C26	Capacitor - Part of 3A7		
2C27	Capacitor - Vacuum - .00015 @ 7.5KV	VC150-30-10	20126
2C28	Capacitor - Feed Thru - .001 @ 10KV	2450285-1	10001
1C29	Capacitor-Oil-5uF @ 5KV	702012-8301	20181

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
1C30	Capacitor - Oil - 5uF @ 5KV	702012-8301	20181
1C31	Capacitor - Oil - 5UF @ 10KV	702013-7603	20181
2C32	N/A		
2C33	Capacitor - Feed Thru - .001 @ 1KV	2251275-501	10001
2C34	Capacitor - Feed Thru - .001 @ 1KV	2251275-501	10001
3C35	Part Of 3A5		
3C36	Part of 3A5		
2C37	Cap - MICA - 820pf @ 500V	CM06FD821J03	30001
2C38	Cap - Ceramic - 10pf @ 5KV	854-10Z	10301
2C39	Capacitor - Oil - 10UF @ 600V	702012-3002	20181
2C40	P/O 2A2		
2C41	P/O 2A2		
2C42	Capacitor - 0.68UF @ 400V	WMF4P68	10307
2C43	Capacitor - Plate Blocker	4152042-1	10001
2C44	Capacitor - Vacuum - .00005 @ 7.5KV	VC50-30-7.5	20126
2C45	Capacitor - Vacuum - .00005 @ 7.5KV	VC50-30-7.5	20126
2C46	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C47	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C48	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C49	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187
2C50	Capacitor - Feed Thru - .001 @ 1KV	54-752-001-102M	20187

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C51	Capacitor - Disc - .01 @ 1KV	DD-103	10301
3C52	Capacitor - Disc - .01 @ 1KV	DD-103	10301
2C53	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
2C54	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
2C64	Capacitor - Vacuum - 3-30pf @ 10KV	CVG-3/30-10KV	10104
2C65	Capacitor - 1.0 - @ 400VDC	P8292ZN	10101
2C66	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C67	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C68	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C69	Capacitor - Disk - .001 @ 1KV	DD-102	10301
2C70	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
2C71	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
2C72	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
2C73	Capacitor - Ceramic - .001 @ 5KV	858S-1000	10301
3CB1	Circuit Breaker - 20A - 2 Pole - Curve 3	2263S	10702
3CB2	Circuit Breaker - 20A - 2 Pole - Curve 3	2263S	10702
1CB3	Circuit Breaker - 225A - 3 Pole - Curve 3	CJ3-G3-U-225-3	10702
2CR1	N/A		
2CR2	N/A		
2CR3	N/A		
3CR4	N/A		
2CR5	Diode Block	SPF-16	20185
1CR6	Rectifier Ass'y - 12A	RS3.5-24-12S	10104

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
1CR7	Rectifier Ass'y - 12A	RS3.5-24-12S	10104
1CR8	Rectifier Ass'y - 12A	RS3.5-24-12S	10104
1CR9	Rectifier Ass'y - 12A	RS3.5-24-12S	10104
1CR10	Rectifier Ass'y - 12A	RS3.5-24-12S	10104
1CR11	Rectifier Ass'y - 12A	RS3.5-24-12S	10104
1DC1	Meter Coupler	261.3, 3252972-502	10202, 1000
1DC2	Filter Coupler	3330A, 2030L-25C, 2030H-25C	10203, 2017
3DS1	Indicator - Part of 3S1	*	20131
3DS3	Indicator	532-70112-51-327	20131
3DS4	Indicator	532-7016-51-327	20131
3DS5	Indicator	532-7017-51-327	20131
3DS6	Indicator	532-7015-51-327	20131
3DS7	Indicator	532-7015-51-327	20131
3DS8	Indicator	532-7015-51-327	20131
3DS9	Indicator	532-7015-51-327	20131
3DS10	Indicator - Part of 3S4	*	20131
3DS11	Indicator - Part of 3S8	*	20131
3F1	Fuse - 1/2A - 250VAC	3AG-250-1/2A	30001
3F2	Fuse - 1/2A - 250VAC	3AG-250-1/2A	30001
3F3	Fuse - 1/2A - 250VAC	3AG-250-1/2A	30001

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3F4	Fuse - 1A - 250VAC Slo-Blo	3AG-250-1A-SLO-BLO	30001
3F5	Fuse - 1A - 250VAC Slo-Blo	3AG-250-1A-SLO-BLO	30001
2J1	BNC Connector - Female Chassis	UG-625B/U	30001
2J2	BNC Connector - Female Chassis	UG-625B/U	30001
2J3	BNC Connector - Female Chassis	UG-625B/U	30001
3K1	Relay - DPDT - 24VDC	KRP11DG	20165
3K2	Relay - DPDT - 24VDC	KRP11DG	20165
3K3	Relay - DPDT - 24VDC	KRP11DG	20165
3K4	Relay - DPDT - 10K Ohm Coil	KCP11-10K	20165
3K5	Relay - DPDT - 24 VDC	KRP11DG	20165
3K6	Relay - DPDT - 24VDC	KRP11DG	20165
3K7	Relay - DPDT - 24VDC	KRP11DG	20165
3K8-3K17	N/A		
3K18	Relay - 20A - 3 Pole - 115VAC	2200-EB-230-AA	20171
3K19	Relay - 20A - 3 Pole - 115VAC	2200-EB-230-AA	20171
1K20	Contactor - 60A - 3 Pole - 230VAC	8903-PO-2	20189
1K21	Contactor - 100A - 3 Pole - 230VAC	8903-QO-2	20189
2L1	N/A		
2L2	N/A		
2L3	Choke Ass'y	2251310-501	10001

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
2L4	Driver Output Tuning Ass'y. Note: Complete Ass'y. Not considered replaceable item. However, Shorting Block No. 2251255-501 may be replaced if required.	*	10001
2L5	N/A		
2L6	Choke - Filament Rod Connector	2155464-1	10001
2L7	Choke - Filament Rod Connector	2155464-1	10001
2L8	Choke - PA	3252927-501	10001
2L9	PA Output Tuning Ass'y Note: Complete Ass'y. not considered replaceable item. However, Shorting Block No. 3252634-501 may be replaced if required.	*	10001
2L10	PA Output Loading Ass'y. Note: See note above on 2L9.	*	10001
1L11	Choke - 10 Hy. @ 1A	3450767-1	10001
1L12	Choke - 2 Hy. @ 5A	2450279-1	10001
2L13	Driver Input Tuning Link - Left	2251269-501	10001
2L14	Driver Grid Tuning Link - Right	3252672-501	10001
2L15	Inductor - Driver Input	74F126AP	20134
2L16	Inductor - Driver Input	74F126AP	20134
3M1	Meter - 0-300VAC	4450222-5	10001
3M2	Meter - 0-500VDC	4450222-8	10001
3M3	Meter - 50-0-50MADC	4450222-11	10001

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3M4	Meter - 0-1ADC	4450222-10	10001
3M5	Meter - 0-6ADC	4450222-3	10001
3M6	Meter - 0-6ADC	4450222-3	10001
3M7	Meter - 0-10KVDC	4450222-2	10001
3M8	Meter - 0-10VAC	4450222-6	10001
3M9	Meter 0-30KW	4450222-9	10001
3M10	Meter - Elapsed Time - 230VAC	K42203-P5	10103
3M11	Meter - VSWR - 0-200uADC	7603-Model 29	20183
3R1	Resistor - Carbon - 47K @ 2W 5%	RC42GC473J	30001
3R2	Resistor - Variable - 10K @ 1/2W	RV6LAYS A103A	30001
3R3	Resistor - Variable - 10K @ 1/2W	RV6LAYS A103A	30001
2R4	Resistor - 0.5 @ 25W	Type 474-0.5	20151
2R5	Resistor - 50 @ 225W	0902	20151
2R6	Resistor - 50 @ 225W	0902	20151
2R7	Resistor - 50 @ 225W	0902	20151
2R8	Resistor - 50 @ 225W	0902	20151
2R9	Resistor - 3K @ 25W	0209	20151
3R10	Resistor - Variable - 5K @ 25W	0162	20151
3R13	Potentiometer - 5K @ 2W 10%	RV4LAYS A502A	30001
3R14	Resistor - 5 @ 11W	4749	20151
2R15	Resistor - Carbon - 100 @ 2W 5%	RC42GF101J	30001
2R16	Resistor - 75K @ 225W	0924	20151

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
2R17	Resistor - 250 @ 225W	0906	20151
2R18	Resistor - 250 @ 225W	0906	20151
2R19	Resistor, 0.03 Ohm		10001
2R20	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R21	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R22	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R23	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R24	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R25	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R26	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R27	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R28	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R29	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R30	Resistor - Carbon - 82K @ 2W 5%	RC42GF823J	30001
2R31	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R32	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R33	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R34	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R35	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R36	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001
2R37	Resistor - 1 Mego @ 2W 1%	RN80B1004F	30001

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
2R38	Resistor - 1 Megohm @ 2W 1%	RN80B1004F	30001
2R39	Resistor - 1 Megohm @ 2W 1%	RN80B1004F	30001
2R40	Resistor - 1 Megohm @ 2W 1%	RN80B1004F	30001
2R41	Resistor - Carbon - 82K @ 2w 5%	RC42GF823J	30001
3R42	Resistor - 0.5 @ 25W	Type 474-0.5	20151
3R43	Pot - 1K @ 2W	RV4NAYSA102A	30001
2R44	Resistor - 100K @ 225W	0925	20151
2R45	Resistor - 100K @ 225W	0925	20151
3R46	Potentiometer - 1K @ 2W	RV4NAYSA102A	30001
3R47-142	See Subassemblies at end.		
3R139	Resistor - 5.6K @ 1/2W	RC20GF562J	30001
2R143	Resistor - 100K @ 225W	0925	20151
2R144	Resistor - 100K @ 225W	0925	20151
2R145	Resistor - 100K @ 225W	0925	20151
3R146	Resistor - 0.5 @ 25W	Type 474-0.5	20151
3R147	Resistor - 4.7K @ 1/2W	RC20GF472J	30001
2RL1	Choke	2251334-501	10001
3S1	Presslite	521-4017-51-327	20131
3S2	Presslite	518-4016-51-327	20131
3S4	Presslite	520-4016-51-327	20131
3S8	Presslite	518-40112-51-327	20131
3S9	Switch - 90° Index - 4 Position	2542	10301
3S10	Switch - 3 Section - Intlk.	3Sect/B301	10301

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3S11	Switch - 2 Section - Intlk.	2Sect/B301	10301
3S12	Switch - 2 Section - Intlk.	2Sect/B301	10301
3S13	Switch - 2 Section - Intlk.	2Sect/B301	10301
3S14	Switch - 5 Section - Intlk.	2155501-1	10001
2S15	Switch - Air Intlk.	2A-1800	20172
2S16	Switch - Air Intlk.	2A-1800	20172
2S17	Switch - Door Intlk.	2AC6	20132
3S18	Switch - Momentary SPDT(Part of 3A4)	7108SYZBE	10303
2S19	Switch - Door Intlk.	2AC6	20132
1S20	Switch - Door Intlk.	2AC6	20132
1S21	Switch - Door Intlk.	2AC6	20132
2S22	Switch - Air Intlk.	2A-1000	20132
2S23	Switch - Control Panel Intlk.	2AC6	20132
1T1	Transformer - 6.3V @ 160A	3450766-1	10001
2T2	Transformer - Sola	20-04-065	20184
2T3	Transformer - Bias	3450768-1	10001
1T4	Transformer - Plate - 40KVA	3450763-1	10001
1TB1	Terminal Block - 7 Terminals	541-7	10302
1TB2	Terminal Block - 15 Terminals	541-15	10302
1TB3	Terminal Block	42704	10206
1TB4	Terminal Block	22204	10206
2V1	Tube	4CX1000K	10402
2V2	Tube	3CX15000A7	10402
2VR1	Zener Diode	1N3340A	20133

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
2VR2	Zener Diode	IN3340A	20133
2VR3	Zener Diode	IN3340A	20133
3XF1	Fuse Holder	HCM-D	10205
3XF2	Fuse Holder	HCM-D	10205
3XF3	Fuse Holder	HCM-D	10205
3XF4	Fuse Holder	HCM-D	10205
3XF5	Fuse Holder	HCM-D	10205
3XF6	Fuse Holder (Spare)	HCM-D	10205
3XF7	Fuse Holder (Spare)	HCM-D	10205
2XV1	Socket - Driver Tube	3252669-501	10001
2XV2	Socket - PA Tube	SK1320	10402
2E1	Protector, Voltage Surge	L2-A230	20190
2XE1	Holder	A2-L1	20190
3E2	Protector, Voltage Surge	L2-A230	20190
3XE2	Holder	A2-L1	20190
2E3	Protector, Voltage Surge	L2-A230	20190
2XE3	Holder	A2-L1	20190

PARTS LIST LAMP DRIVER 3A1

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C74	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C75	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C76	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C77	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C78	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C79	Capacitor 50 uf @ 50 V	TE-1307	20188
3IC10	Integrated Circuit	SN7474N	30001
3IC11	Integrated Circuit	SN7474N	30001
3R100	Resistor 1.2 K 1/4 W 5%	RCR07G122J	30001
3R101	Resistor 1.2 K 1/4 W 5%	RCR07G122J	30001
3R102	Resistor 1.2 K 1/4 W 5%	RCR07G122J	30001
3R103	Resistor 1.2 K 1/4 W 5%	RCR07G122J	30001
3R104	Resistor 1.2 K 1/4 W 5%	RCR07G122J	30001
3R105	Resistor 5.6 K 1/4 W 5%	RCR07G562J	30001
3R113	Resistor 270 Ω 3 W	4403	20151
3Q9	Transistor	JAN 2N2222A	30001
3Q10	Transistor	JAN 2N2222A	30001
3Q11	Transistor	JAN 2N2222A	30001

PARTS LIST LAMP DRIVER 3A1

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3Q12	Transistor	JAN 2N2222A	30001
3Q13	Transistor	JAN 2N2222A	30001
3VR12	Diode, Zener, 5.1 V	1N4733	30001
	Connector, 15 Pin	133-015-03	10102
	Board, Printed Circuit	4152136-1	10001

2A2 - AUTOMATIC LEVEL DETECTOR

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
2C40	Capacitor - 25 uf @ 12 V	TE-1131	20188
2C41	Capacitor - .001 MFD @ 200V	CK06BX102K	30001
2CR3	Diode	1N916*	30001
2CR4	Diode	1N916*	30001
2J4	Connector - Bulkhead BNC	UG/625B/U	30001
2J5	Connector - Bulkhead BNC	UG/625B/U	30001
2R135	Resistor - 10K @ 1/4 W 5%	RCR07G103J	30001
2R136	Resistor - 2.2K @ 1/4 W 5%	RCR07G222J	30001
	Housing	3152921-1	10001
	Board, Printed Wiring	3152924-2	10001

* Or equivalent

3A3 - CONTROL/TIMER ASSEMBLY

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C55	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C56	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C57	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C58	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C59	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C60	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C61	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C62	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C63	Capacitor - 100 MFD @ 6 V	150D107X0500GS2	20188
3C87	Capacitor - 400 MFD @ 6 V	TE-1107	20188
3C88	Capacitor - 15 MF @ 6 V	TE-1089	20188
3C89	Capacitor - 100 MFD @ 6 V	150D107X0500GS2	20188
3C90	Capacitor - Tantalum 330 MFD @ 6 V	150D-337-X900-6S2	20164
3C91	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C92	Capacitor - 1 MFD @ 50 V	5C023-105-X05-00B3	20164
3C93	Capacitor - 0.1 MFD @ 50 V	5C023-104-X05-00B3	20164
3CR13	Diode	1N914*	30001

* Or equivalent

3A3 CONTROL/TIMER ASSEMBLY

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3IC19	Integrated Circuit	SN74121N	30001
3IC20	Integrated Circuit	SN74121N	30001
3IC21	Integrated Circuit	SN74121N	30001
3IC22	Integrated Circuit	SN7493N	30001
3IC23	Integrated Circuit	SN7400N	30001
3IC24	Integrated Circuit	SN7400N	30001
3Q4	Transistor	2N3440	30001
3Q5	Transistor	2N3440	30001
3Q6	Transistor	2N3440	30001
3Q7	Transistor	2N2222A JAN	30001
3Q8	Transistor	2N2222A JAN	30001
3R47	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R48	Resistor - 27K 1/4W 5%	RCR07G273J	30001
3R49	Resistor - 10K 1/4W 5%	RCR07G103J	30001
3R50	Resistor - 22K 1/4W 5%	RCR07G223J	30001
3R51	Resistor - 1M 1/4W 5%	RCR07G105J	30001
3R52	Resistor - 10K 1/4W 5%	RCR07G103J	30001
3R53	Resistor - 3.3K 1/4W 5%	RCR07G332J	30001

3A3 CONTROL/TIMER ASSEMBLY

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3R54	Resistor - 470 1/4W 5%	RCR07G470J	30001
3R55	Resistor - 1.5M 1/4W 5%	RCR07G155J	30001
3R56	Resistor - 10K 1/4W 5%	RCR07G103J	30001
3R57	Resistor - 5.6K 1/4W 5%	RCR07G562J	30001
3R58	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R59	N/A		
3R60	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R61	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R62	N/A		
3R63	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R64	Resistor - 680 1/4W 5%	RCR07G681J	30001
3R65	Resistor - 390 2W 10%	RC42GF391K	30001
3R66	Resistor - 330 2W 10%	RC42GF331K	30001
3R67	Resistor - 560 1W 10%	RC32GF561K	30001
3VR11	Zener Diode	1N5233	30001
	Board, Printed Circuit	4152135-1	10001
	Connector, 15 Pin	133-015-03	10102

3A4 REV. 'C' FAULT LEVEL CONTROL BOARD

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C81	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C82	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C83	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C84	Capacitor 50 MFD @ 50 V	TE-1307	20188
3CR14	Diode	1N914	30001
3CR15	Diode	1N914	30001
3CR16	Diode	1N914	30001
3CR17	Diode	1N914	30001
3IC1	Integrated Circuit	SN7413N	30001
3IC2	Integrated Circuit	SN7413N	30001
3IC3	Integrated Circuit	SN7404N	30001
3IC4	Integrated Circuit	SN7430N	30001
3Q3	Transistor	2N2222A JAN	30001
3Q14	Transistor	2N2222A JAN	30001
3R116	Resistor Variable 2.5K @ 1/2W 10%	RV6LAYS252A	30001
3R117	Resistor Variable 2.5K @ 1/2W 10%	RV6LAYS252A	30001
3R118	Resistor Variable 2.5K @ 1/2W 10%	RV6LAYS252A	30001
3R119	Resistor 47 Ω 3W	4379	20151
3R120	Resistor 47 Ω 3W	4379	20151
3R121	Resistor 47 Ω 3W	4379	20151

3A4 REV. 'C' FAULT LEVEL CONTROL BOARD

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<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3R122	Resistor 10K 1/4 W 5%	RCR07G103J	30001
3R123	Resistor 680 1/4 W 5%	RCR07G681J	30001
3R124	Resistor 2.7K 1/4W 5%	RCR07G272J	30001
3R125	Resistor 2.7K 1/4W 5%	RCR07G272J	30001
3R126	Resistor 220 1/4 W 5%	RCR07G221J	30001
3R127	Resistor 220 1/4 W 5%	RCR07G221J	30001
3R128	Resistor 220 1/4 W 5%	RCR07G221J	30001
3R129	Resistor 220 1/4 W 5%	RCR07G221J	30001
3R130	Resistor 5.6 K 1/4 W 5%	RCR07G562J	30001
3R131	Resistor 5.6 K 1/4 W 5%	RCR07G562J	30001
3R132	Resistor 270 Ω 3W	4403	20151
3R133	Resistor 1.8K 1W	RC32GF182J	30001
3S18	Switch, Momentary	7108SYZBE	10303
3VR5	Zener Diode	1N4733	30001
3VR6	Zener Diode	1N4733	30001
3VR7	Zener Diode	1N5338	30001
3VR8	Zener Diode	1N5338	30001
3VR9	Zener Diode	1N5338	30001
	Board, Printed Circuit	4152137-1	10001
	Connector 15 Pin	133-015-03	10102

3A4 REV. 'G' FAULT LEVEL CONTROL BOARD ASS'Y.

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C82	Capacitor 1 MFD @ 50 V	NLW 1-50	10307
3C83	Capacitor 50 MFD @ 12 V	TE-1133	20188
3CR15	Diode	1N914	30001
3CR16	Diode	1N914	30001
3CR17	Diode	1N914	30001
3CR18	Diode	1N914	30001
3R116	Resistor, Variable 2.5K @ 1/2 W	RV6LAYS252A	30001
3R117	Resistor, Variable 2.5K @ 1/2 W	RV6LAYS252A	30001
3R118	Resistor, Variable 2.5K @ 1/2 W	RV6LAYS252A	30001
3R119	Resistor, 10K @ 1/4 W 5%	RCR07G103J	30001
3R120	Resistor, 680 Ohm @ 1/4 W 5%	RCR07G681J	30001
3R121	Resistor, 330 Ohm @ 2 W 10%	RC42GF331K	30001
3R122	Resistor, 470 Ohm @ 1/4 W 5%	RCR07G471J	30001
3R123	Resistor, 470 Ohm @ 1/4 W 5%	RCR07G471J	30001
3R124	Resistor, 470 Ohm @ 1/4 W 5%	RCR07G471J	30001
3R125	Resistor, 470 Ohm @ 1/4 W 5%	RCR07G471J	30001
3S18	Switch, Momentary	7108SYZBE	10303
3VR5	Zener Diode	1N4733	30001
3IC-1	Integrated Circuit	SN7400N	30001

3A4 REV. 'G' FAULT LEVEL CONTROL BOARD ASS'Y.

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<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3K11	Relay	GB821B-3	20124
3K12	Relay	GB821B-3	20124
3K13	Relay	GB821B-3	20124
3XIC-1	Socket	014ST-7519	20125
3XK11	Socket	014ST-7519	20125
3XK12	Socket	014ST-7519	20125
3XK13	Socket	014ST-7519	20125
	Board, Printed Circuit	4152137-1	10001
	Connector, 15 Pin	133-015-03	10102
3VR6	Zener Diode	IN5338	30001
3VR7	Zener Diode	IN5338	30001
3VR8	Zener Diode	IN5338	30001
3R126	Resistor - 100 Ohms @ 3W	4392	20151
3R127	Resistor - 100 Ohms @ 3W	4392	20151
3R128	Resistor - 100 Ohms @ 3W	4392	20151

3A5 - MASTER MODULE ASSEMBLY

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C35	Capacitor - 50 UF @ 50 V	TE-1307	20188
3C36	Capacitor - 50 UF @ 50 V	TE-1307	20188
3CR12	Diode	1N2070*	30001
	Board, Printed Circuit	3152920-501	10001
	Connector, 15 Pin	143-015-03	10102

* Or equivalent

3A7 - ALC ASS'Y

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART NO.</u>	<u>MANUFACTURER</u>
3C25	Capacitor - Disk - .01 @ 100V	Z-5U	10301
3C26	Capacitor - Disk - .01 @ 100V	Z-5U	10301
3Q1	Transistor	2N5415	30001
3Q2	Transistor	40406	20173
3R11	Resistor - 3.3K @ 11 W	4836	20151
3R137	Resistor - 1K @ 1/4 W 5%	RCR07G102J	30001
3R138	Resistor - 1K @ 1/4 W 5%	RCR07G102J	30001
3R140	Resistor - 10K @ 11 W	4854	20151
3R141	Resistor - 22K @ 1 W 5%	RC32GF223J	30001
3R142	Resistor - 4.7K @ 1/4 W 5%	RCR07G472J	30001
3VR4	Diode - Zener	1N4749	30001
	Case, Housing	2155557-1	10001
	Board, Printed Circuit	3152924-1	10001

3A9 - EXTENDER CARD

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>MANUF. PART. NO.</u>	<u>MANUFACTURER</u>
	Board, Printed Wiring	2155617-1	10001
	Connector, 15 Pin	133-015-03	10102
	Connector, 15 Pin	143-015-03	10102

2A10 - B+ FILTER ASSEMBLY - 4254253-501

2C95	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2C96	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2C97	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2C98	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2C99	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2C100	Capacitor - 500 PF @ 30 KV	30DK-T5	20188
2L17	Inductor - 8 turns #10 formvar	1.50 ID	10001

FM-12KD SUPPLEMENTAL PARTS LIST

<u>SYMBOL</u>	<u>DESCRIPTION</u>	<u>PART NO.</u>	<u>MANUFACTURER</u>
1C31	Capacitor, 4uF @ 8 KV	AOC8M4	20122
3CB	Circuit Breaker, 150A	CJ3-G3-U-150-3	10702
1L12	Choke, 3HY @ 3A	2450280-1	10001
3M5	Meter, 0-3.0 A	4450222-4	10001
3M6	Meter, 0-3.0 A	4450222-4	10001
3M7	Meter, 0-7.5 KVDC	4450222-1	10001
3M9	Meter, 0-15 KW	4450222-17	10001
2R4	Resistor, 1.0 Ohm @ 25W	0200J	20151
2R27	Resistor, 500K @ 2 W 1%	RN80B5003F	30001
2R28	N/A		
2R29	N/A		
2R38	Resistor, 500K @ 2 W 1%	RN80B5003F	30001
3R42	Resistor, 1.0 Ohm @ 25W	0200J	20151
3R43	Potentiometer, 3 Ohms @ 75 W	1103	20151
3R148	Resistor, 3K @ 11W	4835	20151
1T1	Transformer, Filament	3450765-1	10001
1T4	Transformer, Plate	3450764-1	10001
2V2	Tube, Power	3CX10,000A7	10402

MANUFACTURERS' DESIGNATION LISTING

<u>DESIGNATION NO.</u>	<u>MANUFACTURER</u>	<u>DESIGNATION NO.</u>	<u>MANUFACTURER</u>
10001	American Electronic Labs	20131	Marco Oak
10101	Aerovox	20132	Microswitch
10102	Amphenol	20133	Motorola
10103	A. W. Haydon	20134	Miller
10104	Amperex		
10202	Bendix	20135	Mullard
10203	Bird	20141	Nothelfer Winding Labs
10205	Buss	20151	Ohmite
10206	Buchannan		
10301	Centralab	20162	Phaotron
10302	Cinch Jones	20165	Potter & Brumfield
10303	C-K		
10304	Dale Electronics	20164	Pytronics
10307	Cornell-Dublier	20170	RDI
10401	E. F. Johnson	20171	Rowan
10402	Eimac	20172	Rotron
10403	Elmenco	20181	Sangamo
10700	Hammarlund	20183	Simpson
10702	Heinemann	20184	Sola
10902	Jennings	20185	Solitron

MANUFACTURERS' DESIGNATION LISTING

<u>DESIGNATION NO.</u>	<u>MANUFACTURER</u>	<u>DESIGNATION NO.</u>	<u>MANUFACTURER</u>
10903	E. F. Johnson	20187	Spectrum Control
20112	Kooltronic	20188	Sprague
20121	Loyola	20189	Sq D
20122	Condenser Products	20190	Siemens
20123	Electro Engineering	20221	Wanlass
20124	Grisby-Barton	30001	Mil Std.
20125	Texas Instruments		
20126	Dolenko-Wilkens		
20173	RCA		
20174	Unitrode		
20175	Sarkes-Tarzian		
20176	Carborundum		
20177	Triad		
20178	Shively Labs		

**AUDIO AMPLIFIER OR MODULATOR Class AB₁**

MAXIMUM RATINGS	-	-	-	-	-
DC PLATE VOLTAGE	-	-	-	-	3000 MAX. VOLTS
DC SCREEN VOLTAGE	-	-	-	-	400 MAX. VOLTS
DC PLATE CURRENT	-	-	-	-	1.0 MAX. AMP
PLATE DISSIPATION	-	-	-	-	1000 MAX. WATTS
SCREEN DISSIPATION	-	-	-	-	12 MAX. WATTS
GRID DISSIPATION	-	-	-	-	0 MAX. WATTS

TYPICAL OPERATION (Sinusoidal wave, two tubes unless noted)

DC Plate Voltage	-	-	-	-	2000	2500	3000 volts
DC Screen Voltage	-	-	-	-	325	325	325 volts
DC Grid Voltage ¹	-	-	-	-	-60	-60	-60 volts
Zero-Signal DC Plate Current	-	-	-	-	500	500	500 mA
Max-Signal DC Plate Current	-	-	-	-	1.78	1.77	1.75 amps
Zero-Signal DC Screen Current*	-	-	-	-	16	12	10 mA
Max-Signal DC Screen Current*	-	-	-	-	70	70	70 mA
Effective Load, Plate to Plate	-	-	-	-	2040	2850	3680 ohms
Driving Power	-	-	-	-	0	0	0 watts
Max-Signal Plate Output Power	-	-	-	-	1860	2600	3260 watts

*Approximate values.

¹Adjust grid bias to obtain listed zero-signal plate current.

"TYPICAL OPERATION" data are obtained by calculation from published characteristic curves; NO ALLOWANCE is made for circuit losses. Adjustment of the grid bias to obtain the specific zero-signal plate current is assumed. The screen voltage required to obtain the listed value of maximum plate current, without drawing grid current, MAY VARY from the typical values shown. These conditions are valid to approximately 100 Mc. at higher frequencies, power output will be lower due to tube and circuit losses.

APPLICATION**MECHANICAL**

Cooling—Sufficient cooling must be provided for the anode and ceramic-to-metal seals to maintain operating temperatures below the rated maximum values:

Ceramic-to-Metal Seals	250°C
Anode Core	250°C

A flow rate of 25 cubic feet per minute will be adequate for operation at maximum rated plate dissipation at sea level and with inlet air temperatures up to 40°C. Under these conditions, 25 cfm of air flow corresponds to a pressure difference across the tube and socket of 0.2 inch of water column. Experience has shown that if reliable long-life operation is to be obtained, the cooling air flow must be maintained during standby periods when only the heater voltage is applied to the tube.

At higher altitudes and at UHF increased air flow will be required. For example, at an altitude of 10,000 feet, a flow rate of 37 cfm will be required and will be obtained with a pressure drop across tube and socket of 0.3 inch of water column. In selecting a blower for use at high altitudes, care must be taken to assure that the blower is designed to deliver the desired volume of air at the corresponding pressure drop and at the particular altitude.

In cases where there is any doubt regarding the adequacy of the supplied cooling, it should be borne in mind that operating temperature is the sole criterion of cooling effectiveness. Surface temperatures may be easily and effectively measured by using one of the several temperature-sensitive paints or sticks available from various chemical or scientific-equipment suppliers. When these materials are used, extremely thin applications must be made to avoid interference with the transfer of heat from the tube to the air stream, which would cause inaccurate indications.

ELECTRICAL

Heater—The rated heater voltage for the 4CX1000K is 6.0 volts. The voltage, as measured at the socket, should be maintained at this value to minimize variations in operation and to obtain maximum tube life. In no case should the voltage be allowed to exceed 5% above or below the rated value.

The cathode and one side of the heater are internally connected.

It is recommended that the heater voltage be applied for a period of not less than 3 minutes before other operating voltages are applied. From an initial cold condition, tube operation will stabilize after a period of approximately 5 minutes.

Control Grid Operation—The grid dissipation rating of the 4CX1000K is zero watts. The design features which make the tube capable of maximum power operation without driving the grid into the positive region also make it necessary to avoid positive-grid operation.

Although the average grid-current rating is zero, peak grid currents of less than five milliamperes as read on a five-milliamperes meter may be permitted to flow for peak-signal monitoring purposes.

Screen Grid Operation—Tetrode tubes may exhibit reversed screen current to a greater or lesser degree depending on individual tube design. This characteristic is prominent in the 4CX1000K and, under some operating conditions, indicated negative screen currents in the order of 25 milliamperes may be encountered.

The maximum rated power dissipation for the screen grid in the 4CX1000K is 12 watts and the screen power should be kept below this level. The product of the peak screen voltage and the indicated dc screen current approximates the screen input power except when the screen current indication is near zero or negative. In the usual tetrode amplifier, where no signal voltage appears between cathode and screen, the peak screen voltage is equal to the dc screen voltage. Experience has shown that the screen will operate within the limits established for this tube if the indicated screen current, plate voltage and drive voltage approximate the "Typical Operation" values.

The screen supply voltage must be maintained constant for any values of negative and positive screen currents that may be encountered. Dangerously high plate currents may flow if the screen power supply exhibits a rising voltage characteristic with negative screen current. Stabilization may be accomplished in several different ways. A bleeder resistor may be connected from screen to cathode; a combination of VR tubes may be connected from screen to cathode; or an electron-tube regulator circuit may be used in the

screen supply. It is absolutely essential to use a bleeder if a series electron-tube regulator is employed. The screen bleeder current should approximate 70 milliamperes to adequately stabilize the screen voltage. It should be observed that this bleeder power may be usefully employed to energize low-power stages of the transmitter.

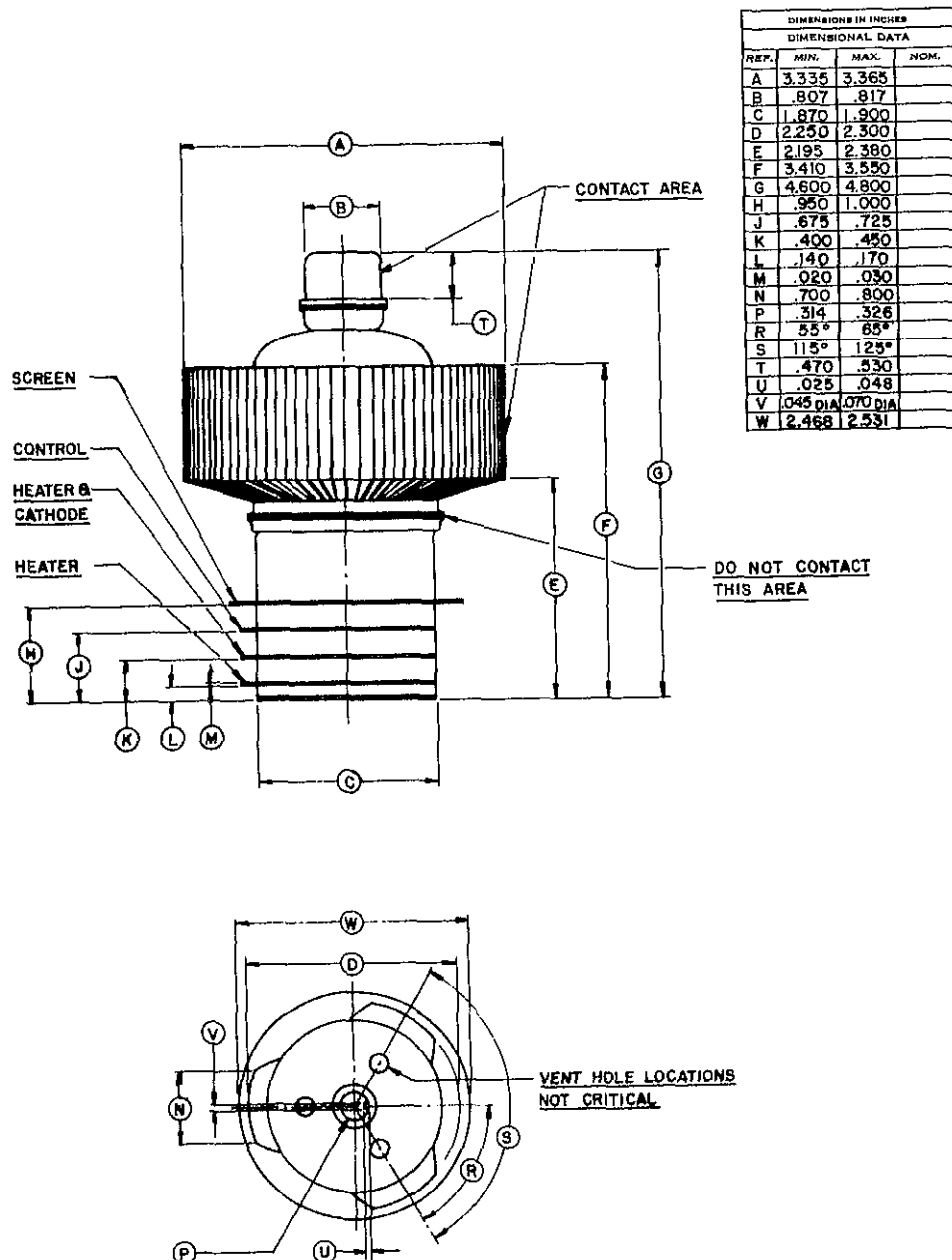
Plate Operation—The maximum rated plate dissipation power is 1000 watts. Except for brief periods during circuit adjustments, this maximum value should not be exceeded.

The top cap on the anode cooler may be used as a plate terminal at low frequencies or a circular clamp or spring-finger collet encircling the cylindrical outer

surface of the anode cooler may be used at high frequencies.

Points of electrical contact with the anode cooler should be kept clean and free of oxide to minimize radio-frequency losses. The anode cooler should be inspected periodically and cleaned when necessary to remove any dirt which might interfere with effective cooling.

Special Applications — If it is desired to operate this tube under conditions different from those given here, write to the Power Grid Tube Marketing, EIMAC, Division of Varian, San Carlos California, for information and recommendations.

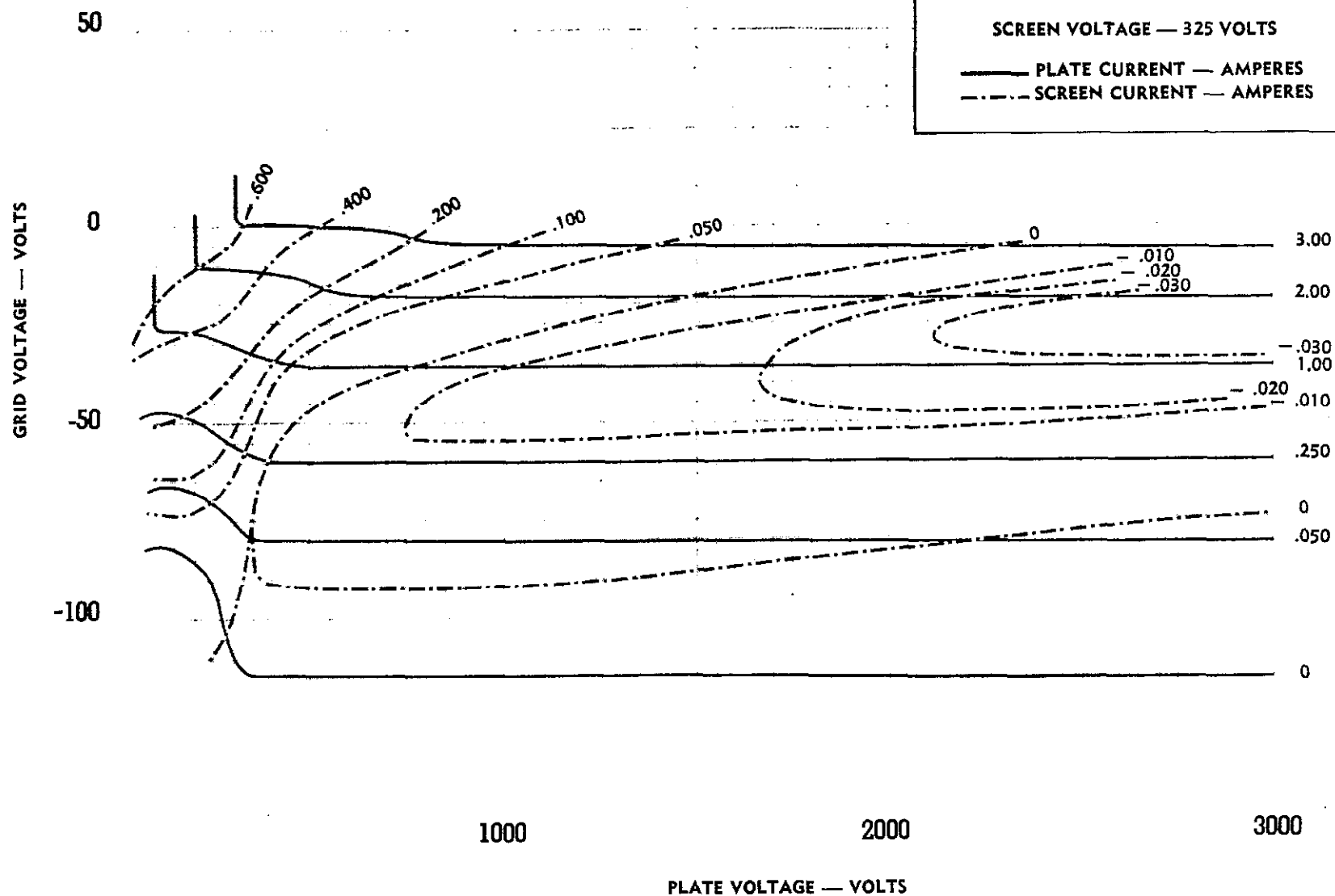


Simul
4CX1000K

EIMAC 4CX1000K
TYPICAL
CONSTANT CURRENT
CHARACTERISTICS

SCREEN VOLTAGE — 325 VOLTS

— PLATE CURRENT — AMPERES
- - - SCREEN CURRENT — AMPERES





E I M A C
Division of Varian
SAN CARLOS
CALIFORNIA

8160
3CX10,000A7

HIGH-MU
POWER TRIODE

The EIMAC 8160/3CX10,000A7 is a ceramic and metal power triode intended to be used as a zero-bias Class-B amplifier in audio radio-frequency applications. Operation with zero grid bias offers circuit simplicity by eliminating the bias supply. In addition, grounded-grid operation is attractive since a power gain as high as twenty times can be obtained with the 8160/3CX10,000A7.



GENERAL CHARACTERISTICS

ELECTRICAL

Filament: Thoriated-Tungsten		<i>Min.</i>	<i>Nom.</i>	<i>Max.</i>	
Voltage - - - - -	- - - - -		7.5		volts
Current - - - - -	- - - - -	94		104	amps
Amplification Factor - - - - -	- - - - -		200		
Direct Interelectrode Capacitances:					
Grid-Filament - - - - -	- - - - -	50.0		62.0	pF
Grid-Plate - - - - -	- - - - -	32.0		40.0	pF
Plate-Filament - - - - -	- - - - -			0.3	pF
Frequency for Maximum Ratings - - - - -	- - - - -			160	MHz

MECHANICAL

Base - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	Coaxial
Recommended Socket - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	EIMAC SK-1300
Operating Position - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	Vertical, base up or down
Cooling - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	Forced air
Maximum Operating Temperatures:					
Anode Core - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	250°C
Ceramic-to-Metal Seals - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	250°C
Maximum Dimensions:					
Height - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	8.75 inches
Diameter - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	7.05 inches
Net Weight - - - - -	- - - - -	- - - - -	- - - - -	- - - - -	12 pounds

RADIO-FREQUENCY LINEAR AMPLIFIER

Grounded Grid, Class-B

MAXIMUM RATINGS

DC PLATE VOLTAGE - - - - -	7000 VOLTS
DC PLATE CURRENT - - - - -	5.0 AMPS
PLATE DISSIPATION - - - - -	12 KW
GRID DISSIPATION - - - - -	500 WATTS

*Approximate value

TYPICAL OPERATION, Single-Tone Conditions

DC Plate Voltage - - - - -	7000	7000 volts
Zero-Sig DC Plate Current* - - - - -	0.60	0.60 amp
Max-Sig DC Plate Current - - - - -	3.72	5.00 amps
Max-Sig DC Grid Current - - - - -	0.71	1.00 amp
Driving Impedance - - - - -	35	32 ohms
Resonant Load Impedance - - - - -	1020	745 ohms
Max-Sig Driving Power - - - - -	885	1540 watts
Peak Envelope Plate Output Power - - - - -	17,700	24,200 watts
Power Gain - - - - -	20.0	15.7 times

**AUDIO-FREQUENCY AMPLIFIER
OR MODULATOR**

Class-B, Grid Driven

MAXIMUM RATINGS (Per Tube)

DC PLATE VOLTAGE	-	-	-	7000 VOLTS
DC PLATE CURRENT	-	-	-	5.0 AMPS
PLATE DISSIPATION	-	-	-	12 KW
GRID DISSIPATION	-	-	-	500 WATTS

*Approximate value

TYPICAL OPERATION, Two Tubes, Sinusoidal Wave

DC Plate Voltage	-	-	-	-	7000	7000 volts
DC Grid Voltage	-	-	-	-	0	0 volts
Zero-Sig DC Plate Current*	-	-	-	-	1.20	1.20 amps
Max-Sig DC Plate Current	-	-	-	-	7.50	10.0 amps
Max-Sig DC Grid Current	-	-	-	-	1.50	2.06 amps
Driving Power	-	-	-	-	315	560 watts
Peak AF Driving Voltage (Per Tube)	-	-	-	-	250	310 volts
Load Resistance, Plate-to-Plate	-	-	-	-	2000	1520 ohms
Max-Sig Plate Output Power	-	-	-	-	35,600	47,700 watts

RADIO-FREQUENCY LINEAR AMPLIFIER

Carrier Conditions, Grounded-Grid

MAXIMUM RATINGS

DC PLATE VOLTAGE	-	-	-	7000 VOLTS
DC PLATE CURRENT	-	-	-	5.0 AMPS
PLATE DISSIPATION	-	-	-	12 KW
GRID DISSIPATION	-	-	-	500 WATTS

*Approximate value

**Modulation Crest Conditions

TYPICAL OPERATION

DC Plate Voltage	-	-	-	-	-	-	7000 volts
DC Grid Voltage	-	-	-	-	-	-	0 volts
Zero-Sig DC Plate Current*	-	-	-	-	-	-	0.60 amp
DC Plate Current	-	-	-	-	-	-	2.40 amps
DC Grid Current	-	-	-	-	-	-	0.25 amp
Driving Impedance**	-	-	-	-	-	-	32 ohms
Peak Driving Voltage**	-	-	-	-	-	-	310 volts
Driving Power	-	-	-	-	-	-	330 watts
Plate Output Power	-	-	-	-	-	-	5650 watts

**RADIO-FREQUENCY POWER AMPLIFIER
OR OSCILLATOR**

Class-C

MAXIMUM RATINGS

DC PLATE VOLTAGE	-	-	-	7000 VOLTS
DC PLATE CURRENT	-	-	-	4.0 AMPS
PLATE DISSIPATION	-	-	-	10 KW
GRID DISSIPATION	-	-	-	500 WATTS

TYPICAL OPERATION

DC Plate Voltage	-	-	-	-	-	-	7000 volts
DC Plate Current	-	-	-	-	-	-	4.0 amps
DC Grid Voltage	-	-	-	-	-	-	-230 volts
DC Grid Current	-	-	-	-	-	-	775 mA
Peak RF Grid Voltage	-	-	-	-	-	-	555 volts
Grid Driving Power	-	-	-	-	-	-	430 watts
Plate Output Power	-	-	-	-	-	-	21.3 kW

PLATE-MODULATED RF POWER AMPLIFIERMAXIMUM RATINGS

DC PLATE VOLTAGE	-	-	-	5500 VOLTS
DC PLATE CURRENT	-	-	-	3.0 AMPS
PLATE DISSIPATION	-	-	-	6.5 KW
GRID DISSIPATION	-	-	-	500 WATTS

TYPICAL OPERATION

DC Plate Voltage	-	-	-	-	-	-	5000 volts
DC Plate Current	-	-	-	-	-	-	3.0 amps
DC Grid Voltage	-	-	-	-	-	-	-200 volts
DC Grid Current	-	-	-	-	-	-	775 mA
Peak RF Grid Voltage	-	-	-	-	-	-	490 volts
Grid Driving Power	-	-	-	-	-	-	380 watts
Plate Output Power	-	-	-	-	-	-	11.9 kW

Note: "TYPICAL OPERATION" data are obtainable by calculation from published characteristic curves. No allowance for circuit losses, either input or output, has been made.

APPLICATION

Mounting—The 3CX10,000A7 must be operated vertically base up or down. The tube must be protected from severe vibration and shock.

Cooling — The maximum temperature rating for the external surfaces of the 3CX10,000A7 is 250°C. Sufficient forced-air cooling must be provided to keep the temperature of the anode core and the temperature of the ceramic-metal seals below 250°C. Tube life is usually prolonged if these areas are maintained at temperatures below this maximum rating. Minimum air-flow requirements to maintain anode-core and seal temperatures below 225°C with an inlet-air temperature of 50°C are tabulated below. The use of these air-flow rates through the recommended socket/chimney and tube combination in the base-to-anode direction provides effective cooling of the tube.

Plate** Dissipation (Watts)	Sea Level		10,000 Feet	
	Air Flow (CFM)	Pressure Drop (Inches of Water)	Air Flow (CFM)	Pressure Drop (Inches of Water)
4000	105	.24	154	.35
6000	178	.50	275	.80
8000	253	.90	370	1.45
10,000	345	1.4	500	2.30
12,000	483	2.25	710	3.40

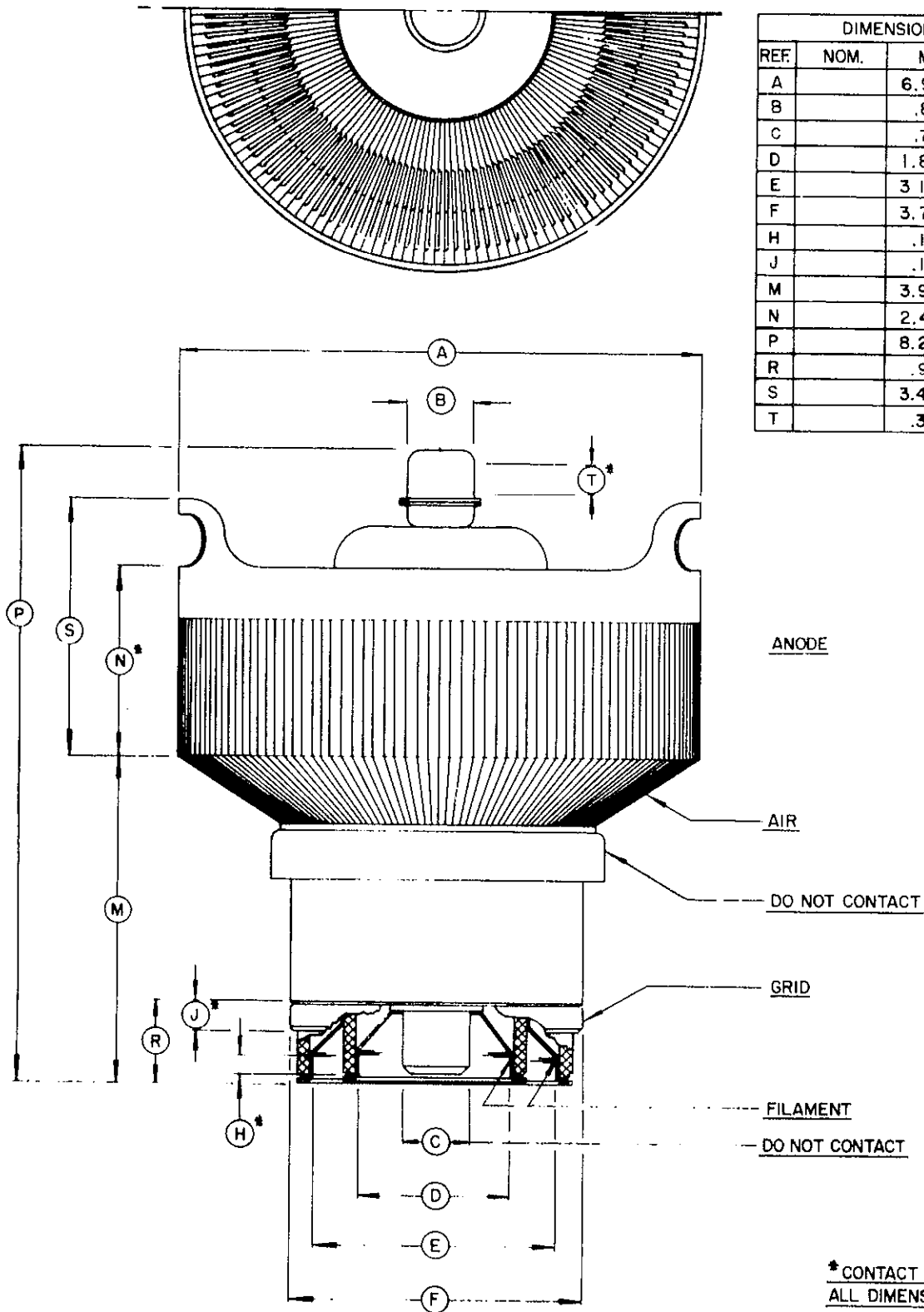
**Since the power dissipated by the filament is about 750 watts and since grid dissipation can, under some circumstances, represent another 500 watts, allowance has been made in preparing this tabulation for an additional 1250 watts dissipation.

Input Circuit — When the 3CX10,000A7 is operated as a grounded-grid rf amplifier, the use of a resonant tank in the cathode circuit is recommended in order to obtain greatest linearity and power output. For best results with a single-ended amplifier it is suggested that the cathode tank circuit operate at a "Q" of two or more.

Class-C Operation — Although specifically designed for class-B service, the 3CX10,000A7 may be operated as a class-C power amplifier or oscillator or as a plate-modulated radio-frequency power amplifier. The zero-bias characteristic of the 3CX10,000A7 can be used to advantage in class-C amplifiers by employing only grid-leak bias. If driving power fails, plate dissipation is then kept to a low value because the tube will be operating at the normal static zero-bias conditions.

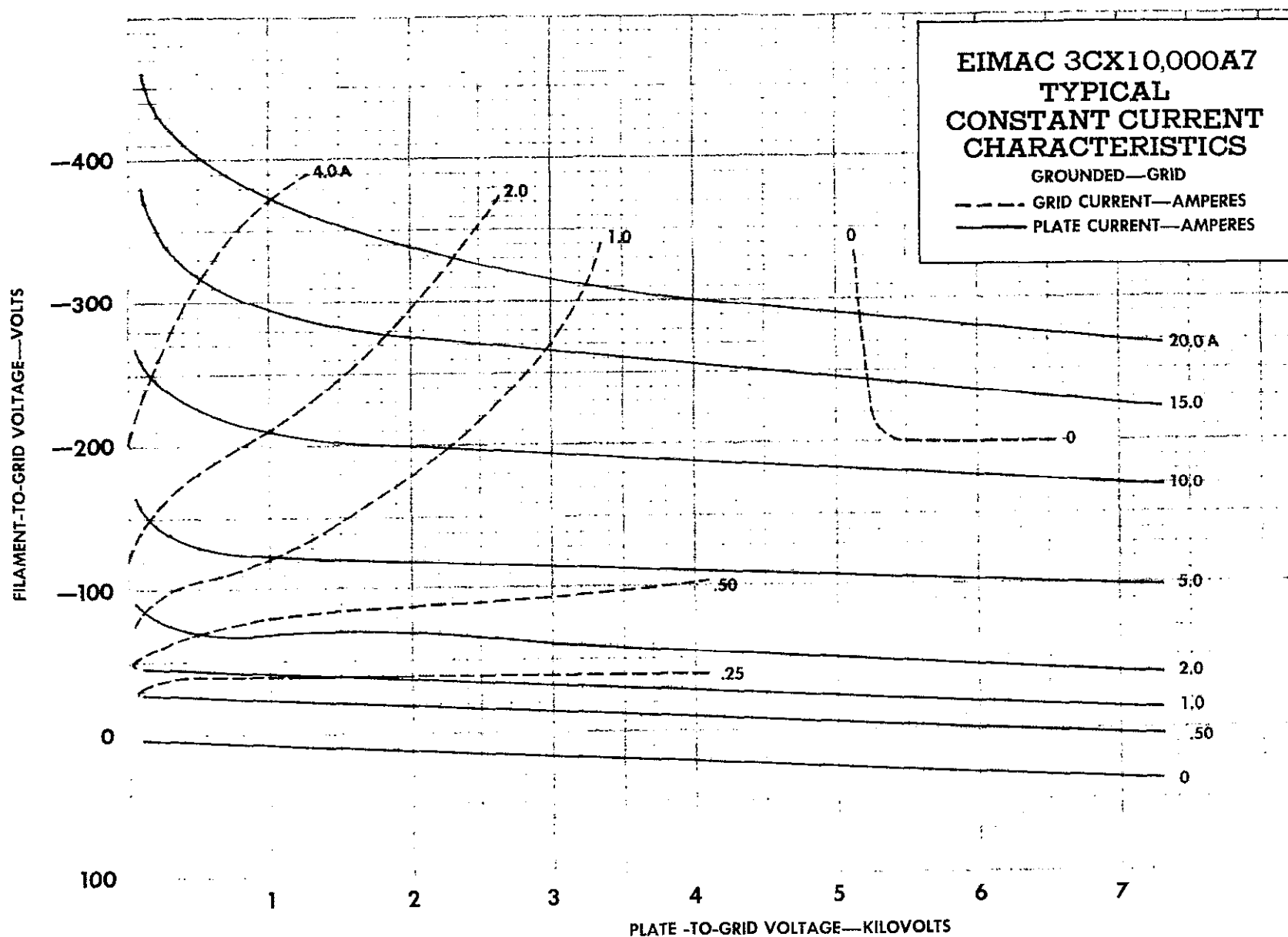
Filament Operation — The rated filament voltage for the 3CX10,000A7 is 7.5 volts. Filament voltage, as measured at the socket, should be maintained at this value to obtain maximum tube life. In no case should it be allowed to deviate from the rated value by more than plus or minus five percent.

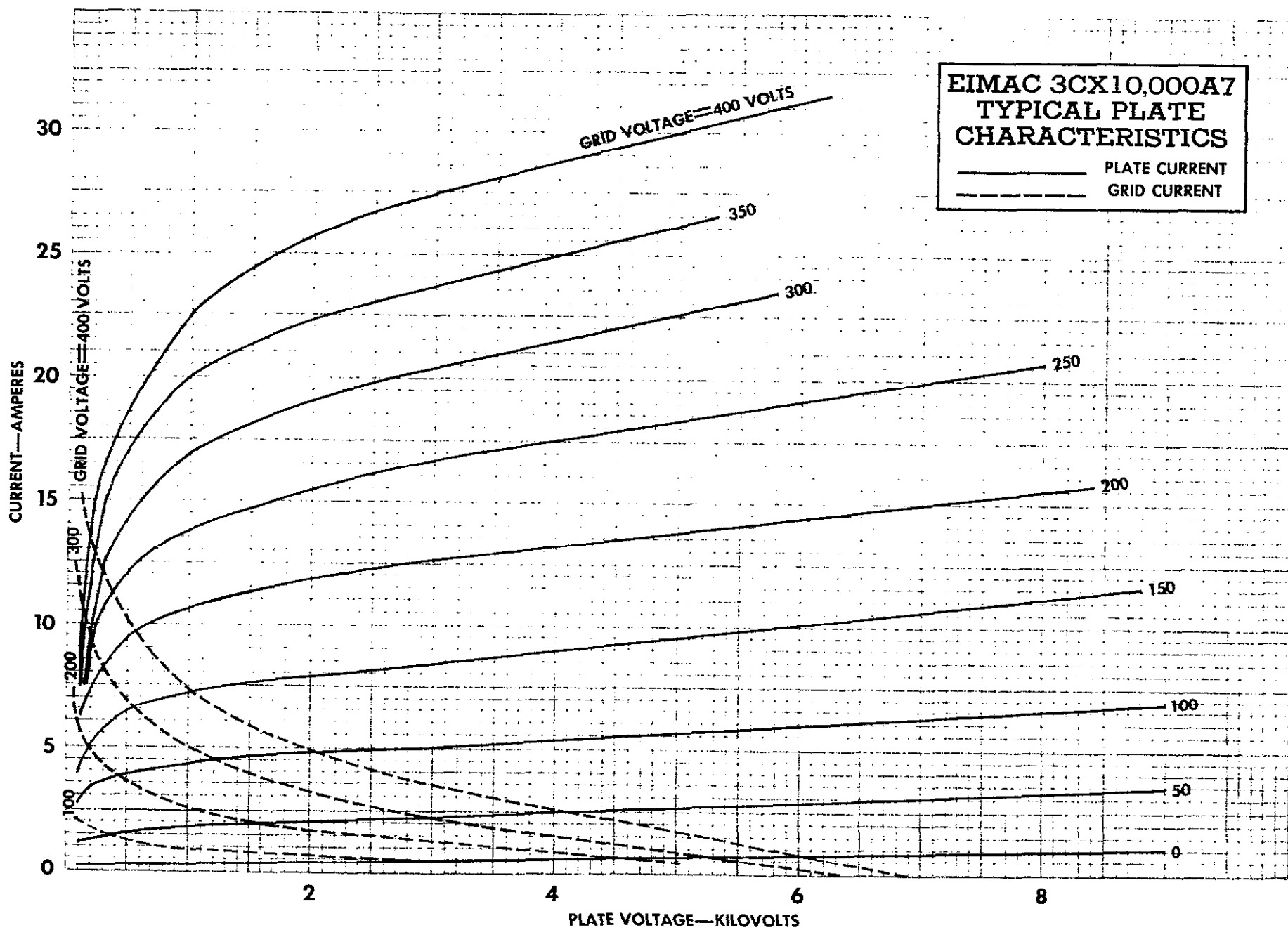
Special Applications — If it is desired to operate this tube under conditions widely different from those given here, write to Power Grid Tube Marketing, EIMAC Division of Varian, 301 Industrial Way, San Carlos, California, for information and recommendations.



DIMENSION DATA

REF.	NOM.	MIN.	MAX.
A		6.928	7.050
B		.855	.895
C		.720	.760
D		1.896	1.936
E		3.133	3.173
F		3.792	3.832
H		.188	
J		.188	
M		3.950	4.300
N		2.412	2.788
P		8.250	8.750
R		.986	1.050
S		3.412	3.788
T		.375	





EIMAC
3CX10,000A7



TECHNICAL DATA

3CX15,000A7

HIGH-MU POWER TRIODE

The EIMAC 3CX15,000A7 is a ceramic/metal power triode intended for use as a zero-bias Class B rf amplifier or Class C power amplifier or oscillator. Class B operation with zero grid bias offers circuit simplicity by eliminating the bias supply. In addition, grounded-grid operation is attractive since a power gain as high as twenty times can be obtained with the 3CX15,000A7.

GENERAL CHARACTERISTICS¹

ELECTRICAL

Filament: Thoriated Tungsten

Voltage	6.3 ± 0.3 V
Current, at 6.3 volts	160 A
Amplification Factor (Average):	200

Direct Interelectrode Capacitance (grounded cathode)²

Cin	56 pF
Cout	0.2 pF
Cgp	36 pF

Direct Interelectrode Capacitance (grounded grid)²

Cin	56 pF
Cout	36 pF
Cpk	0.2 pF

Frequency of Maximum Rating:

CW	110 MHz
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1. Characteristics and operating values are based upon performance tests. These figures may change without notice as the result of additional data or product refinement. EIMAC Division of Varian should be consulted before using this information for final equipment design.

2. Capacitance values are for a cold tube as measured in a special shielded fixture in accordance with Electronic Industries Association Standard RS-191.

MECHANICAL

Maximum Overall Dimensions:

Length	8.75 in; 222.3 mm
Diameter	7.05 in; 179.1 mm
Net Weight	12 lb; 5.5 kg
Operating Position	Vertical base up or down

Maximum Operating Temperature:

Ceramic/Metal Seals	250°C
Anode Core	250°C



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Cooling	Forced air
Base	Coaxial
Recommended Air System Socket	SK-1300 or SK-1320
Recommended Air Chimney	SK-1306

RADIO FREQUENCY LINEAR AMPLIFIER CATHODE DRIVEN

Class AB

ABSOLUTE MAXIMUM RATINGS

DC PLATE VOLTAGE	8000 VOLTS
DC PLATE CURRENT	6.0 AMPERES
PLATE DISSIPATION	15,000 WATTS
GRID DISSIPATION	500 WATTS

1. Approximate values.

TYPICAL OPERATION (Frequencies to 110 MHz)

Class AB₂

Plate Voltage	7000	7000 Vdc
Grid Voltage	0	0 Vdc
Zero-Signal Plate Current ¹	.6	.6 Adc
Single-Tone Plate Current ²	5.92	5.0 Adc
Single-Tone Grid Current ¹	1.22	1.0 Adc
Driving Power ¹	1750	1540 W
Plate Dissipation	13.4	10.8 kW
Single-Tone Plate Output Power	29.6	24.2 kW
Resonant Load Impedance	693	745 Ω
Drive Impedance	27	32 Ω

2. Adjust to obtain specified value.

RADIO FREQUENCY POWER AMPLIFIER OR OSCILLATOR Class C Telephony or FM Telephony

Grid Driven

ABSOLUTE MAXIMUM RATINGS

DC PLATE VOLTAGE	8000 VOLTS
DC GRID VOLTAGE	-500 VOLTS
DC PLATE CURRENT	5.0 AMPERES
PLATE DISSIPATION	15,000 WATTS
GRID DISSIPATION	500 WATTS

TYPICAL OPERATION (Frequencies to 110 MHz)

Plate Voltage	7000 Vdc
Grid Voltage	-230 Vdc
Plate Current	4.0 Adc
Grid Current ¹	775 mAdc
Peak rf Grid Voltage ¹	555 v
Calculated Driving Power ¹	430 W
Plate Input Power	28 kW
Plate Dissipation	6.7 kW
Plate Output Power	21.3 kW
Resonant Load Impedance	963 Ω

1. Approximate value.

NOTE: TYPICAL OPERATION data are obtained by measurement or calculation from published characteristic curves. Adjustment of the rf grid voltage to obtain the specified plate current at the specified bias, and plate voltages is assumed. If this procedure is followed, there will be little variation in output power when the tube is changed, even though there may be some variation in grid current. The grid current which results when the desired plate current is obtained is incidental and varies from tube to tube. These current variations cause no difficulty so long as the circuit maintains the correct voltage in the presence of the variations in current. If grid bias is obtained principally by means of a grid resistor, the resistor must be adjustable to obtain the required bias voltage when the correct rf grid voltage is applied.

RANGE VALUES FOR EQUIPMENT DESIGN

	Min.	Max.
Heater: Current at 6.3 volts	152	168 A
Cathode Warmup Time	5.0	--- sec.
Interelectrode Capacitances (grounded grid) ¹		
C _{in}	50.0	62.0 pF
C _{out}	32.0	40.0 pF
C _{pk}	---	0.3 pF
Interelectrode Capacitances (grounded cathode) ¹		
C _{in}	50.0	62.0 pF
C _{out}	---	0.3 pF
C _{gp}	32.0	40.0 pF

1. Capacitance values are for a cold tube as measured in a shielded fixture in accordance with Electronic Industries Association Standard RS-191.

APPLICATION

MOUNTING & SOCKETING - The 3CX15,000A7 must be operated vertically, base up or down, and should be protected from severe shock and vibration. The use of an EIMAC air-system socket is recommended. For grid-driven applications, the SK-1300 is used; for cathode-driven circuits, the SK-1320 should be used, as the grid is grounded to the socket frame in this unit. The SK-1306 air chimney is designed to fit around the tube's anode cooler and mount with either socket.

COOLING - The maximum temperature rating for the external surfaces of the 3CX15,000A7 is 250°C. Sufficient forced-air cooling must be provided to maintain the temperature of the anode core and the ceramic/metal seals below 250°C. Tube life is usually prolonged if these areas are maintained at temperatures below the maximum rating. Minimum air flow requirements (for air flowing in a base-to-anode direction) to maintain anode core and seal temperatures below 225°C with an inlet-air temperature of 50°C are tabulated below. The use of these air-flow rates through the recommended socket/chimney combination will provide effective cooling of the tube. Air flow should be applied before or simultaneously with the application of electrode voltages (including the filament) and should normally be maintained for a short period of time after all voltages are removed to allow for tube cool-down.

Anode Diss. (watts) *	SEA LEVEL		10,000 FEET	
	Air Flow (cfm)	Approx. Press. drop (In. H ₂ O)	Air Flow (cfm)	Approx. Press. drop (In. H ₂ O)
5,000	242	0.8	350	1.3
7,500	325	1.7	470	2.4
10,000	475	2.8	690	4.1
12,500	640	4.3	930	6.3
15,000	840	6.2	1220	9.7

* Since the power dissipated by the filament is about 1000 watts, and since the grid dissipation can represent another 500 watts, allowance has been made in preparing this tabulation for an additional 1500 watts of dissipation.

FILAMENT OPERATION - The rated filament voltage for the 3CX15,000A7 is 6.3 volts. Filament voltage, as measured at the socket, should be maintained at this value to obtain maximum tube life. In no case should it be allowed to deviate from the rated value by more than plus or minus five percent.

INPUT CIRCUIT - When the 3CX15,000A7 is operated as a ground-grid rf amplifier, the use of a resonant tank in the cathode circuit is recommended in order to obtain greatest linearity and power output. For best results with a single-ended amplifier, it is suggested that the cathode tank circuit operate at a "Q" of two or more.

CLASS-C OPERATION - Although specifically designed for Class-B service, the 3CX15,000A7 may be operated as a Class-C power amplifier or oscillator. The zero-bias characteristic of the 3CX15,000A7 can be used to advantage in Class-C amplifiers by employing only grid-leak bias. If driving power fails, plate dissipation is then kept to a low value because the tube will be operating at the normal static zero-bias conditions.

INTERELECTRODE CAPACITANCE - The actual internal interelectrode capacitance of a tube is influenced by many variables in most applications, such as stray capacitance to the chassis, capacitance added by the socket used, stray capacitance between tube terminals, and wiring effects. To control the actual capacitance values within the tube, as the key component involved, the industry and the Military Services use a standard test procedure as described in Electronic Industries Association Standard RS-191. This requires the use of specially constructed test fixtures which effectively shield all external tube leads from each other and eliminates any capacitance reading to "ground". The test is performed on a cold tube. Other factors being equal, controlling internal tube capacitance in this way normally assures good interchangeability of tubes over a period of time, even when the tube may be made by different manufacturers. The capacitance values shown in the manufacturer's technical data, or test specifications, normally are taken in accordance with Standard RS-191.

The equipment designer is therefore cautioned to make allowance for the actual capacitance values which will exist in any normal application. Measurements should be taken with the socket and mounting which represent approximate final layout if capacitance values are highly significant in the design.

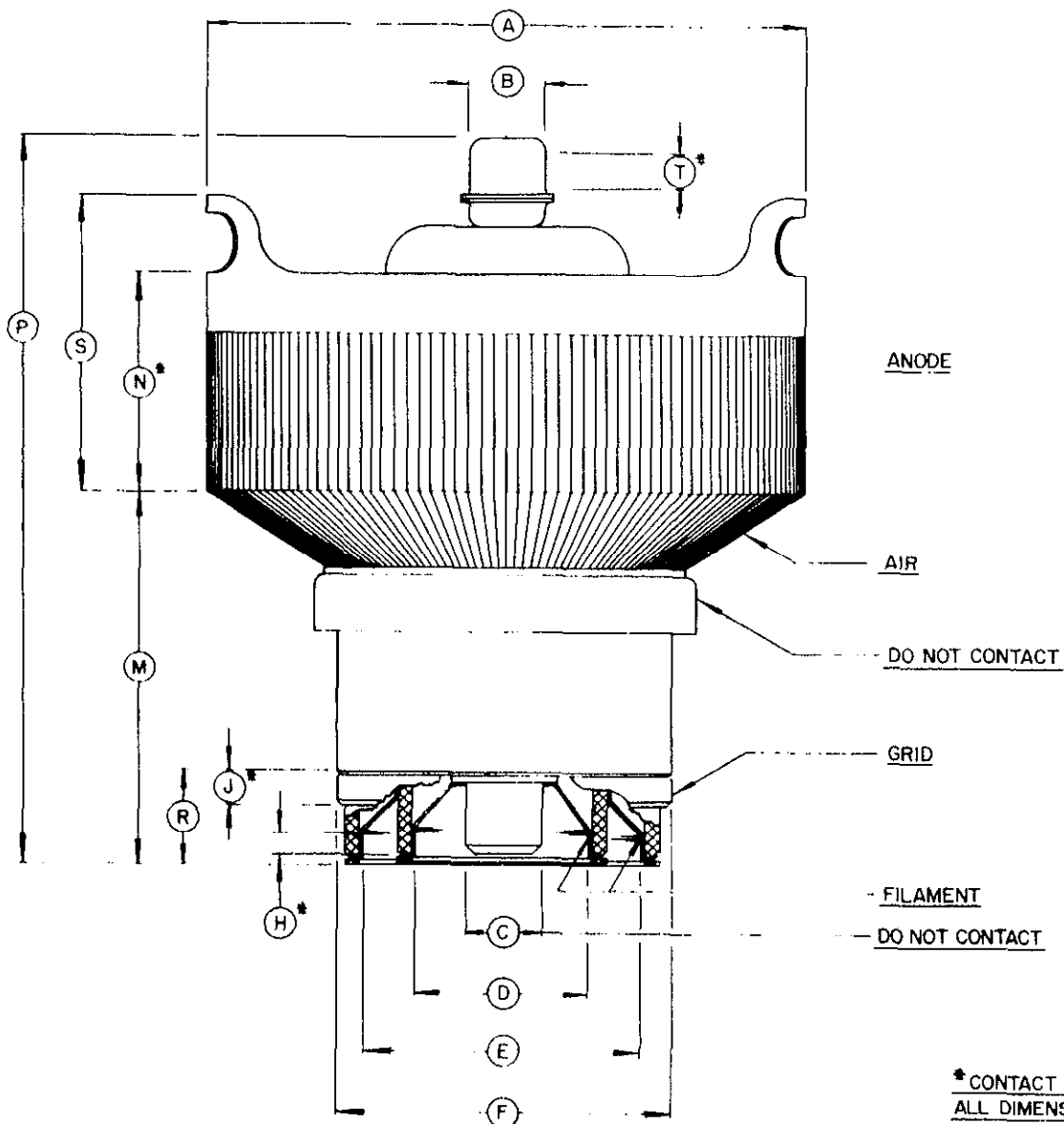
HIGH VOLTAGE - The 3CX15,000A7 operates at voltages which can be deadly, and the equipment must be designed properly and operating

precautions must be followed. Equipment must be designed so that no one can come in contact with high voltages. All equipment must include safety enclosures for high-voltage circuits and terminals, with interlock switches to open the primary circuits of the power supplies and to discharge high-voltage condensers whenever access doors are opened. Interlock switches must not be bypassed or "cheated" to allow

operation with access doors open. Always remember that HIGH VOLTAGE CAN KILL.

SPECIAL APPLICATIONS - If it is desired to operate this tube under conditions widely different from those given here, write to Power Grid Tube Division, EIMAC Division of Varian, 301 Industrial Way, San Carlos, CA 94070, for information and recommendations.

DIM.	INCHES			MILLIMETERS		
	MIN.	MAX.	REF.	MIN.	MAX.	REF.
A	6.928	7.050	--	175.97	179.07	--
B	0.855	0.895	--	21.72	22.73	--
C	0.720	0.760	--	18.29	19.30	--
D	1.896	1.936	--	48.16	49.17	--
E	3.133	3.173	--	79.58	80.59	--
F	3.792	3.832	--	96.32	98.06	--
H	0.188	--	--	4.78	--	--
J	0.188	--	--	4.78	--	--
M	3.950	4.300	--	100.33	109.22	--
N	2.412	2.788	--	61.26	70.82	--
P	8.250	8.750	--	209.55	222.25	--
R	0.986	1.050	--	25.04	26.67	--
S	3.412	3.788	--	86.66	96.22	--
T	0.375	--	--	9.53	--	--

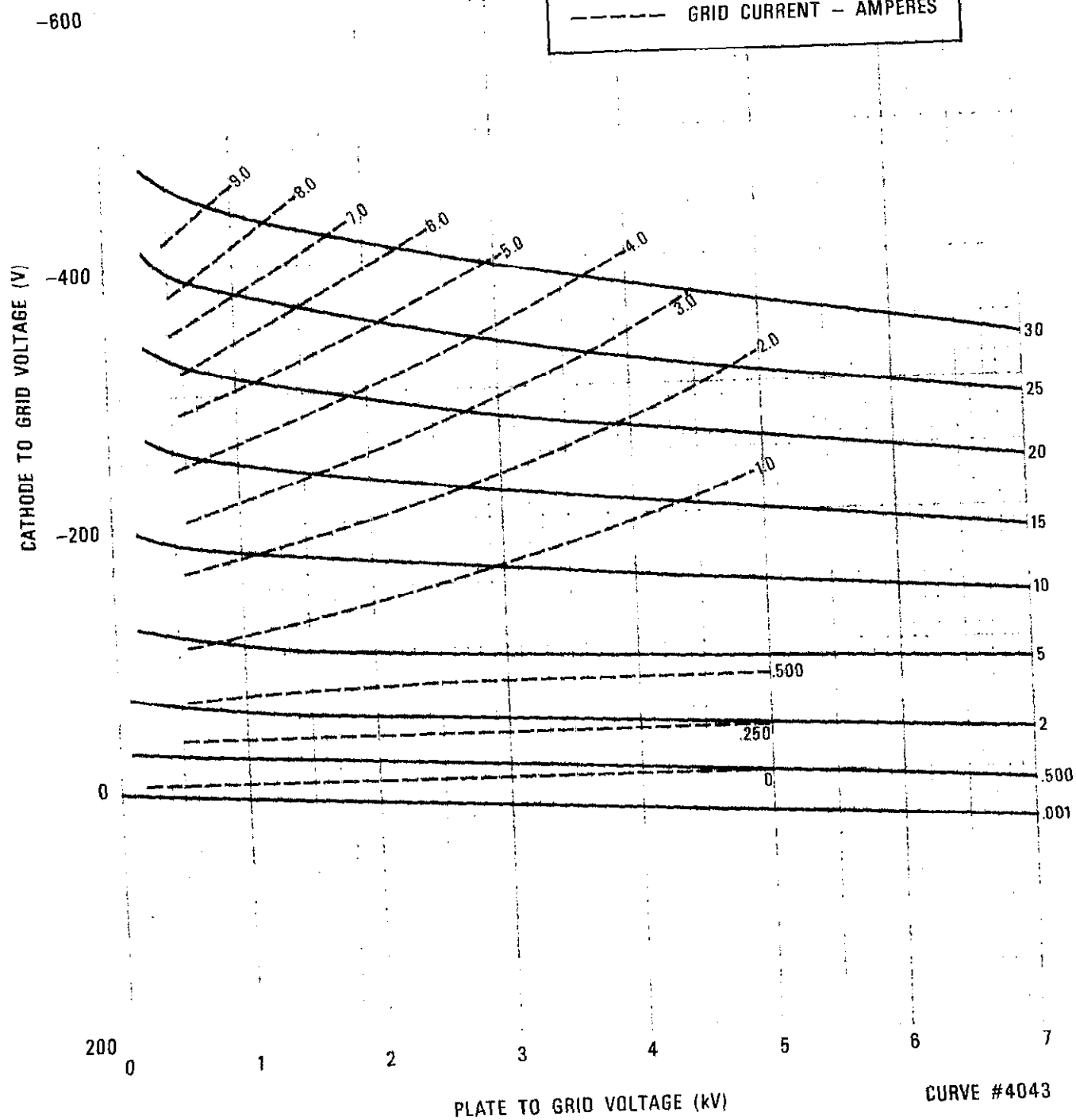


TYPICAL
CONSTANT CURRENT
CHARACTERISTICS

GROUNDING GRID

$E_f = 6.3V$

— PLATE CURRENT — AMPERES
- - - GRID CURRENT — AMPERES



WANLASS

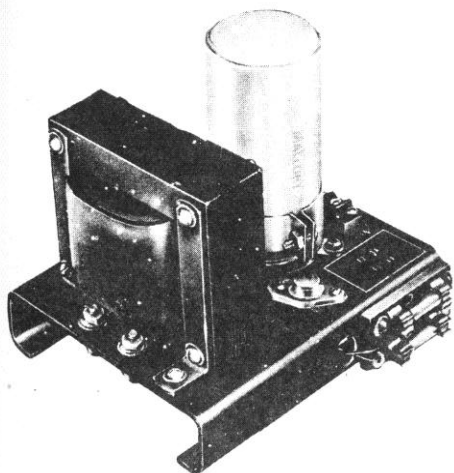
DIVISION OF AMBAC



C214

INSTRUCTION MANUAL

ECONOMY DC RELAY SUPPLY



\$39.00
TO 60 WATTS
QUANTITY PRICE

The C214 provides low cost DC power for inductive load applications such as relays, solenoids, and motors. Pulsed loads up to 4 amperes for short durations (20 ms) are easily accommodated. Circuit simplicity and high volume production line manufacturing have produced a reliable low-cost unit. Internal fusing and easy mounting make the unit suitable for a wide range of applications.

QUANTITY	PRICE
1 - 9	\$46.00
10 - 24	\$43.50
25 - 49	\$41.00
50 - 99	\$39.00

215 224-8510

FOR INDUCTIVE LOADS
SUCH AS
RELAYS
SOLENOIDS
MOTORS

PULSED LOADING
UP TO 4 AMPS

60 WATT
AVERAGE POWER

SIMPLE INSTALLATION

IMMEDIATELY
AVAILABLE
FROM STOCK

SPECIFICATIONS

AC input: 105-125/210-250 volts AC, 1 ϕ , 57 to 63 Hz
(derate output 20% at 50 Hz)

DC output:

Voltage: 26 volts, floating (± 2 volts factory tolerance)

Current: 2.5 amps (designed for pulsed loading of up to
4 amps when operated with 1 amp continuous load
pulsed at 20 ms intervals)

Regulation:

Line: $\pm 2\%$

Load: $\pm 2\%$

Ripple: 0.1% plus 10 mv rms max

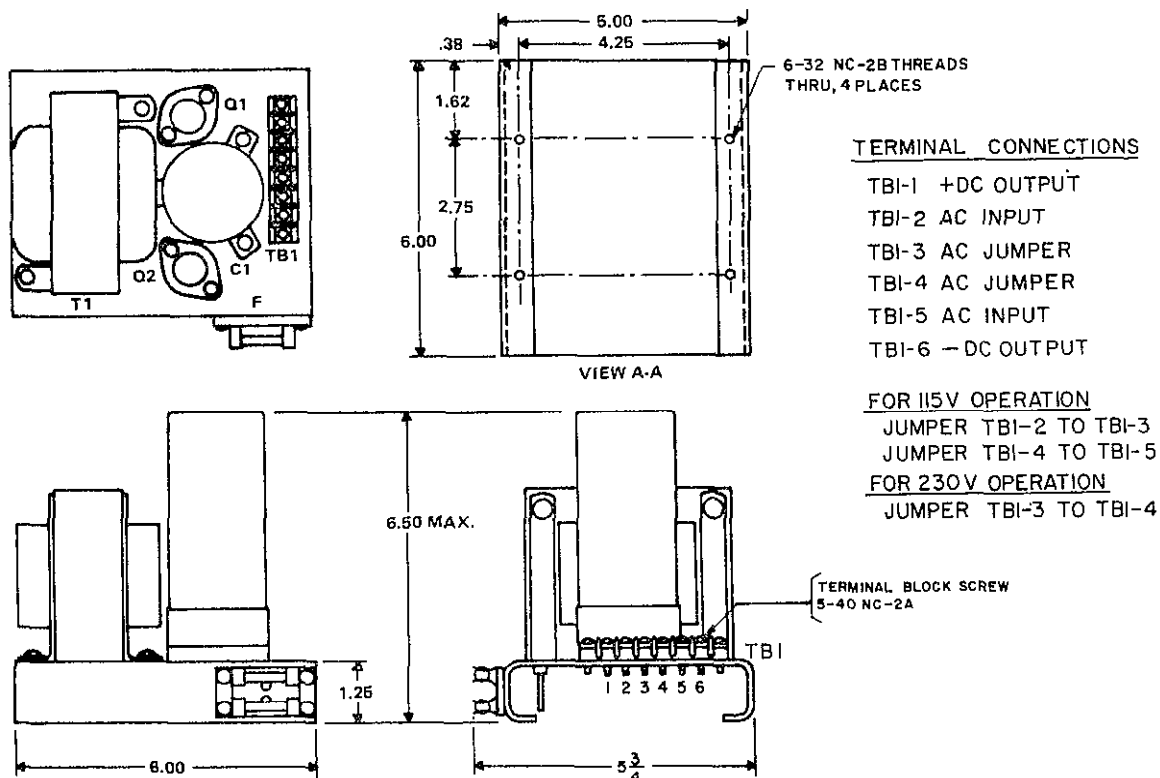
Overload protection: Internally fused

Line fuse: Internally fused: 2 amps input; 3 amps slow blow
output

Temperature: 0 to 40°C (to 70°C with 2%/°C derating from
40°C)

Weight: 5.5 pounds

INSTALLATION DIAGRAM



OPERATION

The C214 is a series-regulated 24-volt dc, 2.5 amp power supply designed for pulsed loading (by inductive loads) of up to 4 amps. Input line and current overload protection is provided by two internal fuses. The dc output is isolated from chassis ground; either the positive or negative terminal can be externally connected to ground or common.

INSTALLATION

Mounting. Outline and mounting dimensions for the C214 are shown on the adjacent installation drawing. The aluminum chassis of the unit serves as a heat sink which may be fastened to a metallic frame to increase heat dissipation. (Allow free air circulation around chassis.)

Electrical. Connect ac-input and dc-output to TB1 as shown on the installation drawing. (Note different jumper connections for 115-vac and 230-vac operation.) Use twisted pairs to separate input and output lines and achieve maximum noise rejection.

NOTE

Input line fuse (F1) is not internally wired. Connect this fuse in series with line when connecting ac input.

ADJUSTMENTS

No adjustments are required for the C214.

TEST PROCEDURE

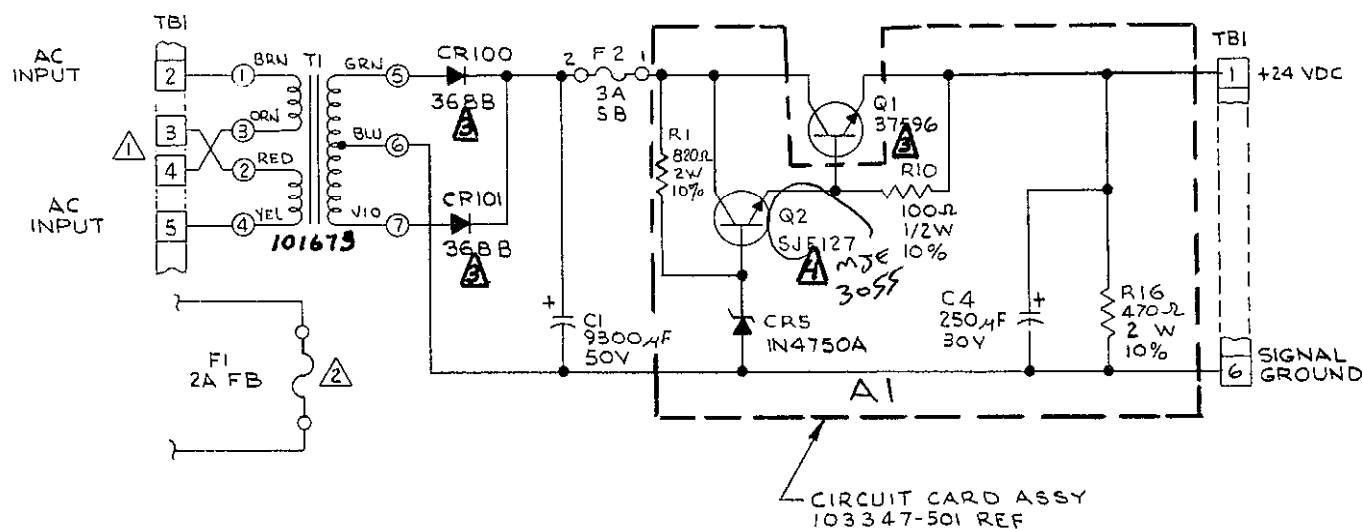
To test the unit, connect the ac input and dc output as instructed for installation and perform the following tests.

Line Regulation. Connect a Variac to ac input line and connect dc output to full load. While varying ac input from 105 to 125 vac (or 210 to 250 vac), use voltmeter to check that dc output voltage variations do not exceed $\pm 2\%$ of output voltage (or more than 1 volt).

Load Regulation. Set ac input to 115 volts (or 230 volts); then measure dc output while varying load from 0% to 100%. Check that dc output voltage variations do not exceed $\pm 2\%$ of output voltage (or less than 1 volt).

Ripple. Set ac input at 115 (or 230) volts and apply full load to dc output. Use oscilloscope with high-gain preamplifier to check that ac ripple at dc output terminals does not exceed 0.1% (plus 10 mv rms) of output voltage.

C-214 SCHEMATIC DIAGRAM



NOTES:

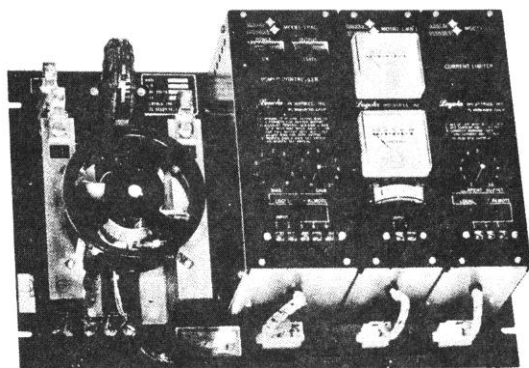
1. Strap TB1-2 to TB1-3 and TB1-4 to TB1-5 for 115-VAC operation. Strap TB1-3 to TB1-4 for 230-VAC operation.
2. F1 is not wired; connect for external AC-input line fusing.
3. Westinghouse Electric Co.
Newark, N. J.
4. Motorola Semiconductor Products
Box 20912 Phoenix, Arizona

MJE 3055

LOYOLA INDUSTRIES, INC.

LPAC-1 CONTROLLER

MAINTENANCE AND REPAIR



1. GENERAL

A. Permit only qualified instrument technicians to service and repair Loyola LPAC-1 Controllers.

B. Evidence of proper operation:

1) Trigger-box neon indicator lamps

a) POWER ON neon indicator lamp: constant bright glow when AC line voltage is connected.

b) OUTPUT LEVEL neon indicator lamp: variable from dim to bright glow with power output level.

2) LMB-1 Meter-box

a) Voltmeter indicates output voltage (i.e. from zero to near line voltage)

b) Ammeter indicates LPAC-1 current output (i.e. from approx. zero to maximum rated output or to maximum load current if less than rated.)

c) Milliammeter indicates command signal current input from external temperature transducers or other controllers (i.e. from zero to 5 MA)

C. Any one or more of the following circumstances or indications may be evidence of improper operations:

1) No output

2) Continuous but irregular output, as a sharp increase to full output for a small increase in command signal strength or for a partial turn of the BIAS control knob.

3) Intermittent output, as a change from stable output to no output and return to stable output for no apparent reason (i.e. for no change in command signal input or BIAS or GAIN control knob settings)

4) Constant uncontrollable full output

5) Fan not rotating or rotating slowly

6) Overheating of any part of the LPAC-1 Controller unit

2. TROUBLESHOOTING

A. General:

1) It is not necessary to disconnect the AC line voltage from the LPAC-1 unit when the evidence of improper operation is "no output". However, do disconnect the AC line voltage from the unit before beginning checking and servicing when disconnection is required for safety.

2) Disconnect the AC line voltage from

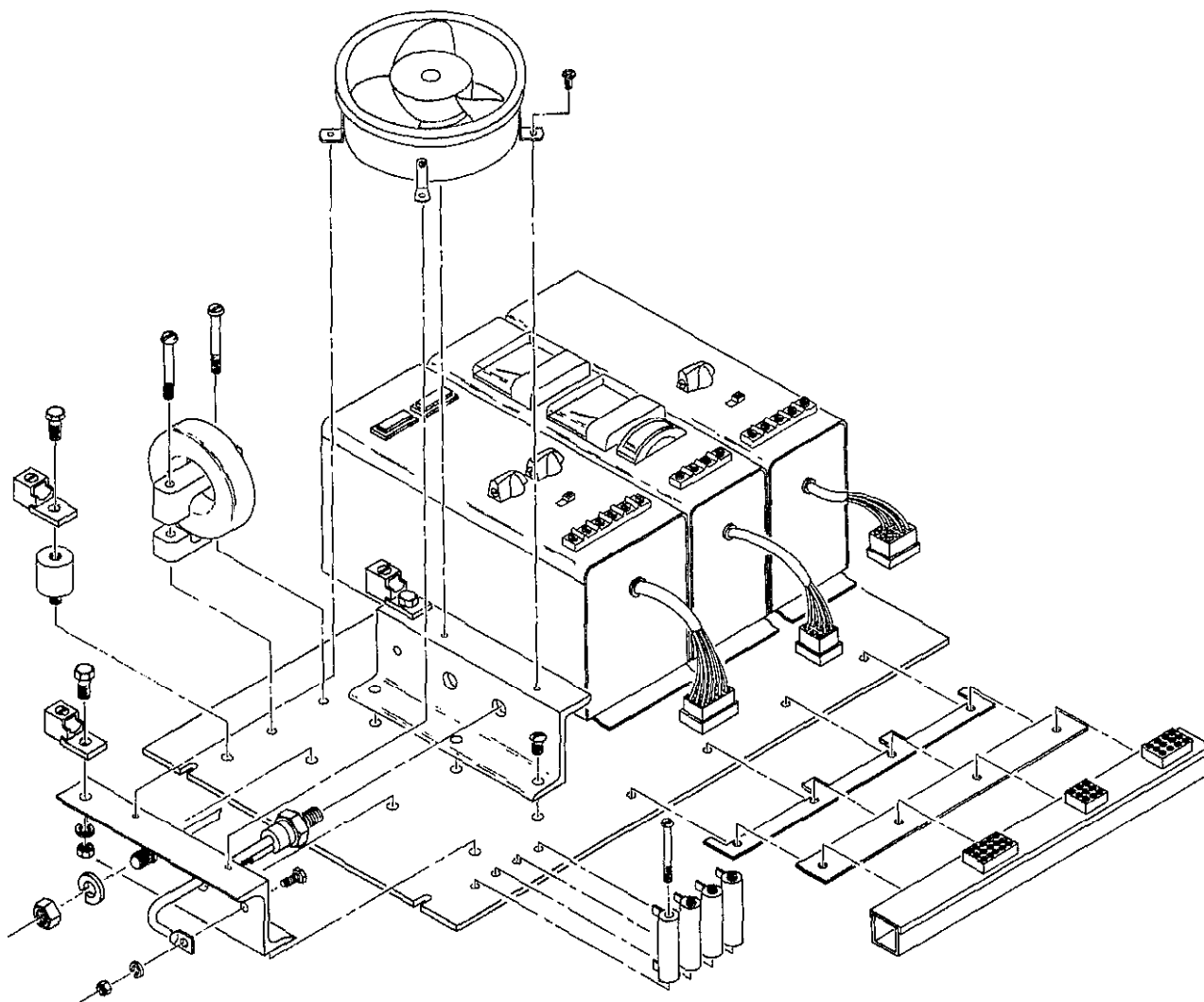


Fig. 1 - Exploded View of LPAC-1 Controller

the LPAC-1 unit immediately for all other evidences of improper operation.

3) Preliminary set-up conditions for testing:

- a) Verify that the neon indicator lamps on the trigger module are not faulty.
- b) Set the LOCAL-REMOTE switch on the trigger module to LOCAL position.
- c) Set the BIAS control knob at zero.
- d) Set the GAIN control knob at zero.

- e) If the LPAC-1 includes the LCL current-limiter accessory, set the CURRENT ADJUST control knob at zero.

- 4) If the LPAC-1 does not include the LMB meter accessory, use ironvane voltmeters and ammeters, such as the General Electric Biglook Series, A090, 91, and 92, or equal, to accurately check operation and performance. Clamp-on-ammeters or other averaging-type ammeters using rectifier elements and d'Arsonval movements may be used as indicators of relative output and general performance, BUT REMEMBER: the indicated value on such an

ammeter may be in error by as much as 50% in its middle range, even though the indicated value at maximum output voltage may be nearly accurate.

- 5) Always use a dummy load to check LPAC-1 performance before putting the unit back in service after it has been serviced or repaired. It is recommended that 100 watt incandescent lamps, connected in series to match the rated output voltage, be used as the dummy load.

6) Start-up procedures:

- a) Verify that switches and control knobs are positioned as required for testing preliminary set-up in A.3) above.
- b) Connect the dummy load to the output terminals.
- c) Connect the AC line voltage to the LPAC-1.
- d) Turn the BIAS control knob slowly in a clockwise direction. The OUTPUT LEVEL neon indicator lamp and the dummy-load lamps should slowly increase in brightness. When the LPAC-1 includes the LMB meter accessory, the LMB voltmeter indicator should move slowly up-scale, but the LMB ammeter may not move off zero unless a sufficient number of dummy-load lamps is used to provide great enough resistance to register on the LMB ammeter.

B. No output

1) Check the AC line voltage input:

- a) The POWER ON neon indicator lamp should glow brightly when the AC line voltage is connected. The LPAC-1 should operate normally when the AC line voltage is between 50% and 110% of the rated input.

- b) If found faulty, connect proper AC line voltage to the LPAC-1.

2) Verify that the white nylon connector plugs are firmly plugged in.

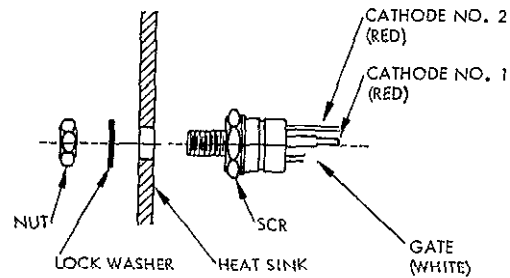


Fig. 2 - Correct installation of SCR

TORQUE VALUES FOR MOUNTING SCR'S		
STUD SIZE	MAXIMUM TORQUE	
	INCH LBS.	FOOT LBS.
1/4 inch	30	5
5/16 inch	150	12
3/8 inch	150	15
1/2 inch	150	18
3/4 inch	300	20

- 3) Verify that the trigger module printed circuit board is firmly and properly plugged into its plug strip. CAUTION: If it is necessary to open the trigger module to do this, then disconnect the AC line voltage from the LPAC-1 unit before opening the trigger module and reconnect the AC line voltage to the LPAC-1 unit after re-closing.
- 4) Check the SCR's visually to see if one or both have ruptured or disintegrated.

- a) If an SCR has ruptured or disintegrated, disconnect the AC line voltage from the LPAC-1 unit. Then carefully unsolder the SCR gate and cathode leads, remove the nut, washers, and terminals from the SCR lug, and remove the defective SCR.

- b) Install a new SCR. Apply a little silicone grease under the

SCR. Do not torque the nut on the SCR lug beyond the values set forth in chart. Lockwasher must be between nut and heatsink NOT between SCR and heatsink.

- c) Carefully re-solder the SCR gate and cathode leads. Do not use acid flux or acid-core solder.
 - d) Re-connect the AC line voltage to the LPAC-1.
- 5) Check external command signal input and the trigger internal signal circuits.
- a) Verify the command signal input voltage and current at the trigger module signal input terminals. If there is no command signal input, then the fault is not in the LPAC-1 unit but in the command signal generating device or in the signal wiring.
 - b) If there is command signal input, then check the trigger internal signal circuits by turning the GAIN control knob slowly from zero in a clockwise direction. As the GAIN control knob is turned the LMB voltmeter indicator or the customer-furnished voltmeter indicator should move slowly up-scale and the OUTPUT LEVEL neon indicator lamp should gradually increase in brightness.
 - c) If the voltmeter and the OUTPUT LEVEL neon indicator lamp do not indicate proper operation in B.5)b) above, then reset the GAIN control knob at zero and turn the BIAS control knob slowly from zero in a clockwise direction. As the BIAS control knob is turned the LMB voltmeter indicator or the customer-furnished voltmeter indicator should move slowly up-scale and the OUTPUT

LEVEL neon indicator lamp should gradually increase in brightness.

- d) If no shut-off option is included in the LPAC-1 unit and the above-described check procedures result in negative indications, remove the trigger module and return it to the Service Department for repair. If a shut-off option is included in the LPAC-1 unit, proceed with the following check procedures.
- 6) Check the LPAC-1 internal latching shut-off circuit:
- a) If the LPAC-1 has the non-latching shut-off terminal option, disconnect one lead to the non-latching shut-off terminal without disconnecting the AC line voltage from the LPAC-1 unit. This should return all circuits to normal operating condition. Then re-connect the disconnected lead to the non-latching shut-off terminal before returning the unit to operation.
 - b) If the LPAC-1 has the latching shut-off terminal option, disconnect one lead to the latching shut-off terminal and then disconnect the AC line voltage from the LPAC-1. Then, with one lead to the latching shut-off terminal still disconnected, re-connect the AC line voltage. This should return all circuits to normal operating condition. Then re-connect the disconnected lead to the latching shut-off terminal before returning the LPAC unit to operation.
 - c) If the procedures for either option do not return the LPAC-1 circuits to normal operating condition, then disconnect the LPAC trigger module and return it to the

Service Department for repair.

7) Check the LCL current limiter:

- a) Set the BIAS and GAIN control knobs on the trigger module at zero, then unplug the current-limiter white nylon plug.
- b) Turn the BIAS control knob very slowly from zero in a clockwise direction. The OUTPUT LEVEL neon indicator lamp should change slowly from a dim to a brighter glow, indicating normal trigger-box operation. (NOTE: The LMB ammeter will not operate when the LCL current limiter is unplugged.)
 - (i) If normal trigger operation is indicated, then the current limiter is defective. Remove it and return it to the Service Department for repair.
 - (ii) If normal trigger operation is not indicated, then the trigger is defective. Remove it and either return it to the Service Department for repair or bench-check it and repair it as bench checking indicates is required. (Refer to Fig. 3 for recommended set-up for bench-check of the trigger PC board.)

C. Continuous but irregular output

- 1) If a fully-competent electronic technician is not available, then remove the trigger module from the LPAC-1 and return it to the Service Department for repair.
- 2) If a fully-competent electronic technician is available, then remove the trigger module from the LPAC unit and bench-check the trigger amplifier circuit voltages and resist-

ances per Circuit Diagram in this manual, and repair carefully or replace defective circuit elements as required. (Refer to Fig. 3 for recommended set-up for bench-check of the trigger-box PC board.)

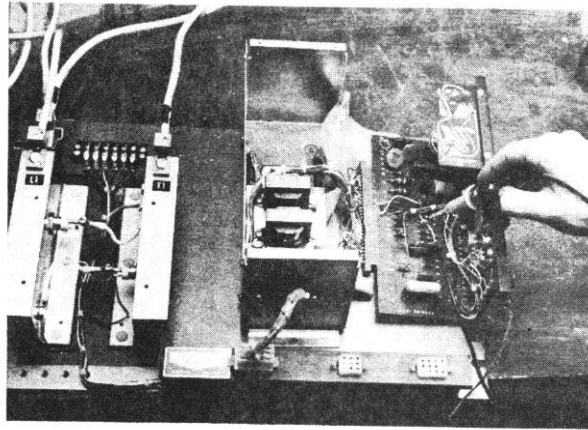


Fig. 3 – Recommended set-up for bench check of P.C. board

D. Intermittent output: If the trigger and the current-limiter have been checked as outlined above and have been found in proper operating condition, then proceed as follows:

- 1) Check for:
 - a) Loose terminals in the power circuit.
 - b) Discontinuity in the external wiring.
 - c) Loose pins in sockets and plugs.
 - d) Unsoundness in solder joints.
 - e) Leaks in the transformer. Use a "meger" or high potential voltage of very low current to check the transformer internal insulation. Check only transformer terminals L, T, and "Common" to the transformer chassis.
- 2) Repair or replace defective parts or installations as required.

E. Constant uncontrollable full output

- 1) If there is a full output indication (i.e. the voltmeter indicates full rated output and the OUTPUT

LEVEL neon indicator lamp glows brightly) but there is no output current, then check the load circuit fuse and the load circuit wiring for an open circuit. Replace the fuse or repair the load circuit wiring as required to obtain normal closed circuits.

- 2) If uncontrollable full output continues after completing 2.E.1) above, then disconnect the trigger-box white nylon connector plug. If uncontrollable full output still continues, then one or both SCR's are probably internally shorted and defective.

a) Disconnect the load from the load terminals. Measure the resistance between L-1 and T-1 with an ohmmeter at low scale (i.e. X1). If the resistance is less than 5 ohms, then at least one SCR is defective.

b) Disconnect one SCR cathode lead. Measure the resistance between L-1 and T-1 as in 2.E.2)a) above. If the resistance is less than 5 ohms, then the remaining connected SCR is defective. If the resistance is very much greater than 5 ohms (i.e. if the circuit appears open) then the disconnected SCR is defective.

c) To test an isolated SCR unit, proceed as follows:

(i) Measure the resistance across the cathode and anode of the SCR with an ohmmeter set at low scale (i.e. X1). Then reverse the ohmmeter leads on the same SCR terminals and measure the resistance again. If the resistance of the SCR measures less than 1K in either direction, the SCR is defective.

(ii) If the SCR does not appear defective when

tested as outlined above in 1), then check the SCR with 1.5 X line voltage DC across its cathode and anode in both directions. If there is current leakage greater than 2 milliamps in either direction, then the SCR is defective.

(d) If a defective SCR is found, remove and replace it as described in 2.B.4)a) through 2.B.4)d).

- 3) If a new SCR is installed, and the output of the unit in service is to a transformer, then check the unit by applying the LPAC-1 current output to a dummy load before returning the LPAC unit to service. (Refer to 2.A.5) for recommended dummy load.)

F. Fan not rotating or rotating slowly

Remove fan unit and repair or replace with a properly operating fan unit.

G. Overheating of any part of the Controller unit

If the air-cooling or water-cooling system is functioning properly and overheating occurs, it indicates one of the following:

a) Shorting or otherwise defective LPAC-1 circuit elements. Check and repair as described in 2.C.1) and 2.C.2).

b) Customer load current too high. Check to verify that the customer load current is within the rating of the LPAC-1 unit.

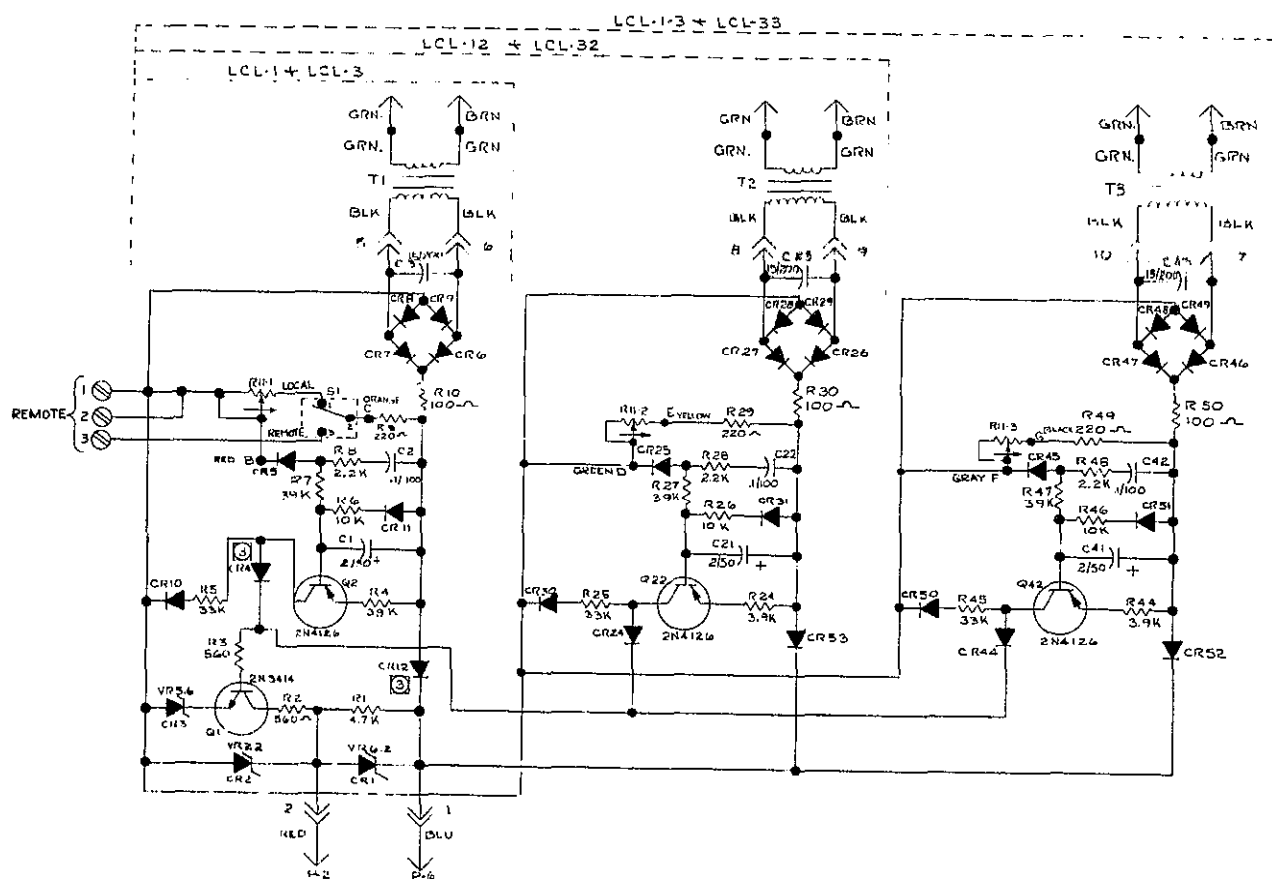


Fig. 4 – Internal schematic LCL Current Limiter

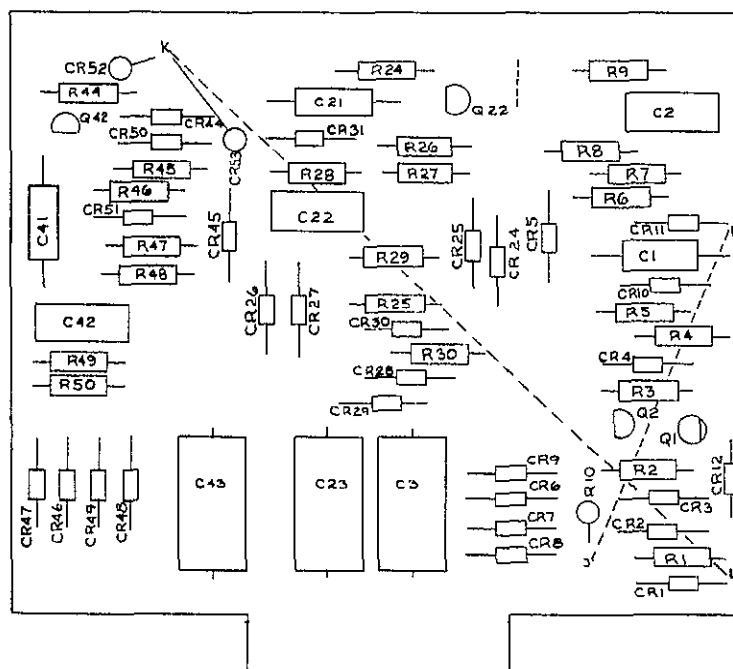


Fig. 5 – Location of components on LCL Current Limiter Printed Circuit Board

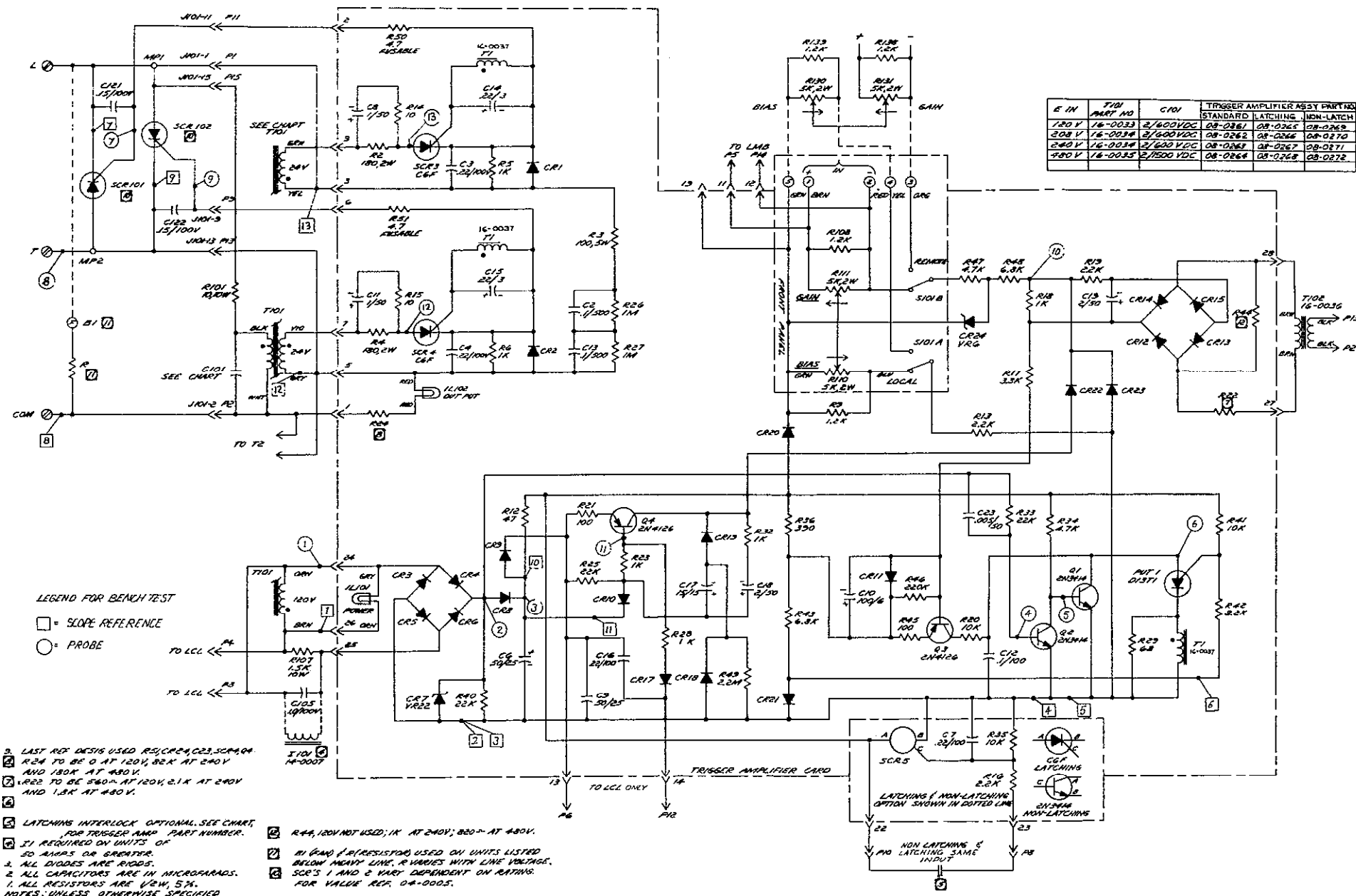


Fig. 6 – Internal schematic - LPAC-1 Trigger Amplifier

AMERICAN ELECTRONIC LABORATORIES, INC.

FIELD SERVICE DATA SHEET

Type of Service FM 25 KG Mod.

Station WAYL Date 6/3/77 Model FM 25 KG S/N 052M

Frequency 93.7 Power Output 24.5 KW

Line Phase 1 240 VAC Driver Screen I 50 MA

Line Phase 2 242 VAC Exciter Forward 20

Line Phase 3 242 VAC Exciter Reflected .1

Driver Filament E 5.1 VAC Power Amp Forward 15.5 = 24.5 KW

Power Amp Filament E 6.1 VAC Power Amp Reflected 400

PA Cathode I 4.9 AMPS Cathode Resistance 12.5 Ω

PA Plate I 4.0 AMPS Transformer Taps 220, +10

Driver Plate E 4.2 KV Efficiency 72.9 %

Power Amp Plate E 8.4 KV Counter Settings

Driver Grid E 85 VOLTS PA Output Loading 02072

Driver Cathode I .67 AMPS PA Output Tuning 00443

Driver Screen E 505 ~~5~~ VOLTS PA Input Tuning 00273

PROOF OF PERFORMANCE

FM Noise	<u>-64</u>	AM Noise	<u>50 dB</u>
Distortion @ 100% Mod.		Input Level (dB)	
50 Hz	<u>.36</u>		<u>10.3</u>
100 Hz	<u>.30</u>		<u>10.0</u>
400 Hz	<u>.33</u>		<u>9.5</u>
1000 Hz	<u>.27</u>		<u>8.4</u>
5000 Hz	<u>.46</u>		<u>0.8</u>
7500 Hz	<u>.46</u>		<u>-3.0</u>
10,000 Hz	<u>.40</u>		<u>-4.6</u>
15,000 Hz	<u>.51</u>		<u>-8.5</u>

Station Engineer

[Signature]
L. Brading

AEL Engineer

[Signature]
Robert C. Moore

75 us DE-EMPHASIS

CUSTOMER ORDER NUMBER 05754 STATION CALL LETTERS _____

CUSTOMER NAME Radio Systems

BEI P/N 909 0009 (19") (21") BEI SERIAL NUMBER 1228

TESTED BY Jim Boley DATE 12-10-84

1. INPUT VOLTAGE SELECTION 120 FUSE 3 AMPS

2. OPERATING FREQUENCY 93.7 MEASURED 93.699999 MHZ. + 10 HZ

3. FREQUENCY CODE 1001 (10) 10MHZ 0011 (9) 1MHZ 0110 (6) 100KHZ 1001 (9)

(0=ON=JUMPER IN) (1=OFF=JUMPER OUT)
OUTPUT FREQUENCY EQUALS CODE + 10KHZ.

4. AFC VOLTAGE 10.6 VOLTS 5. AFC INTERLOCK OK

6. POWER OUTPUT 5 WATTS NOTE: (SET TO 5.0 WATTS "AUTO MODE" UNLESS OTHERWISE REQUESTED)

7. PAV 7 VOLTS PAI 1.22 AMPS 8. HARMONIC AND SPURIOUS SUPPRESSION (58db Min.) OK

9. POWER SUPPLY VOLTAGES OK 10. BARRIER STRIP INPUTS/OUTPUTS OK

11. TEMPERATURE OVERLOAD OK 12. VSWR PROTECTION OK

13. TEST METERING OK 14. COMPOSITE TEST JACKS OK

15. COMPOSITE FM S/N RATIO 79 dB (75 dB MIN. WITH 75 us DE-EMPHASIS)

16. COMPOSITE IMD, 60kHz/7kHz, 1:1 .018 % (75 us DE-EMPHASIS) (0.08% MAX)

17. COMPOSITE THD @ 400Hz .017 % (75 us DE-EMPHASIS) (0.08% MAX)

18. COMPOSITE INPUT LEVELS FOR 100% MODULATION 1.237 V 1.237V RMS, NOMINAL)

19. SCA INPUT LEVELS FOR 10% MODULATION 1.237 V 1.237V RMS, NOMINAL)

20. MONO INPUT LEVELS FOR 100% MODULATION +10 dBm (600 ohm BAL.)

21. MONO FM S/N RATIO 79 dB (75 dB MIN. WITH 75 us DE-EMPHASIS)

22. AM S/N RATIO 75 dB (70 dB MIN. WITH 75 us DE-EMPHASIS)

23. MONO IMD, 60Hz/7kHz, 4:1 .018 % (75 us DE-EMPHASIS) (0.08% MAX)

24. MONO FREQUENCY RESPONSE---50Hz -1.2 dB (0.0 ± 0.5dB) 5kHz +8.6 dB (+8.2 ± 0.5dB)

100Hz 0 dB (Ref 0.0dB) 10kHz +13.8 dB (+13.7 ± 0.5dB)

400Hz +1.2 dB (+0.2 ± 0.5dB) 15kHz +16.8 dB (+17.1 ± 0.5dB)

1000Hz +1 dB (+0.9 ± 0.5dB)

25. MONO THD---50Hz .019 % 5kHz .023 %*

100Hz .018 % 10kHz .057 %*

400Hz .017 % 15kHz .061 %*

1000Hz .018 % *INDICATES NOISE LIMITED AFTER DE-EMPHASIS