INSTRUCTION MANUAL

FM-30 30 Kilowatt FM Broadcast Transmitter

30 July 1982

IM No. 597-0003



BROADCAST ELECTRONICS INC.

a FILMWAY/ company

IMPORTANT INFORMATION

EQUIPMENT LOST OR DAMAGED IN TRANSIT

When delivering the equipment to you, the truck driver or carrier's agent will present a rece for your signature. Do not sign it until you have (a) inspected the containers for visible signs of damage and (b) counted the containers and compared with the amount shown on the shipping papers. If a shortage or evidence of damage is noted, insist that notation to that effect be made on the shipping papers before you sign them.

Further, after receiving the equipment, unpack it and inspect thoroughly for concealed damage. If concealed damage is discovered, immediately notify the carrier, confirming the notification in writing, and secure an inspection report. This item should be unpacked and inspected for damage WITHIN 15 DAYS after receipt. Claims for loss or damage will not be honored without proper notification of inspection by the carrier.

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Technical assistance is available from Broadcast Electronics by letter or prepaid telephone or telegram. Equipment requiring repair or overhaul should be sent by common carrier, prepaid, insured and well protected. Do not mail equipment. We can assume no liability for inbound damage, and necessary repairs become the obligation of the shipper. Prior arrangement is necessary. Contact Customer Service Department for a Return Authorization.

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WARRANTY ADJUSTMENT

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RETURN, REPAIR AND EXCHANGES

Do not return any merchandise without our written approval and Return Authorization. We will provide special shipping instructions and a code number that will assure proper handling and prompt issuance of credit. Please furnish complete details as to circumstances and reasons when requesting return of merchandise. All returned merchandise must be sent freight prepaid and properly insured by the customer.

REPLACEMENT PARTS

Replacement and Warranty Parts may be ordered from the address below. Be sure to include equipment model and serial number and part description and part number.

Broadcast Electronics, Inc. 4100 N. 24th St., P.O. Box 3606 Quincy, Illinois 62305 Tel: (217) 224-9600 Telex: 25-0142 Cable: BCST ELECT QUI

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MODIFICATIONS

Broadcast Electronics, Inc. reserves the right to modify the design and specifications of the equipment in this manual without notice. Any modifications shall not adversely affect performance of the equipment so modified.



PUBLICATION CHANGE NOTICE

EQUIPMENT_	FM TRANSMITTER	MODEL(S) FM-30 SERIAL
PUBLICATION	NUMBER 597-0003	BASIC ISSUE/REVISION 30 JULY 1982
INSTRUCTION	S: Make the changes note	d below as listed.
	Replacement pages wil notice as required.	1 be attached to this change
	This change notice sh	ould be retained with the publication.
CHANGE NO.	DATE	DESCRIPTION
1	5 NOV 1982 1. Two og availa	otional iron vane filament meters are able:
	A.	An iron vane meter is available which replaces the rectifier type meter normally installed in the FM-30 (P/N 909-0109).
	Β.	An additional iron vane meter is available which mounts below the filament HOURS meter (P/N 909-0092). This additional meter is wired in parallel across the PA meter panel FILAMENT VOLTAGE meter (M206).
		he attached parts lists to Part I, Section 6, bles 6-4A and 6-4B, page 6-7A.
		the parts list additions to the FM-30 List Index on page 6-1.
2		he attached discussion of Operating Hazards e front of the manual.
	<u></u>	

REF. DES.	DESCRIPTION	PART NO.	QTY.
M209	Meter, 3.5 inch (8.89 cm) Iron Vane Type, 0-15 Vac ±3% FS, 60 Hz	310-0017	1
	Hole Plug, 1 1/4 inch (3.18 cm)	450-1715	1

Table 6-4A. Additional Iron Vane Filament Metering Option - 909-0092

Table 6-4B. Replacement Iron Vane Filament Metering Option - 909-0109

REF. DES.	DESCRIPTION	PART NO.	QTY.
M206	Meter, 1.5 inch (3.8 cm) Iron Vane Type, O-12 Vac ±2% FS, 60 Hz	317-0010	1
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OPERATING HAZARDS

READ THIS SHEET AND OBSERVE ALL SAFETY PRECAUTIONS

ALL PERSONS WHO WORK WITH OR ARE EXPOSED TO POWER TUBES, POWER TRANSISTORS, OR EQUIPMENT WHICH UTILIZES SUCH DEVICES MUST TAKE PRECAUTIONS TO PROTECT THEMSELVES AGAINST POSSIBLE SERIOUS BODILY INJURY. EX-ERCISE EXTREME CARE AROUND SUCH PRODUCTS. UNINFORMED OR CARELESS OPERATION OF THESE DEVICES CAN RESULT IN POOR PERFORMANCE, DAMAGE TO THE DEVICE OR PROPERTY, SERIOUS BODILY INJURY, AND POSSIBLY DEATH.

DANGEROUS HAZARDS EXIST IN THE OPERATION OF POWER TUBES AND POWER TRANSISTORS

The operation of power tubes and power transistors involves one or more of the following hazards, any one of which, in the absence of safe operating practices and precautions, could result in serious harm to personnel.

- A. HIGH VOLTAGE Normal operating voltages can be deadly. Additional information follows.
- B. RF RADIATION Exposure to RF radiation may cause serious bodily injury possibly resulting in blindness or death. Cardiac pacemakers may be affected. Additional information follows.
- C. BERYLLIUM-OXIDE POISONING Dust or fumes from BeO ceramics used as thermal links with conduction cooled power tubes and power transistors are highly toxic and can cause serious injury or death. Additional information follows.
- D. HOT SURFACES Surfaces of air-cooled radiators and other parts of tubes can reach temperatures of several hundred degrees centigrade and cause serious burns if touched. Additional information follows.

HIGH VOLTAGE

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Many power tubes operate at voltages high enough to kill through electrocution. Personnel should always break the primary circuits of the power supply and discharge high voltage capacitors when direct access to the tube is required.

RADIO FREQUENCY RADIATION

Exposure of personnel to RF radiation should be minimized, personnel should not be permitted in the vicinity of open energized RF generating circuits, or RF transmission systems (waveguides, cables, connectors, etc.), or energized antennas. It is generally accepted that exposure to "high levels" of radiation can result in severe bodily injury including blindness. Cardiac pacemakers may be affected.

The effect of prolonged exposure to "low level" RF radiation continues to be a subject of investigation and controversy. It is generally agreed that prolonged exposure of personnel to RF radiation should be limited to an absolute minimum. It is also generally agreed that exposure should be reduced in working areas where personnel heat load is above normal. A 10 mW/cm² per one tenth hour average level has been adopted by several U.S. Government agencies including the Occupational Safety and Health Administration (OSHA) as the standard protection guide for employee work environments.

RF energy must be contained properly by shielding and transmission lines. All input and output RF connections, such as cables, flanges and gaskets must be RF leakproof. Never operate a power tube without a properly matched RF energy absorbing load attached. Never look into or expose any part of the body to an antenna or open RF generating tube or circuit or RF transmission system while energized. Monitor the tube and RF system for RF radiation leakage at regular intervals and after servicing.

DANGER--BERYLLIUM OXIDE CERAMICS (BeO) - AVOID BREATHING DUST OR FUMES

BeO ceramic material is used as a thermal link to carry heat from a tube or transistor to the heat sink. Do not perform any operation on any BeO ceramic which might produce dust or fumes, such as grinding, grit blasting, or acid cleaning. Beryllium oxide dust or fumes are highly toxic and breathing them can result in serious personal injury or death. BeO ceramics must be disposed of only in a manner prescribed by the device manufacturer.

HOT SURFACES

The anode portion of power tubes is often air-cooled or conduction-cooled. The air-cooled external surface normally operates at a high temperature (up to 200° to 300°C). Other portions of the tube may also reach high temperatures, especially the cathode insulator and the cathode/heater surfaces. All hot surfaces may remain hot for an extended time after the tube is shut off. To prevent serious burns, take care to prevent and avoid any bodily contact with these surfaces both during and for a reasonable cooldown period after tube operation.

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PART II

1. POWER SUPPLY TABLE OF CONTENTS

2. RF CIRCUITRY TABLE OF CONTENTS

3. MICROPROCESSOR CONTROLLER TABLE OF CONTENTS

SCOPE OF MANUAL

THIS MANUAL COMPRISES TWO SECTIONS PROVIDING THE FOLLOWING INFORMATION OF THE BROADCAST ELECTRONICS FM-30 KW FM BROADCAST TRANSMITTER.

- PART I CONTAINS INFORMATION RELATIVE TO Α. INSTALLATION, OPERATION, AND MAINTENANCE APPLICABLE TO THE OVERALL TRANSMITTER.
- PART II CONTAINS DETAILED INFORMATION FOR Β. THE FOLLOWING TRANSMITTER FUNCTIONAL CIRCUITS.

POWER SUPPLIES 1.

2. RF CIRCUITRY

MICROPROCESSOR CONTROLLER —

SECTION I

GENERAL INFORMATION

1-1. INTRODUCTION

Information presented by this section provides a general 1-2. description of the FM-30 FM transmitter and lists equipment specifications.

1-3. RELATED PUBLICATIONS

1-4. The following list of publications provides data for equipment associated with the FM-30 transmitter.

PUBLICATION NUMBER		EQUIPMENT
597-0002	FM-30	FM Exciter
597-0008	FC-30	SCA Generator
597-0009	FS-30	Stereophonic Generator

1-5. EQUIPMENT DESCRIPTION

1-6. The Broadcast Electronics FM-30 is a one tube 30 kW FM Broadcast Transmitter. The transmitter incorporates a folded half wave cavity PA stage, a microprocessor control system, a solid-state IPA, and a solid-state exciter with a digital frequency synthesizer. The transmitter is available in two basic configurations as listed below.

<u>P/N</u>	DESCRIPTION
909-0001	FM-30 Transmitter complete with FX-30 Exciter, $208/240V$ ac, 3 Ø, 60 Hz or 380V ac, 3 Ø, 50 Hz. Power supply cabinet attached.

909-0001-2 Same as 909-0001 less Exciter.

909-0001-1 FM-30 Transmitter complete with FX-30 Exciter, 208/240V ac, 3 Ø, 60 Hz or 380V ac, 3 Ø, 50 Hz. Power supply separate.

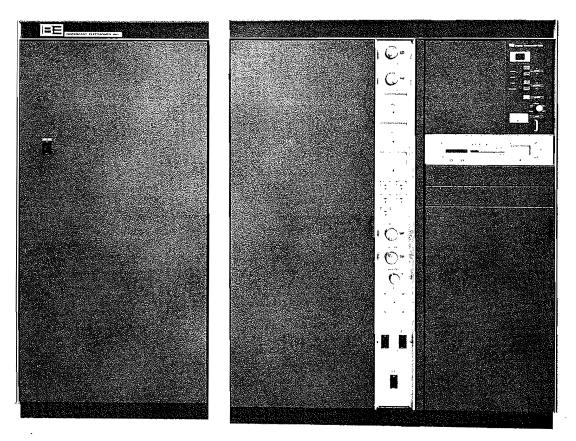
909-0001-3 Same as 909-0001-1 less Exciter.

1-7. PHYSICAL DESCRIPTION

1-8. The Broadcast Electronics FM-30 is a 30 KW FM Transmitter designed for continuous operation in the 87.5 MHz to 108 MHz FM broadcast band. The RF power amplifier, RF driver, FM exciter, and the control circuitry are housed in a single double cubicle cabinet. The high voltage power supply is housed in a separate cabinet which may be remotely located from the cabinets containing the RF circuitry if desired (see Figure 1-1).

1-9. EQUIPMENT SPECIFICATIONS

1-10. Refer to Table 1-1 for electrical specifications or Table 1-2 for physical specifications for the FM-30 FM Transmitter.



597-0003-3

FIGURE 1-1. FM-30 TRANSMITTER

PARAMETER	SPECIFICATION
RF Power Output	15 kW to 30 kW (as ordered)
Automatic Power Control Resolution	±2%
RF Frequency Range	87.5 to 108 MHz (as ordered)
RF Output Impedance	50 Ohms Resistive
RF Output Connector	3 1/8 Inch (7.94 cm) EIA Flange
Tube Complement	8990/4CX20000A (1)
FM Noise	72 dB Below 100% Modulation at 400 Hz, ±75 kHz Deviation
AM Noise	55 dB Below a Reference Carrier AM Modulated 100% at 400 Hz, 75 us Deemphasis
RF Harmonic Suppression	Meets all FCC Requirements and CCIR Recommendations
AC Power Requirements	196 to 252 VRMS, 60 Hz or 50 Hz (as ordered). Three Phase Closed Delta or Wye. 130 Amperes per Phase Maximum at 240V
AC Power Consumption	50 kW Maximum for 30 kW RF Output (Includes Exciter)
Maximum VSWR	1.8 : 1 (Will Operate into Higher VSWR with Automatic Power Reduction)

Table 1-1. Electrical Characteristics

PARAMETER	SPECIFICATION
Ambient Temperature Range	+14°F to +122°F (-10°C to +50°C)
Maximum Altitude	0 to 7,500 Feet Above Sea Level (0 to 2286 Meters)
Maximum Humidity	95%, Non-Condensing
Size: Transmitter (Excluding Power Supply)	Width: 56.6 Inches (143.5 cm) Height: 70 Inches (177.8 cm) Depth: 31.5 Inches (80.0 cm)
Maximum Head Room Required	85.5 Inches (217.17 cm)
High Voltage Power Supply	Width: 34.5 Inches (87.6 cm) Height: 70 Inches (177.8 cm) Depth: 31.5 Inches (80.0 cm)
Weight: Transmitter	1500 Pounds (682 kg) Packed: 1750 Pounds (795 kg)
High Voltage Power Supply	1200 Pounds (545 kg) Packed: 1250 Pounds (568 kg)
Cubage: Transmitter	72 Cubic Feet (2 m ³)
High Voltage Power Supply	44 Cubic Feet (1.25 m ³)
Heat Dissipation (30 kW FM Output): Driver Cabinet	1 kW Maximum
PA Cabinet	18 kW Maximum
Cooling Air Requirements: Driver Cabinet	250 Cubic Feet Per Minute (7.08 m³/min)
PA Cabinet	1250 Cubic Feet Per Minute (35.38 m ³ /min)
Exciter	25 Cubic Feet Per Minute (0.708 m ³ /min)

Table 1-2. Physical Characteristics

DIGIT 1	DIGIT 2	CONTROL STATUS
Unused Unused Unused Unused Unused Unused Unused Unused	1 2 3 4 5 6 7 8 9	Air Interlock Open & Filament Contactor Open AFC Unlocked Air Interlock Open AFC & Air Interlock Open Filament Contactor Open Filament Contactor Open & AFC Unlocked AFC Unlocked, Filament Contactor Open, Air Interlock Open Interlock Open, Door or Auxiliary Exciter Over-Temperature

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Table 1-3. PROCESSOR DISPLAY INDICATIONS

DIGIT 1	DIGIT 2	OVERLOAD STATUS (Overload Lamp On)
0 0 0 1 1 1 2 2 3 5 5 5 5 5 5 5 5	1 2 3 4 2 3 4 2 3 4 2 3 4 2 3 4 5 6	Output VSWR Excessive Plate Current Excessive Screen Current Excessive Dutput VSWR & Plate Current Excessive Output VSWR & Plate Current Excessive Output VSWR & Bias Current Excessive Plate Current & Screen Current Excessive Screen Current & Bias Current Excessive Output VSWR, Plate Current & Screen Current Excessive Output VSWR, Plate Current & Bias Current Excessive Output VSWR, Screen Current & Bias Current Excessive Plate Current, Screen Current & Bias Current Excessive Output VSWR, Plate Current & Bias Current Excessive

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DIGIT 1	DIGIT 2	DIAGNOSTIC INDICATION
0 0 0 0 0 0 0 0 0	1 2 3 4 5 6 7 8 9	PA Power Low PA VSWR High IPA Power Low IPA VSWR High IPA Hybrid Load #3 High IPA Hybrid Load #1 High IPA Hybrid Load #2 High Exciter Power Low Exciter VSWR High
1 1 1 1 1 1 1 1 1 1 1	0 1 2 3 4 5 6 7 8 9	HV Low Low PA Voltage, Low PA Power Low PA Voltage, High VSWR PA Low PA Voltage, IPA Power Low Low PA Voltage, IPA VSWR High Low PA Voltage, IPA Hybrid #3 High Low PA Voltage, IPA Hybrid #1 High Low PA Voltage, IPA Hybrid #2 High Low PA Voltage, Exciter Power Low Low PA Voltage, Exciter VSWR High
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 1 2 3 4 5 6 7 8 9	Bias Voltage Low Bias Voltage Low, PA Power Low Bias Voltage Low, PA VSWR High Bias Voltage Low, IPA Power Low Bias Voltage Low, IPA VSWR High Bias Voltage Low, Hybrid Load #3 High Bias Voltage Low, Hybrid Load #1 High Bias Voltage Low, Hybrid Load #2 High Bias Voltage Low, Exciter Power Low Bias Voltage Low, Exciter VSWR High
3 3 3 3 3 3 3 3 3 3 3 3 3 3	0 1 2 3 4 5 6 7 8 9	IPA Module 1 Voltage Low IPA Module 1 Voltage Low, PA Power Low IPA Module 1 Voltage Low, PA VSWR High IPA Module 1 Voltage Low, IPA Power Low IPA Module 1 Voltage Low, IPA VSWR High IPA Module 1 Voltage Low, IPA Hybrid Load #3 High IPA Module 1 Voltage Low, Hybrid Load #1 High IPA Module 1 Voltage Low, Hybrid Load #2 High IPA Module 1 Voltage Low, Exciter Power Low IPA Module 1 Voltage Low, Exciter VSWR High

DIGIT 1	DIGIT 2	DIAGNOSTIC INDICATION
4 4 4 4 4 4 4 4 4 4	0 1 2 3 4 5 6 7 8 9	IPA Module 5 Voltage Low IPA Module 5 Voltage Low, PA Power Low IPA Module 5 Voltage Low, PA VSWR High IPA Module 5 Voltage Low, IPA Power Low IPA Module 5 Voltage Low, IPA VSWR High IPA Module 5 Voltage Low, IPA Hybrid Load #3 High IPA Module 5 Voltage Low, Hybrid Load #1 High IPA Module 5 Voltage Low, Hybrid Load #2 High IPA Module 5 Voltage Low, Exciter Power Low
4 5 5 5 5 5 5 5 5 5 5 5 5 5	9 0 1 2 3 4 5 6 7 8 9	IPA Module 5 Voltage Low, Exciter VSWR High IPA Module 4 Voltage Low IPA Module 4 Voltage Low, PA Power Low IPA Module 4 Voltage Low, PA VSWR High IPA Module 4 Voltage Low, IPA Power Low IPA Module 4 Voltage Low, IPA VSWR High IPA Module 4 Voltage Low, IPA Hybrid Load #3 High IPA Module 4 Voltage Low, Hybrid Load #1 High IPA Module 4 Voltage Low, Hybrid Load #2 High IPA Module 4 Voltage Low, Exciter Power Low IPA Module 4 Voltage Low, Exciter VSWR High
6 6 6 6 6 6 6 6 6 6	0 1 2 3 4 5 6 7 8 9	IPA Module 3 Voltage Low, Excited Found High IPA Module 3 Voltage Low, PA Power Low IPA Module 3 Voltage Low, PA VSWR High IPA Module 3 Voltage Low, IPA Power Low IPA Module 3 Voltage Low, IPA VSWR High IPA Module 3 Voltage Low, IPA Hybrid Load #3 High IPA Module 3 Voltage Low, Hybrid Load #1 High IPA Module 3 Voltage Low, Hybrid Load #2 High IPA Module 3 Voltage Low, Exciter Power Low IPA Module 3 Voltage Low, Exciter VSWR High

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DIGIT 1	DIGIT 2	DIAGNOSTIC INDICATION
7 7 7 7 7 7 7 7 7 7 7	0 1 2 3 4 5 6 7 8 9	IPA Module 2 Voltage Low IPA Module 2 Voltage Low, PA Power Low IPA Module 2 Voltage Low, PA VSWR High IPA Module 2 Voltage Low, IPA Power Low IPA Module 2 Voltage Low, IPA VSWR High IPA Module 2 Voltage Low, IPA Hybrid Load #3 High IPA Module 2 Voltage Low, Hybrid Load #1 High IPA Module 2 Voltage Low, Hybrid Load #2 High IPA Module 2 Voltage Low, Exciter Power Low IPA Module 2 Voltage Low, Exciter VSWR High
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 1 2 3 4 5 6 7 8 9	40 Volt Supply Low 40 Volt Supply Low, PA Power Low 40 Volt Supply Low, PA VSWR High 40 Volt Supply Low, IPA Power Low 40 Volt Supply Low, IPA VSWR High 40 Volt Supply Low, IPA Hybrid Load #3 High 40 Volt Supply Low, Hybrid Load #1 High 40 Volt Supply Low, Hybrid Load #2 High 40 Volt Supply Low, Exciter Power Low 40 Volt Supply Low, Exciter VSWR High
9 9 9 9 9 9 9 9 9 9 9	0 1 2 3 4 5 6 7 8 9	Screen Voltage Low Screen Voltage Low, PA Power Low Screen Voltage Low, PA VSWR High Screen Voltage Low, IPA Power Low Screen Voltage Low, IPA VSWR High Screen Voltage Low, Hybrid Load #3 High Screen Voltage Low, Hybrid Load #1 High Screen Voltage Low, Exciter Power Low Screen Voltage Low, Exciter VSWR High

SECTION II

INSTALLATION

2–1. INTRODUCTION

2-2. This section contains information required for installation and preliminary checkout of the Broadcast Electronics FM-30 FM Transmitter.

2-3. UNPACKING

2-4. The equipment becomes the property of the customer when the equipment is delivered to the carrier. Carefully unpack the transmitter. Perform a visual inspection to determine that no apparent damage has been incurred during shipment. All shipping materials should be retained until it is determined that the unit has not been damaged. Claims for damaged equipment must be promptly filed with the carrier or the carrier may not accept the claim.

2-5. The contents of the shipment should be as indicated on the packing list (See Table 2-1). If the contents are incomplete, or if the unit is damaged electrically or mechanically, notify both the carrier and Broadcast Electronics, Inc.

2-6. INSTALLATION

2-7. Each transmitter is wired, operated, tested and inspected at the factory prior to shipment and is ready for installation when received. Prior to installation, this publication should be studied to obtain an understanding of the operation circuitry nomenclature, and installation requirements. Installation is accomplished as follows: 1) placement, 2) component installation, 3) remote control connections, 4) wiring, and 5) initial checkout.

2-8. INSTALLATION REQUIREMENTS

2-9. Table 1-2 provides environmental conditions which must be considered prior to transmitter installation.

2-10. COOLING AIR

2-11. If the heated transmitter air is to be ducted from the room, the duct system must not introduce any back-pressure on the equipment. Proper allowances for air flow will ensure that only a limited amount of heat is dissipated into the equipment interior. The duct system must allow for a minimum air flow of 1250 cubic feet of air per minute ($35.38 \text{ m}^3/\text{min}$) from the PA cabinet and 250 cubic feet of air per minute ($7.08 \text{ m}^3/\text{min}$) from the driver cabinet.

2-12. As a minimum requirement, any duct work must have a crosssectional area equal to the exhaust area of the PA cabinet plus the exhaust area of the driver cabinet (refer to Figure 2-1). Sharp bends in the duct system will introduce back pressure and are not permissible. A radius bend must be used if a right angle turn is required. An exhaust fan may be used to overcome duct losses or overcome wind pressures if the duct is vented to the outside.

2-13. PRIMARY POWER

2-14. The FM-30 transmitter is designed for operation from a closeddelta or wye connected three-phase source. Operation from an unsatisfactory power source will void the warranty on this transmitter as any resultant damage is beyond the control of the manufacturer. Before attempting installation of the transmitter, assure that the proper power source is installed. Acceptable power input configurations are shown in Figure 2-2.

2-15. An open-delta, V to V, T to T, T to L, or Scott connected power source will provide unsatisfactory transmitter performance as transients and unstable power can damage components of the FM-30 and provide degraded transmitter specifications. Any of these systems will develop a considerable imbalance between phases in voltage, phase angle, or both voltage and phase angle. These problems can result in premature failure of power supply and RF circuit components.

2-16. It is important that the local electric utility be consulted to ensure that the correct service is provided before connection of the FM-30 transmitter to a primary power source. The proper power source can readily be identified by the use of three transformers or one transformer with three windings instead of the use of two transformers as required for the unacceptable configurations.

2–17. EQUIPMENT PLACEMENT

2-18. Transmitter installation offers two options. The high voltage power supply may be located some distance from the PA and driver cabinets or the power supply can be installed along side the PA cabinet. If the cabinets are positioned apart, access holes in the top and bottom allow either overhead or under floor ducting of interconnecting wiring (see Figure 2-1). The floor must be capable of supporting the total transmitter weight. Also, the floor support should be more than marginal to maintain the proper alignment of the cabinets and reduce vibration.

2-19. After it has been determined how the cabinets will be positioned, set the PA and driver cabinets in place as a single unit on a smooth and level location.

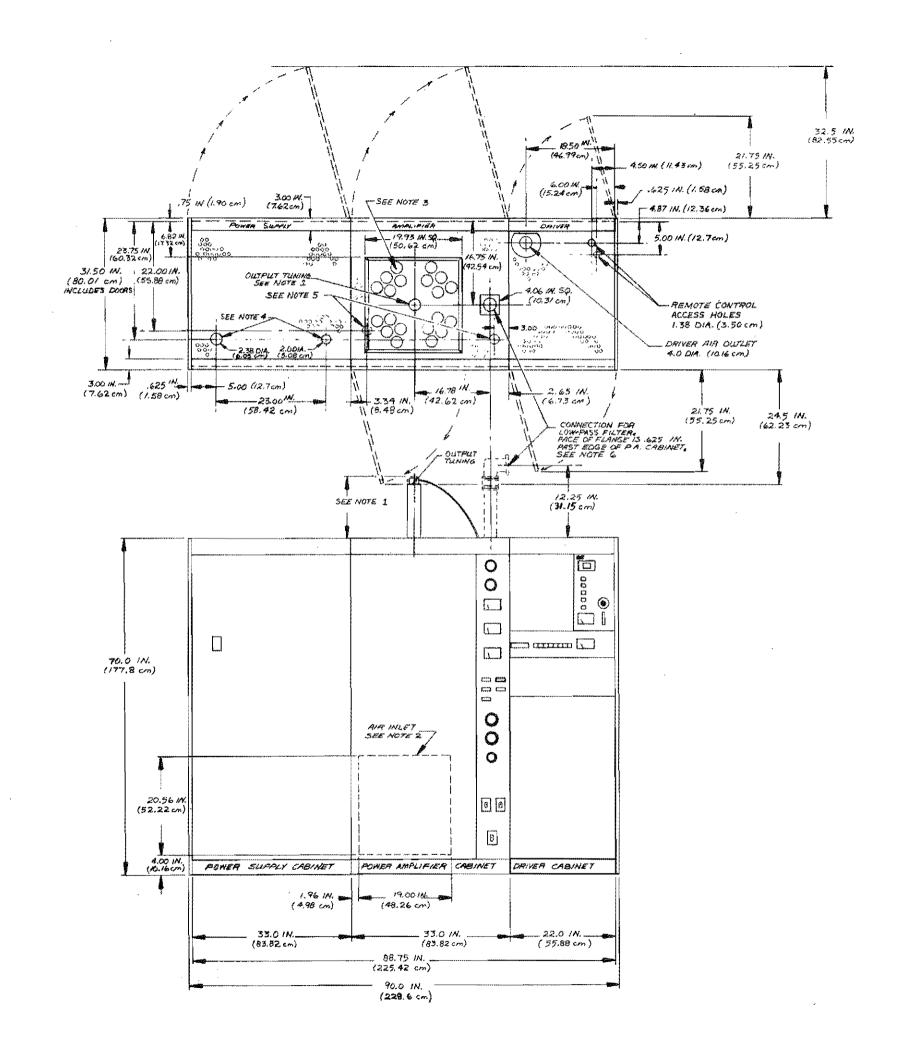
2-20. Remove the rear access door, and the left side panel from the high voltage power supply cabinet. The rear access door simply lifts off hinges. The left side panel is secured by two No. 12 Phillips head screws in the left side rear mounting rail. After the two screws are removed, the side panel lifts up and off the equipment.

ITEM	DESCRIPTION	PART NO.	QTY.	PACKED IN BOX NO.
1	PA CABINET AND DRIVER CABINET (ASSEMBLED)	NPN	1	1
2	HIGH VOLTAGE POWER SUPPLY CABINET (ASSEMBLED)	NPN	1	2
3	PA TUBE, 4CX20,000A/8990	243-0001	1	3
4	PA DIRECTIONAL COUPLER	950-6907	1	4
5	TRANSMISSION LINE ELBOW WITH SAMPLING PORT	427-0016	1	4
6	TRANSMISSION LINE COUPLING FLANGE WITH HARDWARE AND CLAMP	427-0001	1	4
7	TRANSMISSION LINE COUPLING SECTION WITH CLAMP	427-0005	2	4
8	TRANSMISSION LINE INSULATOR	427-0004	1	4
9	STEP START PLUG-IN MODULE (ASSEMBLED)	NPN	1	4
10	RACK CONNECTING SPACERS WITH HARDWARE	476-0006	6	4
11	STRAIN RELIEF (FOR SEPARATE EXCITER AC FEED)	401-0008	1	4
12	RELAY K103	270-1250	1	4
13	RELAY K202	270-0023	1	4
14	MICROPROCESSOR BYPASS ASSEMBLY	959-0053	1	4
15	FM-30 MANUALS	597-0003	2	4
16	SET CONTROL STATUS SHEETS	597-0004	1	4
17	SETS CABINET DOOR KEYS	NPN	3	4
18	FX-30 MANUALS	597-0002	2	4
19	SPARE FUSES AND DIP SWITCHES FOR EXCITER	961-0001	1	4
20	LOW-PASS FILTER	339-0005	1	5

TABLE 2-1. FM-30 PACKING LIST

NOTES - ITEM 10 NOT INCLUDED WHEN POWER SUPPLY CABINET IS TO BE POSITIONED REMOTELY FROM THE PA AND DRIVER CABINETS.

ITEMS 18 AND 19 NOT INCLUDED WHEN SHIPPED LESS EXCITER.



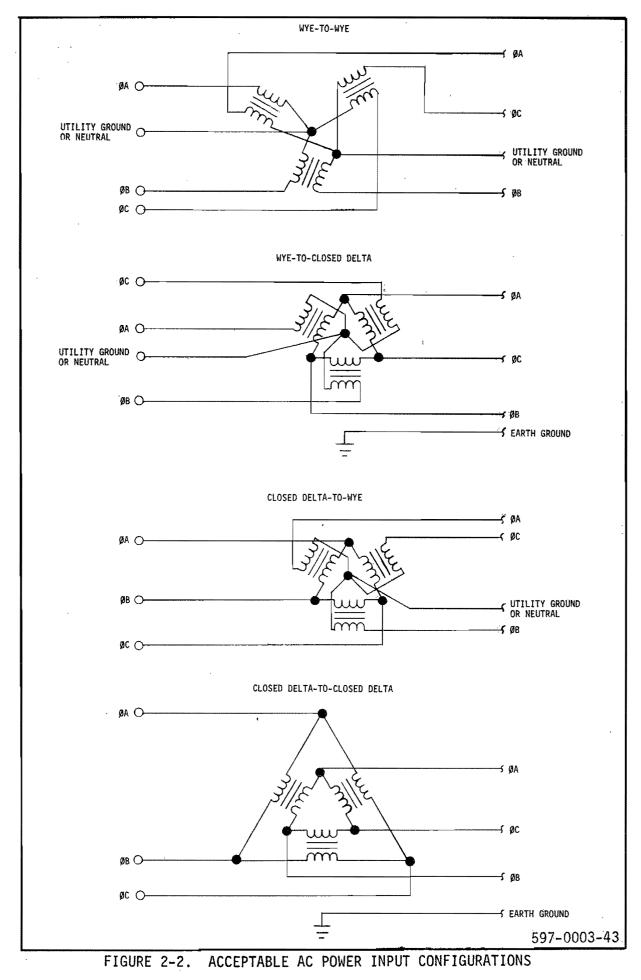
I.) HEIGHT OF OUTPUT TUNING COLUMN IS DETERMINED BY FREQUENCY OF THANSMITTER. MAX. = 15.5 M. (39.37 cm) @ 108 MHz MIN. = 4.5 IN. (11.43 cm) @ 88 MHz APPROX. - . 55 IN. PER MHZ. 2) AIR INLET AT REAR OF CHEMET. 1250 CUBIC FY. OF AIR PER MINUTE. FILTER REQUIRED + 407-1002 3) AIR OLTLET 3.32 DIA. CENTERED IN 20.00 IN. 50. , SURROUNDED BY (20) 2.5 IN. D.A. HOLES. SEE DWG. NO. 5471-0185 FOR FLANGE SCREW DIMENSIONS, 4) TOP ACCESS FOR A.C. INPUTS, BOTTOM ACCESS IS AVAILABLE PROUND THE ENTIRE OUTER PERIMETER OF INSIDE CRBINET. 5) INTER CONNECT CABLE ACCESS HOLES WHEN POWER SUPPLY IS LOCATED REMOTE. 6) LOW-PASS FILTER : 81AD - * 339-0004 LENGTH -60.0 (152. 4 cm) DIAMETER- 6.0 (15.: 4 cm) COMARK-# 339-0005 LENGTH - 104.0 IN. (264.2 cm) DIRMETER - 6, 13 (15.57 cm) OUTPUT ELBON - 3 VE EZA UNFLANGED, 50 0MM (INCLUDES AF SAMPLE PROBE) INPUT JOUTPUT CONNECTION OF LEFF 3 VE EIA FLANGED, 50 0MM 7.) WEIGHT : POWER SUPPLY - 1200 LBS. - 545 KG POWER AMP -1500 LBS.-682 KG RF DRIVER -1500 LBS.-682 KG 8.) POWER SUPPLY MAY BE LOCATED REMOTELY FROM P.A. & DRIVER CABINETS IF CRESIRED. (MUST BE SPECIFIED ON ORIGINAL ORDER.) 9) HEAT DISSIPATION AT 30 KN RE OUTPUT : I KW MAX. FROM DRIVER CABINET 18 KW MAX. FROM P.A. CABINET 10) AIR COOLING REQUIREMENTS : RF AMP CAVITY - 1250 FT. ¥MIN, (35.38 M³/MIN,) RF DRIVER CABINET - 250 FT ¥MIN, (7.08 M¥MIN,)

NOTES :

FIGURE 2-1

FM-30 TRANSMITTER INSTALLATION D905-0002

2-3/2-4



2-21. After the panels are removed from the power supply cabinet, the four bolts securing the high voltage power supply cabinet to the shipping skid must be removed. To remove these bolts, a 9/16 inch (14.3 mm) box-end wrench is required. After the cabinet is unbolted from the skid, the supply may be moved to the final location with a forklift (see Figure 2-3).

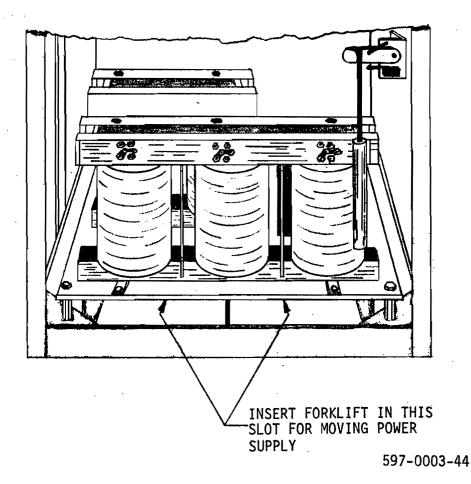


FIGURE 2-3. POWER SUPPLY CABINET MOVING PROVISIONS

2-22. Set the power supply in place. If the location chosen is next to the PA cabinet, the four bolts, one in each corner of the power supply base plate, should be adjusted to align the power supply cabinet with the PA cabinet. A 9/16 inch (14.3 mm) box-end wrench is required. Extreme care should be observed if trim alignment is a prime consideration.

2-19. COMPONENT INSTALLATION



ENSURE NO PRIMARY POWER IS CONNECTED BEFORE PROCEEDING.

2-20. To facilitate component installation and wiring, the rear door of the driver cabinet, the front and rear doors and the lower front access panel of the PA cabinet, and the power supply cabinet rear door should be removed and left off until installation is complete.

2-21. Interconnecting wires and cables are tied in for shipment. Remove all tape, wire ties, string, and packing material used for shipment.

2-22. Cables, connectors, and miscellaneous components to be installed are shipped in separate cartons. The following text provides information concerning the installation of these items. Ensure adjustments are not moved from their factory preset positions.

2-23. HIGH VOLTAGE POWER SUPPLY. Remove the tie wraps securing the two resistors mounted in clips.

2-24. Unwrap the grounding stick and place the stick on its interlocked hanger. Store the cable on top of the plate transformer.

2-25. Locate the plug-in step-start timer (A300). Plug the device into socket XA300 on the step-start relay panel.

2-26. Unwrap the interlock connector (if the cabinets are to be positioned together) or the interlock cable (if the cabinets are to be positioned apart).

2-27. If the cabinets are to be positioned apart, route the interlock cable to the approximate position of the PA cabinet.

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2-28. Route the ac power cables coiled along side the high voltage power supply cabinet to the general location of the PA cabinet. Ensure the cables are routed away from the plate transformer within the cabinet. These cables will be cut to length and connected inside the PA cabinet. Do not store extra cable by pushing the cable back within the high voltage power supply cabinet.

2-29. DRIVER CABINET. Install the 110 volt ac control relay (K103) in socket XK103. Operate the associated OVERRIDE/NORMAL switch to OVER-RIDE.

2-30. Remove the retainers from the microprocessor controller and exciter slides.

2-31. Install the FM exciter on its slides and connect the transmitter wiring to the exciter. Wiring data is provided by Figure 2-4.

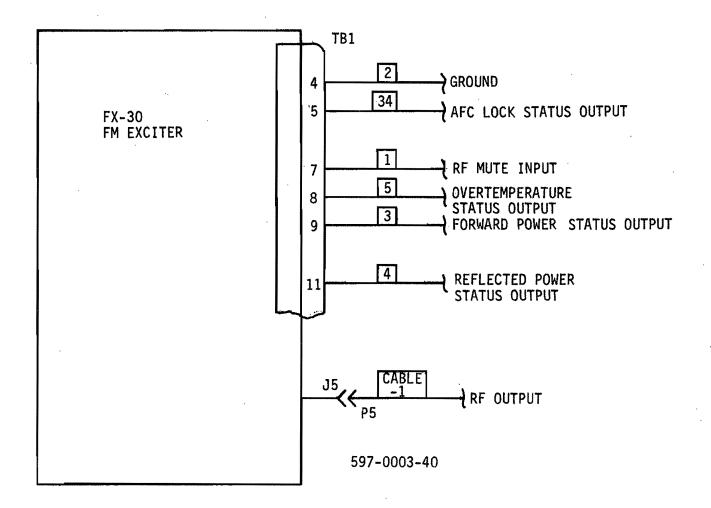


FIGURE 2-4. EXCITER WIRING

2-32. Connect P1 to J1, P2 to J2, and P3 to J3 on the rear of the microprocessor controller.

2-33. Connect the exciter, stereo generator, SCA generator and microprocessor controller power supply switched ac outlets in the cabinet rear (bottom four outlets only).

2-34. Operate the LOCAL/REMOTE switch to LOCAL, the FWD/VSWR/VSWR CAL switch to FWD, and the MAN/AUTO switch to MAN.

2-35. PA CABINET. From the top of the PA cabinet, readjust the moveable portion of plate line so that the line scribed around the tubing aligns with the top of the plate line clamping flange. A flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip is required to secure the strap clamp to the transmission line clamping flange.

2-36. Remove the top from the PA cabinet. A No. 2 Phillips screwdriver is required. Retain all hardware.

2-37. Remove the hardware and semi-circular PA output line clamp. A 3/8 inch (9.53 mm) box-end wrench is required (see Figure 2-5).

2-38. Insert the transmission line inner conductor from the top, down onto the bullet connector in the transmission line coupler until the inner conductor is fully seated.

2-39. Insert the transmission line outer conductor from the top, down into the transmission line coupler until the outer conductor is seated. The FWD sampling port must be oriented downwards and towards the front. The cables associated with the directional coupler will be connected later.

2-40. Secure the top strap clamp on the transmission line coupler using a flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip.

2-41. Replace the top on the transmitter. A No. 2 Phillips screwdriver is required.

2-42. Assemble the elbow with the monitor jack and the elbow inner conductor to two transmission line couplers, one on each end of the elbow. Ensure all parts of the assembly are fully seated and secure the assembly together with strap clamps using a flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip.

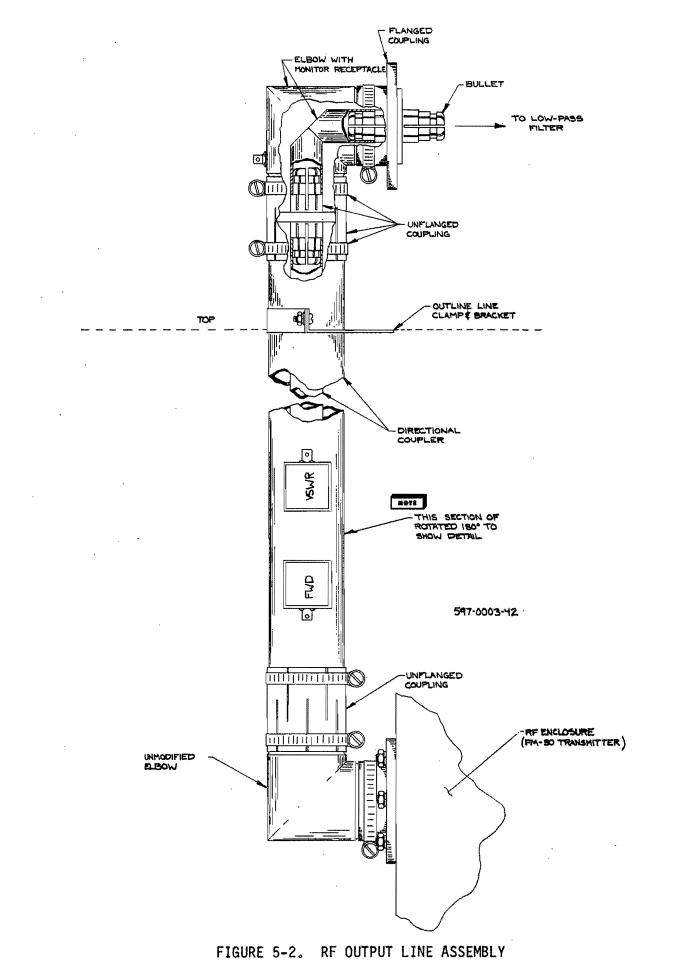
2-43. Insert a bullet connector and insulator into the 3 1/8 inch (7.94 cm) flange.

2-44. Determine if the monitor jack will be positioned horizontally or vertically, then secure the flange into the proper end of the elbow assembly. When the elbow assembly and flange are fully seated, secure the strap clamp using a flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip.

2-45. Mount the assembly on top of the transmission line. When the assembly is fully seated, orient the elbow as desired and secure the elbow strap clamp using a flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip.

CAUTION

NEITHER THE TRANSMITTER OR THE TRANSMISSION LINE WILL SUPPORT THE WEIGHT OF THE LOW-PASS FILTER. ADDITIONAL SUPPORT MUST BE PROVIDED.



2-10

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2-46. Connect the low-pass filter directly at the transmitter between the transmitter and the transmission line. Two 9/16 inch (14.3 cm) open/ box end combination wrenches are required. Each flange secures with six bolts, six lock washers, and six nuts. Both the input and output connections are marked on the filter.

2-47. Open the PA cavity access door, raise the fixed portion of plate line, and remove all packing.

2-48. Carefully install the PA tube with a steady downward pressure. Do not rotate or rock the tube during installation or the tube socket may be damaged.

2-49. After the PA tube is fully seated, lower the fixed portion of plate line over the PA tube. Slowly squeeze the fixed portion of plate line down onto the tube using the palms of both hands and finger tips under the tube cooling fins.

2-50. Ensure the plate choke on the right side of the fixed portion of the plate line is expanded so that the coils do not touch. The choke should not be stressed but must be centered in the deck cutout.

2-51. If the transmitter will operate at 92 MHz or below, loosen the clamp on the plate line extension (see Figure 2-6). Position the extension at the scribed line and secure the strap clamp using a flat-tip screwdriver with a four-inch (10.16 cm) blade and a 1/4 inch (0.635 cm) tip.

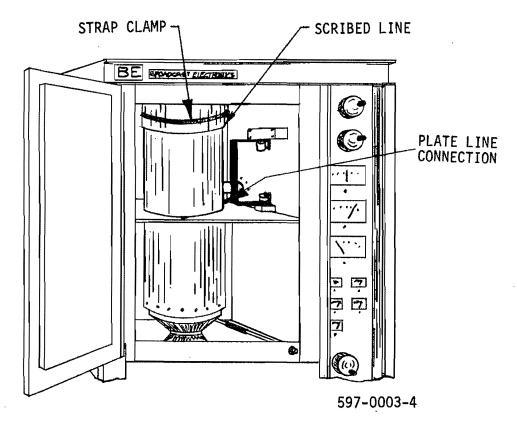


FIGURE 2-6. PLATE LINE EXTENSION

2-52. Align the plate line connections and connect the plate choke to the plate line (see Figure 2-6).

2-53. The two coaxial cables shipped with the section of transmission line mounting the directional coupler sampling ports connects to the auto power control unit adjacent to the sampling ports as follows:

CABLE NO.	FROM-OUTPUT TRANSMISSION LINE	TO-AUTO POWER CONTROL UNIT
21 (longer)	VSWR port	J1 REFL PWR INPUT
22 (shorter)	FWD port	J2 FWD PWR INPUT

2-54. Ensure the second harmonic suppressor on the rear of the PA cabinet is adjusted to the factory preset line scribed on the adjustment rod. A 5/64 inch (1.98 mm) Allen wrench is required for adjustment.

2-55. EXTENDED LOCAL CONTROL

2-56. Extended local control to the FM-30 transmitter is possible up to a maximum of 100 feet (30.48 mm) from the transmitter using the Broadcast Electronics 909-0103 master extended local control unit. A second local control unit which functions as a slave is also available (BE P/N 909-0104).

2-57. REMOTE CONTROL

2-58. Basic features including PA plate current metering, PA plate voltage metering, PA power output metering, screen voltage raise/lower control, and control of on/off functions are available as individually wired remote features when the transmitter LOCAL/REMOTE switch is set to REMOTE (see Figure 2-7). The transmitter will interface with most modern remote control units such as the Moseley Associates, Inc. Model MRC-1 remote control unit.

2-59. WIRING

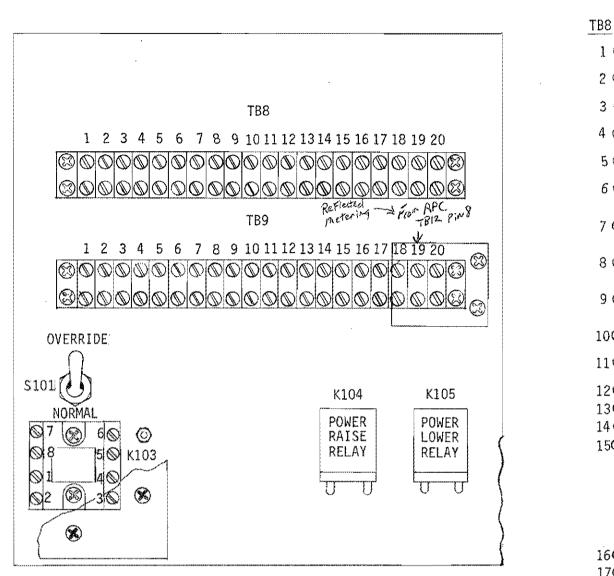


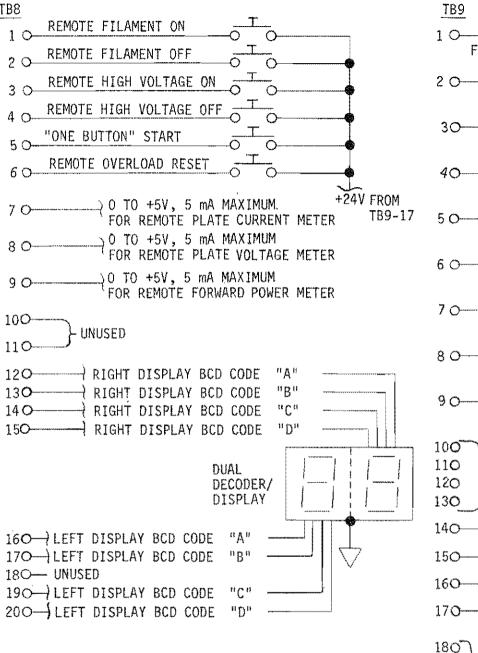
ENSURE PRIMARY POWER IS OFF BEFORE PROCEEDING

2-60. TRANSFORMER TAPS. Ensure all transmitter transformer input taps are wired for the input voltage to be used. The PA plate transformer, PA filament transformer, PA bias transformer, and the IPA power transformer must be checked and changed if required (see Figure 2-8). The PA screen transformer is also tapped, however the wiring should not be changed from the factory installed configuration. The variable transformer connected in the primary circuit allows adequate adjustment for all input potentials. The PA screen transformer wiring is shown for reference only.

2-61. CABINET INTERCONNECTIONS. Cabinet interconnecting wiring for cabinets placed adjacent to each other is shown in Figure 2-9. Connect the wires as follows. If the cabinets are positioned apart, refer to paragraph 2-62.

A. Connect wires 48, 49, 50, 51, 52, 101, and 53 to terminal board TB5 in the front of the PA cabinet.





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FAILSAFE	OR REP	AOTE INT	ERLOCK	CONNECTION
	(JUMPI	ER IF NO	T USED)	

- \rightarrow +4.5V, 4.5 mA MAXIMUM FOR REMOTE OVERLOAD INDICATOR
- INDICATOR
- 6 -+++.5V, 4.5 mA MAXIMUM FOR REMOTE FILAMENT STATUS INDICATOR
- 7 0 +4.5V, 4.5 mA MAXIMUM FOR REMOTE INTERLOCK STATUS INDICATOR
 - _)+4.5V, 4.5 mA_MAXIMUM FOR REMOTE HIGH VOLTAGE INDICATOR
 - +4.5V, 4.5 mA MAXIMUM FOR REMOTE BLOWER INDICATOR

≻UNUSED

GROUND

150-APPLY +24V TO RAISE POWER

160-APPLY +24V TO LOWER POWER

170-+24V SOURCE

USED INTERNALLY IN FM-30 FOR 120 VAC CONNECTIONS TO POWER RAISE AND POWER LOWER RELAY CONTACTS

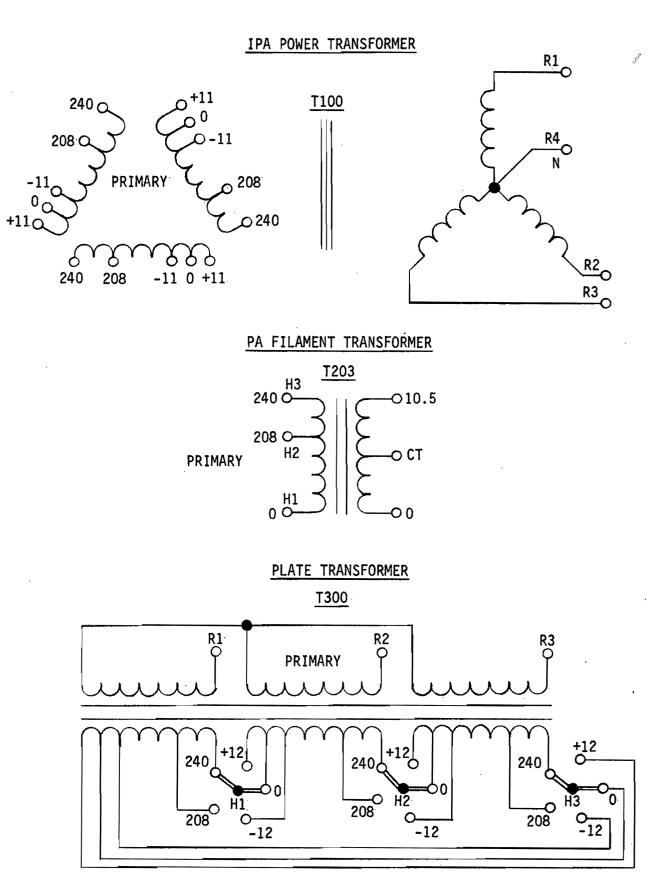
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FIGURE 2-7. REMOTE WIRING

2-13/2-14

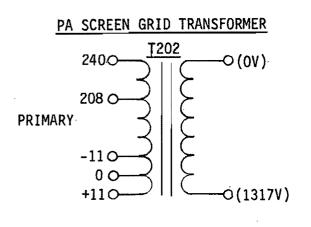
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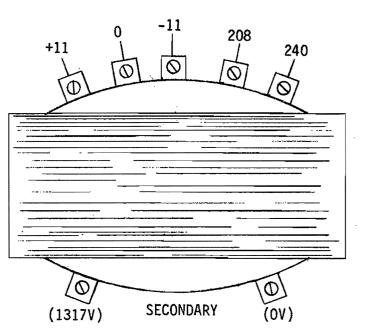


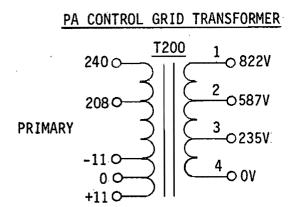
⁵⁹⁷⁻⁰⁰⁰³⁻¹⁴A

FIGURE 2-8. POWER TRANSFORMER WIRING (SHEET 1 of 2)

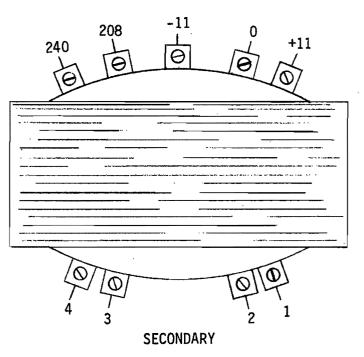
PRIMARY







PRIMARY



597-0003-14B

FIGURE 2-8. POWER TRANSFORMER WIRING (SHEET 2 of 2)

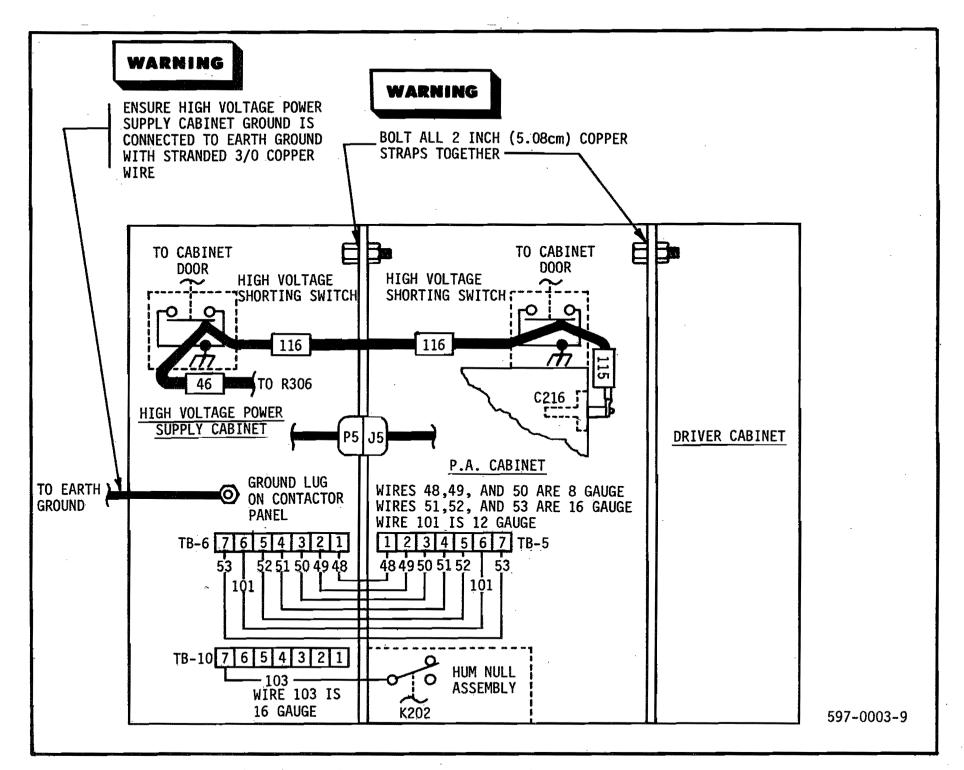


FIGURE 2-9. INTERCONNECTING WIRING, CABINETS POSITIONED TOGETHER

- B. Connect wire 103 to terminal board TB10 behind the high voltage power supply cabinet front panel.
- C. Connect P5 to J5 between the PA and high voltage power supply cabinets.
- D. Connect high voltage wire 116 to the same point in the high voltage cabinets shorting switch assembly where wire 46 connects.
- E. Connect wire 103 to terminal board TB10 on the high voltage power supply contactor panel.



ENSURE ALL GROUNDS IN THE FOLLOWING STEP ARE SECURELY CONNECTED.

F. Bolt each copper ground strap in the top of each adjoining cabinet together securely.

2-62. If the high voltage power supply cabinet is located remotely from the PA and driver cabinets, the following wiring must be completed (see Figure 2-10). If the cabinets are positioned together, refer to paragraph 2-61.

- A. Connect wires 48, 49, 50, 51, 52, 101, and 53 to terminal board TB5 in the front of the PA cabinet.
- B. Connect wire 103 to terminal board TB10 on the high voltage power supply contactor panel.

C. An interlock extension cable is shipped with one end unterminated to allow the cable to be pulled through conduit. A connector shipped with the transmitter cables must be soldered onto the unterminated end as follows before connection.

WIRE NO.	COLOR	PIN NO.	SIGNAL
1	Black	1	High Voltage "E" Sample to Microprocessor Controller
2	Red	2	Door Interlock (N.O. Contact)
3	White	3	Plate Current Meter Sample
4	Green	4	Ground Stick Interlock (N.O. Contact)
. 5	Orange	5	High Voltage "I" Sample to Microprocessor Controller
105	Blue	6	Plate Current Meter Sample
	Brown	7	Spare
	Yellow	8	Spare

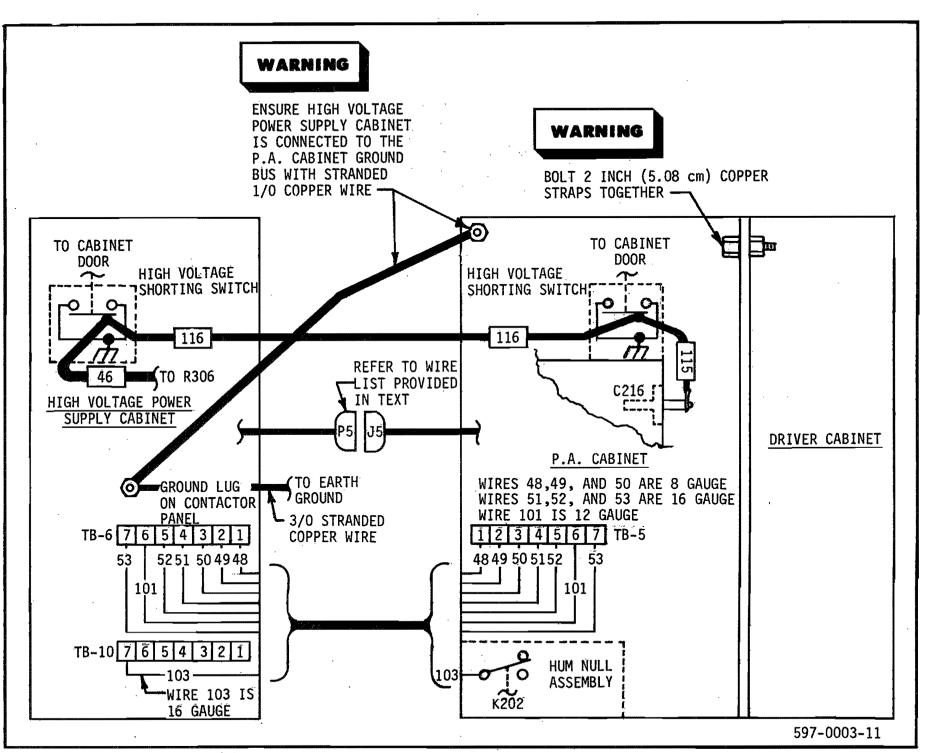


FIGURE 2-10. INTERCONNECTING WIRING, CABINETS POITIONED APART

2-19

WARNING

THE WIRE IN THE FOLLOWING STEP MUST NOT BE BROKEN OR SPLICED. THIS WIRE MUST REMAIN IN ONE UNBROKEN LENGTH, REGARDLESS OF THE DISTANCE INVOLVED.

D. Connect high voltage wire 116 to the same point in the high voltage cabinet shorting switch assembly where wire 46 connects.



ENSURE ALL GROUNDS IN THE FOLLOWING STEPS ARE SECURELY CONNECTED.

- E. Bolt the copper ground strap along the top of the PA and driver cabinets together securely.
- F. Connect a No. 1 stranded bare copper wire from the copper ground strap along the top of the PA cabinet to the ground lug on the high voltage power supply contactor panel.

2-63. GROUND. A common ground conductor must connect to the ground lug on the high voltage power supply contactor panel. This ground must be securely connected to the station common earth ground by the most direct route with No. 3/0 stranded copper wire (see Figures 2-11 and 2-9 or 2-10).

2-64. SIGNAL INPUTS. Refer to the applicable technical manual for the exciter, stereo generator, and SCA generator and wire the inputs and control connections to each unit.

2-65. EXTERNAL INTERLOCK. If an external interlock is required such as for a test load, remove the jumper between terminal TB9-1 and terminal TB9-2 in the driver cabinet. Connect a normally closed interlock switch across these terminals. This interlock must be electrically isolated from ground, any ac, or any dc potentials. The maximum potential on this circuit is 5 V dc. If a fail safe connection is required, it must be connected in series with the remote interlock.



ENSURE PRIMARY POWER IS OFF BEFORE PROCEEDING.

2-66. AC POWER CONNECTIONS. A source of three-phase ac of 196 to 252 Vac, 60 Hz at 200 Amperes-per-phase from an approved power source is required for transmitter operation. It is strongly suggested that each power source be connected to the transmitter through a fused power disconnect (see Figure 2-11).



ENSURE PRIMARY POWER IS OFF BEFORE PROCEEDING.

2-67. <u>Three-Phase Power</u>. Connect the three-phase ac power source to the ac power distribution panel behind the front panel of the high voltage power supply through a fused service disconnect as shown by Figure 2-11.

2-68. INITIAL CHECKOUT

5 min 5 -

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ENSURE PRIMARY POWER IS OFF BEFORE PROCEEDING.

2-69. Replace all panels and doors on the transmitter with the exception of the PA cabinet lower front access panel. This panel must remain off.

2-70. Ensure an RF load is connected to the transmitter.

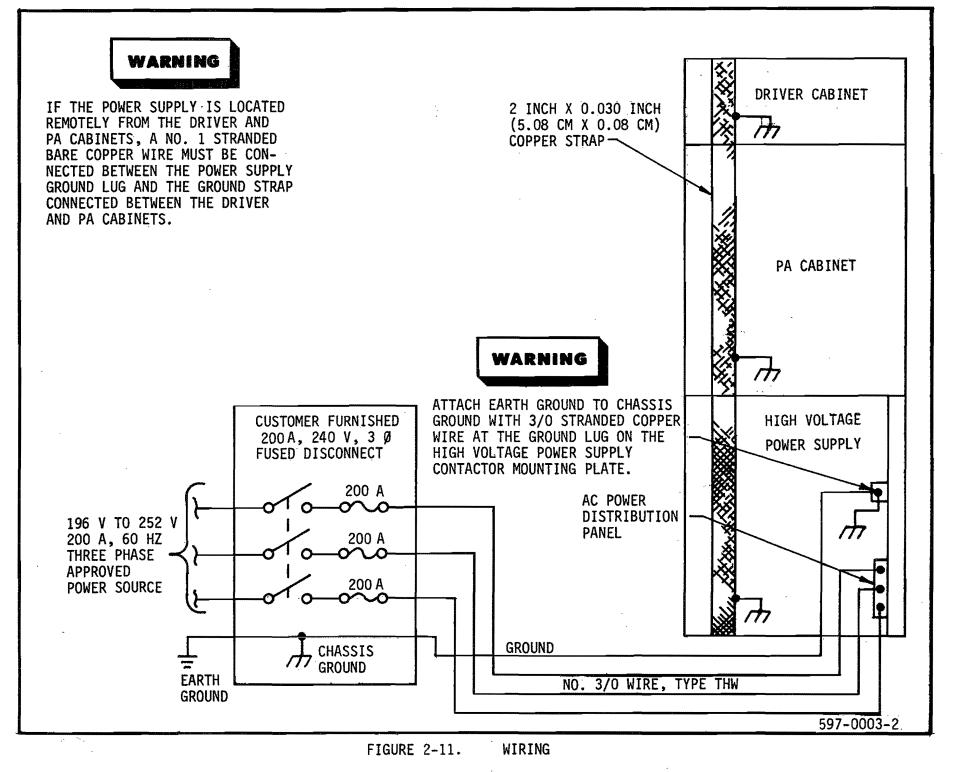
2-71. Adjust the FILAMENT VOLTAGE and SCREEN VOLTAGE controls fully counterclockwise (minimum).

2-72. Ensure that the equipment is completely installed and the station monitors are connected to the RF sample port in the transmission line. Check the following:

- A. Ensure primary power is correctly wired.
- B. Ensure all capacitors on the high voltage rectifier stacks are perpendicular to each respective stack.
- C. Ensure all RF connections are secure.
- D. Ensure all connections at terminal boards are secure, especially in high current areas.
- E. Ensure all ground connections and that chassis ground is properly connected to earth ground.
- F. Rotate the blower by hand to ensure no obstructions are present.
- G. Using an insulator, check relay operation manually to be certain all have free movement.

2-73. Remove any extra hardware and wire lying within the cabinets and close all doors.

2-74. The following procedure will refer to the factory final test data sheets supplied with the transmitter. Some differences in the actual operation may be noted due to differences in primary power or antenna systems. Ensure all controls are preset to the positions indicated on the final test data sheets before proceeding.



2-22

2-75. Refer to Section II of the exciter publication and complete the steps under PRELIMINARY INSTALLATION.

2-76. Operate the exciter POWER switch to ON.

2-77. Reconnect the wire removed from the center battery in the microprocessor controller battery pack in the driver cabinet.

2-78. Depress the FILAMENT OFF and HIGH VOLTAGE OFF switches.

2-79. Operate the HIGH VOLTAGE PRIMARY circuit breaker to OFF. Operate the PRIMARY POWER, FILAMENT, SCREEN, and POWER SUPPLY circuit breakers to ON.

2-80. Open the driver cabinet rear door. Connect a temporary jumper wire from TB1 terminal 5 (AFC) of the exciter to ground. Close the driver cabinet rear door.

2-81. INTERLOCK CHECKOUT. Replace the PA cabinet lower front access panel. The microprocessor controller digital readout will indicate $\boxed{1}$. If not, deenergize all power and ensure all interlocks are closed (including the remote interlock across TB9-1 and TB9-2 in the driver cabinet).

2-82. Complete the following steps, one at a time and note the microprocessor controller digital read-out indication. If difficulties are encountered, deenergize all power and troubleshoot the series interlock string with ohmmeter checks.

NOTE

THE MAXIMUM POTENTIAL ON THE INTERLOCK STRING IS FIVE VOLTS DC TO GROUND.

2-83. Open the driver cabinet rear door. The digital read-out will indicate $\boxed{18}$. Close the driver cabinet rear door. The digital read-out will indicate $\boxed{11}$.

2-84. Open the PA cavity front access door. The digital read-out will indicate $\boxed{18}$. Close the PA cavity front access door. The digital read-out will indicate $\boxed{11}$.

2-85. Open the PA cabinet rear door. The digital read-out will indicate $\boxed{8}$. Depress the PA cabinet rear door interlock. The digital read-out will indicate $\boxed{1}$.

2-86. Continue to depress the PA cabinet rear door interlock and raise the grounding hook from its hanger. The digital read-out will indicate $\boxed{18}$. Replace the grounding hook on its hanger and close the PA cabinet rear door.

2-87. Open the high voltage power supply cabinet rear door. Depress the high voltage shorting switch actuator. The digital read-out will indicate $\boxed{18}$.

2-88. Continue to depress the high voltage power supply cabinet high voltage shorting switch actuator and depress the door interlock. The digital read-out will indicate 11.

2-89. Depress the high voltage power supply cabinet door interlock and release the high voltage shorting switch actuator. The digital readout will indicate [8].

2-90. Depress both the high voltage power supply cabinet door interlock and the high voltage shorting switch interlock and raise the grounding hook from its hanger. The digital read-out will indicate [18].

2-91. Release all interlocks, replace the grounding hook on its hanger, and close the high voltage power supply cabinet rear door. The digital read-out will indicate 11.

2-92. Open the remote interlock. The digital read-out will indicate [8].

2-93. Close the remote interlock. The digital read-out will indicate 1.

2-93A. Open the driver cabinet rear door. Disconnect the jumper wire from TB-1 terminal 5 of the exciter to ground. Close the driver cabinet rear door.

2-94. Close the three phase primary service disconnect to apply power to the transmitter. The INTERLOCK status indicator will illuminate.

2-95. EXCITER CHECKOUT. The presence of the audio programming applied to the exciter will be noted on the exciter digital MODULATION meter and the exciter front panel AFC and POWER indicators will be illuminated.

2-96. Depress the exciter multimeter +20 switch.

A. The exciter multimeter should indicate +20 volts ±2 volts.

2-97. Depress the exciter multimeter -20 switch.

A. The exciter multimeter should indicate -20 volts ± 2 volts.

2-98. Depress the exciter multimeter +5 switch.

A. The exciter multimeter should indicate +5 volts ±0.5 volts.

2-99. Depress the exciter multimeter AFC switch.

A. The exciter multimeter should indicate a potential within the range of +2.5 volts to +13.5 volts, dependent upon carrier frequency. The correct voltage is noted on the final test data sheets accompanying the exciter.



ENSURE PRIMARY POWER IS OFF BEFORE PROCEEDING.

2-100. Open the three phase primary service disconnect.

2-101. Open the driver cabinet rear door and operate the OVERRIDE/ NORMAL switch to NORMAL. Close the driver cabinet rear door. The microprocessor digital readout will indicate [2]. 2-102. BLOWER PHASING. Blower rotation must be visually checked prior to transmitter operation and the blower motor wiring changed if blower rotation is incorrect.

NOTE

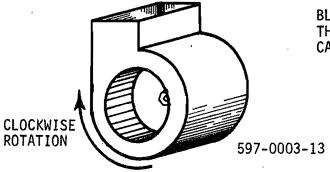
IF THE TRANSMITTER IS EQUIPPED WITH OPTIONAL UNDER-VOLTAGE AND LOSS-OF-PHASE PROTECTION, POWER WILL NOT BE APPLIED TO THE TRANSMITTER CIRCUITRY UNTIL 12 SECONDS AFTER THE MONITOR SENSES THE CORRECT PHASE SEQUENCE. THE TRIP INDICATOR WILL ILLUMINATE TO IN-DICATE INCORRECT PHASING AND GO OUT TO INDICATE PROPER PHASING.

2-103. Remove the blower filter from the PA cabinet rear door.

2-104. Close the three-phase fused ac disconnect.

2-105. Momentarily depress FILAMENT ON. Then depress FILAMENT OFF. The blower will begin operation. Fifteen seconds later the blower will deenergize.

2-106. As the blower slows to a near stop, the direction of rotation can be noted through the PA cabinet air filter grill. Proper rotation is shown by Figure 2-12.



BLOWER AS VIEWED FROM THE REAR OF THE PA CABINET

FIGURE 2-12. BLOWER ROTATION

2-107. If blower rotation is counterclockwise as viewed from the rear of the transmitter through the air filter grill, it will be necessary to change the three-phase primary ac wiring to the transmitter as follows:



ENSURE THE THREE-PHASE AC DISCONNECT IS OPEN BEFORE ATTEMPTING THE FOLLOWING WIRING CHANGES.

- A. Open the three-phase primary ac disconnect.
- B. Interchange any two of the three-phase primary ac wires to the transmitter.

2-108. Replace the blower air filter.

2-109. TUNING PROCEDURE. Close the three-phase primary ac power disconnect if opened.

2-110. Operate the HIGH VOLTAGE PRIMARY circuit breaker to ON.

2-111. Pull the exciter forward on its slides out of the rack until the RF power adjustment control (R3) access hole is visible on the top left of the exciter. Adjust the control fully counterclockwise (minimum RF power output).

CAUTION

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ASSURE AN RF LOAD IS CONNECTED TO THE TRANS-MITTER AND THE FILAMENT VOLTAGE CONTROL IS FULLY COUNTERCLOCKWISE AND THE SCREEN VOLTAGE CONTROL FULLY COUNTERCLOCKWISE.

2-112. Depress the FILAMENT ON switch/indicator. Both the FILAMENT ON switch/indicator and the FILAMENT status indicator will illuminate and the blower will begin operation.

2-113. Adjust the FILAMENT VOLTAGE control to obtain a FILAMENT VOLTAGE meter indication of 10.0 volts ± 0.5 volts or as indicated on the final test data sheets accompanying the transmitter.

2-114. Note the presence of PA stage grid bias on the GRID VOLTAGE meter (approximately -180 volts to -200 volts).

2-115. Depress all five IPA power supply circuit breakers on the driver cabinet so that the breakers latch in the "in" position.

2-116. Operate the MODULE VOLTAGE meter switch through all five positions. A potential of approximately 27.5V dc should be noted on the associated MODULE VOLTAGE meter for each switch position.

2-117. Depress the HIGH VOLTAGE ON switch/indicator. Both the HIGH VOLTAGE ON switch indicator and the HIGH VOLTAGE status indicator will illuminate.

2-118. Note the presence of PA plate voltage on the P.A. VOLTAGE meter.

2-119. Adjust the PA SCREEN control to obtain an indication of 100 volts on the SCREEN VOLTAGE meter.

2-120. Operate the DRIVER meter switch to POWER.

2-121. Adjust the exciter RF power adjustment control (R3) clockwise until an indication of approximately 100% is noted on the DRIVER meter.



IF THE EXCITER HAS BEEN REMOTED AND ADDITIONAL RG-58 CABLE HAS BEEN ADDED BETWEEN THE EXCITER AND THE IPA STAGE INPUT, COMPLETE THE FOLLOWING STEPS:

- A. DEPRESS THE EXCITER RFL SWITCH.
- B. ALTERNATELY, ADJUST ONLY THE IPA STAGE MODULE 1 BASE TUNING AND INPUT LOADING CONTROLS TO MINIMIZE THE EXCITER REFLECTED POWER INDICATION. AN INSULATED ADJUSTMENT TOOL SUCH AS SHIPPED WITH THE FX-30 EXCITER (P/N 710-0001) WILL ASSIST ADJUSTMENT.

2-122. Operate the DRIVER meter switch to VSWR.

2-123. Adjust the PA INPUT TUNING stage and INPUT LOADING controls to obtain a minimum indication on the DRIVER meter. Readjust these controls until a true minimum is obtained.

2-124. Adjust the SCREEN VOLTAGE control to obtain a SCREEN VOLTAGE meter indication of 50% of the value listed on the final test data sheets.

2-125. Adjust the P.A. OUTPUT TUNING control to obtain maximum RF output as indicated by the POWER OUT meter. With 100% RF drive applied, 55% to 80% of RF power should be indicated by the POWER OUT meter.

2-126. Adjust the INPUT TUNING and INPUT LOADING controls to obtain a minimum indication on the DRIVER meter.

2-127. Adjust the SCREEN VOLTAGE control to obtain a SCREEN VOLTAGE meter indication of the value listed on the final test data sheets.

2-128. Compare the plate current, screen current, and the other PA stage metered functions against the indications recorded on the factory final test data sheets.

CAUTION

DO NOT EXCESSIVELY UNLOAD THE PA TANK CIRCUIT IN THE FOLLOWING STEP.

2-129. Adjust the PA stage for the most efficient operation with the P.A. OUTPUT TUNING and P.A. OUTPUT LOADING controls.

2-130. Check all current and voltage indications for the IPA RF modules. All voltages should indicate 27.5 volts +0.5 V, -1.0 volts. The current indication of modules 2, 3, 4, and 5 should be within one ampere of each other (refer to the factory final test data sheets). The driver module (No. 1) however, will indicate somewhat less current than the others as the power output requirement of this amplifier is lower.

2-131. Check the power present in reject loads 1, 2, and 3 to ensure the driver balance is correct (refer to the factory final test data sheets). A slightly better balance and current match may possibly be obtained by a slight readjustment of the PA stage INPUT TUNING and/or INPUT LOADING controls.

SECTION III OPERATION

3-1. INTRODUCTION

3-2. This section identifies all controls and indicators associated with the FM-30 FM transmitter and provides standard operating procedures.

3-3. CONTROLS AND INDICATORS

3-4. Refer to Figures 3-1 and 3-2, and 3-3 for the location of all controls and indicators associated with normal operation of the FM-30 transmitter. The function of each control or indicator is described by the associated table.

3-5. OPERATION

NOTE

THE FOLLOWING PROCEDURE IS PRESENTED UNDER THE ASSUMPTION THAT THE TRANSMITTER IS FULLY IN-STALLED AND IS FREE OF ANY DISCREPANCIES.

3-6. TURN ON

3-7. Operate the LOCAL/REMOTE switch to LOCAL.

3-8. Operate the HIGH VOLTAGE PRIMARY circuit breaker on the high voltage power supply to ON.

3-9. Depress the FILAMENT ON switch/indicator, then depress the HIGH VOLTAGE ON switch/indicator.

3-10. If all interlocks are closed, the transmitter will be operational after ten seconds for PA tube filament warm-up.

3-11. Check and log all meter indications and the status of the various indicators to assure proper equipment operation. Sample log sheets are provided as Tables 3-4 and 3-5.

3-12. If remote operation is desired, operate the LOCAL/REMOTE switch to REMOTE. This will enable both local and remote operation.

3-13. When the LOCAL/REMOTE switch is set to LOCAL, transmitter power may be adjusted manually with the SCREEN VOLTAGE control or automatically with the automatic power control system. Power adjustment when the AUTO/MAN switch is set to AUTO is accomplished by operating the RAISE/LOWER switch, thereby varying the internal automatic power control set point at a slow rate.

3-14. When the LOCAL/REMOTE switch is set to REMOTE, the power can be adjusted only from the remote power control contacts (TB9-15 and 16). When the AUTO/MAN switch is set to MAN, the remote contacts directly control the variable screen transformer control motor. When the AUTO/MAN switch is set to AUTO, the remote contacts vary the internal automatic power control system set point which will also adjust power, but at a much slower rate.

3-15. TURN OFF

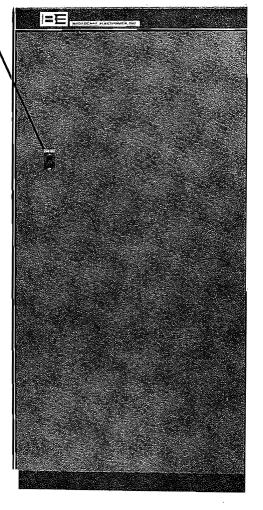
3-16. Depress the FILAMENT OFF switch.

3-17. After a period of blower operation to allow the PA tube to cool, the equipment will deenergize.

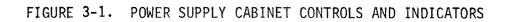
3-18. Operate the HIGH VOLTAGE PRIMARY circuit breaker on the high voltage power supply to OFF.

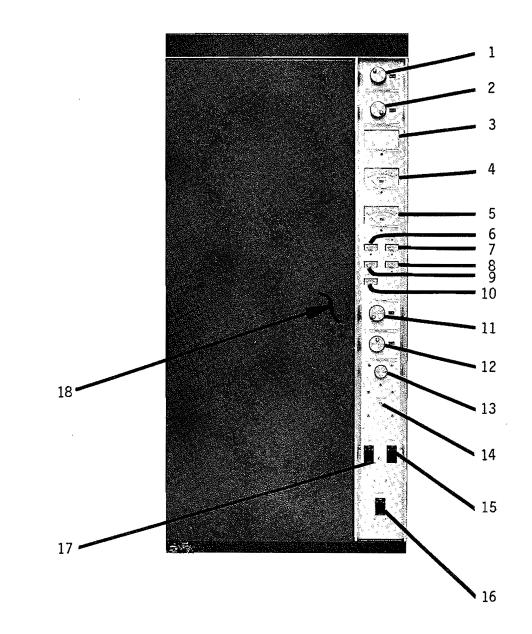
TABLE 3-1. POWER SUPPLY CABINET CONTROLS AND INDICATORS

NOMENCLATURE	FUNCTION
 HIGH VOLTAGE PRIMARY Circuit Breaker	Provides overload protection and primary power control for the PA plate power supply.



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FIGURE 3-2. PA CABINET CONTROLS AND INDICATORS

Table 3-2. PA Cabinet Controls and Indicators (Sheet 1 of 2)

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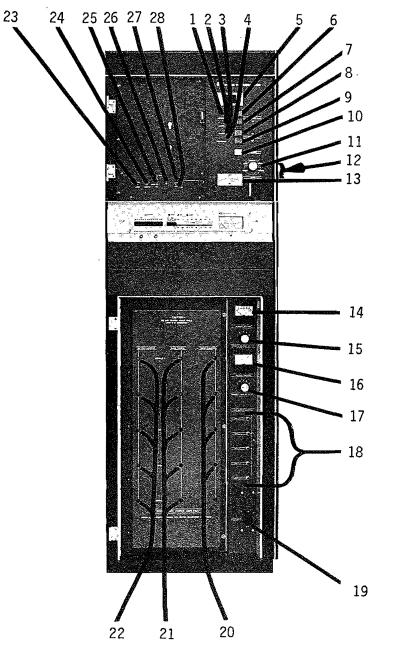
INDEX NO.	NOMENCLATURE	FUNCTION
1	P.A. OUTPUT TUNING Control and Cyclometer	Tunes the PA stage output circuit to resonance.
2	P.A. OUTPUT LOADING Control and Cyclometer	Adjusts the PA stage output loading.
3 .	POWER OUT Meter	Displays VSWR or percentage of RF forward power output as selected by the FWD/VSWR switch.
4	P.A. CURRENT Meter	Displays PA tube plate current.
5	P.A. VOLTAGE Meter	Displays PA tube plate voltage.
6	SCREEN VOLTAGE Meter	Displays PA tube screen grid voltage.
7	GRID VOLTAGE Meter	Displays PA tube control grid voltage.
8	GRID CURRENT Meter	Displays PA tube control grid current.
9	SCREEN CURRENT Meter	Displays PA tube screen grid current.
10	FILAMENT VOLTAGE Meter	Displays the PA tube filament voltage.
11	INPUT TUNING Control and Cyclometer	Tunes the PA input circuit to resonance.
12	INPUT LOADING Control and Cyclometer	Adjusts the PA stage input loading.
13	SCREEN VOLTAGE Control	Adjusts PA tube screen grid voltage when the AUTO/MAN switch is set to MAN. Adjustment of the SCREEN VOLTAGE control should not be attempted when the AUTO/MAN switch is set to AUTO.

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Table 3-2.	PA	Cabinet Controls	and	Indicators
		(Sheet 2 of 2)		

INDEX NO.	NOMENCLATURE	FUNCTION
14	FILAMENT VOLTAGE Control	Adjusts PA tube filament voltage.
15	SCREEN Circuit Breaker	Provides overload protection and con- trol for the PA tube screen grid circuit.
16	PRIMARY POWER Circuit Breaker	Provides overload protection and con- trol for the blower, the hum null assembly, and all equipment powered by the isolation transformer (FM exciter, stereo generator, etc.).
17	FILAMENT Circuit Breaker	Provides overload protection and con- trol for the PA tube filament circuit. The HIGH VOLTAGE CONTACTOR is inter- locked through the FILAMENT circuit breaker so that the plate supply will deenergize whenever the filament supply is interrupted.
18	HOURS Meter	Indicates hours of PA filament operation.
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FIGURE 3-3. DRIVER CABINET CONTROLS AND INDICATORS

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Table 3-3.	Driver Cabinet Control	and	Indicators
	(Sheet 1 of 3)		

INDEX NO.	NOMENCLATURE	FUNCTION
1	INTERLOCK status indicator	Illuminates to indicate all interlocks are closed.
2	BLOWER status indicator	Illuminates to indicate the blower is operational.
3	FILAMENT status indicator	Illuminates to indicate primary ac power is applied to the PA filament transformer.
4	HIGH VOLTAGE status Indicator	Illuminates to indicate the high voltage power supply is operational.
5	Microprocessor Readout	Numerically indicates the status of the transmitter control functions.
6	FILAMENT ON Switch/Indicator	SWITCH: Energizes the filament contactor to apply PA filament voltage.
		INDICATOR: Indicates proper operation of the filament control circuitry when illuminated.
7	FILAMENT OFF Switch	Deenergizes all transmitter functions powered by the three-phase primary ac input. The blower will run for 15 seconds after the FILAMENT OFF switch is depressed.
8	HIGH VOLTAGE ON Switch/Indicator	SWITCH: Energizes the high voltage contactor to apply PA plate potential.
		INDICATOR: Indicates proper operation of the high voltage control circuit when illuminated.
9	HIGH VOLTAGE OFF Switch	Deenergizes high voltage and mutes the exciter RF output.
10	OVERLOAD Switch/Indicator	SWITCH: Clears the overload circuit memory when depressed.
		INDICATOR: Illuminates to indicate an overload or open interlock.

INDEX NO.	NOMENCLATURE	FUNCTION
11	DRIVER Meter Switch	Selects the functions displayed by DRIVER meter.
12	RESET Switch	Initializes the microprocessor controller to start configuration.
13	DRIVER Meter	Displays IPA stage percentage of output power, IPA stage VSWR, or IPA stage combiner reject load relative power levels.
14	MODULE VOLTAGE Meter	Displays the voltage applied to each IPA module as selected by the MODULE VOLTAGE switch.
15	MODULE VOLTAGE Switch	Selects the module voltage to be dis- played by the MODULE VOLTAGE meter.
16	MODULE CURRENT Meter	Displays the dc current to each IPA module as selected by the MODULE CURRENT switch.
17	MODULE CURRENT Switch	Selects the module current to be dis- played by the MODULE CURRENT meter.
18	28 V MODULE () Circuit Breaker	Provides overload protection and con- trol for the associated IPA amplifier and regulator.
19	POWER SUPPLY Circuit Breaker	Provides overload protection and con- trol for the driver power supply.
20	INTERMEDIATE POWER AMPLIFIER INPUT LOADING Controls	Adjusts the RF input loading to each IPA module.
21	INTERMEDIATE POWER AMPLIFIER BASE TUNING Controls	Tunes each IPA stage amplifier base circuit to resonance.
22	INTERMEDIATE POWER AMPLIFIER OUTPUT LOADING Controls	Adjusts the output loading of each IPA module.

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Table 3-3. Driver Cabinet Control and Indicators (Sheet 2 of 3)

Table 3-3. Driver Cabinet Control and Indicators (Sheet 3 of 3)

INDEX NO.	NOMENCLATURE	FUNCTION
23	RAISE/LOWER Switch	Changes the automatic power control circuit operating level (operative only in local control).
24	LOCAL/REMOTE Switch	Selects between transmitter local control or both local and remote control.
25	VSWR CAL/VSWR FWD Switch	Allows calibration of the POWER OUT meter.
26	VSWR CAL Control	Allows calibration of the POWER OUT meter to 100% when the VSWR CAL/VSWR FWD switch is set to VSWR CAL.
27	AUTO Indicator	Illuminates to indicate automatic RF power output level control has been selected.
28	AUTO/MAN Switch	Allows manual control of the PA screen potential in the MAN position or enables automatic screen voltage control in the AUTO position.

TABLE 3-4. INDICATOR CHECKLIST

METER		SWITC	H POSITION/I	NDICATOR
POWER OUT	VSWR	FORWARD POW	IER %	
P.A. CURRENT	А			ELAPSED TIME METER
P.A. VOLTAGE	V			
SCREEN GRID VOLTAGE	V			
SCREEN GRID CURRENT	mA			
GRID VOLTAGE	ν			
GRID CURRENT	mA			
FILAMENT VOLTAGE	v			
MODULE VOLTAGE	1 V	2 V	3 V	4. 5 V VI
MODULE CURRENT	1 A	2 A.	3 A	4 5 A A
DRIVER	POWER %	VSWR C	HYBRID 1 %	HYBRID 2 HYBRID 3 % %
INDICATOR				STATUS
INTERLOCK		(ON)	OFF	
BLOWER		<u>ON</u>	OFF	
FILAMENT			OFF	
HIGH VOLTAGE			OFF	NOTE:
MICROPROCESSOR READOUT			3	OPERATIONAL STATUS SHOWN BY SHADED INDICATOR
FILAMENT ON SWITCH/IN	ON	OFF		
HIGH VOLTAGE ON SWITCH	ON S	OFF		
OVERLOAD SWITCH/INDIC	ATOR	ON.	OFF	

METER	SWITCH POSITION/INDICATOR							
POWER OUT	VSWR	FORWARD P	OWER %					
P.A. CURRENT	··· A					ELAPSE	D TIME METER	2
P.A. VOLTAGE	· V							
SCREEN GRID VOLTAGE	v						······	
SCREEN GRID CURRENT	mA							
GRID VOLTAGE	v							
GRID CURRENT	mA							
FILAMENT VOLTAGE	٧							
MODULE VOLTAGE	1 V	2	٧	3	۷	4 V	5 V]
MODULE CURRENT	1 Ą	2	A	3	A	4 A	5 A	
DRIVER	POWER %	VSWR \$			1 %	HYBRID 2 %	HYBRID 3 %	1
INDICATOR						STATUS		
INTERLOCK			(DFF				
BLOWER			(DFF				
FILAMENT		TON:	(OFF				
HIGH VOLTAGE		ON	(OFF /		NOTE:		,
MICROPROCESSOR READOL		rt Lj				NAL STATUS S D INDICATOR	SHOWN	
FILAMENT ON SWITCH/IN	IONE		OFF.			•		
HIGH VOLTAGE ON SWITC	ION		OFF		•			
OVERLOAD SWITCH/INDIG	CATOR	ON		OFF			• .	

TABLE 3-5. INDICATOR CHECKLIST

SECTION IV THEORY OF OPERATION

4-1. INTRODUCTION

4-2. This section presents detailed theory of operation for the FM-30 FM Transmitter.

4-3. For purposes of definition, the FM-30 Transmitter is divided into functional circuits by the following text. Refer to the detailed block diagram (Figure 4-1) and the overall schematic diagram in Section VII as required by the following explanation.

4-4. ELECTRICAL DESCRIPTION

4–5. FM EXCITER

4-6. The Broadcast Electronics FX-30 is a totally solid-state wideband FM exciter providing a continuously variable RF output from 3 to 30 watts into a 50 Ohm load at any frequency within the 87.5 to 108 MHz FM broadcast band. The exciter may be programmed to any frequency within this band in 10 kHz increments. The FX-30 exciter is mounted in slides to allow easy access to the semi-modular exciter internal circuitry.

4-7. The FX-30 will accept multiple wideband composite inputs from a stereo generator or SCA generator as well as a 600 0hm balanced audio input (see Figure 4-1). Refer to publication 597-0002 for a detailed explanation of the FM exciter features.

4-8. INTERMEDIATE POWER AMPLIFIER

4-9. The solid-state IPA section consists of five identical amplifier modules (one used as a driver for four) conservatively operated in a conventional guadrature hybrid combiner/splitter circuit.

4-10. Failure of any one of the four IPA output modules will typically cause only a 15 percent power reduction. In the event two modules fail, only a 35 percent reduction in transmitter power will result. Any one of the four amplifier modules can be used to replace the driver module should the need arise.

4-11. POWER AMPLIFIER

4-12. The FM-30 uses a high-gain Eimac 8990/4CX20000A tetrode to provide 30 kW of power output between 87.5 MHz to 108 MHz. The power amplifier operates in a high-gain, grid-driven class C configuration. Plate efficiency of the final amplifier approaches 80 percent at 30 kW output, resulting in comparatively low power consumption. Removal and installation of the PA tube in the FM-30 is a quick and simple procedure due to the cavity size and large access area. A large blower and an air switch arrangement ensures cool PA stage operation. 4-13. POWER AMPLIFIER CAVITY. The cavity used in the FM-30 employs a patented half wavelength folded tank circuit. This cavity design eliminates the plate blocking capacitor and all sliding contacts required by full half-wave and quarter-wave cavities. The results are high reliability, high efficiency, and low maintenance.

4-14. <u>Output Loading</u>. Anode voltage is applied to the lower portion of the fixed plate line at the RF voltage null point. Output loading is mechanically controlled by the position of a loop in the magnetic field generated at the RF voltage null point of the PA plate line structure. Multiple phosphor bronze leaves ground one side of the variable output loop to allow mechanical movement of the loading control without sliding contacts.

4-15. <u>Plate Tuning</u>. Plate tuning is provided by mechanically expanding or contracting the physical length of a beryillium copper bellows on the end of the variable or grounded portion of the PA plate line. Coarse frequency adjustment is accomplished by presetting the depth of the variable section of plate line into the tank cavity.

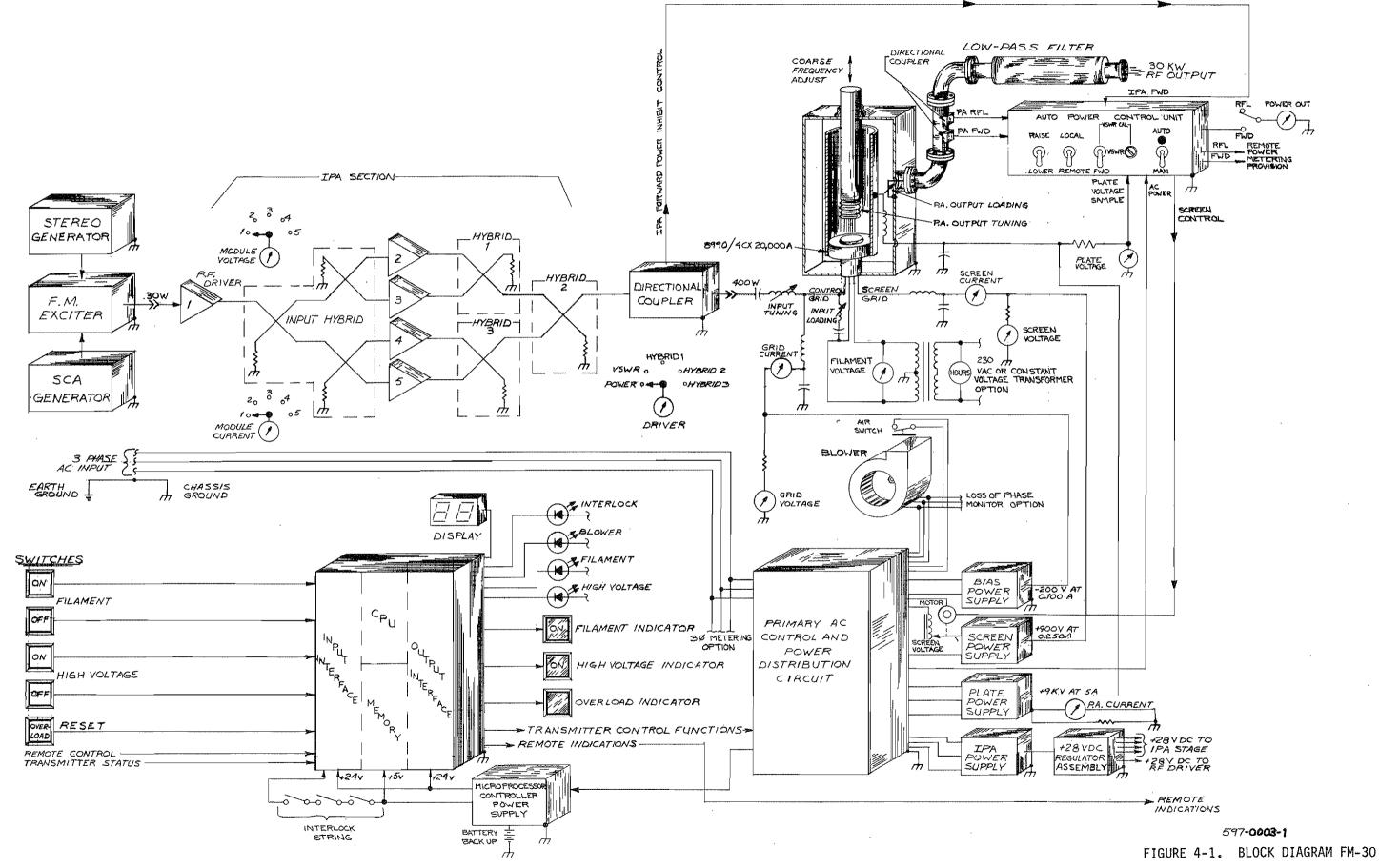
4-16. <u>Second Harmonic Attenuator</u>. A unique approach to second harmonic attenuation suppresses generation of the second harmonic in the power amplifier tank circuit. A suppressor consisting of a lumped coil and a lumped capacitor is placed inside the PA cavity at a point where the second harmonic exhibits a high impedance. This method suppresses generation of the second harmonic with minimal power loss at the fundamental frequency. When compared to a conventional second harmonic filter, the suppressor method results in increased PA efficiency.

4–17. TRANSMITTER CONTROLLER

4-18. All transmitter control and status functions in the FM-30 are performed by a built-in microprocessor controller that monitors the transmitter operating parameters in a series chain and then determines what control actions are necessary. By continuous scanning action, the microprocessor controller provides 123 different status indications, four LED displays, and three indicator lights for diagnostic purposes.

4-19. The microprocessor controller has the ability to initiate certain corrective actions concerning abnormal operating conditions without taking the transmitter off-the-air. Overload functions are retained in non-volatile memory for circuit analysis after equipment or power failure.

4-20. The control logic circuitry in the transmitter will interface directly with most modern remote control devices and ATS units. Two parallel four-bit BCD code outputs from the microprocessor controller provide remote status indications.



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4-21. AUTOMATIC RF OUTPUT LEVEL CONTROL. Part of the control circuitry monitors PA forward power, PA reflected power, and IPA forward power and adjusts the PA screen potential to maintain a constant RF output from the transmitter independent of ac line fluctuations. Manual screen control may be selected with a front-panel switch if desired.

4-22. VSWR FOLDBACK PROTECTION. PA reflected power is monitored by a circuit which automatically reduces RF power output in response to changes in the RF load such as antenna icing conditions. As the condition which caused the high VSWR condition returns to normal, RF output will proportionately increase until the full transmitter power output is restored.

4-23. SOFT START. Plate voltage is monitored by a circuit which reduces screen voltage to zero when the plate supply is turned off. When the plate supply is again turned on, the soft start circuit will gradually increase the screen supply until the rated RF output is achieved unless limited by a high VSWR or low IPA drive condition. The net effect of this circuit extends the life of the PA stage components by limiting stress.

4-24. AUTOMATIC RESTART. In event of a momentary ac power interruption, operation will resume when power returns. If ac power is lost for a prolonged period of time, the transmitter will initiate a complete start cycle to automatically return the equipment to operation.

4-25. RECYCLING. If an overload occurs, the transmitter will deenergize and allow the overload to clear. After several seconds, the transmitter will automatically return to operation. If two overloads occur in rapid succession, the equipment will deenergize and must be manually reset before operation can continue. If two or more overloads occur, spaced more than one minute apart, the transmitter will remain operational after each recycle attempt. This prevents having to manually reset the equipment after sporadic tripping due to lightning or power line surges. The microprocessor controller readout will display a code to indicate the problem whenever an overload occurs.

4-26. METERING

4-27. Twelve meters on the transmitter indicate critical parameters in addition to the microprocessor digital readout and seven status indicators. Additionally, exciter parameters are displayed by two meters and three status indicators. An elapsed time meter indicates hours of filament operation.

4-28. POWER SUPPLIES

4-29. All power supplies in the RF stage operate from a three-phase ac input. A stepdown isolation transformer operates the microprocessor controller power supply, the IPA directional coupler buffer amplifier power supply, and powers the exciter and optional stereo and SCA equipment.

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SECTION V MAINTENANCE

5-1. INTRODUCTION

5-2. This section provides general maintenance information, electrical adjustment procedures, and troubleshooting information for the FM-30 Transmitter. Maintenance is divided into two categories dependent upon the complexity of the procedure and the test equipment required to complete the maintenance.

5-3. SAFETY CONSIDERATIONS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

5-4. The FM-30 transmitter contains high voltages and currents which, if regarded carelessly, could be fatal. The transmitter has many built-in safety features, however good judgement, care, and common sense are the best accident preventives. The maintenance information contained in this section should be performed only by trained and experienced maintenance personnel.

5-5. It is very dangerous to attempt to make measurements or replace components with power energized, therefore such actions are not recommended. The design of the equipment provides safety features such that when a door or access panel is opened, interlock switches will deenergize the plate and screen power supplies. Do not short out or bypass interlock switches as a maintenance short cut.

5-6. The power supply cabinet and the PA cabinet contain switches which discharge the PA plate potential directly to ground whenever either cabinet is opened.

5-7. Grounding sticks are provided as safety features. Each grounding stick consists of a metal rod with a phenolic handle. The metal end is connected to chassis ground. Use a grounding stick to touch every part in the area or circuit on which maintenance is to be performed before attempting maintenance.

5-8. The grounding stick in the high voltage power supply cabinet and the grounding stick in the PA cabinet both rest on hook switches. When either of these grounding sticks is removed, the associated hook switch opens the transmitter interlock string and deenergizes the transmitter PA and screen potentials until each grounding stick is replaced on its respective hook switch.

WARNING

ENSURE THE REMOTE/LOCAL SWITCH IS SET TO LOCAL BEFORE ATTEMPTING MAINTENANCE.

5-10. First level or preventive maintenance consists of those precautionary measures applied to equipment to forestall future failures rather than to eliminate failures after they have occurred. These procedures are performed on a regularly scheduled periodic basis, and the results recorded in a performance log.

5-11. Preventive maintenance of the FM-30 transmitter falls into the category of good housekeeping and is limited to whatever cleaning may be necessary and checking the performance levels using the meters and various indicators built into the equipment.



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

5-12. On a regular basis, clean the equipment of accumulated dust. Check for overheated components, tighten loose hardware, and lubricate mechanical surfaces as required.

5-13. AIR FILTERS

5-14. Air filter replacement is accomplished outside the transmitter without interrupting equipment operation. The filter should be checked once each week with replacement done on an as-needed basis.

5-15. The transmitter uses one disposable type air filter 1 inch X 16 inches X 20 inches (2.54 cm X 40.64 cm X 50.8 cm) mounted in the rear door of the PA cabinet. Additional filters may be ordered for replacement (P/N 407-0062) or locally purchased.



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

5-17. Inspect the blower for dust accumulation and periodically clean the blower. Grease both the front and rear motor bearings at regular intervals (refer to Appendix A of the power supply portion of Part II). The blower mounting bolts should be checked for tightness.

5-18. The blower motor is cooled by the air passing through the motor. If the ambient air temperature is too high or if the air flow is restricted, then the lubricant will gradually vaporize from the motor bearings and bearing failure will occur. If very dirty air passes over the motor, accumulated dust will impair the motor cooling unless the accumulation is wiped from and blown out of the motor.

5-19. The blower impeller blades should be inspected and cleaned periodically. If the unit is operated to move very dusty air, dust will build up on the concave side of the blower impeller. If this happens, blower performance will be reduced and unbalance will result with a possibility of damage to the blower.

5-20. SECOND LEVEL MAINTENANCE



ENSURE THE REMOTE/LOCAL SWITCH IS SET TO LOCAL BEFORE ATTEMPTING MAINTENANCE.

5-21. Second level maintenance consists of procedures required to restore the transmitter to satisfactory operation after a fault has occurred.

5-22. The maintenance philosophy of the FM-30 transmitter consists of problem isolation to a specific area. Subsequent troubleshooting provided by each applicable assembly publication in Part II of this manual will assist isolation to a replaceable assembly or component. If desired, a replaceable assembly may be returned to the factory for repair or exchange.

5-23. ADJUSTMENTS

5-24. Adjustment procedures for all controls on all circuit boards are provided by each applicable assembly publication in Part II of this manual.

5-25. TROUBLESHOOTING



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

5-26. Most troubleshooting consists of visual checks. Because of the voltages and high currents in the equipment, it is considered hazardous to work with power energized. Therefore, the various transmitter indicators (meters, LEDs, fuses, and the digital read-out) should be used to isolate the malfunction to one of the specific areas listed below. Typical meter indications are presented in Table 5-1. Transmitter primary power demand requirements are listed in Table 5-2.

- A. Exciter
- B. Driver and IPA
- C. Power Amplifier
- D. Microprocessor Controller
- E. Automatic Power Control Unit
- F. Power Supplies
- G. Transmitter Load

CAUTION

MANY COMPONENTS IN THE TRANSMITTER ARE MOUNTED TO HEAT SINKS UTILIZING A FILM OF HEAT-SINK COM-POUND FOR THERMAL CONDUCTION.

IF ANY SUCH COMPONENT IS REPLACED, ENSURE A THIN FILM OF A ZINC-BASED HEAT-SINK COMPOUND IS USED (BE P/N 700-0028) TO ASSURE GOOD HEAT DISSIPATION.

5-27. Once the trouble is isolated, refer to the applicable assembly publication in Part II of this manual discussing the theory of operation and providing troubleshooting for the respective assembly to assist in problem resolution. Figures 5-1 through 5-8 provide drawings to assist component location. Pin-out diagrams for all integrated circuits used in the FM-30 are provided by Figure 5-9.

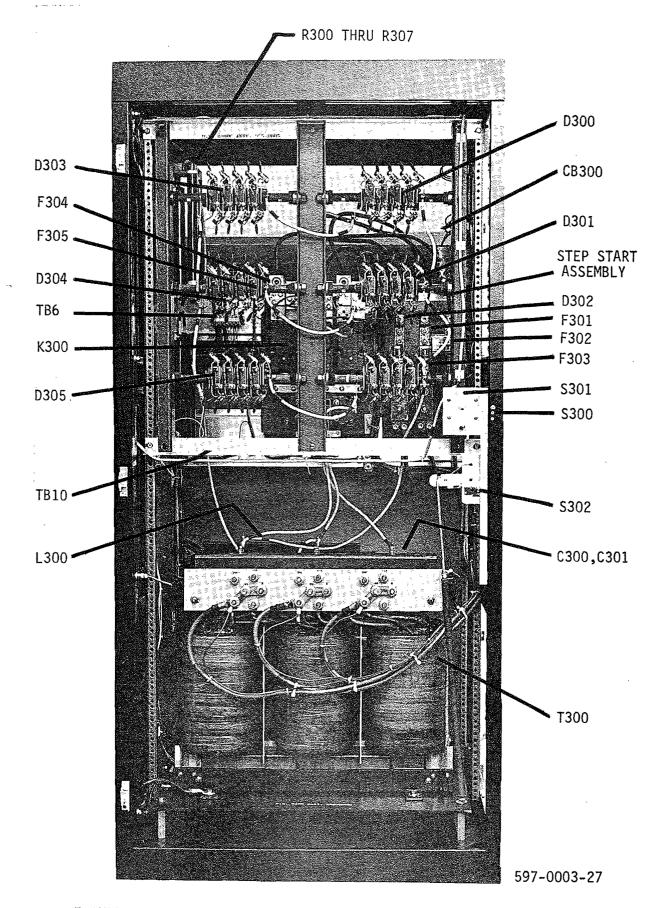
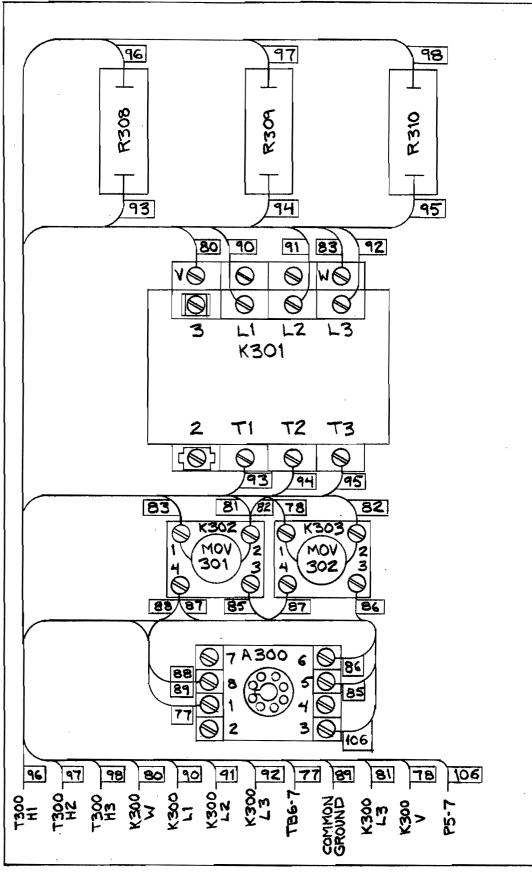


FIGURE 5-1. HIGH VOLTAGE POWER SUPPLY COMPONENT LOCATOR



597-0003-47

FIGURE 5-2. STEP-START ASSEMBLY COMPONENT LOCATOR

5-28. COMPONENT REPLACEMENT ON CIRCUIT BOARDS. Many of the circuit boards used in the FM-30 are double-sided boards with plated throughholes. Because of the plated through-holes, solder fills the holes by capillary action. These conditions require that defective components be removed carefully to avoid damage to the board.

5-29. On all circuit boards, the adhesive securing the copper track to the board melts at almost the same temperature as solder melts. A circuit board track can be destroyed by excessive heat or lateral movement during soldering. Use of a small iron with steady pressure is required for circuit board repairs.

5-30. To remove a component from a double-sided circuit board, cut the leads from the body of the defective component while the device is still soldered to the board.

5-31. Grip each component lead, one at a time, with long nose pliers. Turn the board over and touch the soldering iron to the lead at the solder connection. When the solder begins to melt, push the lead through the back side of the board and cut off the bent outer end of the lead. Each lead may now be heated independently and pulled out of each hole. The holes may be cleared of solder by carefully re-heating with a low wattage iron and removing the residual solder with a soldering vacuum tool.

5-32. Install the new component and apply solder from the bottom side of the board. If no damage has been done to the plated-through holes, soldering of the top side is not required.



MOST SOLVENTS WHICH WILL REMOVE ROSIN FLUX ARE VOLATILE AND TOXIC BY THEIR NATURE AND SHOULD BE USED ONLY IN SMALL AMOUNTS IN A WELL VENTILATED AREA, AWAY FROM FLAME, INCLUDING CIGARETTES AND A HOT SOLDERING IRON.

OBSERVE THE MANUFACTURER'S CAUTIONARY INSTRUCTIONS.

5-33. After soldering, remove flux with a cotton swab moistened with a suitable solvent. Rubbing alchol is highly diluted and is not effective. Solvents are available in electronic supply houses which are useful.

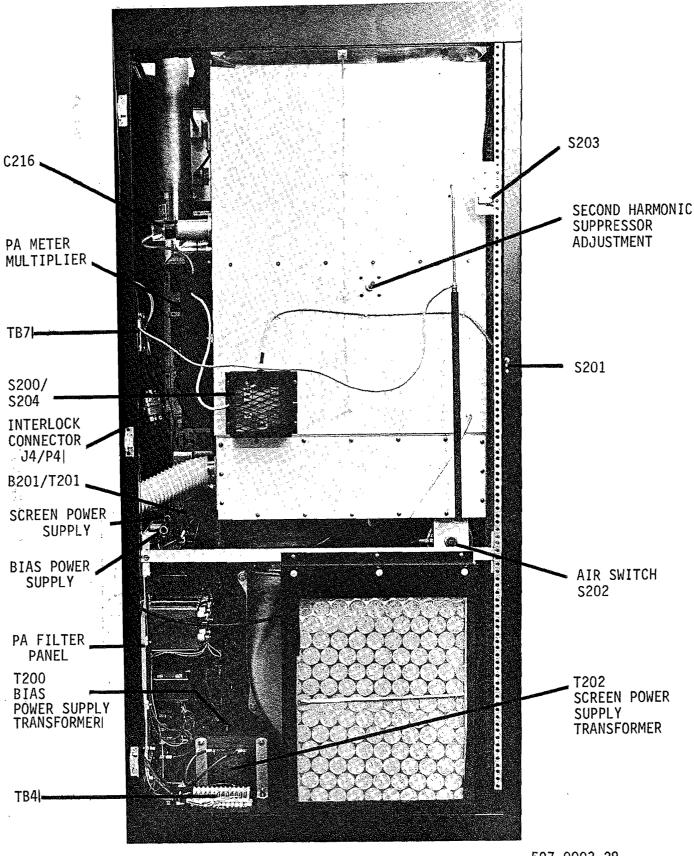
5-34. The board should be checked to ensure the flux has been removed and not just smeared about. Rosin flux is not normally corrosive, but rosin will absorb enough moisture in time to become conductive and cause problems.

METER	SWITCH POSITION/INDICATION					
POWER OUT	VSWR 1:1	FORWARD 100				
P.A. CURRENT	4.2 A					
P.A. VOLTAGE	9300 V					
SCREEN GRID VOLTAGE	500 V					
SCREEN GRID CURRENT	0.240 A					
GRID VOLTAGE	-290 V					
GRID CURRENT	0.140 A					
FILA. VOTLAGE	10.0 V					
MODULE VOLTAGE	27.5 V					
MODULE CURRENT	7.5 A					
DRIVER	POWER 100%	VSWR 1.02:1	HYBRID 1 5%	HYBRID 2 5%	HYBRID 3 5%	

Table 5-1. Typical Meter Indications (30 KW)

Table 5-2. Typical Power Demand (30 KW)

AC Line Frequency		60 Hz	
3 Ø AC Line Voltage	230 V	229	235 V
3 Ø AC Line Current	140 A	139 A	136 A
			~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
AC Line Frequency		50 Hz	
3 Ø AC Line Voltage	380	380	380
3 Ø AC Line Current	93	91	91



597-0003-28

FIGURE 5-3. PA CABINET COMPONENT LOCATOR (REAR)

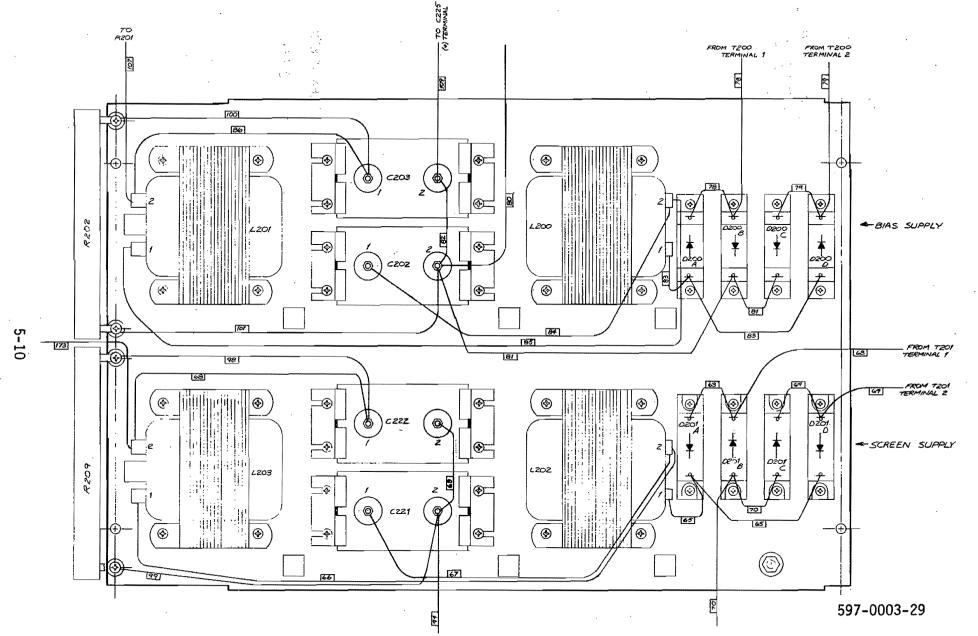
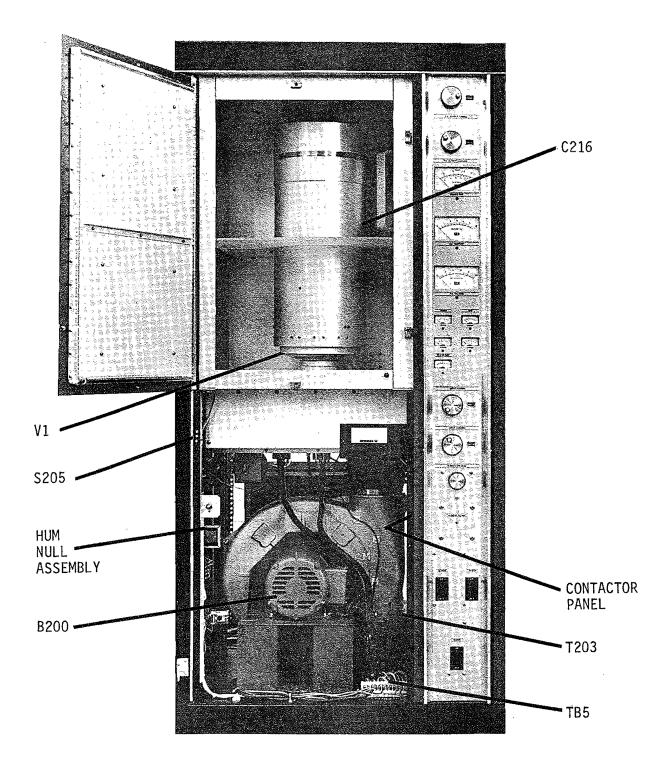


FIGURE 5-4. PA FILTER PANEL COMPONENT LOCATOR

4:



597-0003-31

FIGURE 5-5. PA CABINET COMPONENT LOCATOR (FRONT)

5-11

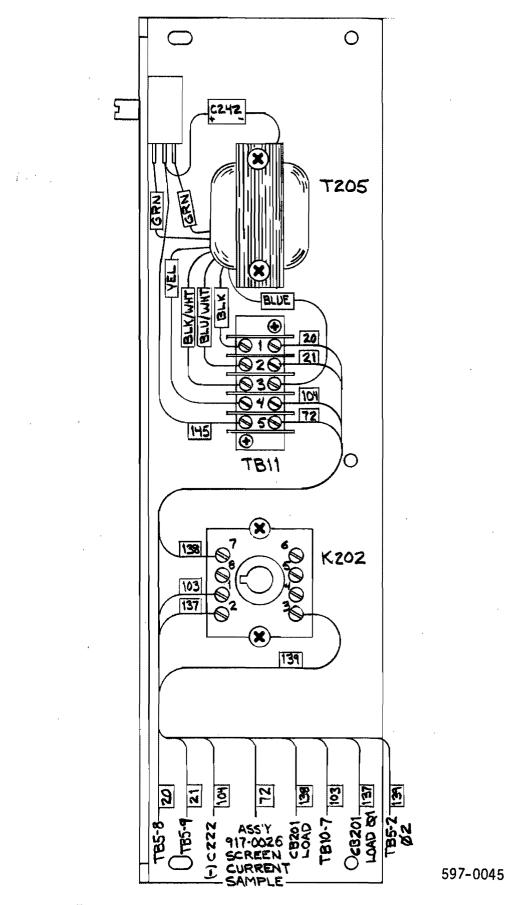
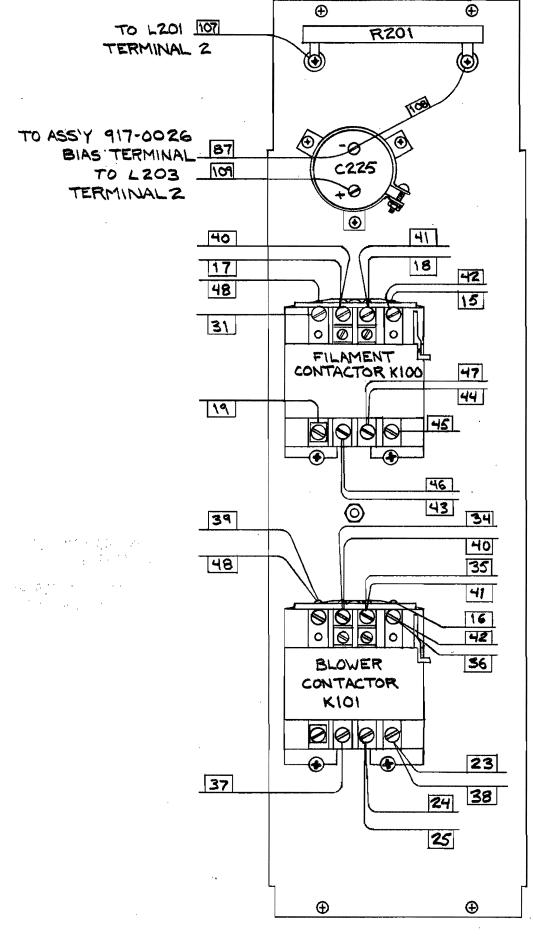


FIGURE 5-6. HUM NULL ASSEMBLY COMPONENT LOCATOR



597-0003-30

FIGURE 5-7. CONTACTOR PANEL COMPONENT LOCATOR

5-13

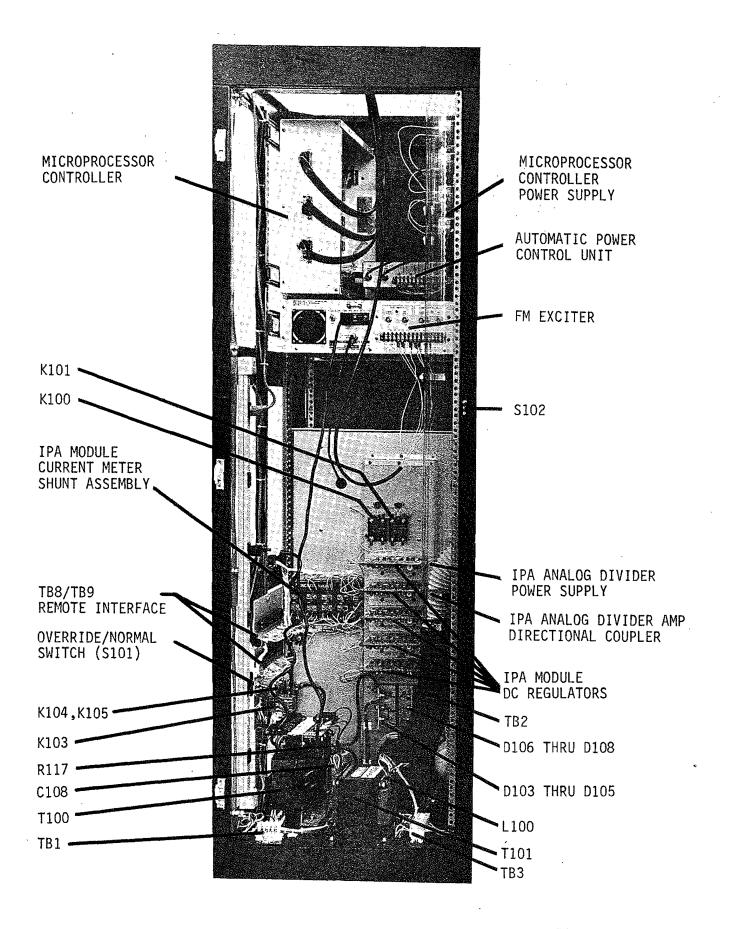


FIGURE 5-8. DRIVER CABINET COMPONENTS

597-0003-32

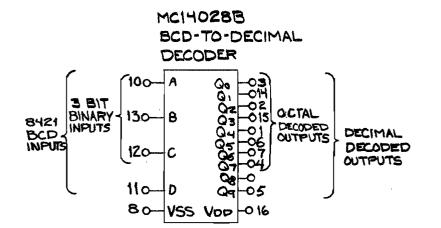
5-14

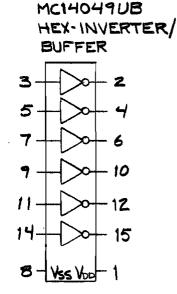
5-15

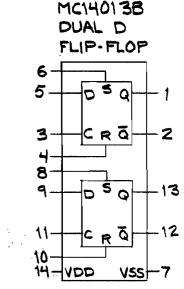
WARNING: DISCONNECT POWER PRIOR TO SERVICING

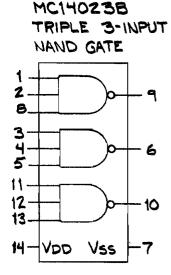
FIGURE 5-9. (Sheet 1 of 6)

597-0003-17A





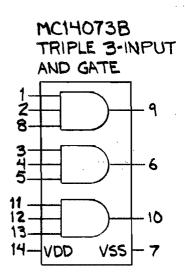


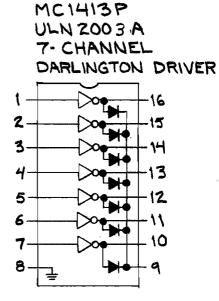


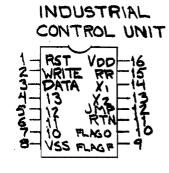
TOP VIEW SHOWN FOR ALL DEVICES UNLESS OTHERWISE NOTED.



INTEGRATED CIRCUIT CONNECTION DIAGRAMS

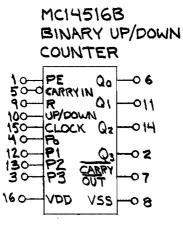






MC14500B

MC14 8-CHA SELEC	NNEL DATA
1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	VOIS - 13 NCBA - 10 NCBA -



2	10145 24 - 5 -Requ	TAGE	. CMOS
	DIVIE		•
-20 - 20 - 20 - 20 - 20 - 20 - 20 - 20	Q24 RESET VSS OUT 2 VOD INZ OUT 1 VSS	E BOOODDS	

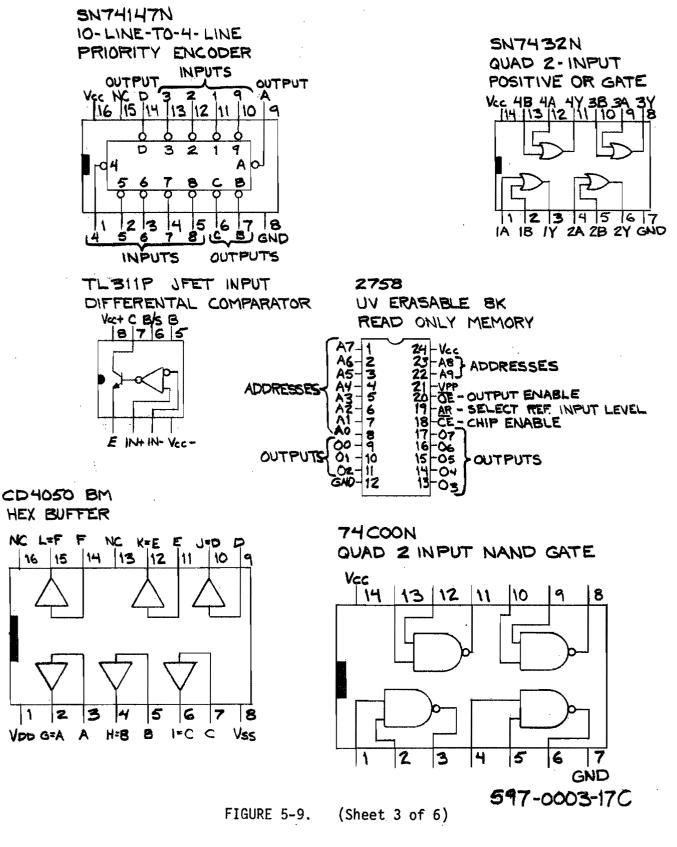
MC14599B 8-BIT ADDRESSABLE LATCH, BIDIRECTIONAL VDD 18 97 RESET QG 17 6 DATA Q5 WRITE DISABLEOH 5 03 Ao A 6 32 Q2 A2 G i CHIP ENABLE QO 11 WRIT 10 VSS

CD4069C HEX INVERTER 14 13 12 111 10 8 VOD S S 3 4 5 7 2 6

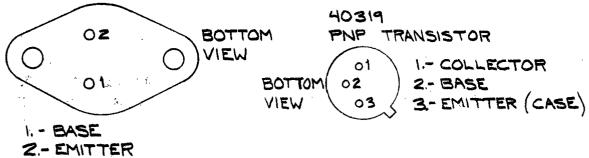
FIGURE 5-9. (Sheet 2 of 6)

597-0003-17B

5-16





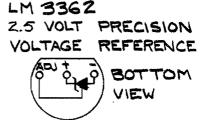


MPSU05 NPN POWER TRANSISTOR

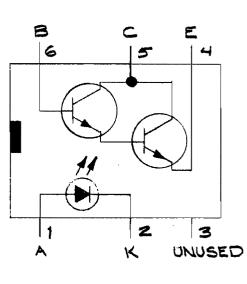




4N33 Optical isolator

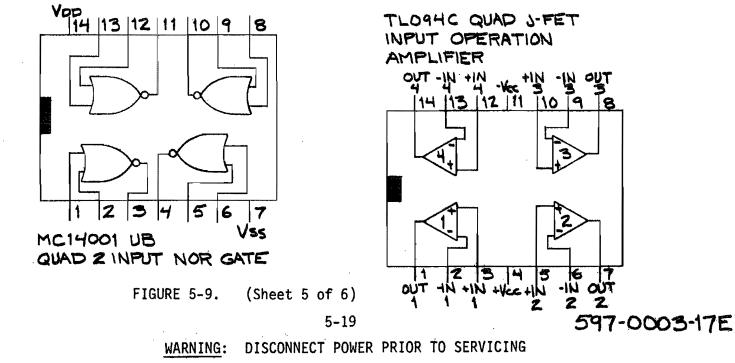


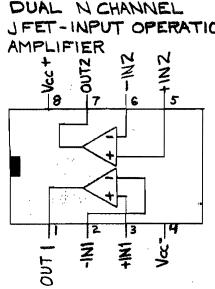
CASE - COLLECTOR



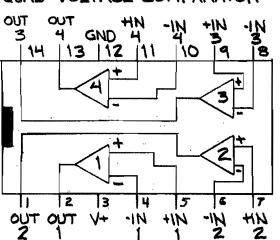
597-0003-170

FIGURE 5-9. (Sheet 4 of 6)

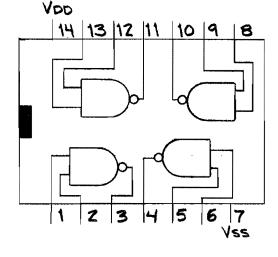




TL092CP DUAL N CHANNEL J FET-INPUT OPERATIONAL







MC14011 UB QUAD 2 INPUT NAND GATE

MC14584B

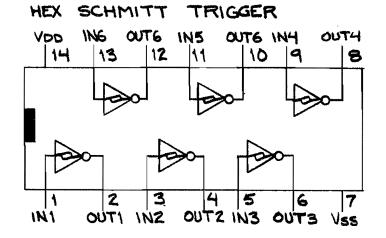
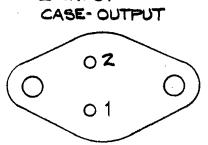
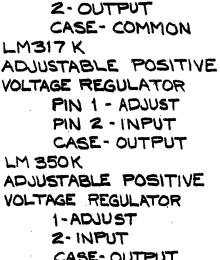


FIGURE 5-9. (Sheet 6 of 6)

BOTTOM VIEW



2N3055 NPN POWER TRANSISTOR 1.- BASE 2-EMITTER CASE · COLLECTOR



1- INPUT



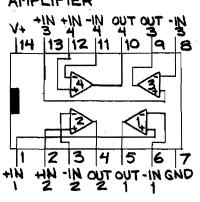
BM100-28 RF OUTPUT TRANSISTOR

Ε

597-0003-17F

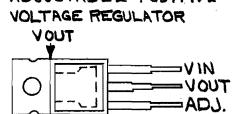
C

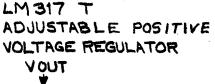
£



MC7824CK +24V REGULATOR







5-20

SECTION VI PARTS LIST

6-1. <u>INTRODUCTION</u>

6-2. This section provides descriptions and part numbers of electrical components, assemblies, and selected mechanical parts required for maintenance of the Broadcast Electronics FM-30 FM Transmitter. Each table entry in this section is indexed by reference designators appearing on the applicable schematic diagram.

PART NO.		TITLE	TABLE	PAGE	
909-0001/-1	FM-30	TRANSMITTER	6-2	6-6	
955-0043		CABLE ASSEMBLY, REMOTE HIGH VOLTAGE POWER SUPPLY INTER- LOCK	6-3	6-6	
909-1000	FM-30	PA CABINET	6-4	6-6	
909-1001		PA CABINET SUB ASSEMBLY	6-5	6-7	
950-6907		PA OUTPUT DIRECTIONAL COUPLER ASSEMBLY	6-6	6-8	
950-6906		OUTPUT DIRECTIONAL COUPLER ASSEMBLY	6-7	6-8	
924-0003		PA LOWER CONTROL PANEL ASSEMBLY	6-8	.6-8	
955-0048		VARIABLE AUTO TRANSFORMER AND MOTOR ASSEMBLY	6-9	6-9	
924-0002		PA FILTER PANEL ASSEMBLY	6-10	6-9	
955-0033		CAPACITOR ASSEMBLY	6-11	6-9	
955-0034		CAPACITOR ASSEMBLY	6-12	6-9	
924-0004		PA UPPER CONTROL ASSEMBLY	6-13	6-10	
924-0005		PA METER PANEL ASSEMBLY	6-14	6-10	
917-0051		FILAMENT VOLTAGE METER FILTER ASSEMBLY	6-15	6-10	
924-0001		PA CONTACTOR PANEL ASSEMBLY	6-16	6-11	

Table 6-1. FM-30 PARTS LIST INDEX (Sheet 1 of 5)

Table 6-1. FM-30 PARTS LIST INDEX (Sheet 2 of	Table 6	-1.	FM-30	PARTS	LIST	INDEX	(Sheet	2	of	5)
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PART NO.	TITLE	TABLE	PAGE
959-0065	HUM NULL ASSEMBLY	6-17	6-11
939-0001	PA CABINET RF ENCLOSURE	6-18	6-11
947-0130	METER MULTIPLIER CABLE ASSEMBLY	6-19	6-12
917-0026	SCREEN AND BIAS SUPPLY METER- ING ASSEMBLY	6-20	6-12
917-0016	HIGH VOLTAGE METER MULTIPLIER ASSEMBLY	6-21	6-13
955-0015	RF ENCLOSURE CHIMNEY ASSEMBLY	6-22	6-13
955-0007	RF INPUT CIRCUIT ASSEMBLY	6-23	6-13
955-0009	OUTPUT TUNING LINE ASSEMBLY	6-24	6-13B
909-2000	FM-30 DRIVER CABINET	6-25	6-13B
947-0003,4, 5,14,15, 20,21,22	CABLE ASSEMBLY, RF DRIVER	6-26	6-14
947-0006 THRU 947-0012	CABINET ASSEMBLY, RF DRIVER	6-27	6-14
947-0013	CABLE ASSEMBLY, RF DRIVER	6-28	6-14
947-0016	CABLE ASSEMBLY, DIRECTIONAL COUPLER TO PA GRID	6-29	6-14
947-0026	CABLE ASSEMBLY, DRIVER CABINET AC POWER	6-29A	6-15
947-0030	CABLE ASSEMBLY, RF DRIVER CABINET METERING	6-30	6-16
947-0091	CABLE ASSEMBLY, MICRO- PROCESSOR POWER INPUT	6-31	6-16
924-0007	IPA ASSEMBLY	6-32	6-16
917-0004	RF AMPLIFIER MODULE, FM	6-33	6-17
955-0018	OUTPUT HYBRID NO. 1	6-34	6-17

6-2

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PART NO.	TITLE	TABLE	PAGE			
917-0009	DIODE DETECTOR CIRCUIT BOARD ASSEMBLY	6-35	6-18			
955-0016	OUTPUT HYBRID NO. 2	6-36	6-18			
955-0012	OUTPUT HYBRID NO. 3	6-37	6-18			
955-0011	INPUT HYBRID ASSEMBLY	6-38	6-18			
955-0003	ASSEMBLY, POWER SUPPLY, IPA ANALOG DIVIDER	6-39	6-19			
917-0012	IPA ANALOG DIVIDER POWER SUPPLY ASSEMBLY	6-40	6-19			
917-0021	28V REGULATOR	6-41	6-19			
955-0031	METER SHUNT BOARD	6-42	6-21			
955-0035	METAL OXIDE VARISTOR ASSEMBLY	6-43	6-21			
924-0006	RF DRIVER CABINET CONTROL PANEL	6-44	6-21			
917-0003	PROCESSOR CIRCUIT BOARD ASSEMBLY	6-45	6-22			
919-0013	OUTPUT CIRCUIT BOARD ASSEMBLY	6-46	6-23			
917-0006	CONTROL/TIMER CIRCUIT BOARD ASSEMBLY	6-47	6-24			
919-0030	INPUT BOARD 1 CIRCUIT BOARD ASSEMBLY	6-48	6-25			
919-0054	INPUT BOARD 2 CIRCUIT BOARD ASSEMBLY	6-49	6-27			
919-0003	REMOTE CONTROL INTERFACE CIRCUIT BOARD ASSEMBLY	6-50	6-29			
917-0020	METER CIRCUIT BOARD ASSEMBLY	6-51	6-31			
917-0027	PRIMARY FUNCTION INDICATOR CIRCUIT BOARD ASSEMBLY	6-52	6-31			

Table 6-1. FM-30 PARTS LIST INDEX (Sheet 3 of 5)

Tab	le 6-1.	FM-30	PARTS	LIST	INDEX	(Sheet 4 of !	5)

TITLE MICROPROCESSOR PATCH PANEL CIRCUIT BOARD ASSEMBLY MICROPROCESSOR CONTROLLER	TABLE 6-53	PAGE 6-31
CIRCUIT BOARD ASSEMBLY	6-53	6-31
WIRING HARNESS	6-54	6-32
AUTOMATIC POWER CONTROL ASSEMBLY	6-55	6-32
DUAL 120 MHz LOW-PASS FILTER CIRCUIT BOARD ASSEMBLY	6-56	6-32
POWER SUPPLY/CONTROL CIRCUIT BOARD ASSEMBLY	6-57	6-33
ANALOG CIRCUIT BOARD ASSEMBLY	6-58	6-33
RESISTOR AND LUGS ASSEMBLY	6-59	6-35
IPA DIRECTIONAL COUPLER ASSEMBLY	6-60	6-36
VSWR ASSEMBLY	6-61	6-36
IPA DIRECTIONAL COUPLER ASSEMBLY	6-62	6-36
BUFFER AMPLIFIER CIRCUIT BOARD	6-63	6-36
EXCITER AC CONTROL	6-64	6-37
MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER	6-65	6-37
MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER CIRCUIT BOARD ASSEMBLY	6-66	6-38
ROPROCESSOR CONTROLLER BYPASS ASSEMBLY	6~67	6-39
	AUTOMATIC POWER CONTROL ASSEMBLY DUAL 120 MHz LOW-PASS FILTER CIRCUIT BOARD ASSEMBLY POWER SUPPLY/CONTROL CIRCUIT BOARD ASSEMBLY ANALOG CIRCUIT BOARD ASSEMBLY RESISTOR AND LUGS ASSEMBLY IPA DIRECTIONAL COUPLER ASSEMBLY VSWR ASSEMBLY IPA DIRECTIONAL COUPLER ASSEMBLY BUFFER AMPLIFIER CIRCUIT BOARD EXCITER AC CONTROL MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER CIRCUIT BOARD ASSEMBLY ROPROCESSOR CONTROLLER BYPASS	WIRING HARNESSAUTOMATIC POWER CONTROL ASSEMBLY6-55DUAL 120 MHz LOW-PASS FILTER CIRCUIT BOARD ASSEMBLY6-56POWER SUPPLY/CONTROL CIRCUIT BOARD ASSEMBLY6-57ANALOG CIRCUIT BOARD ASSEMBLY6-58RESISTOR AND LUGS ASSEMBLY6-59IPA DIRECTIONAL COUPLER ASSEMBLY6-60VSWR ASSEMBLY6-61IPA DIRECTIONAL COUPLER ASSEMBLY6-61IPA DIRECTIONAL COUPLER ASSEMBLY6-61BUFFER AMPLIFIER CIRCUIT BOARD6-62EXCITER AC CONTROL6-63EXCITER AC CONTROL6-64MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER6-66MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER CIRCUIT BOARD ASSEMBLY6-66MICROPROCESSOR CONTROLLER POWER SUPPLY AND BATTERY CHARGER CIRCUIT BOARD ASSEMBLY6-67

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Table 6-1.	FM-30	PARTS	LIST	INDEX ((Sheet
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PART NO.	TITLE	TABLE	PAGE
919-0009	MICROPROCESSOR CONTROLLER BYPASS CIRCUIT BOARD ASSEMBLY	6-68	6-40
919-0014	MICROPROCESSOR CONTROLLER BYPASS ASSEMBLY 24 VOLT CONTROL CIRCUIT BOARD	6-69	6-41
909-3000	HIGH VOLTAGE POWER SUPPLY CABINET ASSEMBLY	6-70	6-41
955-0030	HIGH VOLTAGE SHORTING AND INTERLOCK SWITCH ASSEMBLY	6-71	6-42
955-0038	GROUND STICK HANGER	6-72	6-42
955-0005	POWER SUPPLY DIODE ASSEMBLY	6-73	6-42
955-0006	POWER SUPPLY BASE ASSEMBLY	6-74	6-43
947-0090	WIRING HARNESS, HIGH VOLTAGE POWER SUPPLY INTERLOCK	6-75	6-43
959-0067	AC POWER DISTRIBUTION PANEL	6-76	6-43
959≓0064	HIGH VOLTAGE STEP START ASSEMBLY	6-77	6-43
919-0199	STEP START CIRCUIT BOARD ASSEMBLY	6-78	6-44
	· · · · ·		

6-5

REF. DES.	DESCRIPTION	PART NO.	QTY.
V1	PA Tube, 4CX20000A/8990	243-0001	1
	FM-30 FM Exciter (-0001 and -0001-1 configurations)	909-0002	ī
	FM-30 PA Cabinet Assembly	909-1000	1 1
	FM-30 Driver Cabinet Assembly	909-2000	lil
	FM-30 High Voltage Power Supply Cabinet Assembly	909-3000	1
*	Alternate Harmonic Filter, Low-Pass, 30 kW, 88 to 108 MHz	339-0005	1
	Transmission Line Insulator-Connector Assembly	427-0004	1
	Adapter, Transmission Line, 3.125 inches (7.94 cm) flange to clamping ring	427-0001	1
	Assembly, Transmission Line Coupling, 3.125 inches (7.94 cm)	427-0005	1
	Assembly, 90° elbow, 3.125 inches (7.94 cm), modified with RF sample port	427-0016	1
	Microprocessor readout conversion sheets	839-0004	
	High Voltage Cable (for -1 and -3 configurations)	610-0204	75 ft (22.86m
	Cable Assembly, Remote High Voltage Power Supply Interlock (for -1 and -3 configurations)	955-0043	1
	Microprocessor Controller Bypass Assembly	959-0053	1

Table 6-2. FM-30 Transmitter - 909-0001/-1-2-3

Table 6-3. Cable Assembly, Remote High Voltage Power Supply Interlock - 955-0043

REF. DES.	DESCRIPTION	PART NO.	QTY.
J5	Connector, 14-Pin	418-0008	1
P5	Connector, 14-Pin	417-0008	1

Table 6-4. FM-30 PA Cabinet - 909-1000 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
B200	Blower, CCW rotation, 1500 ft ³ /min (42.5 m ³ /min at 3450 r/min MOTOR: 230/460V, 3Ø, 60 Hz	387-5002	1
B202 C244,C245 J4	HOURS Indicator, 0-99,999 Hours, 230V ac, 60 Hz Capacitor, Ceramic Disc, 0.01 uF, 500V Alternate 50 Hz Meter Connector, 24-Pin	315-0002 001-1044 315-0002-1 418-0009	1 2 1 1

Table 6-4.	FM-30	PA	Cabinet	-	909-1000	(9
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(Sheet 2 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
J5	Connector, 14-Pin	418-0008	1
S201	Door Interlock Switch SPDT, 15A at 125 or 250V ac, 0.5A at 125V dc, 0.25A at 250V dc	346-3302	1
S202	Switch, Air Presssure, 1.5 to 5.0 inches Water Column (3.81 cm to 12.7 cm), 15A, 120/480V, 60 Hz Resistive, 1/8 H.P. @ 125V 60 Hz, 1/4 H.P. @ 250V 60 Hz	340-0005	1.
S205	Door Interlock Switch SPDT, 15A at 125 or 250 V ac, 0.5A at 125V dc, 0.25A at 250V dc	346-3302	1
T200	Bias Transformer: PRIMARY: 208/240V ±11V, 60 Hz, 1Ø SECONDARY: 235V ac, 0.4 Amperes	376-0016	1
T202	Screen Transformer: PRIMARY: 208/240V ±11V, 60 Hz, 1Ø SECONDARY: 777V ac, 0.4 Amperes	376-0015	1
T203	Filament Transformer: PRIMARY: 208/240V, 60 Hz, 1Ø SECONDARY: 10.5V ac CT, 147 Amperes	376-0530	1
TB4,TB5	Barrier Strip, Screw Terminal	412-0724	25
TB7	Barrier Strip, 4 Terminal	412-0011	1
	End Caps for TB4 and TB5	412-0730	2
	PA Cabinet RF Enclosure	939-0001	1
	Air Filter, 1 inch X 16 inches X 20 inches (2.54 cm X 40.64 cm X 50.8 cm)	407-0062	1
	PA Cabinet Sub-Assembly	909-1001	1
	Air Filter Grill Mounting consisting of: Stud, Turn Lock	424-0008	2
	Receptacle	424-0008	2 2 2
	Stud Retainer	424-0009	2
	Air Filter Mounting Retainer consisting of:	727-0000	4
	Stud, Turn Lock	424-0004	3.
	Receptacle	424-0005	3
	Stud Retainer	424-0006	3

	Table 6-5. PA Cabinet Subassembly - 909-1001	(Sheet 1 of	f 2)
REF. DES.	DESCRIPTION	PART NO.	QTY.
	PA Output Directional Coupler Assembly PA Lower Control Assembly PA Filter Panel Assembly Capacitor Assembly Capacitor Assembly PA Upper Control Assembly	950-6907 924-0003 924-0002 955-0033 955-0034 924-0004	1 1 1 1

6-7

REF. DES.	DESCRIPTION	PART NO.	QTY.
	PA Meter Panel Assembly	924-0005	1
	PA Contactor Panel Assembly	924-0001	1
	Hum Null Assembly	959-0065	1
	Ground Stick Hanger Assembly	955-0038	1

Table 6-5. PA Cabinet Subassembly - 909-1001 (Sheet 2 of 2)

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Table 6-6. PA Output Directional Coupler Assembly - 950-6907

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Output Directional Coupler Assembly	950-6906	2

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Table 6-7. Output Directional Coupler Assembly - 950-6906

REF. DES.	DESCRIPTION	PART NO.	QTY.
J1	BNC Connector	417-0203	1
R215	Resistor, 68 Ohm ±5%, 2W	132-6832	1

Table 6-8. PA Lower Control Panel - 924-0003

REF. DES.	DESCRIPTION	PART NO.	QTY.
CB200,	Circuit Breaker, 2 Pole, 15A, 240V ac, Modified (FILAMENT and SCREEN)	341-0003-1	2
CB201 CB202	(FILAMENT and SCREEN) Circuit Breaker, 3 Pole, 20A, 240V ac, Modified (PRIMARY POWER)	341-0012-1	1
T204	Variable Auto Transformer, Single-Phase, 60 Hz, 0-40V, 15A, 0.6 kV A (FILAMENT VOLTAGE)	374-0001-1	1
	Variable Auto Transformer and Motor Assembly Knob, Black (For INPUT TUNING and INPUT LOADING	955-0048 482-0007	1 2
	Controls) Knob, Black (For SCREEN VOLTAGE Control)	482-0008	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
B201 C226	Motor, Reversible, 2 RPM, 30 in/oz output Torque, 117V ac, 60 Hz, Magnetic Clutch, 5.5 vA Capacitor, Mylar, 0.47 uF ±10%, 300V ac	380-0001	1
Ţ201	Transformer, Variable, 240V, 0.59 kVA, 60 Hz, 2.25A output	374-0002	1
S205,S206	Micro Switch, Modified, SPDT, 125V @ 4 Amperes Inductive (Motor limit switches)	346-6100-1	2

Table 6-9. Variable Auto Transformer and Motor Assembly - 955-0048

Table 6-10	. PA	Filter	Panel	Assembly	-	924-0002
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C202,C203,	Capacitor, Electrolytic, oil filled, 10 uF, 2 kV	047-0002	4
C221,C222 D200A THRU D200D, D201A THRU D201D	Rectifier, Silicon, 4000V PIV, 2 Amperes	234-0002	8
L200 THRU L203	Choke, 10H @ 0.4 Adc dc Resistance: 92 Ohms	377-0002	4
R202 R209	Resistor, 1 k Ohm ±5%, 100W, W/W Resistor, 10 k Ohm ±5%, 100W, W/W	132-1043 132-1053	1 1

Table 6-11. Capacitor Assembly - 955-0033

REF. DES.	DESCRIPTION	PART NO.	QTY.
C204,C205, C206,C217, C218,C223, C224	Capacitor, Disc Ceramic, 0.01 uF, 500V	001-1044	7

Table 6-12.	Capacitor	Assembly .	- 955-0034
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C225	Capacitor, Disc Ceramic, 0.005 uF, 500V	001-5034	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Knob, Black (For PA OUTPUT TUNING and PA OUTPUT LOADING Controls)	482-0007	2

Table 6-13. PA Upper Control Assembly - 924-0004

Table 6-14. PA Meter Panel Assembly	- 924-0005
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REF. DES.	DESCRIPTION	PART NO.	QTY.
M200	Meter, 4.5 inch (11.4 cm) Taut Band Type, FS = 200 uA dc ±2%, 208 Ohm movement (POWER OUT)	310-0004-2	1
M201	Meter, 1.5 inch (3.8 cm) Taut Band Type, FS = 1 mA ±2%, 15 Ohm movement (GRID VOLTAGE)	317-0002-1	1
M202	Meter, 1.5 inch (3.8 cm) Taut Band Type, FS = $500 \text{ mA} \pm 2\%$, 15 0hm movement (GRID CURRENT)	310-0001-1	1
M204	Meter, 1.5 inch (3.8 cm) Taut Band Type, FS = 1 mA ±2%, 15 Ohm movement (SCREEN VOLTAGE)	317-0006-1	1
M205	Meter, 1.5 inch (3.8 cm) Taut Band Type, FS = 500 mA ±2%, 15 0hm movement (SCREEN CURRENT)	310-0001-1	· 1
M206	Meter, 1.5 inch (3.8 cm) Taut Band Type, FS = 15V ac ±2%, 870 Ohms/Volt sensitivity (FILAMENT VOLTAGE)	317-0003-1	• 1
M207	Meter, 4.5 inch (11.4 cm) Taut Band Type, FS = 1 mA ±2%, 15 Ohm movement (P.A. VOLTAGE)	317-0001-1	1
M208	Meter, 4.5 inch (11.4 cm) Taut Band Type, FS = 1V ±2%, 1000 Ohm/Volt sensitivity (P.A. CURRENT)	310-0002-1	1
	FILAMENT VOLTAGE Meter Filter Assembly	917-0051	1

Table 6	-15.	FILAMENT	VOLTAGE	Meter	Filter	Assembly -	917-0051
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C1,C2	Capacitor, Polycarbonate, 0.01 uF ±5%, 50V	037-1042	2
L1	Molded Indicator, 47 uH ±10%, 700V Maximum	360-0012	1
	Blank Circuit Board	517-0051	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
C225 K200,K201	Capacitor, Electrolytic, 300 uF, 450V Contactor Contacts: 3 sets SPST, 30A @ 600V Coil: 110/120V ac, 50/60 Hz	025-9086 341-0006	1 2
R211	Resistor, 500 Ohm, 50W, W/W	132-5033	1

Table 6-16. PA Contactor Panel Assembly - 924-0001

Table 6-17. Hum Null Assembly - 959-0065

REF. DES.	DESCRIPTION	PART NO.	QTY.
C242	Capacitor, Electrolytic, 25 uF, 100V	013-1084	1
K202	Relay, Plug-in: Coil - 240V ac Contacts - DPDT, 240V @ 5 Amperes	270-0023	1
R216	Rheostat, 50 Ohm, 25W, 0.707 Ampere	195-0149	1
T205	Transformer, Power: Primary: 230V CT, 50/60 Hz Secondary: 12.6V @ 1 Ampere	376-0232	1
TB11	Barrier Strip, 5 Terminal	412-0005-1	1
XK202	Socket, 8-Pin, Screw Terminal	417-0400	1
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Table 6-18.	PA Cabinet	RF Enclosure	- 939-0001	(Sheet 1 of 2)
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C215	Capacitor, RF Feedthru, 800 pF, 3 kV	008-8024	1
C216	Capacitor, HV Feedthru, 800 pF, 30 kV (Broadcast Electronics Manufacture)	995-0049	1
C232	Capacitor plate for second harmonic suppressor	474-6440	1
L208	RF Choke, plate circuit, 26 Turns AWG 13 Nichrome wire, 0.37 inches (0.94 cm) ID, 2.75 inches (6.99 cm) long	360-0004	1
L211	High frequency strap for second harmonic suppressor	479-0053	1
	Low frequency strap for second harmonic suppressor	479-0054	1
S200,S203	High Voltage Interlock Switch, SPDT, 11A @ 125 or 250V ac, 0.5A @ 125V dc, 0.25A @ 250V dc	346-6100	2
	Screen and Bias Supply Metering Assembly	917-0026	1
	High Voltage Meter Multiplier Assembly	917-0016	1
	RF Input Circuit Assembly	955-0007	
	Meter Multiplier Cable Assembly	947-0130	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
P200	Banana Plug	418-0188	1
	Door Fastener Stud Door Retainer Nut	420-5008 421-0014	4 4
	Door Retainer Bracket	479-6451	4
	Door RF Gasket, Top and Bottom Door RF Gasket, Sides	469-0371 469-0372	2 2
	Transmission Line Elbow, 90°, 3.125 inches (7.94 cm)	427-0002	1
	Transmission Line Coupling with Inner Connector, 3.125 inches (7.94 cm)	427-0005	1
	RF Enclosure Chimney Assembly Output Tuning Line Assembly	955-0015 955-0045	1 1
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Table 6-18. PA Cabinet RF Enclosure - 939-0001 (Sheet 2 of 2)

Table 6-19. Meter Multiplier Cable Assembly - 947-0130

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Resistor, 100 k Ohm ±5%, 2W	130-1062	1

Table 6-20. Screen and Bias Supply Metering Assembly - 917-0026

REF. DES.	DESCRIPTION	PART NO.	QTY.
REF. DES. C200,C201 C220 R200 R201 R203 R206 R207 R208 R210 R211,R212	Capacitor, Ceramic Disc, 0.001 uF, 1000V Capacitor, Electrolytic, 100 uF ±10%, 20V, Dipped Tantalum Resistor, 2 Meg Ohm ±5%, 1/2W Resistor, 5 Ohm ±5%, 8W, W/W Resistor, 0.5 Meg Ohm ±1%, 2W Resistor, Copper Wire, No. 22 AWG Resistor, 12 k Ohm ±5%, 2W Resistor, 1 Meg Ohm ±1%, 2W Resistor, 5 Ohm ±5%, 8W, W/W Resistor, 0.5 Meg Ohm ±1%, 2W	002-1034 063-1083 110-2073 132-5013 140-0005 601-0022 130-1253 140-0003 132-5013 140-0005	2 1 1 0.083ft (2.53m) 1 1 2
	Blank Circuit Board	517-0026	- -

REF. DES.	DESCRIPTION	PART NO.	QTY.
R1 THRU R10 	Resistor, 1 Meg Ohm ±1%, 2W Blank Circuit Board	140-0003 517-0016	10 1

Table 6-21. High Voltage Meter Multiplier Assembly - 917-0016

Table 6-22. RF Enclosure Chimney Assembly - 955-0015

REF. DES.	DESCRIPTION	PART NO.	QTY.
J200	Banana Jack	417-0157	1
	Plate Line Contact Fingers	469-0369-1	12

REF. DES.	DESCRIPTION	PART NO.	QTY.
C208	Capacitor, Input, Printed Circuit Board, 300 pF	917-0040	1
C209	Capacitor, Ceramic, 1000 pF ±20%, 5 kV	008-1036	1 1
C210	Capacitor, Ceramic, Feedthru, 800 pF $\pm 20\%$, 3 kV	008-8024	1
C211	Filament Bypass Capacitor, 2.25 inch X 2.5 inch X 0.062 inch (5.715 cm X 6.35 cm X 0.158 cm), Fiberglass	467-0088	1
C212	Capacitor, Ceramic, 1000 pF ±20%, 5 kV	008-1036	1
C213	Filament Bypass Capacitor, 2.25 inch X 2.5 inch X 0.062 inch (5.715 cm X 6.35 cm X 0.158 cm), Fiberglass	467-0088	1
C215	Capacitor, Ceramic, Feedthru, 800 pF ±20%, 3 kV	008-8024	1
C227 THRU C230	Screen Bypass Capacitor, 0.005 inch (0.013 cm) Kapton	407-0953	1 4
C231 THRU C234, C236 THRU C241, C246	Capacitor, Ceramic, 500 pF ±20%, 5 kV	008-5024	11
J201	Receptacle, Type N, coaxial	417-0204	1
L204	Loading Coil	360-0005	$\begin{array}{c} 1\\ 1\end{array}$
L205	Grid Choke	360-0006	1
L212A THRU L212D	Neutralizing Slide	479-6454	4
	Neutralizing Contact	469-0411	4
R204	Resistor, 750 Ohm ±10%, 50W, Non-Inductive	139-7532	1 1
R205	Resistor, 300 Ohm ±10%, 50W, Non-Inductive	139-3332	1
XU1	Socket, 8990/4CX20, Eimac SK300A, Modified	417-0007-8	1
	Control Grid Contact Ring only for XU1	417-0007-1	1 1
	Screen Grid Contact Ring only for XU1	417-0007-2	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Ceramic Post Insulator Spacer only for XU1 Ceramic Sleeve Insulator Spacer only for XU1	417-0007-9 417-0007-A	4 4
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e na Second			

Table 6-23. RF Input Circuit Assembly - 955-0007 (Sheet 2 of 2)

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Table 6-24. Output Tuning Line Assembly - 955-0009

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Plate Tuning Bellows and Plate Assembly	955-0045	1

Table 6-25. FM-30 Driver Cabinet - 909-2000

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(Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C108	Capacitor, Electrolytic, 22,000 uF, 50V	027-2200	1
J4 ·	Connector, 24-Pin (Interlock)	417-0009	1
L100	Choke, Reactor, 0.0005 H @ 40A dc, 0.0066 Ohm	377-0001	1
S102	Door Interlock Switch, SPDT, 15A @ 125 or 250V ac, 0.5A @ 125V dc, 0.25A @ 250V dc	346-3302	1
T100	Driver Transformer:	378-0001	¹¹ 1
T101	PRIMARY: 3Ø, 60 Hz, Delta connected, 208/240 ±11V SECONDARY: Wye connected, 14.8V ac, 32.6A Isolation Transformer, 1000 VA PRIMARY: 115/230, Single Phase DUAL SECONDARY: 115V, 4.35A	371-0003	1
TB1,TB3	Barrier Strip, Screw Terminal	412-0724	15
1019103	End Caps for TB1 and TB3	412-0730	2
	RF Driver Cabinet Control Panel	924-0006	1
		924-0007	1
	Assembly, IPA	959-0069	1
	Assembly, Power Supply and Battery Charger		1
	Assembly, Resistor and Lugs	955-0037	1
	Exciter ac Control	955-0020	1 1 2 1
	Automatic Power Control Assembly	959-0023	1
	Assembly, IPA Directional Coupler	959-0050	1
	Slide Rails for Microprocessor Drawer	489-0001	Z
	Cable Assembly, RF Driver	947-0003	1
	Cable Assembly, RF Driver	947-0004	1
	Cable Assembly, RF Driver	947-0005	1
	Cable Assembly, RF Driver	947-0006	1
	Cable Assembly, RF Driver	947-0007	1
	Rack Mounting Hardware Kit for exciter	961-0003	1
	Cable Assembly, RF Driver	947-0008	1
	Cable Assembly, RF Driver	947-0009	1
	Cable Assembly, RF Driver	947-0010	1
	Cable Assembly, RF Driver	947-0011	1
	Cable Assembly, RF Driver	947-0012	1
	Cable Assembly, RF Driver	947-0013	1
	Cable Assembly, RF Driver	947-0014	1
	Cable Assembly, RF Driver	947-0015	1
	Cable Assembly, Directional Coupler to PA Grid	947-0016	1
	Cable Assembly, RF Driver	947-0020	ĩ
	Cable Assembly, RF Driver	947-0021	ī

6-13B

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Cable Assembly, RF Driver Cable Assembly, RF Driver Cabinet Metering Cable Assembly, Microprocessor Power Input Cable Assembly, Driver Cabinet ac Power	947-0022 947-0030 947-0091 947-0026	1 1 1 1
	Table 6-26. Cable Assembly, RF Driver - 947-0014	THRU 947-0005 THRU 947-0015 THRU 947-0022	

Table 6-25.	FM-30 Driver	• Cabinet - 909-2000	(Sheet 2 of 2)
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 PART NO.
 QTY.

 --- BNC Connector for RG/58 cable
 917-0205
 2

Table 6-27. Cable Assembly, RF Driver - 947-0006 THRU 947-0012

REF. DES.	DESCRIPTION	PART NO.	QTY.
	BNC Connector for RG/58 cable	417-0205	2

Table 6-28. Cable Assembly, RF Driver - 947-0013

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Type N Connector for RG/8 cable Adapter, BNC plug to Type N Jack, UG-349 A/U Adapter, Right angle Type N plug jack, UG27C/U	417-0102 417-0103 417-0105	2 1 1

Table 6-29. Cable Assembly, Directional Coupler to PA Grid - 947-0016

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Type N Connector for RG/8 cable	418-0102	2

REF. DES.	DESCRIPTION	PART NO.	QTY.
D109,D110 XK104, XK105	Diode, 1N4005, Silicon, 1 Ampere, 600V Socket, Relay	203-4005 270-0015	2 2
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Table 6-29A. Cable Assembly, Driver Cabinet ac Power - 947-0026

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REF. DES.	DESCRIPTION	PART NO.	QTY.
S100	Switch, Modified, Rotary, 1-Pole, 2-12 positions, 2.75A, 15V dc, 230 mA, 115V ac (MODULE VOLTAGE)		1
S101	Switch, Modified, Rotary, 2-Pole, 2-12 positions, 2.75A, 15V dc, 230 mA, 115V ac (MODULE CURRENT)		1

Table 6-30. Cable Assembly, RF Driver Cabinet Metering - 947-0030

Table 6-31. Cable Assembly, Microprocessor Power Input - 947-0091

REF. DES.	DESCRIPTION	PART NO.	QTY.
	BNC Connector, RF, UG10-94/U, for RG316/U cable	417-0015	3
	Connector, 24-Pin	417-0009	1

Table 6-32. IPA Assembly - 924-0007 (Sheet 1 of 2)			
REF. DES.	DESCRIPTION	PART NO.	QTY.
CB100	Circuit Breaker, 3 Pole, 15 Ampere, 600V ac, modified (POWER SUPPLY circuit breaker)	341-0002-1	1
CB101 THRU CB105	Circuit Breaker, Single Pole, 10 Ampere, 28V dc (28V MODULE () circuit breakers)	341-0004	5
D103 THRU D105	Diode, Silicon, S3620, 200 PIV, 70 Amperes, Stud Mount	237-0001	3
D106 THRU D108	Diode, Silicon, R3620, 200 PIV, 70 Amperes, Reverse Polarity, Stud Mount	237-0002	3
K100,K101	Relay, Solid State 120 D10, 120V ac @ 10 Amperes, 2500V Isolation, Control: 3-32V dc @ 5.0 mA	270-0002	2
M100	<pre>Meter, 2.5 inch (6.35 cm) Taut Baud Type, FS =</pre>	317-0004	1
M101	Meter, 2.5 inch (6.35 cm) Taut Baud Type, FS = 1 mA, 150 Ohm movement (MODULE CURRENT meter)	317-0005	1
TB2	Barrier Strip, 2 Terminals	412-0002	1
	Meter Shunt Board	955-0031	1 5 1
	28V Regulator	917-0021	5
	Assembly, Power Supply, IPA VSWR	955-0003	1
	RF Amplifier Module, FM	917-0004	5
	Input Hybrid Assembly	955-0011	1
	Output Hybrid No. 1 Assembly	955-0018 955-0016	
	Output Hybrid No. 2 Assembly	955-0018 955-0012	1 1
una, ann ain an an	Output Hybrid No. 3 Assembly Capacitor Tubing and Lugs Assembly	955-0012	2

6-16

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Metal Oxide Varistor Tubing and Lugs Assembly Knob, Black (for MODULE VOLTAGE and MODULE CURRENT Switches)	955-0035 482-0009	3 2
	Diode Bracket Insulator, 0.005 inch (0.013 cm) Kapton	907-0957	1

Table 6-32. IPA Assembly - 924-0007 (Sheet 2 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1	Capacitor, Variable Compression, Mica, 15-115 pF, 250V	099-4006	1
C2 C3,C4 C5	Capacitor, Mica, 1000 pF ±10%, 350V Capacitor, Mica, 80 pF ±10%, 350V Capacitor, Variable Compression, Mica, 6-300 pF, 250V	046-0002 046-0003 099-4207	1 2 1
C6,C7 C8,C9 C10,C11 C12 C13 C14	Capacitor, Mica, 1000 pF ±10%, 350V Capacitor, Mica, 100 pF ±10%, 350V Capacitor, Tantalum Dipped, 4.7 uF ±10%, 35V Capacitor, Mica, 100 pF ±10%, 350V Capacitor, Mica, 1000 pF ±10%, 350V Capacitor, Variable Compression, Mica, 15-115 pF, 250V	046-0002 046-0001 064-4763 046-0001 046-0002 099-4006	2 2 1 1 1
C15 J1,J2 L1 THRU L4 L5,L6	Capacitor, Mica, 80 pF ±10%, 350V BNC Connector	046-0003 417-0014 364-0001 640-1800	1 2 4 2
Q1,Q2	Transistor, RF Output, Silicon, BM100-28, 100W, 175 MHz, CTC Company Case SS	213-0001	2
R1,R2	Resistor, 16 Ohm ±10%, 3W, Non-Inductive, Flashed Ends	100-1622	2
	Blank Circuit Board	517-0004	1

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Table 6-33. RF Amplifier Module (FM) - 917-0004

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Table 6-34.	Output	Hybrid No	o. 1 -	955-0018
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C104 J9,J10,J11 R109	Capacitor, Mica, 1 pF, 500V BNC Connector Resistor, 50 Ohm ±5%, Thin Film RF Termination, 150W, Non-Inductive	042-5025 417-0203 131-5027	1 3 1
	Diode Detector Circuit Board Assembly	917-0009	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 D1 R1 THRU R3 	Capacitor, Ceramic Disc, 0.005 uF, 50V Diode, HP5082-2800, High Voltage, Schottky Barrier Type, 70V, 15 mA Resistor, 15 k Ohm ±5%, 1/4W Blank Circuit Board	000-5034 201-2800 100-1553 517-0009	1 1 3 1

Table 6-35. Diode Detector Assembly - 917-0009

Table 6-36. Output Hybrid No. 2 - 955-0016

REF. DES.	DESCRIPTION	PART NO.	QTY.
C102 J11A,J12, J13	Capacitor, Mica, 1 pF, 500V BNC Connector	042-5025 417-0203	1 3
R106	Resistor, 50 Ohm ±5%, Thin Film RF Termination, 150W, Non-Inductive	131-5027	1
·	Diode Detector Circuit Board Assembly	917-0009	1

Table 6-37. Output Hybrid No. 3 - 955-0012

REF. DES.	DESCRIPTION	PART NO.	QTY.
C100 J7,J8,J12A R103	Capacitor, Mica, 1 pF, 500V BNC Connector Resistor, 50 Ohm ±5%, Thin Film RF Termination, 150W, Non-Inductive Diode Detector Circuit Board Assembly	042-5025 417-0203 131-5027 917-0009	1 3 1 1

Table 6-38. Input Hybrid Assembly - 955-0011

REF. DES.	DESCRIPTION	PART NO.	QTY.
J2 THRU J6 R100 THRU R102	BNC Connectors Resistor, 50 Ohm ±5%, Thin Film RF Termination, 150W, Non-Inductive	417-0206 131-5027	5 3

Table 6-39. Assembly, Power Supply, IPA Analog Divider - 955-0003

REF. DES.	DESCRIPTION	PART NO.	QTY.
T1	Transformer: Control/Rectifier Primary: 117V, 50/60 Hz Three Secondaries: 12V (one Center Tapped),	378-0002	1
	IPA VSWR Power Supply Circuit Board Assembly	917-0012	1

Table 6-40. IPA Analog Divider Power Supply Assembly - 917-0012

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 C2 D1 D2 THRU D4 D5 R1 R2 R3 R4 R5 R6 U1	Capacitor, Tantalum Dipped, 33 uF, 35V Capacitor, Tantalum Dipped, 100 uF, 20V Bridge Rectifier, Silicon, MDA 101A, 1.0A, 100V Diode, 1N4004, Silicon, 1.0A, 400V Diode, Zener, 1N4733, 5.1V, 1W Potentiometer, 2 k Ohm ±10%, 1/2W Potentiometer, 500 Ohm ±10%, 1/2W Resistor, 560 Ohm ±5%, 1/4W Resistor, 120 Ohm ±5%, 1/4W Resistor, 1.2 k Ohm ±5%, 1/4W Resistor, 10 k Ohm ±5%, 1/4W Voltage Regulator, LM317T, Positive 3 Terminal, Adjustable, 1.2V to 37V, TO-220 Case Blank Circuit Board	064-3373 063-1083 239-0005 203-4004 200-4733 177-2044 177-5032 100-5633 100-1233 110-1243 100-1053 227-0317 517-0012	1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

Table 6-41.	287	Regulator	-	917-0021
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(Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	Q⊤Y.
C1	Capacitor, Ceramic Disc, 0.005 uF, +80%, -20%, 50V	000-5034	1
C2,C3 C4	Capacitor, Mylar Film, 0.1 uF, 100V Capacitor, Ceramic Disc, 0.005 uF, +80%, -20%, 50V	030-1053 000-5034	2 1
C5 C6	Capacitor, Mylar Film, 0.1 uF, 100V Capacitor, Ceramic Disc, 0.005 uF, +80%, -20%, 50V	030-1053 000-5034	1 1
C7 C8 C9,C10	Capacitor, Electrolytic, 330 uF, 63V Capacitor, Electrolytic, 100 uF, 64V Capacitor, Electrolytic, Tantalum Dipped, 1 uF ±10%, 35V	015-3383 015-1084 064-1063	1 1 2
D1 THRU D3		203-4148	3

j .,	Table 6-41. 28V Regulator - 917-0021 (S	heet 2 of 2)	
REF. DES.	DESCRIPTION	PART NO.	QTY.
D4 D5 L1,L2,L3	Diode, Zener, 1N4746, 18V ±10%, 1W Diode, Power Rectifier, MR506, 3A, 600V Wire, Enameled 18 gauge, 18 inches (45.72 cm)	200-4746 203-0506 640-1800	1 1 3
L1,L2,L3 Q1 Q2 Q3 THRU Q5 R1 R2 R3 R4 R5 R6 R7 R8 R9 R10,R11 R12 R13 R14 R15 R16 R17 R18 R19,R20 R21 THRU R23 U1 U2 XQ2 XQ3 THRU XQ2 XQ3 THRU XQ2 XQ3 THRU XQ2 XQ3 THRU R23 U1	each Transistor, 40319, Silicon, PNP, TO-5 Case Transistor, 2N3054, Silicon, NPN, TO-66 Case	640-1800 211-4032 211-3054 219-3055 100-1553 120-3023 100-1553 100-1563 100-4743 100-3653 100-6853 178-1044 100-1063 100-9143 130-1043 178-1044 100-1043 178-1044 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2243 100-2350 221-3900 227-0350 417-0012 417-0298 418-0010 407-0100 409-0005 517-0021	3 1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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RÉF. DES.	DESCRIPTION	PART NO.	QTY.
	Meter, Shunt, O-50 mV	316-0003	5
	Blank Meter Shunt Circuit Board	467-0034	1

Table 6-42. Meter Shunt Board - 955-0031

Table 6-43. Metal Oxide Varistor Assembly - 955-0035

REF. DES.	DESCRIPTION	PART NO.	QTY.
MOV100, MOV101	Metal Oxide Varistor, V130LA10A, 130V ac RMS, 10 Joules	140-0006	2

Table 6-44. RF Driver Cabinet Control Panel - 924-0006 (Sh	Table 6-44.	RF Driver	Cabinet	Control	Panel -	924-0006	(Shee
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heet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C3 DS1,DS3, DS5	Capacitor, Electrolytic, 100 uF +10%, +50%, 25V Lamp, No. 327, 28V, 40 mA	013-1084 321-0327	1 3
J1 THRU J3 M1	Connector, 25-Pin Meter, 3.5 inches (8.89 cm), Taut Baud Type, FS= 200 uA dc, 208 Ohm movement (DRIVER meter)	418-3219 310-0003-2	3 1
S1 THRU S5		343-0003	5
S6	Switch, Modified, Rotary, 1-Pole, 1 Section, 6 Position, 1.5A @ 28V dc, 230 mA @ 115V ac, Resistive Load (DRIVER switch)	344-1564-1	1
S7	Switch, Miniature, Push, SPST, Normally Open, 1/2A @ 125V ac (RESET switch)	340-0043	1
TB1,TB2	Barrier Strip, 3 Terminal	412-0003	2
	Knob, Black with clear skirt (for DRIVER switch)	344-1564	
	Processor Circuit Board Assembly	917-0003	1 1 1 1
	Output Circuit Board Assembly	919-0013	1
	Control/Timer Circuit Board Assembly	917-0006	1
	Input Board 1 Circuit Board Assembly	919-0030	
	Remote Control Interface Circuit Board Assembly	919-0003	1
	Input Board 2 Circuit Board Assembly	919-0054	1 1
	Meter Circuit Board Assembly	917-0020	
	Primary Function Indicator Circuit Board Assembly	917-0027	1
	Patch Panel Circuit Board Assembly	917-0029	1
	Decoder/Driver/Dual Seven Segment Solid State Display	323-0001	î

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Lens, Yellow (for OVERLOAD switch) Lens, Green (for HIGH VOLTAGE ON and FILAMENT ON switches)	343-0004 343-0006	1 2
	Lens, Red (for HIGH VOLTAGE OFF and FILAMENT OFF switches)	343-0007	2
	Microprocessor Controller Wiring Harness	947-0025	1
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Table 6-44. RF Driver Cabinet Control Panel - 924-0006 (Sheet 2 of 2)

Table 6-45. Processor Circuit Board Assembly - 917-0003

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1	Capacitor, Ceramic Disc, 0.001 uF, 1000V	002-1034	1
C2	Capacitor, Mica, 120 pF, 500V	042-1222	1
СЗ	Capacitor, Electrolytic, 10 uF, 16V	013-1074	1
C4	Capacitor, Ceramic Disc, 0.01 uF, 500V	001-1044	1
D1 THRU	Diode, Silicon, 1N4148, 75V @ 0.3 Ampere,	203-4148	10
D10	Fast Switching		
J1	Connector, 12-Pin	417-1276	1
J2	Connector, 4-Pin	418-0255	1
J3	Connector, 12-Pin	417-1276	1
L1	Inductor, 0.68 uH $\pm 10\%$, 700V maximum	364-0068	1 1 2 1 1
R1,R2	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	2
R3	Resistor, 2.2 k Ohm $\pm 5\%$, $1/4W$	100-2243	1
R4	Resistor, 470 k Ohm ±5%, 1/4W	100-4763	1
U1	Integrated Circuit, CMOS, MC14013B, Dual D Flip-	228-4013	1
U2	Flop, 14-Pin DIP Integrated Circuit, 2758, UV Erasable 8K Read	228-2758-1	1
	Only Memory, TTL compatable, 24-Pin DIP (programmed EPROM labeled TN2176)		
U3	Integrated Circuit, CMOS, MC14028B, BCD-to- Decimal Decoder, 16-Pin DIP	228-4028	1
U 4	Integrated Circuit, CMOS, MC14049UB, Hex- inverter/Buffer, 16-Pin DIP	228-4049	1
U5	Integrated Circuit, TTL, SN7432N, Quad 2-Input Positive OR Gate, Logic, 14-Pin DIP	228-7432	1
U6	Integrated Circuit, CMOS, MC14500B, Industrial Control Unit, 16-Pin DIP	228-4500	1
U7 , U8	Integrated Circuit, CMOS, MC14516B, Binary UP/ DOWN Counter, 16-Pin DIP	228-4516	2
XU1	Socket, 14-Pin	417-1400	1
XU2	Socket, 24-Pin	417-2400	1
XU3,XU4	Socket, 16-Pin	417-1601	2
XU5	Socket, 14-Pin	417-1400	1 2 1 3
XU6 THRU	Socket, 16-Pin	417-1601	3
XU8	SOURCE, IN-FILL	.17 1001	Ŭ
	Blank Circuit Board	517-0003	1

Table 6-46.	Output	Circuit	Board	Assembly	_	919-0013
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REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 THRU C3 C4,C5 C6 THRU C8 C9,C10 C11 THRU C20	Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Ceramic Disc, 0.1 uF, 10V Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Ceramic Disc, 0.1 uF, 10V Capacitor, Mica, 390 pF ±5%, 100V	042-3922 000-1055 042-3922 000-1055 042-3922	3 2 3 2 10
D1 D2 J1 THRU J3 L1 THRU L7	Diode, Zener, 1N4733A, 5.1V ±5%, 1W Diode, Silicon, 1N4005, 600V @ 1 Ampere Connector, 12-Pin Molded Inductor, 2.2 uH ±10%, Resistance: 0.19 Ohm, 1.1 Ampere Maximum	200-4733 203-4005 417-1276 364-2200	1 1 3 7
Q1 THRU Q5 Q6 THRU	Transistor, Silicon, 2N3904, NPN, TO-92 Case Transistor, Silicon, MPSA56, PNP, TO-92 Case	211-3904 210-0056	5 5
010 011 012 R1 THRU R10	Transistor, Silicon, 2N3904, NPN, TO-92 Case Transistor, Silicon, MPSA56, PNP, TO-92 Case Resistor, 10 k Ohm ±5%, 1/4W	211-3904 210-0056 100-1053	1 1 10
R11 THRU	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	14
R24 R25 THRU	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	4
R28 R29 THRU	Resistor, 150 Ohm ±5%, 1/4W	100-1533	4
R32 R33 R34 U1	Resistor, 10 k Ohm ±5%, 1/4W Resistor, 470 Ohm ±5%, 2W Integrated Circuit, CMOS, MC14073B, Tripple	100-1053 130-4733 228-4073	1 1 1
U2,U3	3-Input AND Gate, 14-Pin DIP Integrated Circuit, CMOS, MC14599B, 8-bit Addressable latch, Bidirectional Data Port,	228-4599	2
U4	18-Pin DIP Integrated Circuit, 2758, UV Erasable 8K Read Only Memory, TTL compatable, 24-Pin DIP (Programmed EPROM labeled XMTR-3)	228-2758-2	1
XU1 XU2,XU3 XU4	Socket, 14-Pin Socket, 18-Pin Socket, 24-Pin	417-1400 417-1804 417-2400	1 2 1

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 THRU C3	Capacitor, Mica, 100 pF, 50V	040-1022	3
C4,C5	Capacitor, Mica, 390 pF ±5%, 100V	042-3922	2
C6 THRU	Capacitor, Electrolytic, 10 uF, 35V	023-1076	5
C10	capacitor, Electrolytic, to ur, 550	023-1070	5
C11 THRU C16	Capacitor, Ceramic Disc, 0.1 uF, 10V	000-1055	5
C17	Capacitor, Mica, 390 pF ±5%, 100V	042-3922	1
C18 THRU	Capacitor, Ceramic Disc, 0.1 uF, 10V	000-1055	3
C20	· • • • • • • • • • • • • • • • • • • •	000 1000	Ŭ
D1 THRU D4	Diode, Silicon, 1N4148, 75V @ 0.3 Ampere Fast Switching	203-4148	4
D5	Diode, Zener, 1N4733A, 5.1V ±5%, 1W	200-4733	1
J1	Connector, 12-Pin	417-1276	1
J2	Connector, 4-Pin	418-0255	1
J3	Connector, 12-Pin	417-1276	1 1 1
L1	Molded Inductor, 2.2 uH $\pm 10\%$, Resistance: 0.19	364-2200	1
L I	Ohm, 1.1 Ampere Maximum	004-2200	-
R1	Resistor, 180 k Ohm $\pm 5\%$, $1/4W$	100-1863	1
R2	Resistor, 91 k Ohm $\pm 5\%$, 1/4W	100-9153	-
		110-6823	1
R3	Resistor, 68 Ohm $\pm 5\%$, $1/2W$		1
R4	Resistor, 180 k Ohm $\pm 5\%$, 1/4W	100-1863	L L
R5	Resistor, 15 k Ohm $\pm 5\%$, $1/4W$	100-1553	L
R6,R7	Resistor, 68 Ohm ±5%, 1/2W	110-6823	2
R8	Resistor, 180 k Ohm ±5%, 1/4W	100-1863	1 1 2 1 3
R9	Resistor, 91 k Ohm $\pm 5\%$, $1/4W$	100-9153	1
R10 THRU	Resistor, 100 k Ohm ±5%, 1/4W	100-1063	3
R12		100 1042	2
R13,R14	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	2
R15,R16	Resistor, 100 k Ohm $\pm 5\%$, 1/4W	100-1063	2
R17	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	2 2 1 1 3
R18	Resistor, 100 k Ohm ±5%, 1/4W	100-1063	1
R19	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	1
R20 THRU R22	Resistor, 1.5 k Ohm $\pm 5\%$, 1/2W	110-1543	3
R23,R24	Resistor, 100 k Ohm ±5%, 1/4W	100-1063	2
U1 THRU U3	Integrated Circuit, CMOS, MC14521B, 24-Stage	228-4521	2 3
	CMOS Frequency Divider, 16-Pin DIP	000 4500	4
U4	Integrated Circuit, CMOS, MC14599B, 8-bit Addressable latch, Bidirectional Data Port, 18-Pin DIP	228-4599	1
U5	Integrated Circuit, CMOS, MC14512B, 8 Channel	228-4512	1
U6	Data Selector, 16-Pin DIP Integrated Circuit, CMOS, MC14049UB,	228-4070	1
	Hex Inverter, 14-Pin DIP		
U7,U8	Integrated Circuit, CMOS, 74COON, Quad 2-Input	221-7400	2
U9	NAND Gate, 14-Pin DIP Integrated Circuit, ULN2003A, 7-Channel Driver, CMOS/TTL Compatable, 16-Pin DIP	229-2003	1

Table 6-47. Control/Timer Circuit Board Assembly - 917-0006 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
U10	Integrated Circuit, CMOS, MC14023B, Triple 3- Input NAND Gate, 14-Pin DIP	228-4023	1
XU1 THRU XU3	Socket, 16-Pin	417-1601	3
XU4	Socket, 18-Pin	417-1804	1 1
XU5	Socket, 16-Pin	417-1601	1
XU6 THRU XU8	Socket, 14-Pin	417-1400	3
XU9	Socket, 16-Pin	417-1601	1
XU10	Socket, 14-Pin	417-1400	1
	Blank Circuit Board	517-0006	1

Table 6-47. Control/Timer Circuit Board Assembly - 917-0006 (Sheet 2 of 2)

Table 6-4	8. Input Board 1 Circuit Board Assembly - 919-0030)(Sheet 1	of 3)
REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 C2 THRU C9 C10,C11 C12 THRU C18	Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V	023-1084 042-3922 023-1084 042-3922	1 8 2 7
C19,C20 D1 THRU D3 D5 THRU D8		023-1074 200-4733	2 7
D9 D10 THRU D15	Diode, Silicon, 1N4004, 400V @ 1 Ampere Diode, Zener, 1N4733A, 5.1V $\pm 5\%$, 1W	203-4004 200-4733	1 6
D16	Diode, Silicon, 1N4148, 75V @ 0.3 Ampere, Fast Switching	203-4148	1
J1 THRU J3 R1 THRU R7 R8 R9 R12,R13 R14 R15 R16 R17 R18 R19 R20 R21 R22 R22 R23	Resistor, 10 k Ohm $\pm 5\%$, 1/4W Resistor, 20 k Ohm $\pm 5\%$, 1/4W Resistor, 100 Ohm $\pm 5\%$, 1/4W Potentiometer, 1 k Ohm $\pm 10\%$, 1/2W Resistor, 27 k Ohm $\pm 5\%$, 1/4W Potentiometer, 200 Ohm $\pm 10\%$, 1/2W Resistor, 1 k Ohm $\pm 5\%$, 1/4W Resistor, 22 Ohm $\pm 5\%$, 1/4W Resistor, 1 k Ohm $\pm 5\%$, 1/4W	417-1276 100-1053 100-2053 100-1033 177-2044 100-2753 177-2034 100-1043 100-1043 100-1043 100-1043 100-1043 100-6833 100-1043 100-2233	3 7 1 2 1 1 1 1 1 1 1 1
R24 R25	Resistor, 1 k Ohm ±5%, 1/4W Resistor, 510 Ohm ±5%, 1/4W	100-1043 100-7533	1 1

Table 6	-48. Input Board 1 Circuit Board Assembly - 919-00	30 (Sheet	2 of 3
REF. DES.	DESCRIPTION	PART NO.	QTY.
R26	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	1
R27	Resistor, 680 Ohm $\pm 5\%$, 1/4W	100-6833	1
R28	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	1
R29			
	Resistor, 100 0hm $\pm 5\%$, 1/4W	100-1033	
R30	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1 1
R31	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
R32	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	1
R33	Resistor, 1 Meg Ohm ±5%, 1/4W	100-1073	1
R34	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R35	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	
R36	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R37	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	
R38			
	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	
R39	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	
R40	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R41	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
.R42	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R43	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
R44	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	1
R45 THRU	Resistor, 10 Meg Ohm $\pm 5\%$, 1/4W	100-1083	7
R51			
R52 THRU R64	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	13
R65	Potentiometer, 500 Ohm $\pm 10\%$, $1/2W$	177-5032	1
R66	Resistor, 12 k Ohm ±5%, 1/4W	100-1253	
R67	Resistor, 1 k Ohm $\pm 5\%$, $1/4W$	100-1043	Î Î
R68	Resistor, 2.7 k Ohm $\pm 5\%$, 1/4W	100-2743	ī
R69	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	1
R70	Resistor, 620 Ohm $\pm 5\%$, 1/4W	100-6233	1
			1
R71	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	1
R72	Resistor, 680 Ohm $\pm 5\%$, $1/4W$	100-6833	1 1 1 1 1 1 1
R73	Resistor, 1 k Ohm $\pm 5\%$, $1/4W$	100-1043	1
R74	Resistor, 680 Ohm ±5%, 1/4W	100-6833	1
R75	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	1
R76	Resistor, 680 Ohm ±5%, 1/4W	100-6833	1
R77	Resistor, 1 k Ohm $\pm 5\%$, $1/4W$	100-1043	1
R78	Resistor, 150 Ohm $\pm 5\%$, $1/4W$	100-1533	1
R79	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R80	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
R81	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R82	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
R83	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R84	Resistor, 1 Meg Ohm ±5%, 1/4W	100-1073	1
R85	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	1
R86	Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1073	1
R87	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R88	Resistor, 1 Meg Ohm $\pm 5\%$, $1/4W$	100-1073	1
R89	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	1
103	NESISCOI, IO N UNIN 100, 1/4W	100-1002	1

n ь1 Table 6-18 Innut Boand <u>.</u> л ь 010 0000

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	to. Input board I officult board Assembly - 515-00		01 0/
REF. DES.	DESCRIPTION	PART NO.	QTY.
R90 R91 THRU R96	Resistor, 1 Meg Ohm ±5%, 1/4W Resistor, 10 Meg Ohm ±5%, 1/4W	100-1073 100-1083	1 6
R97 THRU R102	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	6
R102 R103 R104 THRU R107	Resistor, 100 k Ohm ±5%, 1/4W Resistor, 18 k Ohm ±5%, 1/4W	100-1063 100-1853	1 4
R108 R109 R110	Resistor, 10 k Ohm ±5%, 1/4W Resistor, 47 k Ohm ±5%, 1/4W Resistor, 100 k Ohm ±5%, 1/4W	100-1053 100-4753 100-1063	1 1 1 4
U1 THRU U4	Integrated Circuit, LM339AN, Quad Voltage Comparator, 14-Pin DIP	221-0339	4
U5	Integrated Circuit, MC14049UB, CMOS, Inverting Hex Buffer, 16-Pin DIP	228-4049	1
U6	Integrated Circuit, SN74147N, 10 line-to-4 line priority Encoder, 16-Pin DIP	228-4147	1
U7,U8	Integrated Circuit, CMOS, MC14013B, Dual-D Flip-Flop, 14-Pin DIP	228-4013	2
U9	Integrated Circuit, CMOS, MC14512B, 8 Channel Data Selector, 16-Pin DIP	228-4512	1
U10	Integrated Circuit, CMOS, MC14023B, 3-Input NAND Gate, 14-Pin DIP	228-4023	1
XU1 THRU XU4	Socket, 14-Pin	417-1404	4
XU5,XU6 XU7,XU8	Socket, 16-Pin Socket, 14-Pin	417-1604 417-1404	2
XU9 XU10	Socket, 16-Pin Socket, 14-Pin Blank Circuit Board	417-1604 417-1404 519-0030	2 2 1 1 1
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Table 6-48.	Input Board 1	Circuit Board	Assembly -	- 919-0030	(Sheet 3	of 3)
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Table 6-49. Input Board 2 Circuit Board Assembly - 919-

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 C2_THRU	Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V	023-1084 042-3922	1 14
C15 D1 THRU D7 D8 D9 THRU D14	Diode, Zener, 1N4733A, 5.1V ±5%, 1W Diode, Silicon, 1N4004, 400V @ 1 Ampere Diode, Zener, 1N4733A, 5.1V ±5%, 1W	200-4733 203-4004 200-4733	7 1 6
D14 D15	Diode, Silicon, 1N4148, 75V @ 0.3 Ampere	203-4148	1
J1 THRU J3	Fast Switching Connector, 12-Pin	417-1276	3

J4, J5Connector, 3-Pin417-0003J6Connector, 12-Pin417-0412J7Connector, 18-Pin417-0412L1Molded Inductor, 2.2 uH ±10%, Resistance: $364-2200$ 0.19 Ohm, 1.1 Ampere Maximum100-1053R8Resistor, 10 k Ohm ±5%, 1/4W100-1053R9THRU R1Resistor, 1 k Ohm ±5%, 1/4W100-4753R12,R13Resistor, 1 k Ohm ±5%, 1/4W100-1043R12,R13Resistor, 100 Ohm ±5%, 1/4W100-1043R16Resistor, 100 Ohm ±5%, 1/4W100-1043R17Resistor, 1 k Ohm ±5%, 1/4W100-1043R18Resistor, 1.2 k Ohm ±5%, 1/4W100-1043R20Resistor, 1.2 k Ohm ±5%, 1/4W100-1043R20Resistor, 1.2 k Ohm ±5%, 1/4W100-1043R20Resistor, 1.2 k Ohm ±5%, 1/4W100-1043R21Resistor, 1.2 k Ohm ±5%, 1/4W100-1043R22Resistor, 1 k Ohm ±5%, 1/4W100-1043R23THRUResistor, 1 k Ohm ±5%, 1/4W100-1043R24Resistor, 1 k Ohm ±5%, 1/4W100-1053R34R35THRUResistor, 1 0 k Ohm ±5%, 1/4W100-1053R44R65Resistor, 1 0 k Ohm ±5%, 1/4W100-1053R44R65Resistor, 1 0 k Ohm ±5%, 1/4W100-1053R44R65R64THRUResistor, 1 0 k Ohm ±5%, 1/4W100-1053R44R65Resistor, 1 k Ohm ±5%, 1/4W100-1053R64R68Potentiometer, 200 Ohm ±5%, 1/4W100-1043R70R68Potentiomete	QTY.
J6Connector, $12-Pin$ $417-0412$ J7Connector, $18-Pin$ $417-1800$ L1Molded Inductor, 2.2 uH ±10%, Resistance: $364-2200$ 0.19 Ohm, 1.1 Ampere Maximum $100-1053$ R8Resistor, 10 k Ohm ±5%, $1/4W$ $100-1053$ R9 THRU R11Resistor, 47 k Ohm ±5%, $1/4W$ $100-4753$ R14Resistor, 100 Ohm ±5%, $1/4W$ $100-1033$ R15Resistor, 100 Ohm ±5%, $1/4W$ $100-1033$ R16Resistor, 100 Ohm ±5%, $1/4W$ $100-1033$ R17Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R18Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R20Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R21Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R22Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R23THRUResistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R24Resistor, 1.2 k Ohm ±5%, $1/4W$ $100-1043$ R25Resistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R26Resistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R27Resistor, 1 Meg Ohm ±5%, $1/4W$ $100-1073$ R41R42THRUResistor, 1 Meg Ohm ±5%, $1/4W$ $100-1043$ R43R49THRUResistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R44Resistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R45R45 $1/4W$ $100-1043$ R46Resistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R47Resistor, 1 k Ohm ±5%, $1/4W$ $100-1043$ R68Potentiometer,	
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L1Molded Inductor, 2.2 uH ±10%, Resistance: 0.19 Ohm, 1.1 Ampere Maximum $364-2200$ R1 THRU R7Resistor, 10 k Ohm ±5%, 1/4W100-1053R8Resistor, 1 k Ohm ±5%, 1/4W100-4753R9 THRU R11Resistor, 47 k Ohm ±5%, 1/4W100-1043R12,R13Resistor, 47 k Ohm ±5%, 1/4W100-1043R14Resistor, 100 Ohm ±5%, 1/4W100-1033R15Resistor, 1 k Ohm ±5%, 1/4W100-1043R16Resistor, 100 Ohm ±5%, 1/4W100-1043R17Resistor, 1 k Ohm ±5%, 1/4W100-1043R18Resistor, 1 k Ohm ±5%, 1/4W100-1043R19Resistor, 1 k Ohm ±5%, 1/4W100-1043R20Resistor, 1 k Ohm ±5%, 1/4W100-1043R21Resistor, 1 k Ohm ±5%, 1/4W100-1043R22Resistor, 1 k Ohm ±5%, 1/4W100-1043R23THRUResistor, 1 k Ohm ±5%, 1/4W100-1043R24R25R64THRUResistor, 1 k Ohm ±5%, 1/4WR25THRUResistor, 1 N Ohm ±5%, 1/4W100-1053R34R35THRUResistor, 10 k Ohm ±5%, 1/4W100-1053R61R62Resistor, 10 k Ohm ±5%, 1/4W100-1043R63Resistor, 1 k Ohm ±5%, 1/4W100-1043R64R64Potentiometer, 200 Ohm ±10%, 1/2W177-2034R66R66Potentiometer, 200 Ohm ±10%, 1/2W177-2034R70Resistor, 1.5 k Ohm ±5%, 1/4W100-1043R71Resistor, 1.5 k Ohm ±5%, 1/4W100-1043R74Resistor, 1.5 k Ohm ±5%, 1/4W100-1043<	2 1 1 1
0.19 Ohm, 1.1 Ampere Maximum0.10101R1 THRU R7Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R8Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R9 THRU R11Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R12,R13Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1043R14Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1033R15Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 12 k Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R24R25Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R25R26Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R27R28Resistor, 1 O k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1083R44R42THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R62Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R64R64R64Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/4W100-1043R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R71Re	1
R8Resistor, 47 k Ohm $\pm 5\%$, 1/4W100-4753R9 THRU R11Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R12,R13Resistor, 47 k Ohm $\pm 5\%$, 1/4W100-1043R14Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1033R15Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R19Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R24Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R25THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R26Resistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1073R34R35THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1073R41R63Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R64R64Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043R71Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043R72R63Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043R64R69Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W <t< td=""><td>1</td></t<>	1
R9 THRU R11Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R12,R13Resistor, 47 k Ohm $\pm 5\%$, $1/4W$ 100-4753R14Resistor, 100 Ohm $\pm 5\%$, $1/4W$ 100-1033R15Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R16Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R17Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R18Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R19Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R20Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R21Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R22Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R24R25Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R25R27R28THRUResistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R27R28THRUResistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1053R34R35THRUResistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1053R48R49THRUResistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1043R63Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R66R66Potentiometer, 200 Ohm $\pm 10\%$, $1/2W$ 177-2034R69Resistor, 1.5 k Ohm $\pm 5\%$, $1/4W$ 100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, $1/4W$ 100-1043R72Resistor, 2.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043R74Resistor, 1.5 k Ohm	7
R12,R13Resistor, 47 k Ohm $\pm 5\%$, 1/4W100-4753R14Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1033R15Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R41R42THRUResistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1053R61R62Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R61R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72,R73Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	1
R14Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1033R15Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R23Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R24Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R25REsistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R26Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1083R48R49THRUResistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1043R61Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R62Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72,R73Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	3
R15Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R19Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R24Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R25THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1083R48R49THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R61Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R62Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72R73Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	2
R15Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R16Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1043R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R19Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R24Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 1 Meg Ohm $\pm 5\%$, 1/4W100-1073R41R42THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R42R49THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R61Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R62Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72R73Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243	1
R16Resistor, 100 Ohm $\pm 5\%$, 1/4W100-1033R17Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R19Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R27Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 1 Meg Ohm $\pm 5\%$, 1/4W100-1073R41R42THRUResistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1053R61Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R64Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R65Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R70Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72,R73Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	1
R17Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R18Resistor, 1.2 k 0hm $\pm 5\%$, 1/4W100-1243R19Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k 0hm $\pm 5\%$, 1/4W100-1043R21Resistor, 1.2 k 0hm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k 0hm $\pm 5\%$, 1/4W100-1043R23THRUResistor, 1.2 k 0hm $\pm 5\%$, 1/4W100-1043R24Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R25REsistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 10 k 0hm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 10 Meg 0hm $\pm 5\%$, 1/4W100-1073R41R42THRUResistor, 10 Meg 0hm $\pm 5\%$, 1/4W100-1043R61Resistor, 10 k 0hm $\pm 5\%$, 1/4W100-1043R62Resistor, 10 k 0hm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 0hm $\pm 10\%$, 1/2W177-2034R69Resistor, 100 k 0hm $\pm 5\%$, 1/4W100-1043R69Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1043R70Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1043R71Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1043R72R73Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W100-1043	l ī
R18Resistor, 1.2 k Ohm $\pm 5\%$, $1/4W$ 100-1243R19Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043R21Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1243R22Resistor, 1.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043R22Resistor, 1.2 k Ohm ± 5 , $1/4W$ 100-1043R27R28 THRUResistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1053R34R35 THRUResistor, $1 \text{ Meg Ohm } \pm 5\%$, $1/4W$ 100-1053R41R42 THRUResistor, $10 \text{ Meg Ohm } \pm 5\%$, $1/4W$ 100-1083R48R49 THRUResistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1053R61R62Resistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1053R61R62Resistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1043R63Resistor, 10 k Ohm $\pm 5\%$, $1/4W$ 100-1043R66R66Potentiometer, 200 Ohm $\pm 10\%$, $1/2W$ 177-2034R66R68Potentiometer, 200 Ohm $\pm 5\%$, $1/4W$ 100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043R71Resistor, 1.5 k Ohm $\pm 5\%$, $1/4W$ 100-1043R72,R73Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, $1/4W$ 100-1043	1 î
R19Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R20Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W100-1043R21Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k Ohm ± 5 , 1/4W100-1043R23THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R27R28THRUResistor, 1 0 k Ohm $\pm 5\%$, 1/4W100-1053R34R35THRUResistor, 1 Meg Ohm $\pm 5\%$, 1/4W100-1073R41R42THRUResistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1083R48R49THRUResistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R61R62Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 1.00 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1063R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R72,R73Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	1
R20Resistor, $1.2 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1243R21Resistor, $1 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043R22Resistor, $1.2 k ext{ 0hm } \pm 5$, $1/4W$ 100-1043R23THRUResistor, $1 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043R27R28THRUResistor, $1 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1053R34R35THRUResistor, $1 ext{ Meg 0hm } \pm 5\%$, $1/4W$ 100-1073R41R42THRUResistor, $1 ext{ Meg 0hm } \pm 5\%$, $1/4W$ 100-1083R48R49THRUResistor, $10 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1053R61R62Resistor, $1 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043R63Resistor, $22 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043R66R66Potentiometer, 200 ext{ 0hm } \pm 5\%, $1/4W$ 100-1043R66R68Potentiometer, 200 ext{ 0hm } \pm 5\%, $1/4W$ 100-1063R70Resistor, $1.2 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1063R71Resistor, $1.5 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-2243R72,R73Resistor, $1 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043R74Resistor, $2.2 k ext{ 0hm } \pm 5\%$, $1/4W$ 100-1043	7 1 3 2 1 1 1 1 1 1 1 1 5
R21Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R22Resistor, 1.2 k 0hm ± 5 , 1/4W100-1043R23THRUResistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R27R28 THRUResistor, 10 k 0hm $\pm 5\%$, 1/4W100-1053R34Rasistor, 1 Meg 0hm $\pm 5\%$, 1/4W100-1073R41R42 THRUResistor, 10 Meg 0hm $\pm 5\%$, 1/4W100-1073R41R42 THRUResistor, 10 Meg 0hm $\pm 5\%$, 1/4W100-1053R61Resistor, 10 k 0hm $\pm 5\%$, 1/4W100-1053R62Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R63Resistor, 22 k 0hm $\pm 5\%$, 1/4W100-2253R64THRUResistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R66Potentiometer, 200 0hm $\pm 10\%$, 1/2W177-2034R69Resistor, 100 k 0hm $\pm 5\%$, 1/4W100-1063R70Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-2243R71Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1043R72,R73Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W100-2243R74Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W100-2243	
R22 R23 THRU R23 THRU R27 R28 THRU R41 R42 THRU R42 THRU R42 THRU R42 THRU R42 THRU R42 THRU R43 THRU R43 THRU R44 R45 THRU R45 THRU R45 THRU R45 THRU R46 R49 THRU R66 R66 R66 R68 R68 R69 R69 R69 R69 R69 R61 R69 R61 R69 R61 R61 R62 R63 R64 THRU R64 R65 R65 R65 R65 R66 R66 R66 R66 	
R23 THRU R27 R28 THRU R34 R35 THRU R41 R42 THRU R42 THRU R42 THRU R42 THRU R42 THRU R43 THRU R43 THRU R44 R45 THRU R44 R45 THRU R45 THRU R45 THRU R45 THRU R45 THRU R46 R45 THRU R46 R46 R46 R46 R46 R46 R46 R46 R46 R46	
R27 R28 THRU R34 R35 THRU R41 R42 THRU R42 THRU R42 THRU R43 THRU R43 THRU R44 Resistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1053 100-1073 100-1083 100-1083 R48 R49 THRU R62 R62 R63 R63 R64 THRU R66 R68 R68 R68 Potentiometer, 200 Ohm $\pm 5\%$, 1/4W Resistor, 1 k Ohm $\pm 5\%$, 1/4W 100-1043 100-2253 14W 100-1043 100-1043 100-2253 14W 100-1043 100-2253 14W 100-1043 100-2253 166 R68 R68 Potentiometer, 200 Ohm $\pm 10\%$, 1/2W R69 Resistor, 1 k Ohm $\pm 5\%$, 1/4W 100-1063 R70 R70 Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W 100-1063 R70 R70 Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W 100-1043 R71 R72,R73 Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W 100-1043 R74 Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W 100-2243 100-2243	
R28 R34 R35 R34 R35 THRU R41 R42 R42 R49 R49 R61 R62 R63 R63 R63 R64 THRU R66 R68 R68 R69 R68 R69 R69 R61 R61 R62 R63 R64 THRU R65 R64 THRU R65 R64 R65 R64 R66 R68 R68 R69 R69 R61 R61 R61 R62 R63 R64 THRU R65 R64 THRU R66 R68 R68 R69 R69 Resistor, 100 k 0hm $\pm 5\%$, 1/4W R66 R68 R68 R69 Resistor, 22 k 0hm $\pm 5\%$, 1/4W R66 R68 R68 R69 Resistor, 100 k 0hm $\pm 5\%$, 1/4W R66 R68 R68 R69 Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W R66 R68 R69 Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W R60 R70 Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W R66 R71 R65 R72,R73 Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W R66 R74 R65 R74 R65 R65 R74 R65 R65 R74 R65 R74 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R74 R65 R74 R65 R74 R65 R74 R65 R74 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R74 R65 R65 R65 R74 R65 R65 R65 R65 R66 R66 R66 R66 R66 R66 R66 R66 R66 R67 R66 R67 R66 R67 R66 R67 R66 R68 R68 R68 R68 R68 R69 R66 R68 R68 R68 R68 R68 R69 R66 R68 R68 R68 R68 R68 R69 R69 R69 R60 R	5
R35 THRU R41 R42 THRUResistor, 1 Meg Ohm $\pm 5\%$, 1/4W100-1073R41 R42 THRU R48 R49 THRU R61 R62 R62 R63 R63 R63 R64 THRU R66 R68 R68 R68 Potentiometer, 200 Ohm $\pm 5\%$, 1/4W100-1033R61 R62 R64 THRU R66 R68 R68 R69 R69 R70 R70 R70 R71 R71 Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-1043 100-2243 100-2243 100-1043 100-1043 100-2243 100-2243 100-1043 100-2243 100-2243 100-1043 100-2243 100-2243	7
R42 THRU R48Resistor, 10 Meg Ohm $\pm 5\%$, 1/4W100-1083R49 R49 R49Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R61 R62 R63 R63 R64 R64 R66Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66 R68 R68 R69 R69 R70 R71 R71 R72,R73 R74Potentiometer, 200 Ohm $\pm 5\%$, 1/4W100-1063 100-1043R74Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1063 100-1043100-1063 100-1043	7
R49 THRU R61 R62Resistor, 10 k Ohm $\pm 5\%$, 1/4W100-1053R62 R63 R63 R64 THRU R66 R66 R68 R69Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66 R68 R70 R70 R71 R72,R73 R74Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R74Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1063	7
R62Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R63Resistor, 22 k Ohm $\pm 5\%$, 1/4W100-2253R64 THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 100 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1543R72,R73Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243	13
R63 R64 THRUResistor, 22 k Ohm $\pm 5\%$, 1/4W100-2253R64 THRUResistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66 R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69 R70Resistor, 100 k Ohm $\pm 5\%$, 1/4W100-1063R70 R71 R72,R73Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1543R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-1043	1
R64 THRU R66Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R66Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69Resistor, 100 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1543R72,R73Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243	1
R66 R68Potentiometer, 200 Ohm $\pm 10\%$, 1/2W177-2034R69 R70 R71 R72,R73 R74Resistor, 100 k Ohm $\pm 5\%$, 1/4W100-1063R70 R72,R73 R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243R71 R72,R73 R74Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043	1 3
R68Potentiometer, 200 0hm $\pm 10\%$, 1/2W177-2034R69Resistor, 100 k 0hm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W100-2243R71Resistor, 1.5 k 0hm $\pm 5\%$, 1/4W100-1543R72,R73Resistor, 1 k 0hm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k 0hm $\pm 5\%$, 1/4W100-2243	3
R69Resistor, 100 k Ohm $\pm 5\%$, 1/4W100-1063R70Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243R71Resistor, 1.5 k Ohm $\pm 5\%$, 1/4W100-1543R72,R73Resistor, 1 k Ohm $\pm 5\%$, 1/4W100-1043R74Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243	1
R70Resistor, 2.2 k Ohm ±5%, 1/4W100-2243R71Resistor, 1.5 k Ohm ±5%, 1/4W100-1543R72,R73Resistor, 1 k Ohm ±5%, 1/4W100-1043R74Resistor, 2.2 k Ohm ±5%, 1/4W100-2243	ÎÎ
R71Resistor, 1.5 k Ohm ±5%, 1/4W100-1543R72,R73Resistor, 1 k Ohm ±5%, 1/4W100-1043R74Resistor, 2.2 k Ohm ±5%, 1/4W100-2243	1
R72,R73Resistor, 1 k Ohm ±5%, 1/4W100-1043R74Resistor, 2.2 k Ohm ±5%, 1/4W100-2243	
R74 Resistor, 2.2 k Ohm ±5%, 1/4W 100-2243	
	2 1
R75 Resistor, 1 k 0hm $\pm 5\%$, 1/4W 100-1043 D26 Desistor 2 2 k 0hm $\pm 5\%$, 1/4W 100-2243	
R76Resistor, 2.2 k Ohm $\pm 5\%$, 1/4W100-2243D77D77D77	
$R77, R78$ Resistor, 1 k Ohm $\pm 5\%$, $1/4W$ 100-1043 100-1043 100-1043	2
R79Resistor, 43 Ohm $\pm 5\%$, 1/4W100-4323100-4323	1 1 2 1 2 6
R80,R81 Resistor, 1 k Ohm ±5%, 1/4W 100-1043	2
R82 THRU Resistor, 10 k Ohm ±5%, 1/4W 100-1053	6
R87 R88 THRU Resistor, 1 Meg Ohm ±5%, 1/4W 100-1073	6
R93 R94 THRU Resistor, 10 Meg Ohm ±5%, 1/4W 100-1083 R99	6

Table 6-49.	Input Board	2 Circuit	Board Assembly	/ - 919-0054	(She

(Sheet 2 of 3)

	The board 2 chicult board Assembly - 919-00	54 (Sheet S	
REF. DES.	DESCRIPTION	PART NO.	QTY.
R100 THRU R105	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	6
R106 R107 THRU R110	Resistor, 100 k Ohm ±5%, 1/4W Resistor, 18 k Ohm ±5%, 1/4W	100-1063 100-1853	1 4
R111,R112 U1 THRU U4	Resistor, 1 k Ohm ±5%, 1/4W Integrated Circuit, LM339AN, Quad Voltage Comparator, 14-Pin DIP	100-1043 221-0339	2 4
U5,U6	Integrated Circuit, CMOS, MC14049UB, Inverting Hex Buffer, 16-Pin DIP	228-4049	2
U7	Integrated Circuit, SN74147N, 10 line-to-4 line priority Encoder, 16-Pin DIP	228-4147	1
U8	Integrated Circuit, CMOS, MC14013B, Dual-D Flip-Flop, 14-Pin DIP	228-4013	1
U9	Integrated Circuit, CMOS, MC14512, 8 Channel Data Selector, 16-Pin DIP	228-4512	1
U10	Integrated Circuit, CMOS, MC14023B, 3-Input NAND Gate, 14-Pin DIP	228-4023	1
W12 THRU W22	Programmable Jumper	340-0004	11
XU1 THRU XU4	Socket, 14-Pin	417-1404	4
XU5 THRU XU7	Socket, 16-Pin	417-1604	3
XU8 XU9 XU10	Socket, 14-Pin Socket, 16-Pin Socket, 14-Pin Blank Circuit Board	417-1404 417-1604 417-1404 519-0054	1 1 1

Table 6-49. Input Board 2 Circuit Board Assembly - 919-0054 (Sheet 3 of 3)

Table 6-50. Remote Control Interface Circuit Board Assembly - 919-0003 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 THRU C6 C7 C8 THRU C22	Capacitor, Electrolytic, 10 uF, 16V Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V	023-1074 023-1084 042-3922	6 1 15
C22 D2 THRU D7 D8 J1 THRU J5 L1 THRU L3 R4,R5 R6 R7 THRU R13 R14	Molded Inductor, 47 uH $\pm 10\%$, 700V Maximum Resistor, 1 k Ohm $\pm 5\%$, 1/4W Resistor, 27 k Ohm $\pm 5\%$, 1/4W	023-1084 203-4005 200-4742 417-1276 360-0012 100-1043 100-2753 100-1043 177-1054	1 6 1 5 3 2 1 7 1

abie 0-50.	Remote Control Interface Circuit Board Assembly - S	ala-0003 (20	eet 2 o
REF. DES.	DESCRIPTION	PART NO.	QTY.
R16	Resistor, 2 k Ohm ±5%, 1/4W	100-2043	1
R17	Potentiometer, 10 k Ohm $\pm 10\%$, 1/2W	177-1054	1
R18	Potentiometer, 20 k Ohm $\pm 10\%$, $1/2W$	177-2054	1
			1 8
R19 THRU	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	8
R26		100.0010	
R27	Resistor, 2 k Ohm $\pm 5\%$, 1/4W	100-2043	1
R28	Resistor, 1.8 k Ohm $\pm 5\%$, 1/4W	100-1843	1
R29	Resistor, 100 Ohm ±5%, 1/4W	100-1033	1
R30	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	1
R31	Resistor, 24 k Ohm ±5%, 1/4W	100-2453	1
R32 THRU	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	3
R34			
R35,R36	Resistor, 33 k Ohm ±5%, 1/4W	100-3353	2
R37 THRU	Resistor, 100 k Ohm $\pm 5\%$, 1/4W	100-1063	2 3
R39	Resistory 100 K ona 20/03 17 m	100-1000	5
R40	Resistor, 1 k Ohm ±5%, 1/2W	110-1043	1
		100-2453	1
R41,R42	Resistor, 24 k Ohm $\pm 5\%$, $1/4W$		24
R43 THRU	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	4
R46			
R47	Resistor, 24 k Ohm ±5%, 1/4W	100-2453	1
R48 THRU	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	5
R52			
R53 THRU	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	7
R59			
R60 THRU	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	3
R62			
R63 THRU	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	11
R73			
U1	Integrated Circuit, TL094C, Quad JFET-Input	221-0094	1
01	Operational Amplifier, 14-Pin DIP	221-0034	-
U2 THRU U7	Integrated Circuit, 4N33, Optical Isolator,	229-0033	6
		229-0035	0
	Infared LED-Photo, NPN, Darlington		
	Transistor Coupled Pair, 1500V Isolation,		
	Response: 30 kHz Maximum, Current: 50 mA		
	Maximum, 6-Pin DIP		
U8	Integrated Circuit, CD4050BM, CMOS, Hex Buffer,	228-4050	1
	16-Pin DIP		
U9	Integrated Circuit, CD4069C, CMOS, Hex Inverter,	228-4069	1
	14-Pin DIP		
U10	Integrated Circuit, CD4050BM, CMOS, Hex Buffer,	228-4050	1
	16-Pin DIP		
XU1	Socket, 14-Pin	417-1400	1
XU8	Socket, 16-Pin	417-1604	ī
		417-1400	1.
XU9	Socket, 14-Pin		
XU10	Socket, 16-Pin	417-1604	
anny ann ann aight	Blank Circuit Board	519-0003	1

Table 6-50. Remote Control Interface Circuit Board Assembly - 919-0003 (Sheet 2 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 R1 R2 R3 R4 R5 R6 R7 R8	Capacitor, Ceramic Disc, 0.01 uF, 500V Potentiometer, 50 k Ohm $\pm 10\%$, 1/2W Resistor, 1 k Ohm $\pm 5\%$, 1/4W Potentiometer, 2 k Ohm $\pm 10\%$, 1/2W Resistor, 4.7 k Ohm $\pm 5\%$, 1/4W Potentiometer, 2 k Ohm $\pm 10\%$, 1/2W Resistor, 4.7 k Ohm $\pm 5\%$, 1/4W Potentiometer, 2 k Ohm $\pm 10\%$, 1/2W Resistor, 4.7 k Ohm $\pm 5\%$, 1/4W Blank Circuit Board	001-1044 178-5054 100-1043 178-2044 100-4743 178-2044 100-4743 178-2044 100-4743 517-0020	1 1 1 1 1 1 1 1

Table 6-51. Meter Circuit Board Assembly - 917-0020

Table 6-52. Primary Function Indicator Circuit Board Assembly - 917-0027

REF. DES.	DESCRIPTION	PART NO.	QTY.
D1,D2	Indicator, LED, Yellow, 521-9176, 2.3V @ 30 mA Maximum (Interlock/BLOWER Indicators)	323-9225	2
D3	Indicator, LED, Green, 521-9175, 2.3V @ 40 mA Maximum (FILAMENT Indicator)	323-9224	1
D4	Indicator, LED, Red, 521-9212, 1.7V @ 50 mA Maximum (HIGH VOLTAGE Indicator)	323-9217	1
R1 THRU R3	Resistor, 5.1 k Ohm $\pm 5\%$, 1/2W	110-5143	3
R4	Resistor, 22 k Ohm,±5%, 1/2W	110-2253	1
R5 THRU R8	Resistor, 1.5 k Ohm $\pm 5\%$, 1/2W	110-1543	4
U1	Integrated Circuit, CMOS, ULN2003A, 7-Channel Driver, CMOS/TTL compatable, 16-Pin DIP	229-2003	1
XU1	Socket, 16-Pin	417-1601	1
	Blank Circuit Board	517-0027	1

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Table 6-53.	Microprocessor	Patch	Panel	Circuit	Board	Assembly	-	917-0029
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REF. DES.	DESCRIPTION	PART NO.	QTY.
	Pin, Disconnect (PC Mount) Blank Circuit Board	418-0161 517-0029	99 1

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Receptacle, 12-Pin Receptacle, 4-Pin Pin, Receptacle (for above receptacles) Receptacle, Edge Connector Pin, Receptacle (for Microprocessor Patch Panel Assembly)	418-1271 418-0240 417-0053 417-0011 417-0160	18 2 157 2 93

Table 6-54. Microprocessor Controller Wiring Harness - 947-0025

Table 6-55. Automatic Power Control Assembly - 959-0023

REF. DES.	DESCRIPTION	PART NO.	QTY.
<u>.</u> B1	Motor, Reversible, 2 RPM, 30 in/oz Output Torque, 117V ac, 60 Hz, Magnetic Clutch, 5.5vA	380-0001	1
C1 THRU C12	Capacitor, 1000 pF, Feedthru	008-1033	12
C13,C14	Capacitor, Ceramic Disc, 0.01 uF, 500V	008-1044	2
DS1	Light Emitting Diode, Green, 521-9175, 2.3V @ 40 mA	323-9224	1
F1	Fuse, Slow-Blow, 3 AG, 1/2 Ampere	334-0050	1
J1,J2	BNC Connector	417-0206	12213
R1, R2	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	2
R3	Resistor, 4.42 k Ohm $\pm 1\%$, 1/4W	103-4441	1
R4 THRU R6	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	3
TB12	Barrier Strip, 18 Terminal	412-0018	1
XF1	Fuseholder, 3 AG	415-2012	1
	Dual 120 MHz Low-Pass Filter Circuit Board Assembly	919-0031	1
	Power Supply/Control Circuit Board Assembly	919-0032	1
	Analog Circuit Board Assembly	919-0033	1

Table 6-56. Dual 120 MHz Low-Pass Filter Circuit Board Assembly - 919-0031 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1,C2 C3,C4 C5,C6 D1,D2 L1 THRU L4 R1,R2	Capacitor, Ceramic, 10 pF ±10%, 1 kV Capacitor, Mica, 33 pF ±5%, 500V Capacitor, Ceramic, 10 pF ±10%, 1 kV Diode, HP5082-2800, High Voltage Schottky Barrier Type, 70V, 15 mA Inductor, Fixed, 0.110 uH, 50 to 450 MHz, 1A dc Maximum Resistor, 100 0hm ±5%, 1/2W	001-1014 042-3312 001-1014 201-2800 364-0011 110-1033	2 2 2 4 2

REF. DES.	DESCRIPTION	PART NO.	QTY.
R3,R4	Resistor, 120 Ohm ±5%, 1/2W	110-1233	2
R5,R6	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	2
	Blank Circuit Board	519-0031	1

Table 6-56. Dual 120 MHz Low-Pass Filter Circuit Board Assembly - 919-0031 (Sheet 2 of 2)

Table 6-57. Power Supply/Control Circuit Board Assembly - 919-0032

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1	Capacitor, Electrolytic, 1000 uF, 35V	024-1000	1
C2	Capacitor, Mylar, 0.47 uF, 1 kV	031-4753	1 6
D1 THRU D6	Diode, 1N4005, Silicon, 600V, 1 Ampere	203-4005	6
K1 THRU K4	Relay, Plug-In	270-1253	4
	Contacts: 4 Sets SPDT, 2 Amperes,	ч. - С	
	28V dc or 115V ac		
RV1,RV2	Coil: 12V dc, 185 Ohm ±10% Metal Oxide Varistor, V130LA10A, 130V ac RMS,	140-0006	2
RV1,RV2	10 Joules	140-0000	-
S1	Switch, SPDT Center Off, Miniature Toggle,	348-0002	1
•-	2A, 250V ac, 5A, 125V ac (RAISE/LOWER Switch)		_
S2	Switch, Toggle, DPDT, 2A 250V ac, 5A 125V ac	348-0005	1
	(LOCAL/REMOTE Switch)		
T1 ·	Transformer, Power, Circuit Board Mount	376-0524	1
	Primary: 115/230V, 50/60 Hz		
	Secondary: Dual 12V @ 1 Ampere		
XK1 THRU	Relay Socket, PC Board Mount	270-0008	4
Х К4	Diaula Criverist Desud	F10 0022	4
	Blank Circuit Board	519-0032	Ŧ
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Table 6-58.	Analog	Circuit	Board	Assembly		919-0033	(
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(Sheet 1 of 3)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1,C2 C3 C4,C5 C6 THRU C11 C12 THRU C16 C17 THRU C19 D1	Capacitor, Electrolytic, 4.7 uF, 35V Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Electrolytic, 4.7 uF, 35V Capacitor, Mylar Film, 0.1 uF, 100V Capacitor, Electrolytic, 100 uF, 25V Diode, 1N4005, Silicon, 600V, 1 Ampere	024-4764 023-1084 042-3922 024-4764 030-1053 023-1084 203-4005	2 1 2 6 5 3 1

Table 6-58. Analog Circuit Board Assembly - 919-0033	Table 6-58.	Analog	Circuit Boar	d Assembly	у –	919-0033
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(Sheet 2 of 3)

REF. DES.	DESCRIPTION	PART NO.	QTY.
D2	Diode, 1N4148, Silicon, Fast-Switching,	203-4148	1
L1,L2	100V, 10 mA Inductor, Molded, 2.20 mH $\pm 10\%$, 100 MHz,	364-2200	2
Q1 THRU Q3	0.19 Ohm dc Resistance, 1100 mA Maximum Transistor, 2N3906, Silicon, PNP, TO-92 Case	210-3906	3
R1	Resistor, 115 Ohm $\pm 1\%$, 1/4W	100-1131	1
R2	Resistor, 909 Ohm $\pm 1\%$, 1/4W	103-9031	1
R3,R4	Resistor, 15 k Ohm $\pm 5\%$, $1/4W$	100-1553	3 1 2 1 1
R5	Resistor, 100 k Ohm $\pm 5\%$, $1/4W$	100-1063	1
R6	Potentiometer, 50 k Ohm $\pm 10\%$, $1/2W$	178-5054	1
	(RFL CAL Control)		-
Ŕ7	Resistor, 22 k Ohm $\pm 5\%$, 1/4W	100-2253	1
R8	Potentiometer, 50 k Ohm ±10%, 1/2W (FWD CAL Control)	178-5054	1 1
Ŕ9	Resistor, 22 k Ohm $\pm 5\%$, 1/4W	100-2253	1
R10	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	1 1 2 1 1 2 1 1
R11	Resistor, 3.3 k Ohm $\pm 5\%$, 1/4W	100-3343	1
R12,R13	Resistor, 4.7 k Ohm $\pm 5\%$, 1/4W	100-4743	2
R14	Resistor, 47 k Ohm $\pm 5\%$, $1/4W$	100-4753	1
R15	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R16,R17	Resistor, 1 k Ohm $\pm 5\%$, $1/4W$	100-1043	2
R18	Potentiometer, 1 k Ohm, 2W, W/W, 10 Turn	190-0051	1
R19	Resistor, 47 k Ohm $\pm 5\%$, $1/4W$	100-4753	1
R20	Potentiometer, 50 k Ohm ±10%, 1/2W (LOW DRIVE TRIP Control)	178-5054	1
R21,R22	Resistor, 18 k Ohm $\pm 5\%$, $1/4\text{W}$	100-1853	2 3
R23 THRU R25	Resistor, 4.7 k Ohm $\pm 5\%$, 1/4W	100-4743	3
R26 THRU R28	Resistor, 10 Ohm ±5%, 1/4W	100-1023	3
R29 THRU R31	Resistor, 10 k Ohm ±5%, 1/4W	100-1053	3
R32 THRU	Resistor, 4.7 k Ohm ±5%, 1/4W	100-4743	3
R35 R36	Resistor, 150 Ohm ±5%, 1/4W	100-1533	1
R37	Resistor, 4.7 k Ohm $\pm 5\%$, $1/4W$	100-4743	111111111111
R38	Resistor, 4.3 k Ohm $\pm 5\%$, $1/4W$	100-4343	1
R39	Resistor, 150 Ohm $\pm 5\%$, 1/4W	100-1533	1
R40	Resistor, 4.7 k Ohm $\pm 5\%$, $1/4W$	100-4743	1
R41	Resistor, 150 Ohm $\pm 5\%$, 1/4W	100-1533	1
R42	Resistor, 4.75 k Ohm $\pm 1\%$, 1/4W	103-4741	1
R42	Resistor, 5.11 k Ohm $\pm 1\%$, 1/4W	103-5141	1
R43	Resistor, 7.50 k Ohm $\pm 1\%$, 1/4W	103-7541	ī
R45	Resistor, 3.65 k Ohm $\pm 1\%$, $1/4W$	103-3641	1
R46 THRU R52	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	7
R52 R53,R54	Resistor, 1 Meg Ohm ±5%, 1/4W	100-1073	2
R55,R54 R55 THRU	Resistor, 51 k Ohm $\pm 5\%$, 1/4W	100-5153	2 3
R55 11K0 R57	NGSISON'S ST N ONN 20/05 1/TH		-
NJ7 .			

Table 6-58.	Analog	Circuit	Board	Assembly	y -	919-0033	(Sheet 3	of 3	3)
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REF. DES.	DESCRIPTION	PART NO.	QTY.
R58,R59 R60	Resistor, 470 k Ohm ±5%, 1/4W Potentiometer, 10 k Ohm ±10%, 1W, Linear Taper,	100-4763 192-1052 ±	2
R61 R62 THRU R69	Modified (VSWR CAL Control) Resistor, 25.5 k Ohm ±1%, 1/4W Resistor, 4.7 k Ohm ±5%, 1/4W	103-2551 100-4743	1 8
R70 R71	Resistor, 1.2 k Ohm $\pm 5\%$, 1/4W Resistor, 1 Meg Ohm $\pm 5\%$, 1/4W	100-1243 100-1073 100-4743	1 1 1
R72 R73 R74	Resistor, 4.7 k Ohm ±5%, 1/4W Resistor, 820 Ohm ±5%, 1/4W Resistor, 1 k Ohm ±5%, 1/4W	100-8233 100-1043	1 1
S1 S2	Switch, DPDT, Miniature Toggle, 3A 250V ac, 5A 125V ac, (FWD/VSWR/VSWR CAL Switch) Switch, SPDT Center Off, Miniature Toggle,	348-0003 348-0004	1 1
U1	3A 250V ac, 5A 125V ac (AUTO/MAN Switch) Integrated Circuit, LM317T, Adjustable Positive Voltage Regulator, 1.2 to 37V, 1.5 Ampere,	227-0317	1
U2 THRU U4	TO-220 Case Integrated Circuit, TLO92CP, Dual N-Channel JFET Input Operational Amplifier, 8-Pin DIP	221-0092	3
U5,U6	Integrated Circuit, LM339AN, Quad Voltage Comparator, 14-Pin DIP	221-0339	2
U7,U8	Integrated Circuit, MC14001B, CMOS, Quad Input Nor Gate, 14-Pin DIP	228-4001	2
U9	Integrated Circuit, MC1413P, CMOS, Seven Circuit NPN Darlington Driver, 16-Pin DIP	229-2003	1
XU2 THRU XU4	Socket, 8-Pin	417-0804	3
XU5 THRU XU8	Socket, 14-Pin	417-1404	4
XU9 	Socket, 16-Pin Insulator, TO-220 Case Screw, Nylon, 6-32 Thread Blank Circuit Board	417-1604 409-7403 420-6998 519-0033	1 1 1 1

Table 6-59. Resistor and Lugs Assembly - 955-0037

REF. DES.	DESCRIPTION	PART NO.	QTY.
R117	Resistor, 400 Ohm ±10%, 25W, W/W	132-4032	1.
			- -

6-35

REF. DES.	DESCRIPTION	PART NO.	QTY.
	VSWR Assembly	955-0001	1
	IPA Directional Coupler Assembly	951-1012	1

Table 6-60. IPA Directional Coupler Assembly - 959-0050

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Table 6-61. VSWR Assembly - 955-0001

1033	7
0011	1

Table 6-62. IPA Directional Coupler Assembly - 951-1012

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1,C2	Capacitor, Ceramic Feed-Thru, 1000 pF ±20%, 500V	008-1033	2
D1,D2	Diode, HP5082-2800, High Voltage Schottky Barrier Type, 70V, 15 mA	201-2800	2
J2,J3 R1,R2	Type N Coaxial Connector Resistor, 56 Ohm ±5%, 1/2W	417-0204 110-5623	2 2

Table 6-63. Buffer Amplifier Circuit Board - 919-0011 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
C3,C4 C5 R1,R2 R3 R4 R5 R6 R7 THRU R9 R11,R12 R13 R14 THRU R16 R17	Capacitor, Mica, 390 pF $\pm 5\%$, 100V Capacitor, Electrolytic, 10 uF, 16V Resistor, 47 k Ohm $\pm 5\%$, 1/4W Potentiometer, 50 k Ohm $\pm 10\%$, 1/2W Resistor, 33 k Ohm $\pm 5\%$, 1/4W Potentiometer, 50 k Ohm $\pm 10\%$, 1/2W Resistor, 33 k Ohm $\pm 5\%$, 1/4W Resistor, 10 k Ohm $\pm 5\%$, 1/4W Resistor, 3.3 k Ohm $\pm 5\%$, 1/4W Resistor, 100 Ohm $\pm 5\%$, 1/4W Resistor, 1 k Ohm $\pm 5\%$, 1/4W Resistor, 10 k Ohm $\pm 5\%$, 1/4W	042-3922 023-1074 100-4753 177-5054 100-3353 177-5054 100-3353 100-1053 100-3343 100-1033 100-1043 100-1053	2 1 2 1 1 1 3 2 1 3 1

REF. DES.	DESCRIPTION	PART NO.	QTY.
U1	Integrated Circuit, TL092CP, Dual N-Channel JFET Operational Amplifier, 8-Pin DIP	221-0092	1
XU1 	Socket, 8-Pin Blank Circuit Board	417-0804 519-0011	1 1

Table 6-63. Buffer Amplifier Circuit Board - 919-0011 (Sheet 2 of 2)

Table 6-64. Exciter ac Control - 955-0020

REF. DES.	DESCRIPTION	PART NO.	QTY.
К103	Relay, Plug-In Coil: 120V ac	270-1250	1
K104,K105	Contacts: 2 Sets DPDT, 10A/240V ac Resistive Relay, Plug-In Coil: 2500 Ohm ±10%, Nominal 24-48V dc Contacts: 2 Sets DPDT, 2A/28V or 115V Resistive	271-0154	2
S101	Switch, Toggle, DPST, 125V, 15A; 250V, 10A Screw Terminals	348-7360	1
TB8,TB9	Terminal Strip, 20 Terminals	418-0019	2
XK103	Socket, 8-Pin, Screw Terminals (for K103)	417-0400	1
	AC.Outlet_Strip, 6 Receptacles	840-4007	1

Table 6-65. Microprocessor Controller Power Supply and Battery Charger - 959-0069

(Sheet 1 of 2)

	and bactery charger - 333-0009	(Sheet 1	. 01 27
REF. DES.	DESCRIPTION	PART NO.	QTY.
BT1 THRU BT4	Battery, X Cell, 2V, 5 AH, Rechargeable Lead-Acid	357-6900	4
D15	Bridge Rectifier, Full Wave, MDA2502, 200 PIV, 25 Amperes	239-0006	1
F1 L1 THRU L11	Fuse, MDL, 240V, 1.5 A, Slow-Blow Ferrite Beads	334-0150 360-0003	1 11
P1 P2	Plug, 12-Pin Plug, 6-Pin Transformer Daven	418-1271 418-0670 276 0218	1
Τ1	Transformer, Power Primary: 95/115/210/230V, 50/60 Hz Dual Secondary: 25.5V @ 1A 13.2V @ 3A	376-0218	Ţ
TB1	Terminal Board, 7 Terminal	412-0007	1

	and bactery charger - 959+0009	(Sheet Z	01 2)
REF. DES.	DESCRIPTION	PART NO.	QTY.
U3	Integrated Circuit, LM317K, 3 Terminal Adjustable Voltage Regulator, 1.2 to 37V @ 1.5 Ampere, TO-3 Case	227-0318	1
U4	Integrated Circuit, MC7824CK, Fixed Positive Voltage Regulator, +24V, 1.5 Ampere, TO-3 Case	227-7824	1
U5	Integrated Circuit, LM317K, 3 Terminal Adjustable Voltage Regulator, 1.2 to 37V @ 1.5 Ampere, TO-3 Case	227-0318	1
XF1	Fuse Holder, In-Line, 3 AG	415-0145	1
XU3,XU4, XU5	Transistor Socket, TO-3	417-0298	3
,	Mica Insulator, TO-3 (for U3,U4,U5)	418-0010	3
	Connector Pins (for P1 and P2)	417-0053	17
	Microprocessor Power Supply and Battery Charger Circuit Board Assembly	919-0034	1

Table 6-65. Microprocessor Controller Power Supply and Battery Charger - 959-0069

(Sheet 2 of 2)

Table 6-66. Microprocessor Controller Power Supply and Battery Charger Circuit Board Assembly - 919-0034 (Sheet 1 of 2)

	Dattery thanger thrunt board Assembly - 313-0004		
REF. DES.	DESCRIPTION	PART NO.	QTY.
C1	Capacitor, Mylar, 0.01 uF, 100V	031-1043	1
C2 THRU C4	Capacitor, Electrolytic, 4700 uF, 35V	014-4795	1 3 2 1
C5,C6	Capacitor, Electrolytic, 10 uF, 35V	023-1076	2
C7	Capacitor, Electrolytic, 33 uF, 35V	024-3374	1
C8	Capacitor, Mylar, 0.1 uF, 100V	030-1053	1.
C9	Capacitor, Electrolytic, 10 uF, 35V	023-1076	1
C10	Capacitor, Electrolytic, 100 uF, 25V	023-1084	1
C11	Capacitor, Electrolytic, 10 uF, 35V	023-1076	1
· C12	Capacitor, Electrolytic, 100 uF, 25V	023-1084	1
C13	Capacitor, Mylar, 0.1 uF, 100V	030-1053	1
D1 THRU D4	Diode, MR502, Silicon, 200V, 3 Ampere	202-0502	1 4 4 1 5
D5 THRU D8	Diode, 1N4005, Silicon, 600V, 1 Ampere	203-4005	4
D 9	Diode, MR751, Silicon, 100V, 6 Ampere	202-0751	1
D10 THRU	Diode, 1N4005, Silicon, 600V, 1 Ampere	203-4005	5
D14 DT1	Diode, 1N6279A, Silicon Transient Voltage Suppressor, 22V ±5%	206-0001	1
DT2	Diode, 1N6284A, Silicon Transient Voltage Suppressor, 36V ±5%	206-0002	1
J1	Connector, 12-Pin	417-1276	1
J2	Connector, 6-Pin	417-0677	1
K1	Relay, Circuit Board Mount	272-0106	1
Q1	Contacts: SPDT, 100V dc @ 8 Amperes Coil: 12V dc, 140 mA, 85 Ohms ±10 Ohms Transistor, MPS-U05, Silicon, NPN, Motorola Case 152-02	211-0005	1

REF. DES.	DESCRIPTION	PART NO.	QTY.
R1	Resistor, 820 Ohm ±5%, 1/4W	100-8233	1
R2	Potentiometer, 100 Ohm ±10%, 1/2W	177-1034	
R3	Resistor, 30 Ohm ±5%, 1W	120-3023	1
R4	Resistor, 121 Ohm $\pm 1\%$, 1/4W	100-1231	1
R5	Resistor, 10 Ohm $\pm 5\%$, $1/4W$	100-1023	1
R6	Resistor, 3.9 k Ohm $\pm 5\%$, 1/4W	100-3943	1
R7	Resistor, 365 Ohm ±1%, 1/4W	103-3631	1
R8	Potentiometer, 10 k Ohm ±10%, 1/2W	177-1054	1
R9	Resistor, 2.32 k Ohm $\pm 1\%$, $1/4W$	103-2341	1
R10	Resistor, 1.33 k Ohm $\pm 1\%$, 1/4W	103-1331	1
R11	Resistor, 20 k Ohm $\pm 5\%$, $1/4W$	100-2051	
R12	Resistor, 121 Ohm $\pm 1\%$, 1/4W	100-1231	1
R13	Resistor, 4.7 k Ohm ±5%, 1/4W	100-4743	1
R14	Resistor, 2 k Ohm $\pm 5\%$, $1/4W$	100-2043	1
TB2	Barrier Strip, 4 Terminal	412-0004	1
U1	Integrated Circuit, LM336Z-2.5, Precision Voltage Reference, 2.5V ±4%-0 to 70°C, T0-92 Case	229-0336	1
U2	Integrated Circuit, TL311P, JFET Input Differential Comparator, 8-Pin DIP	220-0311	1
XU2	Socket, 8-Pin	417-0804	1
	Blank Circuit Board	519-0034	1

Table 6-66. Microprocessor Controller Power Supply and Battery Charger Circuit Board Assembly - 919-0034

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(Sheet 2 of 2)

Table 6-67. Microprocessor Controller Bypass Assembly - 959-0053

REF. DES.	DESCRIPTION	PART NO.	QTY.
DS1	Light Emitting Diode, Red, CM4-86B, 5V @ 20 mA	323-0023	1
· DS2	Light Emitting Diode, Green, 521-9175, 2.3V @ 40 mA	323-9224	
DS3,DS4	Incandescent Lamp, No. 345, 6V, 0.04 Ampere (for START Switch/Indicators)	321-0328	. 2
P2	Plug, 25-Pin	418-3219	1
S1 THRU S4	Switch/Indicator, SPST Push, Normally open 12V @ 100 mA Maximum Resistive Load	343-0012	4
	Switch Cap, Red (STOP)	343-0016	2
	Switch Cap, Green (START)	343-0015	2 2 1
	Microprocessor Controller Bypass Circuit Board Assembly	919-0009	1
: :	Microprocessor Controller Bypass Assembly 24 Volt Control Circuit Board	919-0014	1

		(Sheet 1 of 2)	
REF. DES.	DESCRIPTION	PART NO.	QTY.
01		010 0000	
C1	Capacitor, Mica, 390 pF $\pm 5\%$, 100V	042-3922	
C2,C3	Capacitor, Electrolytic, Dipped Tantalum,	064-2263	2
	2.2 uF ±20%, 35V		
C4	Capacitor, Mica, $390 \text{ pF} \pm 5\%$, 100V	042-3922	1
C5	Capacitor, Electrolytic, Dipped Tantalum,	063-1083	1
	100 uF ±20%, 20V		
C6 THRU	Capacitor, Mica, 390 pF ±5%, 100V	042-3922	7
C12			
C13,C14	Capacitor, Electrolytic, 100 uF, 25V	023-1084	2 1
C15	Capacitor, Mica, 390 pF ±5%, 100V	042-3922	1
C16	Capacitor, Electrolytic, 100 uF, 25V	023-1084	
C18	Capacitor, Electrolytic, 10 uF, 35V	023-1076	1
D1 THRU D7	Diode, Silicon, 1N4148, 75V @ 0.3 Ampere	203-4148	7
	Fast Switching		
L1	Molded Inductor, 47 mH ±10%, 700V Maximum	360-0012	1
Q1 THRU Q3	Transistor, Silicon, MPSA14, NPN, TO-92 Case	211-0014	3
R1	Resistor, 1 k Ohm ±5%, 1/4W	100-1043	1
R2	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	1
R3 THRU R7	Resistor, 100 k Ohm $\pm 5\%$, 1/4W	100-1063	Ē
R8,R9	Resistor, 10 k Ohm $\pm 5\%$, $1/4W$	100-1053	2
R10	Resistor, 150 Ohm $\pm 5\%$, 1/4W	100-1533	1
R10 R11	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	1 3 1 5 2 1 1 2 4
R11 R12	Resistor, 180 Ohm $\pm 5\%$, 1/4W Resistor, 180 Ohm $\pm 5\%$, 1/4W	100-1833	
		100-1043	2
R13,R14	Resistor, 1 k Ohm $\pm 5\%$, 1/4W		
R15 THRU	Potentiometer, 100 k Ohm $\pm 10\%$, 1/2W	177-1064	4
R18	Desister $2 + 0$ by $(5\% + 1/4)$	100 0040	
R19	Resistor, 2 k Ohm ±5%, 1/4W	100-2043	
R20	Resistor, 1.8 k Ohm $\pm 5\%$, 1/4W	100-1843	
R21	Resistor, 2 k Ohm $\pm 5\%$, 1/4W	100-2043	
R22	Resistor, 1.8 k Ohm $\pm 5\%$, 1/4W	100-1843	
R23	Resistor, 2 k Ohm $\pm 5\%$, 1/4W	100-2043	
R24	Resistor, 1.8 k Ohm $\pm 5\%$, $1/4W$	100-1843	
R25	Resistor, 2 k Ohm $\pm 5\%$, 1/4W	100-2043	
R26	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R27	Resistor, 100 k Ohm $\pm 5\%$, 1/4W	100-1063	1
R28	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1
R29	Resistor, 20 k Ohm $\pm 5\%$, $1/4W$	100-2053	1
R30	Resistor, 1.8 k Ohm ±5%, 1/4W	100-1843	1
R31	Resistor, 1 k Ohm $\pm 5\%$, 1/4W	100-1043	1
R32	Resistor, 100 Ohm ±5%, 1/4W	100-1033	
R33	Resistor, 330 Ohm ±5%, 1/4W	100-3333	1
R34	Resistor, 10 k Ohm $\pm 5\%$, 1/4W	100-1053	1 1 1 1 1 1 2 1
R35,R36	Resistor, 330 Ohm ±5%, 1/4W	100-3333	2
R37, R38	Resistor, 470 Ohm $\pm 5\%$, $1/4W$	100-4733	2
U1	Integrated Circuit, MC14011UB, CMOS, Quad	228-4011	1
	2-Input NAND Gate, 14-Pin DIP		
U2	Integrated Circuit, TL094C, Quad JFET-Input	221-0094	1
	Operational Amplifier, 14-Pin DIP		
	cherweigner umbritte.? zie tim een		
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Table 6-68. Microprocessor Controller Bypass Circuit Board Assembly - 919-0009 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
U3	Integrated Circuit, MC14049UB, CMOS, Inverting Hex Buffer, 16-Pin DIP	228-4049	1
U4	Integrated Circuit, 4N33, Optical Isolator, Infared LED-Photo NPN Darlington Transistor Coupled Pair, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP	229-0033	1
XU1,XU2 XU3	Socket, 14-Pin Socket, 16-Pin Blank Circuit Board	417-1404 417-1604 519-0009	2 1 1
	Bypass Assembly, 24 Volt Control Circuit Board	919-0014	1

Table 6-68. Microprocessor Controller Bypass Circuit Board Assembly - 919-0009 (Sheet 2 of 2)

Table 6-69.Microprocessor Controller Bypass Assembly24Volt Control Circuit Board - 919-0014

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REF. DES.	DESCRIPTION	PART NO.	QTY.
C1 R1 R2 R3 R4 U1	Capacitor, Mica, 390 pF ±5%, 100V Resistor, 1 k Ohm ±5%, 1/4W Resistor, 10 k Ohm ±5%, 1/4W Resistor, 1 k Ohm ±5%, 1/4W Resistor, 1 k Ohm ±5%, 1/2W Integrated Circuit, 4N33, Optical Isolator, Infared LED-Photo NPN Darlington Transistor Coupled Pair, 1500V Isolation, Response: 30 kHz Maximum, Current: 50 mA Maximum, 6-Pin DIP Blank Circuit Board	042-3922 100-1043 100-1053 100-1043 110-1043 229-0033	1 1 1 1 1

Table 6-70. High Voltage Power Supply Cabinet Assembly - 909-3000 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
CB300	Circuit Breaker, 3 Pole, 200 Ampere, 600V ac (HIGH VOLTAGE PRIMARY)	341-0001	1
К300	Contactor Coil: 110/120V ac, 50/60 Hz Contacts: 3 sets SPST, 270 Amperes, 600V ac	341-0005	1
R300	Resistor, Ceramic, clip mounting, 5 Ohm ±10%, 275W, Non-Inductive	140-0002	1.
R301 THRU R304	Resistor, 50 k Ohm ±5%, 225W, W/W	132-0001	4
R305 R306	Resistor, 100 Ohm ±5%, 25W, W/W Resistor, Ceramic, clip mounting, 5 Ohm ±10%, 275W, Non-Inductive	132-1011 140-0002	1 1

DESCRIPTION r Shunt, 1 Volt, 6 Amperes, 0.1667 Ohm nterlock Switch, SPDT, 15A at 125 or ac, 0.5A at 125V dc, 0.25A at 250V dc	PART NO. 316-0001 346-3302	QTY.
nterlock Switch, SPDT, 15A at 125 or ac, 0.5A at 125V dc, 0.25A at 250V dc		1
nterlock Switch, SPDT, 15A at 125 or ac, 0.5A at 125V dc, 0.25A at 250V dc		1
oltage Shorting and Interlock Switch	955-0030	1
	412-0724	14
	415-1003	4
p for TB6 and TB10	412-0730	2
	955-0005	1
Supply Base Assembly	955-0006	1
Harness, Power Supply Interlock	947-0090	1
	959-0067	1
oltage Step Start Assembly	959-0064	1
	embly er Strip, Screw Terminal (7 per Strip) Fuse Mounting, Type FRS ap for TB6 and TB10 Supply Diode Assembly Supply Base Assembly g Harness, Power Supply Interlock wer Distribution Panel /oltage Step Start Assembly	er Strip, Screw Terminal (7 per Strip)412-0724Fuse Mounting, Type FRS415-1003ap for TB6 and TB10412-0730Supply Diode Assembly955-0005Supply Base Assembly955-0006g Harness, Power Supply Interlock947-0090wer Distribution Panel959-0067

Table 6-70. High Voltage Power Supply Cabinet Assembly - 909-3000 (Sheet 2 of 2)

Table 6-71. High Voltage Shorting and Interlock Switch Assembly - 955-0030

REF. DES.	DESCRIPTION	PART NO.	QTY.
	Ground Stick Hanger	955-0038	1

Table 6-72. Ground Stick Hanger - 955-0038

REF. DES.	DESCRIPTION	PART NO.	QTY.
S302	Interlock Microswitch, SPDT, 11A at 125 or 250V ac, 0.5A at 125V dc, 0.25A at 250V dc	346-6100	1

Table 6-73. Power Supply Diode Assembly - 955-0005

REF. DES.	DESCRIPTION	PART NO.	QTY.
D300 THRU D305	Half Wave Silicon Rectifier Stack with transient compensation, 28 kV, 6 Ampere	234-0001	6

REF. DES.	DESCRIPTION	PART NO.	QTY.
C300,C301 L300 T300	Capacitor, Oil Filled, 2 uF, 15 kV Choke, Filter, 6H, 5A dc Plate Transformer: Primary: 3Ø, 60 Hz, Delta connected, 208/240V ±12V Secondary: Wye connected, 6780V ac, 4.08A	047-0001 376-0014 376-0013	2 1 1

Table 6-74. Power Supply Base Assembly - 955-0006

Table 6-75. Wiring Harness, High Voltage Power Supply Interlock - 947-0090

REF. DES.	DESCRIPTION	PART NO.	QTY.
P5	Plug, 14-Pin	417-0008	1

Table 6-76. AC Power Distribution Panel - 959-0067

REF. DES.	DESCRIPTION	PART NO.	QTY.
F301 THRU F303	Fuse, Clip Mounting, 40 Ampere, 250V, Dual	330-0601	3
F304,F305 XF301 THRU	Fuse, 3 AG, 20 Amperes, 250V Clip, Fuse Mounting, Type S2 (2 per fuse)	334-0020 415-0001	2 6
XF303 XF304, XF305	Fuse Holder, In-Line, 3 AG	330-0300	2

Table 6-77. High Voltage Step Start Assembly - 959-0064 (Sheet 1 of 2)

REF. DES.	DESCRIPTION	PART NO.	QTY.
A300 K301	Step Start Circuit Board Assembly Contactor Coil: 110/230V, 50/60 Hz Contacts: 3 Sets SPST, 40 Amperes, 600V	919-0199 341-0023	1 1
K302,K303	Relay, Solid State, 240D10, 240V @ 10 Amperes, 2500V Isolation, Control: 3-32V dc @ 5.0 mA	273-0002	2 1
MOV301, MOV302	Metal Oxide Varistor, V250LA15A, 250V ac RMS	140-0008	2
R308 THRU R310	Resistor, 2 Ohm ±5%, 50W, W/W	132-1004	3

REF. DES.	DESCRIPTION	PART NO.	QTY.
XA300	Socket, 8-Pin	417-0400	1
	Housing with 8-Pin Plug (for A300)	418-0650	1

Table 6-77. High Voltage Step Start Assembly - 959-0064 (Sheet 2 of 2)

Table 6-78. Step Start Circuit Board Assembly - 919-0199

REF. DES.	DESCRIPTION	PART NO.	QTY.
C1,C2 C3,C4 C5,C6 C7 C8 C9,C10 D1,D2	Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Polystyrene, 0.47 uF, 100V Capacitor, Mica, 390 pF ±5%, 100V Capacitor, Electrolytic, 1 uF, 50V Capacitor, Electrolytic, 100 uF, 25V Capacitor, Mica, 390 pF ±5%, 100V Diode, 1N4148, Silicon, Fast-Switching, 100V, 10 mA	042-3922 038-4753 042-3922 024-1064 023-1084 042-3922 203-4148	2 2 1 1 2 2
D3,D4 D5 L1,L2	Diode, 1N4742A, Zener, $12V \pm 5\%$, 1W Diode, 1N4004, Silicon, 400V, 1 Ampere Inductor, Molded, 2.20 mH $\pm 10\%$, 100 MHz,	200-4742 203-4004 364-2200	2 1 2
Q1,Q2 R1,R2 R3 R4 R5 R6,R7 R8,R9 R10 R11 U1 XU1 	0.19 Ohm dc Resistance: 1100 mA Maximum Transistor, 2N3904, Silicon, NPN, TO-92 Case Resistor, 1 k Ohm ±5%, 1/4W Resistor, 4.7 k Ohm ±5%, 1/4W Resistor, 150 k Ohm ±5%, 1/4W Resistor, 820 k Ohm ±5%, 1/4W Resistor, 560 Ohm ±5%, 1/4W Resistor, 1 k Ohm ±5%, 1/2W Resistor, 680 Ohm ±5%, 1/4W Integrated Circuit, MC14584B, CMOS, Hex Schmitt Trigger, 14-Pin DIP Socket, 14-Pin Blank Circuit Board	211-3904 100-1043 100-4743 100-1563 100-8263 100-1043 100-5633 110-1043 100-6833 228-4584 417-1400 519-0199	2 1 1 2 1 1 2 1 1 1 1

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SECTION VII DRAWINGS

7-1. <u>INTRODUCTION</u>

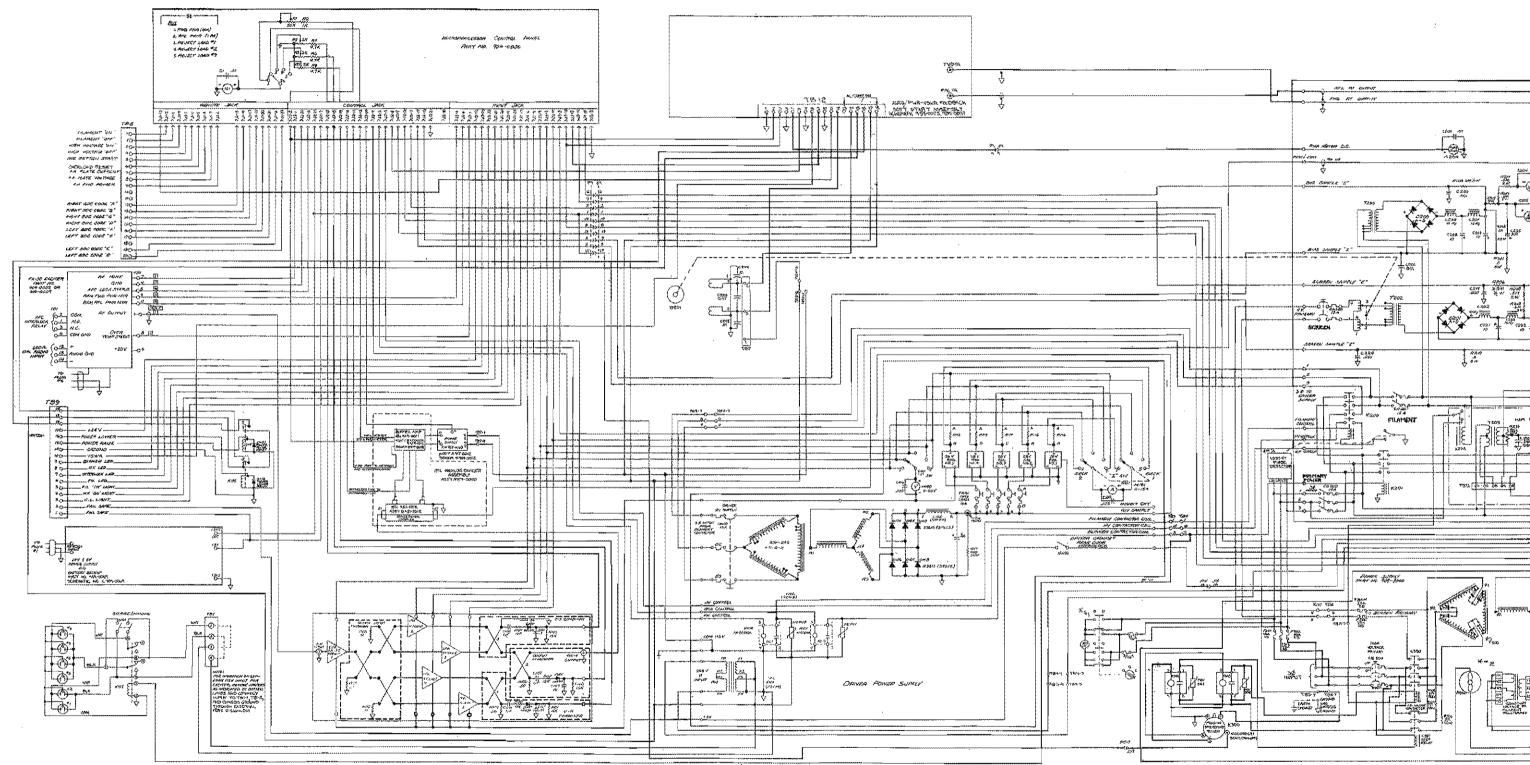
7-2. This section provides assembly drawings, schematic diagrams, and wire lists as indexed below applicable to the overall FM-30 Transmitter.

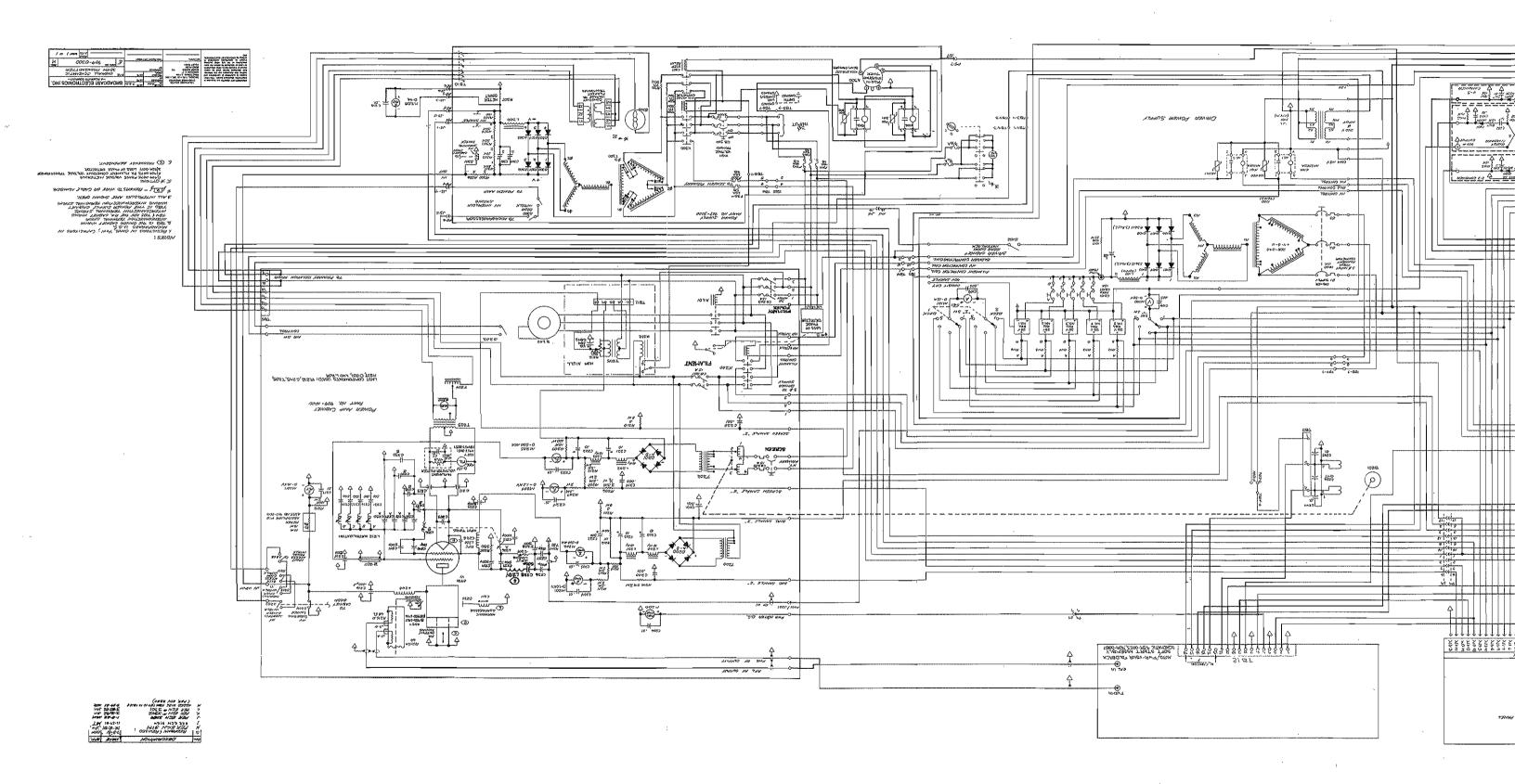
FIGURE

TITLE

NUMBER

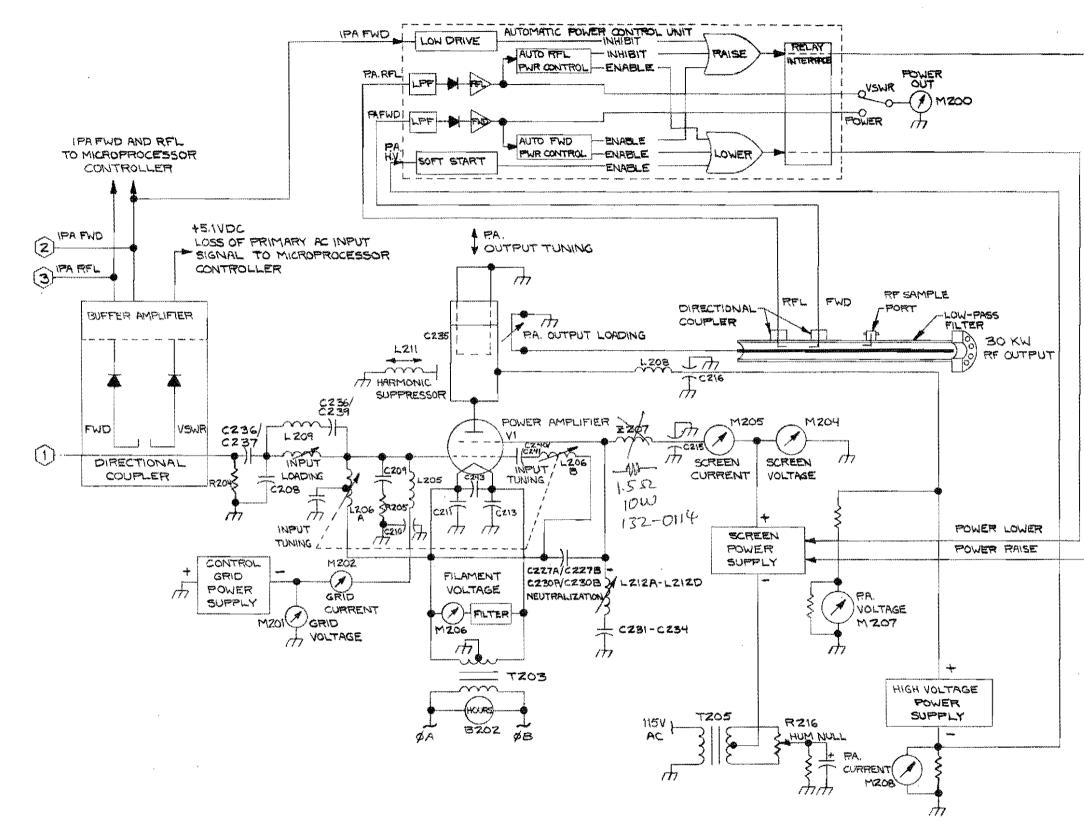
7-1 Overall Schematic, 30 kW Transmitter D909-0300





PART II

1.	POWER SUPPLIES	
2.	RF CIRCUITRY	
3.	MICROPROCESSOR CONTROLLER	



597-0003-8B

1-5/1-6

FIGURE 1-1. RF CIRCUIT SIMPLIFIED SCHEMATIC (SHEET 2 OF 2)

1-13. After amplification, the four IPA section outputs are combined in phase by three separate output combiners. First the output of amplifiers 2 and 3 are combined in hybrid 3 and the output of amplfiers 4 and 5 are combined in hybrid 1. Finally the output from hybrid 1 and hybrid 3 are combined in hybrid 2 to furnish full power output from the IPA stage. The reject load voltage on the three output combiners are monitored by the microprocessor controller for operational status. A metered display of this information is available on the DRIVER meter located on the front of the microprocessor controller. The dc voltage to each amplifier module is also monitored by the microprocessor controller as an indication of amplifier status.

1-13A. The FM-30 uses four separate IPA amplifiers and sums the output of the IPA amplifiers in two separate combiners. As all IPA amplifiers share any mismatch equally, increased isolation to high VSWR conditions is evident when compared to single combiner approaches. Evidence of the IPA stage sharing mismatches equally may be noted during tuning as a mismatch in grid tuning will cause all IPA amplifier currents to rise or fall together, indicating equal load sharing between output amplifiers. Correct phasing between amplifiers and at each hybrid coupler port is established by coaxial cables cut to the proper length (see Figure 1-2A).

1-14. A directional coupler located in the cable feeding the PA grid circuit provides dc output voltages proportional to the IPA stage forward and reflected power. The voltages are used as samples for the micro-processor controller and provide forward and reflected DRIVER meter in-dications.

1-15. PA STAGE. The PA stage contains a single 4CX20,000A/8990 tetrode operated class C in a folded half-wave cavity to output 30 kW of RF power with approximately 400 Watts of RF drive. The grid circuit is adjusted for proper operation with two inductors. The INPUT LOADING controls changes inductance with a sliding short in a hairpin configuration to match the 50 Ohm output of the IPA stage to the higher grid circuit impedance. The INPUT TUNING control is a double hairpin configuration adjusting parallel circuit inductance with two sliding shorts.

1-16. The PA tank circuit is a half-wave circuit electrically folded back on itself with no wiping or sliding contacts, blocking capacitors, or output loading capacitor (see Figure 1-3). Incorporated into the tank design is a second harmonic suppressor. Rather than attenuating the second harmonic after the signal has been generated and amplified, the circuitry in the FM-30 essentially eliminates formation of this signal.

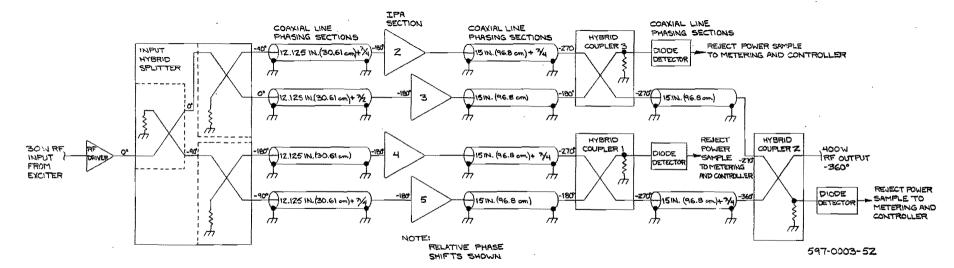
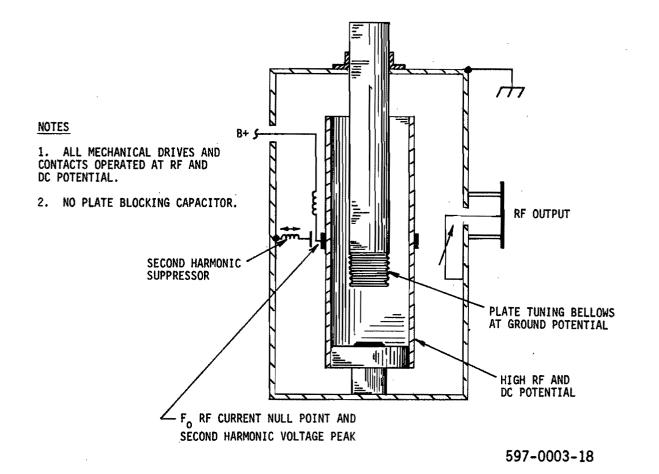


FIGURE 1-2A. FM-30 HYBRID SPLITTER/COMBINER PHASING



2

FIGURE 1-3. FM-30 PA CAVITY

1-17. Plate tuning is accomplished by adjustable bellows on the grounded or center portion of the plate line which is maintained at chassis ground potential. The PA plate potential is applied to the outer or fixed portion of plate line at the fundamental frequency RF circuit null point. As this point is also the point at which the second harmonic will peak in voltage, a basic resonant L-C circuit at this point will essentially eliminate the second harmonic.

1-18. Energy is coupled into the transmission line by an adjustable untuned link which functions in the electromagnetic field within the cavity. One end of the output link is connected to ground, while the other connects to the center conductor of the output transmission line.

1-19. A directional coupler located in the output transmission line provides RF output voltages proportional to the PA forward and reflected power. The RF output voltages are rectified and amplified to provide power and VSWR indications on the POWER OUT meter, samples for the microprocessor controller, and inputs to the automatic power control unit.

1-20. AUTOMATIC POWER CONTROL UNIT. The automatic power control unit monitors a number of transmitter parameters to function as part of a closed loop which maintains a constant RF output level from the transmitter (see Figure 1-4). As an additional function, a soft start circuit slowly increases RF power output at start to limit stress on the PA and power supply components.

1-21. PA forward and reflected power samples are input through individual low-pass filters which assure the samples will be sensed at the frequency of operation only. These samples are amplified and applied to the POWER OUT meter to provide indications of transmitter operation. The amplified power samples are also applied to the forward and reflected automatic power control circuits which control the adjustable autotransformer when the AUTO/MAN switch is set to AUTO. As RF power varies, the forward automatic power control circuit will act to maintain the established RF output level. If inadequate IPA drive exists for normal operation or if PA reflected power increases, any power increase will be inhibited. The microprocessor controller will display either of these conditions on the readout. If the PA reflected power increases to a point which may damage the external low-pass filter on the transmitter, the circuit will reduce the RF output to a safe level and the transmitter will continue to operate. Full power will be automatically reestablished when the IPA defect or VSWR condition is corrected.

1-22. As an additional function, a soft start circuit monitors PA plate voltage. This circuit reduces the PA screen potential to minimum whenever plate voltage is off. Whenever the plate voltage is energized, the circuit will gradually increase the PA screen voltage until the rated transmitter RF output is established unless limited by low IPA drive or a high VSWR condition.

1-23. <u>IPA Forward Power Sense Circuit</u>. A sample of forward power from the IPA directional coupler is input to dc amplifier U2A. The signal is amplified and applied to the inverting inputs of comparators U5A and U5B.

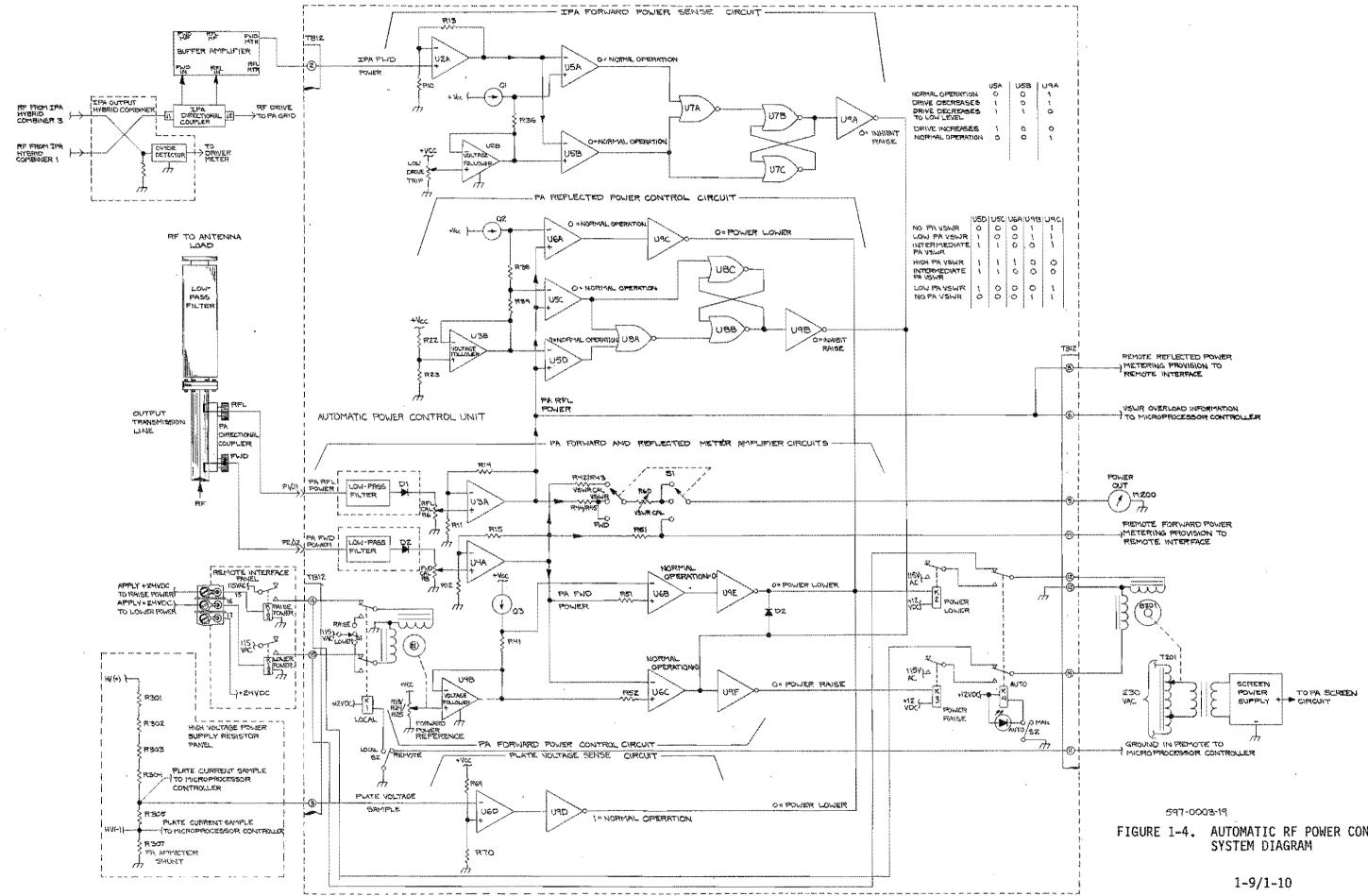


FIGURE 1-4. AUTOMATIC RF POWER CONTROL

1-24. Voltage follower U2B in combination with constant current source Q1 establishes a precise voltage drop across R36. This voltage drop creates a dead-band or window which determines how the IPA reflected power control circuit will react when IPA power falls below a level preset with R20. The circuit configuration used assures that system operation will not become erratic with minor drive power fluctuations.

1-25. The circuit remains idle when the IPA stage RF power level remains constant. If the IPA power falls and the level applied to the inverting input of U5A falls below the potential on the non-inverting input of U5A, the output of voltage comparator U5A will change states and output a HIGH. This may be considered a preset as no further action will be taken by the circuit at this time.

1-26. If IPA RF power continues to fall, the level on the inverting input of U5B will fall below the fixed reference on the non-inverting input and U5B will change states to output a HIGH. With two HIGH states input to U7A, U7A will output a LOW causing the bistable flip-flop comprising U7B and U7C to change states and input a HIGH to inverter U9A. The resultant LOW from U9A holds the output of inverter U9F HIGH which inhibits raise functions. This prevents the forward power control circuit from attempting to increase screen voltage when IPA RF power falls below a nominal range.

1-27. When IPA stage output power increases and the level on the inverting input of U5B rises above the fixed reference on the non-inverting input, U5B will output a LOW. With one LOW and one HIGH input to U7A, no further action will occur.

1-28. If IPA drive power continues to rise, the level on the inverting input of U5A will increase above the fixed reference on the non-inverting input and U5A will output a LOW. With two LOW states input to U7A, U7A will output a HIGH causing the bistable flip-flop comprising U7B and U7C to change states and input a LOW to inverter U9A. The resultant HIGH from U9A will enable inverter U9F to allow raise functions as required by the forward power control circuit.

1-29. <u>PA Reflected Power Control Circuit</u>. A dc sample of reflected power from the PA meter amplifier circuit is applied to the non-inverting inputs of comparators U5D, U5C, and U6A.

1-30. Voltage follower U3B in combination with constant current source Q2 establishes three precise voltages across the series string of resistors R38 and R39. These voltages create dead-bands or windows which determine how the PA reflected power control circuit will react when PA reflected power increases beyond the level established with R22 and R23.

1-31. The circuit remains idle when the PA reflected power is within acceptable limits. If the PA reflected power increases and the level applied to the non-inverting input of U5D rises above the fixed reference on the inverting input of U5D, the output of voltage comparator U5D will change states and output a HIGH. This may be considered a preset as no further action will be taken by the circuit at this time.

1-32. If the PA reflected power continues to rise, the level on the noninverting input of U5C will rise above the fixed reference on the inverting input and U5C will change states to output a HIGH. With two HIGH states input to U8A, U8A will output a HIGH and U5C will output a HIGH causing the bistable flip-flop comprising U8C and U8B to change states and input a HIGH to inverter U9B. The resultant LOW from U9A holds the output of inverter U9F HIGH which inhibits raise functions.

1-33. If the PA reflected power should continue to rise to the point which could cause equipment damage, the level on the non-inverting input of U6A will rise above the fixed reference on the inverting input and U6A will change states to output a HIGH to U9C. The resultant LOW from inverter U9C will energize the power lower relay to decrease the transmitter RF power output. This LOW is steered through diode D2 to hold the output of inverter U9F HIGH to assure any attempt to raise power is inhibited.

1-34. When the PA reflected power falls to a safe level and the level on the non-inverting input of U6A falls below the fixed reference on the inverting input, U6A will output a LOW. This LOW will halt the power reduction and remove the inhibit on U9F through Diode D2.

1-35. If the PA reflected power continues to fall, the level on the non-inverting input of U5C will fall below the fixed reference on the inverting input and U5C will change states to output a LOW. With one HIGH and one LOW input to U8A, the bistable flip-flop comprising U8C and U8B will be held in its present state and no further action will occur.

1-36. As the PA reflected power returns to a minimal level, the level on the non-inverting input of U5D will decrease below the fixed reference on the inverting input and U5D will output a LOW. With two LOW states input to U8A, U8A will output a HIGH causing the bistable flip-flop comprising U8C and U8B to change states and input a LOW to inverter U9B. The resultant HIGH from U9B will enable inverter U9F to allow raise functions as required by the forward power control circuit.

1-37. Forward and Reflected Meter Amplifiers. The directional coupler located in the output transmission line provides ac voltages proportional to the PA forward and reflected power. These voltages are coupled through low-pass filters which assure that harmonics do not affect the samples. The reflected power sample is rectified by diode D1, calibrated by R6, and amplified by U3A. The forward power sample is rectified by diode D2, calibrated by R8, and amplified by U4A. Five volts output by U3A represents an approximate 2:1 VSWR and five volts output from U4A represents 100% forward power (preset at factory for customer specified power level).

1-38. The reflected power is applied to the PA reflected power control circuit, the processor for VSWR overload information, and the metering circuit. The forward power sample is applied to the forward PA power control circuit and the metering circuit. All metering information is applied to the VSWR CAL/VSWR/FWD switch and displayed by the POWER OUT meter.

1-39. <u>PA Forward Power Control Circuit</u>. A sample of forward power from the PA meter amplifier circuit is applied to the non-invering input of U6B and the inverting input of U6C.

1-40. Voltage follower U4B in combination with constant current source Q3 establishes a precise voltage drop across R41. This voltage drop creates a dead-band or window which determines how the PA forward control circuit will react when PA output power differs from the level preset with B1/R18. The circuit configuration used assures that system operation will not become erratic with minor power fluctuations.

1-41. The circuit is idle when the transmitter output power remains established at the correct level. If the PA forward input falls below the fixed reference on the bottom of R41, comparator U6C will change states and output a HIGH. The resultant LOW from inverter U9F will energize the power raise relay until the correct transmitter RF output power is sensed by the PA directional coupler and input to U6C.

1-42. If the PA forward input rises above the fixed reference on the top of R41, comparator U6B will change states and output a HIGH. The resultant LOW from inverter U9E will energize the power lower relay until the correct transmitter RF output power is sensed by the PA directional coupler and input to U6B. This LOW is coupled through diode D2 to hold the output of inverter U9F HIGH to assure any attempt to raise power is inhibited. 2

1-43. Remote control of the forward power control circuit is permitted through +24 volt inputs to the remote interface panel when the AUTO/MAN switch is set to AUTO and the LOCAL/REMOTE switch is set to REMOTE. The level set by R18 is varied by remote control of motor B1. If the AUTO/MAN switch is switched to MAN, control of the screen transformer motor control circuit is removed from the PA forward power control circuit and is routed directly to the remote interface power control relays to allow remote power control. When the LOCAL/REMOTE switch is set to LOCAL, screen control may be accomplished with the transmitter front panel RAISE/LOWER switch. Whenever the AUTO/MAN switch is set to MAN, screen control must be accomplished with the transmitter front panel SCREEN control.

1-44. <u>Plate Voltage Monitor Circuit</u>. A plate voltage sample derived from the high voltage bleeder resistor chain is applied to the inverting input of voltage comparator U6D in the plate voltage monitor circuit. When the plate voltage sample decreases below the fixed level on the noninverting input of U6D (such as when PLATE OFF is depressed), U6D will output a HIGH. The resultant LOW from inverter U9D will energize the power lower relay to minimize the transmitter RF power output. This LOW is coupled through diode D2 to hold the output of inverter U9F HIGH to assure any attempt to raise power is inhibited. Consequently, whenever the transmitter is deenergized, the automatic power control system will hold U9D LOW to maintain zero screen voltage.

1-45. When the PLATE ON swtich/indicator is depressed and the high voltage sample on the inverting input of U6D rises above the fixed reference on the non-inverting input, U6D will output a LOW. This LOW will remove the inhibit on U9F through diode D2 and allow the PA forward power control unit to reestablish RF power output unless limited by low IPA drive or a high VSWR condition.

SECTION II

RF CIRCUIT MAINTENANCE

2-1. INTRODUCTION

2-2. This section provides maintenance information for the FM-30 FM transmitter RF circuitry.

2-3. SAFETY CONSIDERATIONS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND THE SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-4. The FM-30 transmitter contains high voltages and currents which, if regarded carelessly, could be fatal. The transmitter has many built-in safety features, however, good judgement, care, and common sense are the best accident preventives. The maintenance information contained in this section should be performed only by trained and experienced maintenance personnel.

2-5. It is very dangerous to attempt to make measurements or replace components with power energized, therefore such actions are not recommended. The design of the equipment provides safety features such that when a door or access panel is opened, interlock switches will deenergize the plate and screen power supplies. Do not short out or bypass interlock switches as a maintenance short cut.

2-6. The power supply cabinet and the PA cabinet contain switches which discharge the PA plate potential directly to ground whenever either cabinet is opened.

2-7. Grounding sticks are provided as safety features. Each grounding stick consists of a metal rod with a phenolic handle. The metal end is connected to chassis ground. Use a grounding stick to touch every part in the area or circuit on which maintenance is to be performed before attempting maintenance.

2-8. The grounding stick in the high voltage power supply cabinet and the grounding stick in the PA cabinet both rest on hook switches. When either of these grounding sticks is removed, the associated hook switch opens the transmitter interlock string and deenergizes the transmitter PA and screen potentials until each grounding stick is replaced on its respective hook switch.

2-9. MAINTENANCE



ENSURE THE REMOTE/LOCAL SWITCH IS SET TO LOCAL BEFORE ATTEMPTING MAINTENANCE.



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND THE SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-10. GENERAL

2-11. The FM-30 maintenance philosophy consists of preventative maintenance such as cleaning applied to the equipment to forestall future failures and second level maintenance consisting of procedures required to restore the equipment to operation after a fault.

2-12. PA STAGE. Power amplifier tube life is a result of several circuit parameters. Usually, the first indication of the decline of a tube is a slight reduction in power output. This can normally be corrected by a small increase in filament voltage. It may be wise to order a new tube at this time. Further reductions in power output can be compensated in the same manner only a limited number of times. Excess grid or screen dissipation is detrimental to the life expectancy of a tube. Also, excess plate dissipation signals nothing but trouble.

2-13. Occasionally a bit of heavy lubricant should be applied sparingly to the drives and tuning mechanism, especially the right angle gear drives.

2-14. IPA STAGE. The transistors in the IPA RF modules will normally last many times longer than the power amplifier tube unless some major problem occurs. An open circuit on the output, an extreme output VSWR, or an over voltage condition due to a regulator malfunction can shorten the life of the transistors. One indication of a transistor fault will be that IPA amplifier module RF output power will slowly decline while the dc input power remains constant. Under no circumstances should the RF input from the exciter be increased over 10% above that indicated by the factory test data sheets. When the driver output power declines with a fixed power input, the fault will usually be traced to mistuning, a high VSWR condition, or a faulty transistor and/or regulator.

WARNING

NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND THE SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-16. Adjustment of many controls is considered obvious and may be accomplished with the information provided on the applicable schematic diagram. The following information is provided to assist adjustment of the more complex adjustments. However, it is never suggested that maintenance be performed on any circuitry within the transmitter with power applied to any portion of the transmitter.

2-17. SECOND HARMONIC TRAP. Adjustment of the second harmonic trap in the field will not normally be required, even if the PA tube is replaced. Adjustment should be attempted only when absolutely necessary. If it is certain that adjustment of the second harmonic trap is required, proceed as follows.

2-18. <u>Required Equipment</u>. The following equipment is required to complete adjustment of the second harmonic trap.

- A. 5.64 inch (0.2 cm) hex wrench.
- B. Tektronix 7613 Oscilloscope with 7L12 Spectrum Analyzer plug-in accessory or the equivalent capable of displaying frequencies at twice the frequency of operation.
- C. 50 Ohm 10 dB resistive attenuator pad, BNC jack to BNC plug (Texscan FP-50).
- D. A cable for the spectrum analyzer comprising the following:
 - 10 feet (3.05 m) of Belden RG 58A/U coaxial cable (BE P/N 622-0050).
 - 2. Two BNC plugs (Pomona UG88/U--BE P/N 417-0205).

2-19. <u>Procedure</u>. To adjust the second harmonic trap, proceed as follows:



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

WARNING: DISCONNECT POWER PRIOR TO SERVICING

2-20. Deenergize all primary power to the transmitter.

2-21. Open the PA cabinet rear door.

2-22. Loosen the hex-head lock-screw securing the second harmonic trap adjustment rod very slightly--just enough to allow in and out adjustment.

2-23. Close and lock the PA cabinet rear door.

2-24. Connect one end of the spectrum analyzer cable (Item D) to the RF sample port (J1) on the elbow just before the low-pass filter.

2-25. Connect the attenuator pad (Item C) in series with the cable and attach the attenuator pad to the spectrum analyzer input.

2-26. Energize the transmitter primary ac input.

2-27. Operate the transmitter at the normal power output and ensure all PA stage turning and loading controls are correctly adjusted.

2-28. Record the level of the second harmonic displayed on the spectrum analyzer .

WARNING

DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.

2-29. Disconnect all transmitter primary power.

2-30. Open the PA cabinet rear door.

CAUTION

THE SECOND HARMONIC SUPPRESSOR IS ADJUSTED BY SLIDING THE ADJUSTMENT ROD IN OR OUT. DO NOT ROTATE THE ROD.

2-31. Move the second harmonic trap adjustment rod slightly. Record the amount moved and the direction (in or out)

2-32. Close and lock the PA cabinet rear door.

2-33. Energize the transmitter primary ac input and operate the transmitter at the normal power output.

2-34. Repeat paragraphs 2-28 through 2-88, moving the second harmonic trap adjustment rod slightly in or out as required to minimize the second harmonic indication.

WARNING: DISCONNECT POWER PRIOR TO SERVICING

WARNING

DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.

-2-35. After the correct setting of the second harmonic suppressor is determined, disconnect all transmitter primary power.

2-36. Open the PA cabinet rear door.

2-37. Secure the hex-head lock-screw on the second harmonic trap adjustment rod.

2-38. Close and lock the PA cabinet rear door.

2-39. Disconnect the spectrum analyzer cable from J1 on the elbow just before the low-pass filter.

2-40. NEUTRALIZATION. PA neutralization in the field will not normally be required, even if the PA tube is replaced. If it is certain that adjustment of the neutralization circuitry is required, proceed as follows.

2-41. <u>Required Equipment</u>. The following equipment is required to complete PA neutralization.

A. RF microvoltmeter, 100 MHz, 1 millivolt scale (Boonton Electronics Corporation Model 92 B or equivalent with the following items):

- 1. RF probe (Boonton Model 91-12F).
- 2. 50 Ohm probe adapter (Boonton Model 91-88).
- 3. Adapter, BNC plug-to-plug (Pomona UG 491 A/U).

B. Locally fabricated adapter cable comprising the following:

- 1. 36 inches (91.44 cm) of Belden RG 58A/U coaxial cable (BE P/N 622-0050).
- 2. Two BNC plugs (Pomona UG88/U--BE P/N 417-0205).

C. Adapter, BNC receptacle to type N plug (Pomona UG 201A/U--BE P/N 417-3288).

D. No. 1 Phillips offset screwdriver.

E. Flat tip screwdriver, 4 inch (10.16 cm) blade and 1/4 inch (0.635 cm) tip.

F. AC extension cord, 3-wire, 12 feet (3.7 mm) long.

2-42. Procedure. To adjust PA neutralization, proceed as follows:

2-43. Operate the transmitter at the normal power output and ensure all PA stage tuning and loading controls are correctly adjusted.

2-44. Secure the INPUT LOADING, P.A. OUTPUT TUNING, and P.A. OUTPUT LOADING control knobs in position with tape. The controls must not be moved until the entire procedure has been completed.

2-45. Record the INPUT TUNING cyclometer indication,



ENSURE ALL TRANSMITTER PRIMARY POWER IS DIS-CONNECTED BEFORE OPENING THE EQUIPMENT.

2-46. Deenergize all primary power to the transmitter.

2-47. Open the IPA cabinet rear door.

2-48. Disconnect the coaxial cable from the exciter RF OUTPUT connector.

2-49. Disconnect the cable from the input to the IPA directional coupler (front connector) mounted to the cabinet right side rail.

2-50. Connect the BNC receptacle-to-type N plug adapter to the IPA directional coupler input.

2-51. Connect the adapter cable between the adapter on the IPA directional coupler input and the exciter RF OUTPUT connector.

2-52. Disconnect wire No. 1 from TB1 terminal 7 on the rear of the exciter and connect a temporary wire jumper from TB1 terminal 6 to TB1 terminal 7.

2-53. Connect the exciter to an external power source with an electrical extension cord.

2-54. Route the extension cord along the cabinet base. Close and lock the IPA cabinet rear door.

2-55. Connect the RF microvoltmeter (item A) to the RF sample port in the output transmission line. Adjust the meter to the 1 microvolt scale and position the meter so that the scale may be viewed from the front of the FM-30.

WARNING

THREE-PHASE PRIMARY AC POWER MUST REMAIN OFF THROUGHOUT THE FOLLOWING PROCEDURE.

2-56. Energize the exciter ac input only. The three phase primary ac input must remain deenergized as the following procedure is completed without power applied.

2-57. Ensure the exciter is operating.

2-58. Depress the exciter RFL switch.

2-59. Adjust the INPUT TUNING control to minimize the exciter VSWR indication.

2-60. Secure the INPUT TUNING control in position with tape. The control must not be moved until the entire procedure has been completed.

2-61.

Open the PA cabinet front door and note the grounding stick.

WARNING

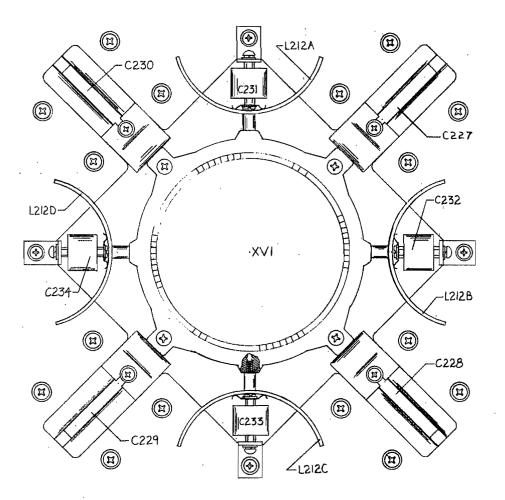
USE THE GROUNDING STICK PROVIDED TO ENSURE NO PA TUBE POTENTIALS ARE PRESENT IN THE FOLLOWING STEP BY GROUNDING THE PA TUBE PLATE AND SCREEN CONNECTIONS BEFORE PROCEEDING.

Open the PA cabinet access door and ground the PA tube plate 2-62. and screen connections to ensure no potentials are present in the cavity before attempting to touch anything within the cavity.

2-63. After it has been determined that no PA tube potentials are present, mark the position of the four neutralization adjustments. Correct neutralization will be found very close to the present position of the neutralization adjustments.

2-64. Loosen the retaining screws in the bottom of each capacitor mounting bracket very slightly--just enough to allow adjustment. The capacitors can be swung in an arc, restricted only by the ends of the neutralizing segments.

2-65. When the neutralization procedure is properly completed, the four capacitors will be positioned approximately in the same relative location and direction relevant to the axis of the tube socket. Each capacitor fingerstock contact must rest on its respective neutralizing segment entirely, without exception (see Figure 2-1).



597-0003-38

FIGURE 2-1. PA NEUTRALIZATION

2-66. Neutralization is adjusted in the following manner.

A. Remove all foreign objects from the cavity and close the cavity access door.

B. Note the millivoltmeter indication.

C. Open the cavity access door and adjust one capacitor very slightly.

D. Remove all foreign objects from the cavity and close the cavity access door.

E. Note the change in the millivoltmeter indication.

F. Repeat steps A through E until a minimum millivoltmeter indication is noted and secure the capacitor.

G. Repeat steps A through F for the remaining segments.

H. Ensure the following conditions exist before closing the cavity access door:

1. Each capacitor contact plate rests completely against its respective neutralizing segment entirely.

2. All four capacitors are secured.

2-67. Close the cavity access door and replace the grounding stick in its hanger.

2-68.

Disconnect the millivoltmeter from the output transmitter line.

WARNING

ENSURE ALL TRANSMITTER PRIMARY POWER IS DIS-CONNECTED BEFORE OPENING THE EQUIPMENT.

2-69. Deenergize all primary power to the transmitter.

2-70. Open the IPA cabinet rear door.

2-71. Remove the electrical extension cord and reconnect the exciter power cord to the driver cabinet ac outlet strip.

2-72. Remove the test cable and adapter between the exciter and IPA directional coupler input.

2-73. Replace the IPA input cable on the exciter RF OUTPUT connector.

2-74. Replace the IPA output cable on the IPA directional coupler input.

2-75. Remove the temporary wire jumper from TB1 on the exciter rear panel and reconnect wire No. 1 to TB1-7.

2-76. Close and lock the IPA cabinet rear door.

2-77. Readjust the INPUT TUNING control to the indication recorded in paragraph 2-30.

2-78. IPA MODULE TUNING. Due to the complexity of the procedure, field adjustment of the entire IPA section is not recommended. If it is certain that total adjustment of the entire IPA section is required, contact the Broadcast Electronics, Inc. Customer Service Department for a recommended procedure. The following procedure provides information required to adjust the IPA Section MODULE 1 BASE TUNING and INPUT LOADING controls to maximize the match between the exciter and IPA section.

2-79. <u>Required Equipment</u>. The following equipment is required to adjust the IPA section MODULE 1 BASE TUNING and INPUT LOADING controls.

A. Insulated adjustment tool, flat screwdriver tip (BE P/N 710-0001).

2-80. <u>Procedure</u>. To adjust the IPA section MODULE 1 BASE TUNING and INPUT LOADING controls, proceed as follows:

2-81. With the transmitter operational, depress the exciter RFL switch.

2-82. Alternately, adjust the IPA stage MODULE 1 INPUT LOADING and BASE TUNING controls to minimize the exciter reflected power indication.

2-83. AUTOMATIC POWER CONTROL UNIT. To adjust the automatic power control unit, remove the panel adjacent to the AUTO/MAN switch. Adjustment data is provided by Figure 2-2.

2-84. TROUBLESHOOTING



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING MAINTENANCE.

2-85. Most troubleshooting consists of visual checks. Because of the voltages and high currents in the equipment, it is considered hazardous to work with power energized. Therefore, the various transmitter indications (meters, LEDs, fuses, and the digital read-out) should be used to isolate the malfunction to one specific area.

CAUTION

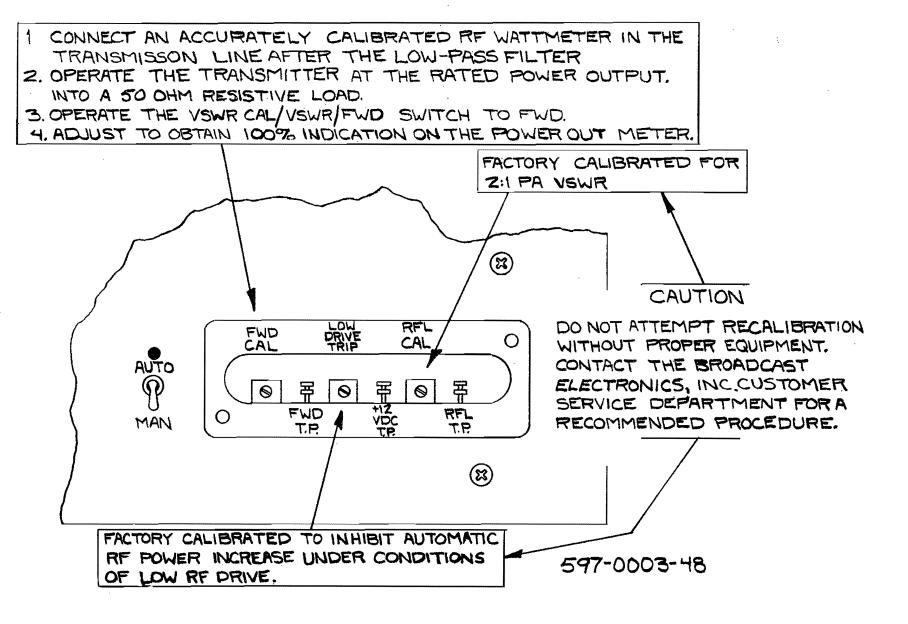
THE IPA STAGE RF AMPLIFIER TRANSISTORS ARE ATTACHED TO A LARGE HEAT SINK. ENSURE A THIN FILM OF A ZINC-BASED HEAT-SINK COM-POUND IS USED (BE P/N 700-0028) WHENEVER AN AMPLIFIER DEVICE IS INSTALLED.

2-86. Once the trouble is isolated and power is totally deenergized it is suggested that the exact problem be located with resistance checks using the schematic diagrams and theory of operation presented throughout the text. IPA stage RF cabling is shown in Figure 2-3.

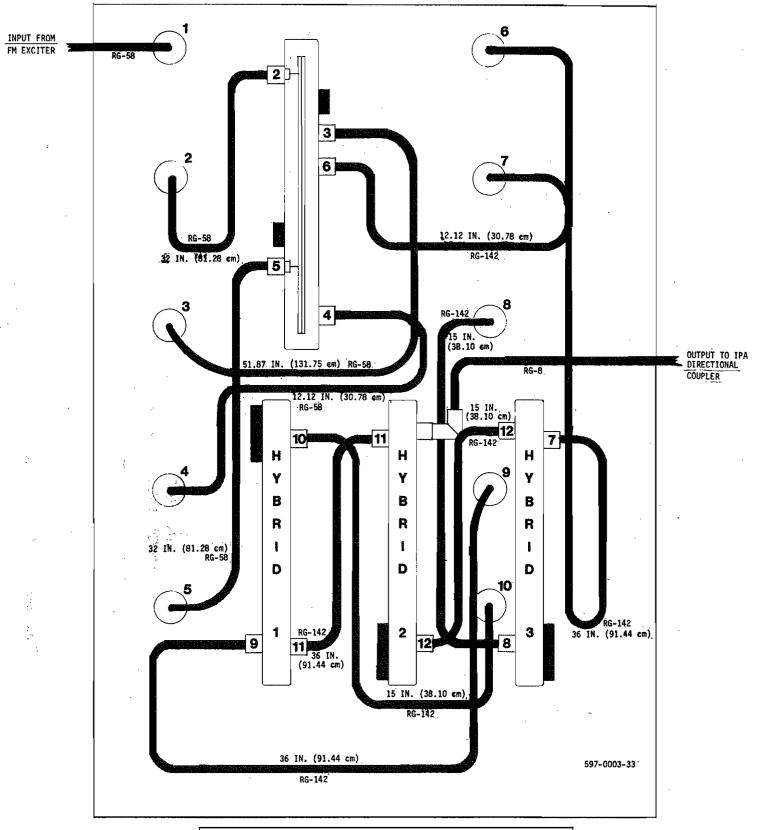
2-87. If a circuit is diagnosed as faulty, the circuit fault may be isolated and repaired locally or the entire device may be returned to Broadcast Electronics, Inc. for exchange, alignment, or replacement.

FIGURE 2-2. AUTOMATIC POWER CONTROL UNIT ADJUSTMENTS

2



2-11



CABLE INFORMATION				
CABLE MANUFACTURER		MANUFACTURERS TYPE	BE P/N	
RG-58 C/U	BELDEN	8262	622-0050	
RG-8 A/U	BELDEN	9251	622-9251	
RG-142 B/U	BELDEN	83242	621-0001	

FIGURE 2-3. IPA STAGE RF AMPLIFIER CABLING

ς.

SECTION III

RF CIRCUIT DRAWINGS

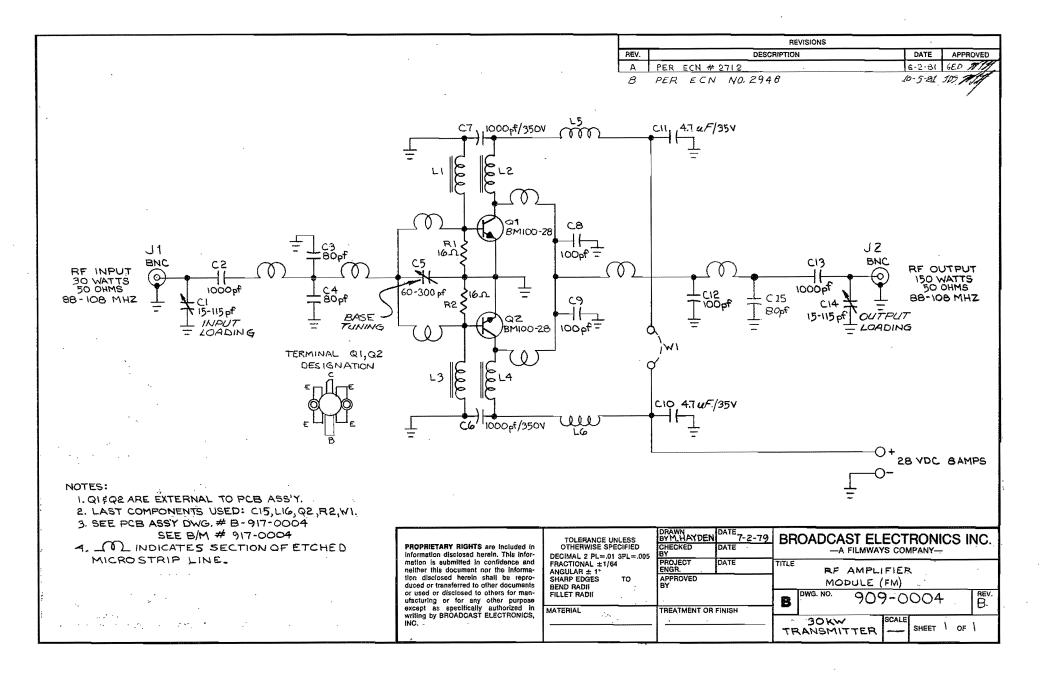
3-1. INTRODUCTION

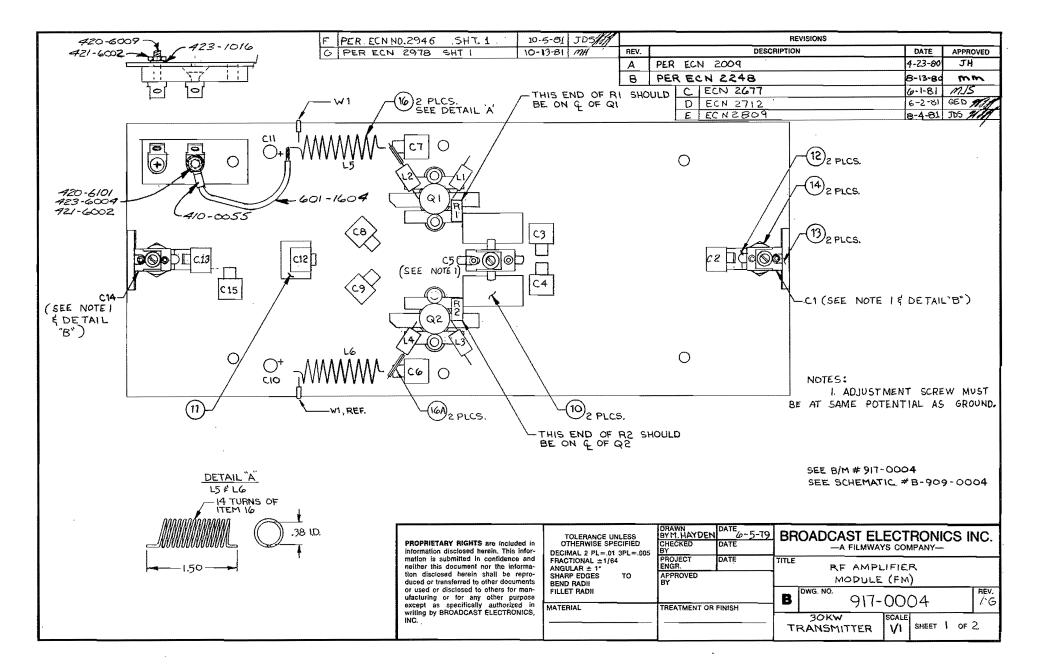
3-2. This section provides assembly drawings, schematic diagrams, and wire lists as indexed below for the FM-30 Transmitter RF circuitry.

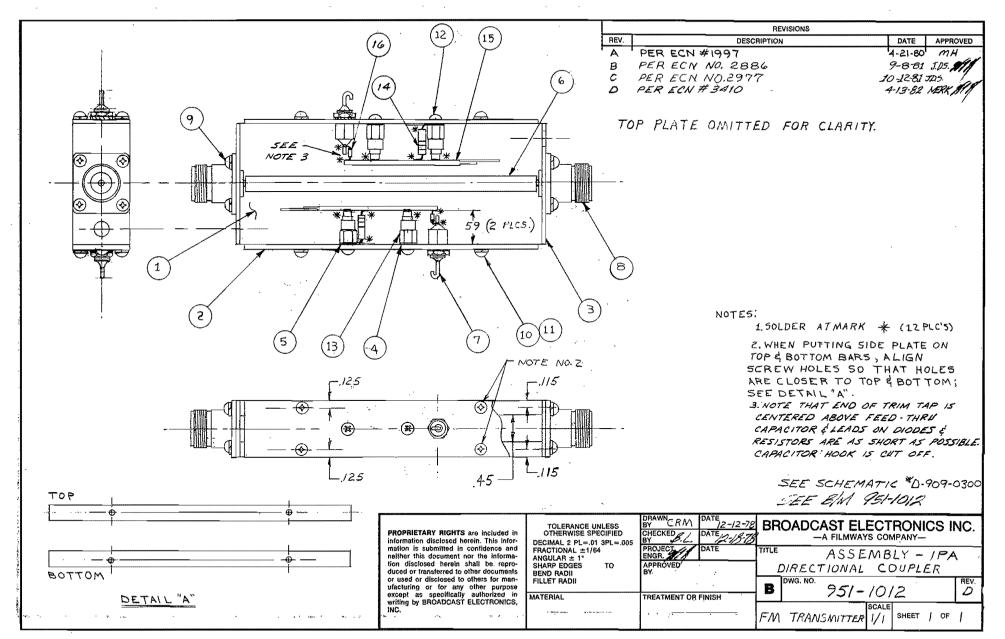
FIGURE	TITLE	NUMBER
3-1	Schematic, IPA RF Amplifier	B909-0004
3-2	Assembly, IPA RF Amplifier	B917-0004
3-3	Assembly, IPA Directional Coupler	B951-1012
3-4	Assembly, IPA Directional Coupler Buffer Amplifier	B955-0001
3-5	Schematic, IPA Directional Coupler Buffer Amplifier	B979-0058
3-6	Assembly, IPA Directional Coupler Buffer Amplifier Circuit Board	8919-0011
3-7	Assembly, IPA Hybrid Combiner Diode Detector	A917-0009
3-8	Assembly, PA Cabinet Input Circuit	597-0003-37A,B
3-9	Assembly, IPA Ammeter Meter Shunt Board	B955-0031
3-10	Schematic, IPA Multimeter	B909-0020
3-11	Assembly, IPA Multimeter	A917-0020
3-12	Schematic, Automatic Power Control Unit Assembly	D979-0032
3-13	Assembly, Automatic Power Control Unit Power Supply and Control Assembly	C919-0032
3-14	Assembly, Automatic Power Control Unit Low-Pass Filter	B919-0031
3-15	Schematic, Automatic Power Control Unit Circuit Board	D979-0033
3-16	Assembly, Automatic Power Control Unit Circuit Board	C919-0033
3-17	Schematic, Screen and Bias Supply Metering Board	B909-0026
3-18	Assembly, Screen and Bias Supply Metering Board	B917-0026
3-19	Assembly, Hours Meter Filter Circuit Board	A917-0051
3-20	Assembly, PA Meter Multiplier	B917-0016
3-21	Final Assembly, PA Directional Coupler	B950-6907
3-22	Sub-Assembly, PA Directional Coupler	B950-6906

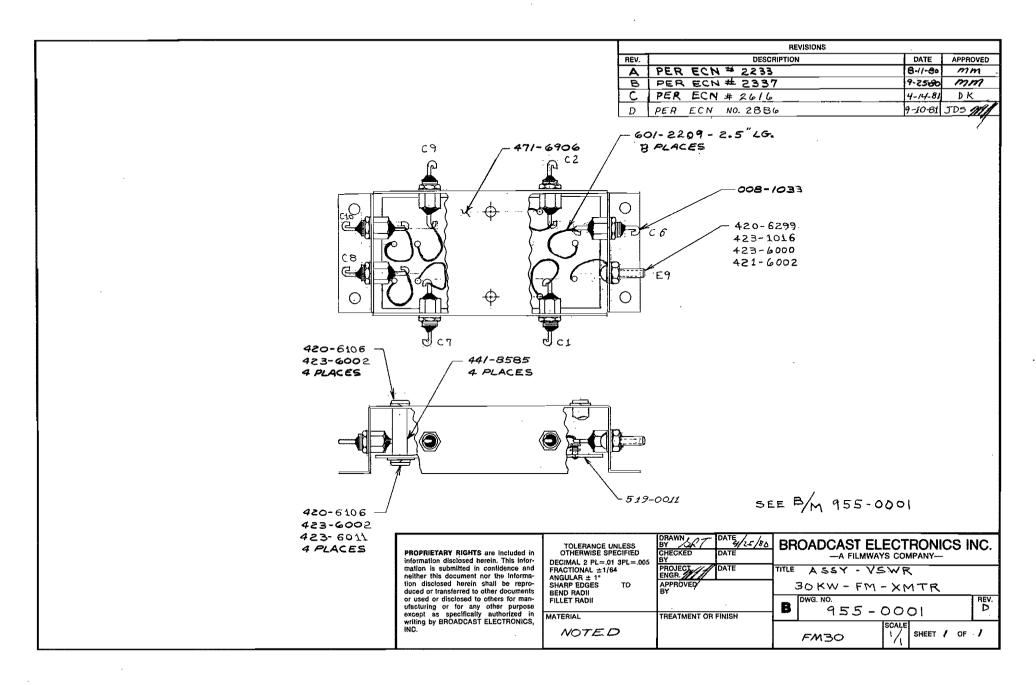
3-1/3-2

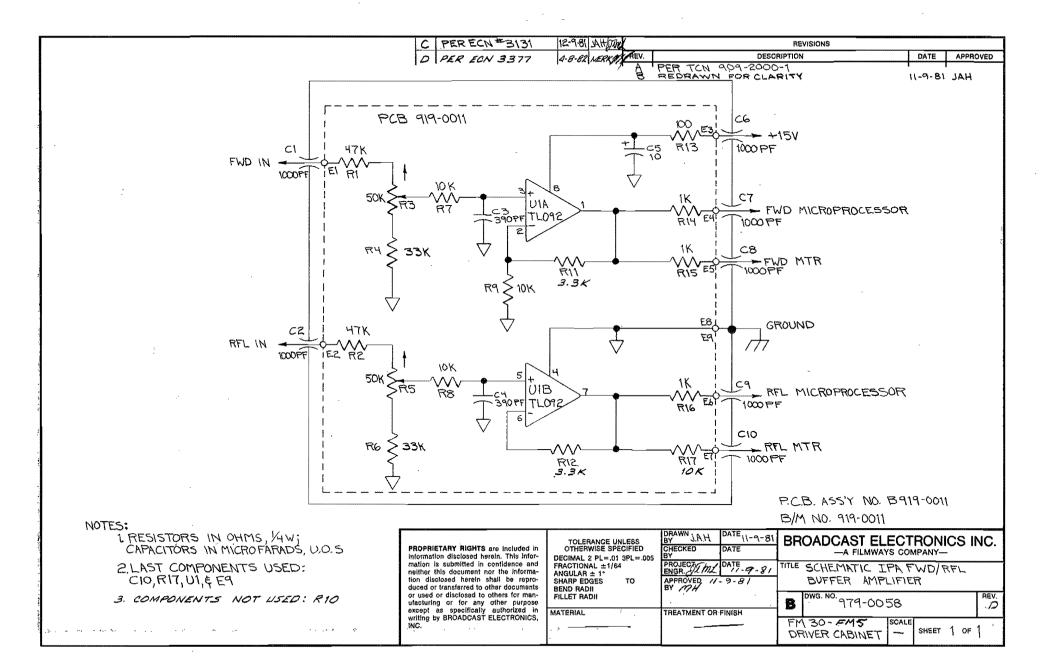
2

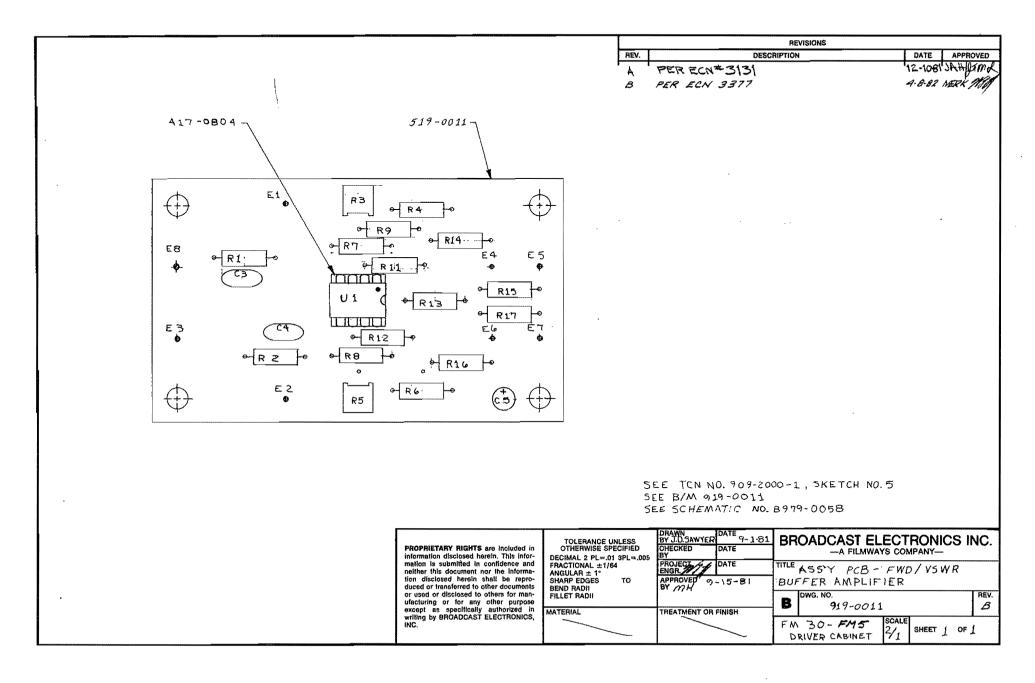












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PROPRIETARY RIGHTS are included in information disclosed herein. This information is submitted in confidence and	TOLERANCE UNLESS OTHERWISE SPECIFIED DECIMAL 2 PL=.01 3PL=.005	DRAWN BYM.HAYDEN DATE CHECKED DATE BY DATE	—A FILMWAYS C	TRONICS INC.
mation is submitted in confidence and neither this document nor the informa- tion disclosed herein shall be repro- duced or transferred to other documents or used or disclosed to others for man- ufacturing or for any other purpose except as specifically authorized in writing by BROADCAST ELECTRONICS, INC.	FRACTIONAL ±1/64 ANGULAR ± 1° SHARP EDGES TO BEND RADII FILLET RADII MATERIAL	PROJECT DATE ENGR. APPROVED BY TREATMENT OR FINISH	TITLE ASSE HYBRID COMBINER DIC DWG. NO. 917-00 TRANSMITTER SCAL 2/	

POWER SUPPLIES

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SECTION I

POWER SUPPLY THEORY OF OPERATION

1–1. INTRODUCTION

1-2. The following text provides detailed theory of operation with supporting diagrams for the FM-30 FM transmitter power supplies. For purposes of definition, the text is divided into functional circuits (see Figure 1-1).

1-3. SEQUENCE OF OPERATION

1-4. Three-phase power is distributed throughout the transmitter circuitry whenever primary power is applied to the transmitter.

1-5. When the high voltage power supply HIGH VOLTAGE PRIMARY circuit breaker is closed, power is applied to the start contactor and the step relay. When the PA cabinet PRIMARY POWER circuit breaker is closed, power is applied to the hum null circuit, the filament relay, the blower contactor, and the primary isolation transformer. The primary isolation transformer applies 115 Vac power to the IPA direct-ional coupler buffer power supply, the microprocessor controller power supply, and the accessory control relay and accessory outlets in the driver cabinet.

1-6. When the FILAMENT ON switch is depressed, the blower relay will close. At the same time, the accessory control relay in the driver cabinet will energize and apply power to the exciter and optional equipment. After the blower comes up to speed and closes the air switch, the filament relay will close and apply power to the control grid power supply, the PA filament circuit, and the IPA power supply.

1-7. Assuming the HIGH VOLTAGE ON switch has been depressed, the start sequence will continue after a 15 second delay to allow PA tube heating. When the PA tube heating delay expires, the step/start timer will energize the step relay, then energize the start contactor, then deenergize the step relay to apply full power to the plate and screen supplies.

1-8. If the power to the filament supply should open during operation, the high voltage filament interlock relay will open the start contactor and deenergize the plate and screen supplies.

1-9. When the HIGH VOLTAGE OFF switch is depressed, the start contactor will open immediately and deenergize the plate and screen supplies. When the FILAMENT OFF switch is depressed, the remainder of the transmitter supplies will deenergize. The blower will continue to operate for 15 seconds to allow the PA stage to cool.

1-10. FUNCTIONAL DESCRIPTION

1-11. A 196 to 252 volt, 60 Hz, three-phase ac input from a closed delta or wye power source is required for proper operation of the FM-30 transmitter. The following supplies operate from the three-phase input. All values shown are typical for 30 kW operation.

Α.	PA PLATE	+9300V at 4.2 Amperes
Β.	PA SCREEN GRID	+500V at 0.240 Amperes
С.	PA CONTROL GRID	-290V at 0.140 Amperes
D.	PA FILAMENT	10 Vac at 140 Amperes
E.	IPA	+36V at 37.5 Amperes
	1. IPA RF MODULE	+27.5V at 7.5 Amperes
F.	IPA DIRECTIONAL COUPLER BUFFER	+15V at 0.1 Amperes +5.1V at 0.01 Amperes
G.	AUTOMATIC POWER CONTROL UNIT	+12V at 0.1 Amperes
Η.	CONTROLLER	+24V at 2 Amperes +5V at 0.3 Amperes
Ι.	AUXILIARY AC	AC input to exciter, stereo

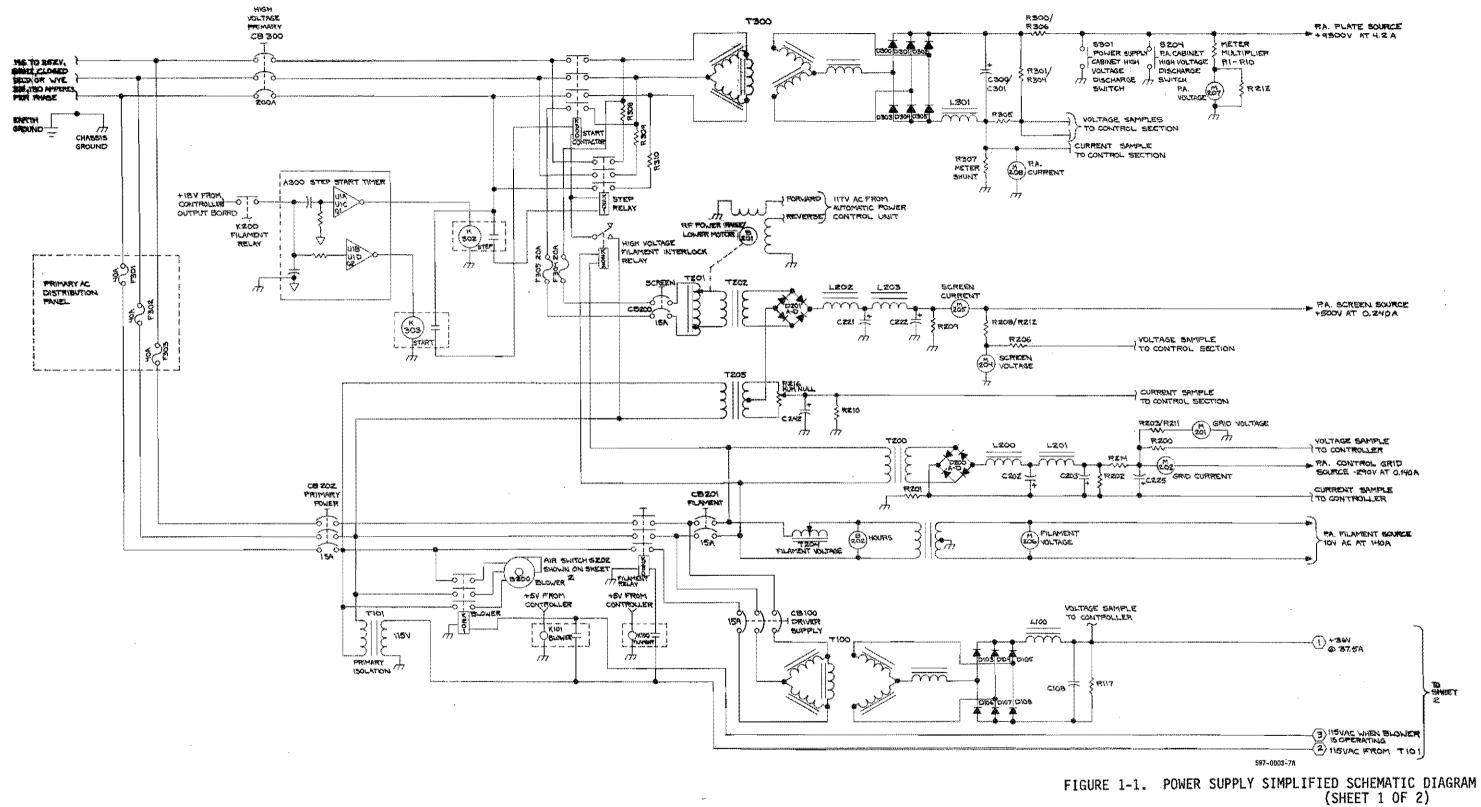
generator, SCA generator, etc.

1–12. PA PLATE POWER SUPPLY

1-13. The high voltage power supply is a three-phase primary, sixphase secondary supply. The primary circuit is connected in a closed delta arrangement and protected by circuit breaker CB300. Component stress at power on is eliminated by a step/start circuit which limits supply inrush current.

1-14. A +18 volt "high voltage on" signal from the controller is applied to a circuit containing two dual schmitt-trigger drivers. The input is interlocked through contacts of the filament relay to assure that the filament circuit is energized before a high voltage on sequence is initiated. The step driver energizes the step relay to energize the primary of T300 through three limiting resistors. After a short delay, the second schmitt-trigger driver will energize the start contactor and apply the full primary potential to T300. The step relay will deenergize after the relay has been energized for 160 milliseconds. In this manner the current limiting resistors will only be subject to heating during the short interval between step and start closures.

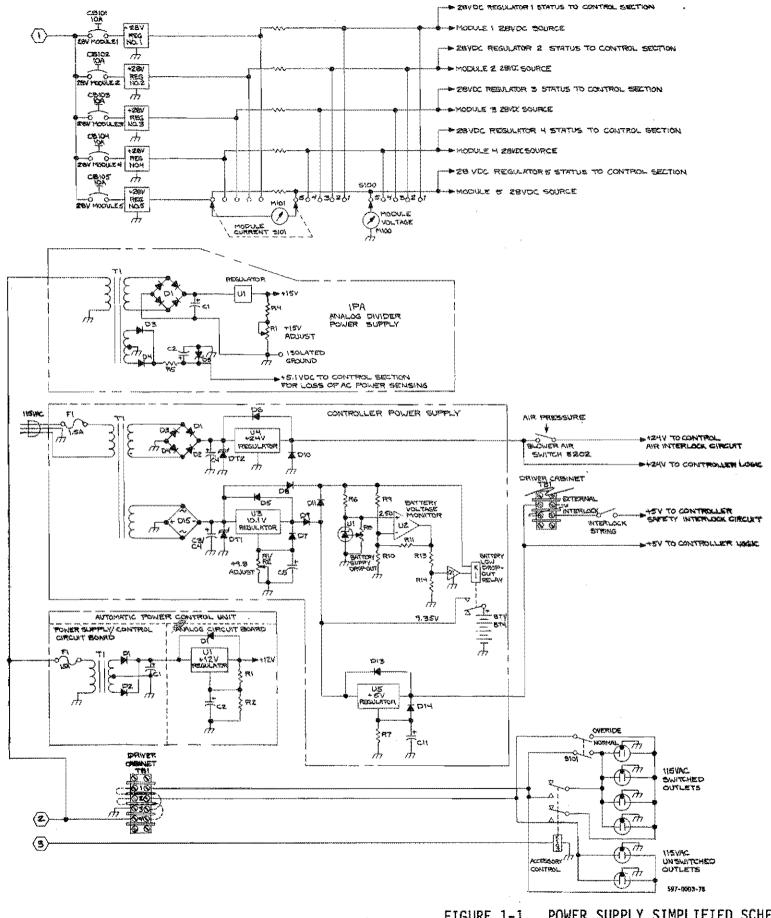
1-15. The secondary of the high voltage transformer is connected in a wye configuration. Due to the physical construction of the transformer, each phase appearing in the secondary will lead and lag a respective phase appearing in the primary by 60 degrees. The secondary phase separation of 60 degrees divided into one primary phase of 360 degrees equals six secondary phases.



1-3/1-4

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1-5/1-6

FIGURE 1-1. POWER SUPPLY SIMPLIFIED SCHEMATIC DIAGRAM (SHEET 2 OF 2)

1-16. Little filtering is required as only 4.2 percent ripple is output from the rectifiers. One requirement of the multiphase supply, however is that the primary ac input must be balanced to within the percentage of ripple voltage which is to be obtained from the supply. Constant primary ac line unbalance can be corrected by the use of primary taps or a tapped three-phase autotransformer.

1-17. Filtering for the supply is accomplished by a one-section choke-input filter. The choke is inserted in the negative leg of the rectifier output to eliminate the dc potential between the choke and ground. The negative leg of the supply is referenced to ground through the PA stage current meter shunt. Bleeder resistors connected across the supply increase regulation and in conjunction with interlocked high voltage discharge switches, enhance safety. A series resistance in the anode dc feedline limits peak energy in case of arc-overs in the power amplifier stage or grounding switch operations.

1-18. Status outputs from this supply provide voltage and current samples to the microprocessor controller and a voltage sample to the automatic power control unit.

1-19. PA SCREEN GRID POWER SUPPLY

1-20. The screen power supply is a full-wave bridge rectified supply with a two section filter. The primary of the screen transformer is connected through CB200 to two phases of the three-phase ac input to the high voltage power supply transformer. The output of the screen supply is manually adjustable with a variable autotransformer connected in the primary of the screen transformer. A motor connected to the variable autotransformer allows remote adjustment. The ground return path for the screen supply is routed through the hum null circuit which introduces a small 60 Hz component into the screen supply to cancel hum. The amount of voltage added to the negative side of the screen supply is adjusted by R216.

1-21. Status outputs from the screen supply provide voltage and current samples to the microprocessor controller.

1-22. PA CONTROL GRID POWER SUPPLY

1-23. The control grid bias supply is a full-wave bridge rectified supply with a two section filter. The primary of the supply is connected across two phases of the three-phase ac input at the filament relay. Circuit breaker CB201 provides overload protection for the supply. Voltage and current samples from the supply are applied to the microprocessor controller as status indications.

1-24. IPA POWER SUPPLY

1-25. The IPA stage power supply is a three-phase primary six-phase secondary supply similiar to the PA plate power supply. All the general considerations listed for the PA plate power supply also apply to the IPA supply. The output of the supply is sampled by the microprocessor controller as a status indication.

1-7

1-26. The secondary of the IPA transformer is connected in a wye configuration. After rectification, the output is applied to a single section choke input filter and bleeder. The output of the supply terminates in five 10 Ampere circuit breakers which provide overlaod protection for the following five regulators. Each circuit breaker can be used as a switch for troubleshooting purposes.

1-27. IPA MODULE SUPPLY. Each plug-in regulator module is a 28 volt, 10 ampere current limiting unit providing safe area dissipation protection and remote shutdown (see Figure 1-2).

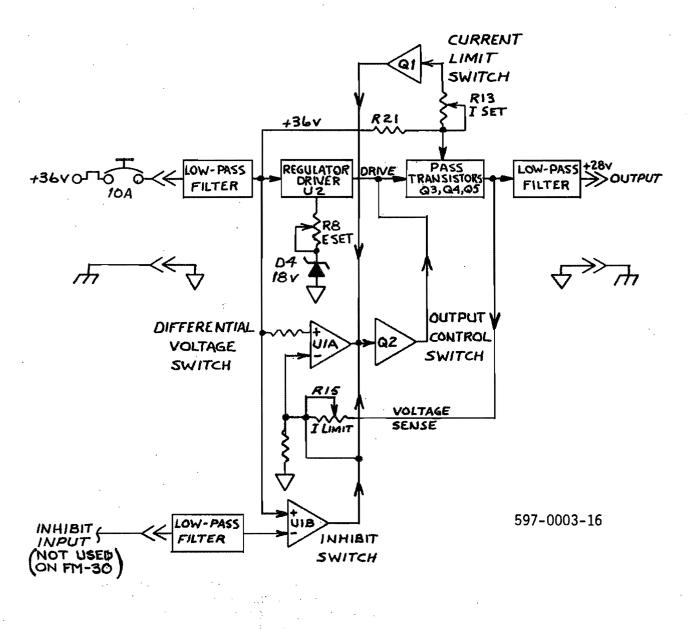


FIGURE 1-2. REGULATOR BLOCK DIAGRAM

1-28. <u>Regulator Circuit</u>. The input and output from each supply is routed through a low-pass filter to prevent RF interference with the supply operation. The input potential is applied to three-terminal regulator U2 which drives the output stage pass transistors (Q3, Q4, and Q5). The drive level is adjusted by the E SET control (R8) and stabilized by zener diode D14. An additional output from each regulator is applied to the microprocessor controller as a status indication.

1-29. <u>Current Limiting</u>. Current flow in the output stage is sensed by a voltage drop across resistor R21. When a preset limit established by the I SET control (R13) is exceeded, the current limit switch (Q1) will operate and trigger the output control switch (Q2) which decreases the drive applied to the pass transistors.

1-30. <u>Safe Area Protection</u>. Output voltage from the pass transistors is monitored by differential voltage switch UIA and compared to the module input potential. When a drop in output voltage is sensed, UIA will trigger the output control switch (Q2) which will decrease the drive applied to the pass transistors. The sense line to UIA is calibrated by the I LIMIT control (R15).

1-31. <u>Remote Shutdown</u>. As an optional feature used in some transmitters, circuitry exists which allows interruption of the output of the IPA section RF amplifiers. Inhibit switch U1B accommodates this feature by triggering the output control switch (Q2) which removes drive from the pass transistors.

1-32. IPA DIRECTIONAL COUPLER BUFFER POWER SUPPLY

1-33. The IPA directional coupler buffer power supply contains two supplies. Both supplies are operated from a common transformer powered by 115 Vac from primary isolation transformer T101.

1-34. The +15 volt supply is a full-wave bridge rectified supply with a one section filter. The rectifier is followed by a three-terminal voltage regulator which is adjustable with control R1.

1-35. The +5.1 volt supply is full-wave rectified and followed by a one section filter. A zener diode stabilizes the output of the supply which is applied to the microprocessor controller to signal loss of ac power.

1-36. AUTOMATIC POWER CONTROL UNIT POWER SUPPLY

1-37. The automatic power control unit power supply operates from a primary potential of 115 Vac obtained from primary isolation transformer T101. Fuse F1 provides overload protection.

1-38. The supply is full-wave rectified and followed by a one section filter. The filter section is followed by a three-terminal adjustable voltage regulator which provides a stable +12 Vdc source from the +18 Vdc input.

1-39. MICROPROCESSOR CONTROLLER POWER SUPPLY

1-40. The power supply for the microprocessor controller provides +24 and +5 volt outputs to operate the controller and its interface. The supply operates from a 115 volt ac input obtained from primary isolation transformer T101. Fuse F1 provides overload protection.

1-41. The 24 volt supply is full-wave bridge-rectified and followed by a single section filter. The supply is regulated by fixed three-terminal regulator U4 which outputs a +24 volt dc potential.

1-42. The second supply functions as a voltage source for the five volt regulated supply and acts as a charger source for the built-in battery back-up supply. The batteries are on charge whenever the primary input is energized. In event ac power fails, enough energy is contained in the batteries to operate the microprocessor controller display for a period of approximately three hours to assist troubleshooting.

1-43. This supply is full-wave bridge rectified and followed by a single section filter. The supply is preregulated to 10.1 Vdc by U3. U5 re-regulates this potential to output +5 Vdc.

1-44. The preregulated 10.1 volt potential is also applied to a circuit comprising U1, U2, and Q1 which monitors the battery voltage in case the power fails and disconnects the battery stack when the output falls low to prevent damage to the batteries.

1-45. The battery disconnect circuit operates as follows: Precision voltage reference U1 is adjusted with control R8 to establish a threshold of 2.50 volts on the non-inverting input of comparator U2. When the inverting input of U2 (battery supply line) falls below this 2.50 volt threshold, the output of U2 will enable Q1 which deenergizes relay K1 and disconnects the battery supply output.

11 A.

SECTION II POWER SUPPLY MAINTENANCE

í

2-1. INTRODUCTION

2-2. This section provides maintenance information for the FM-30 FM transmitter power supplies.

2-3. SAFETY CONSIDERATIONS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND THE SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-4. The FM-30 transmitter contains high voltages and currents which, if regarded carelessly, could be fatal. The transmitter has many built-in safety features. However, good judgement, care, and common sense are the best accident preventives. The maintenance information contained in this section should be performed only by trained and experienced maintenance personnel.

2-5. It is very dangerous to attempt to make measurements or replace components with power energized, therefore such actions are not recommended. The design of the equipment provides safety features such that when a door or access panel is opened, interlock switches will deenergize the plate and screen power supplies. Do not short out or bypass interlock switches as a maintenance short cut.

2-6. The power supply cabinet and the PA cabinet contain switches which discharge the PA plate potential directly to ground whenever either cabinet is opened.

2-7. Grounding sticks are provided as safety features. Each grounding stick consists of a metal rod with a phenolic handle. The metal end is connected to chassis ground. Use a grounding stick to touch every part in the area or circuit on which maintenance is to be performed before attempting maintenance.

2-8. The grounding stick in the high voltage power supply cabinet and the grounding stick in the PA cabinet both rest on hook switches. When either of these grounding sticks is removed, the associated hook switch opens the transmitter interlock string and deenergizes the transmitter PA and screen potentials until each grounding stick is replaced on its respective hook switch.



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.



ENSURE THE REMOTE/LOCAL SWITCH IS SET TO LOCAL BEFORE ATTEMPTING ANY MAINTENANCE.

2-10. The FM-30 maintenance philosophy consists of preventative maintenance such as cleaning applied to the equipment to forestall future failures and second level maintenance consisting of procedures required to restore the equipment to operation after a fault.

2-11. ADJUSTMENTS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-12. Adjustment of many controls is considered obvious and may be accomplished with the information provided on the applicable schematic diagram. The following information is provided to assist adjustment of the more complex controls. However, it is never suggested that maintenance be performed on any circuitry within the transmitter with power applied to any portion of the transmitter.

2-13. IPA MODULE REGULATORS. To adjust the IPA module regulators, proceed as follows.

2-14. <u>Required Equipment</u>. The following equipment is required to complete adjustment of the IPA module regulators.

A. External 36 volt, low current dc power supply.

B. Calibrated dc voltmeter (Simpson 260 or equivalent).

- C. Number 1 Phillips screwdriver, 4 inch (10.16 cm) blade.
- D. Insulated adjustment tool, Flat screwdriver tip (BE P/N 710-0001).
- E. Soldering Iron, 60 Watt.
- F. Solder Removal Tool.

2-15. <u>Procedure</u>. To adjust the IPA module regulators, proceed as follows:

WARNING

DISCONNECT PRIMARY POWER BEFORE PROCEEDING.

2-16. Disconnect all primary power.

2-17. Open the IPA cabinet rear access door.

2-18. Four wires are soldered to each regulator. Unsolder the wires from each circuit board to be removed.

2-19. Each circuit board assembly is mounted to the main heat sink assembly with two Phillips head screws. Remove the screws from each regulator to be removed.

2-20. Adjust the following controls as indicated (see Figure 2-1).

A. E Set control (R8) to center of its range.

B. I Set control (R13) fully counterclockwise (the I Set control remains fully counterclockwise).

2-21. Connect the voltmeter positive lead to terminal 13 and the negative lead to terminal 1.

2-22. Connect the external 36 volt dc power supply positive to terminal 14 and the negative to terminal 15.

2-23. Energize the power supply and adjust R8 to obtain a voltmeter indication of 27.5 volts.

CAUTION

THE IPA STAGE REGULATORS ATTACH TO A LARGE HEAT SINK. ENSURE A THIN FILM OF A ZINC-BASED HEAT-SINK COMPOUND IS USED (BE P/N 700-0028) WHENEVER A REGULATOR IS INSTALLED.

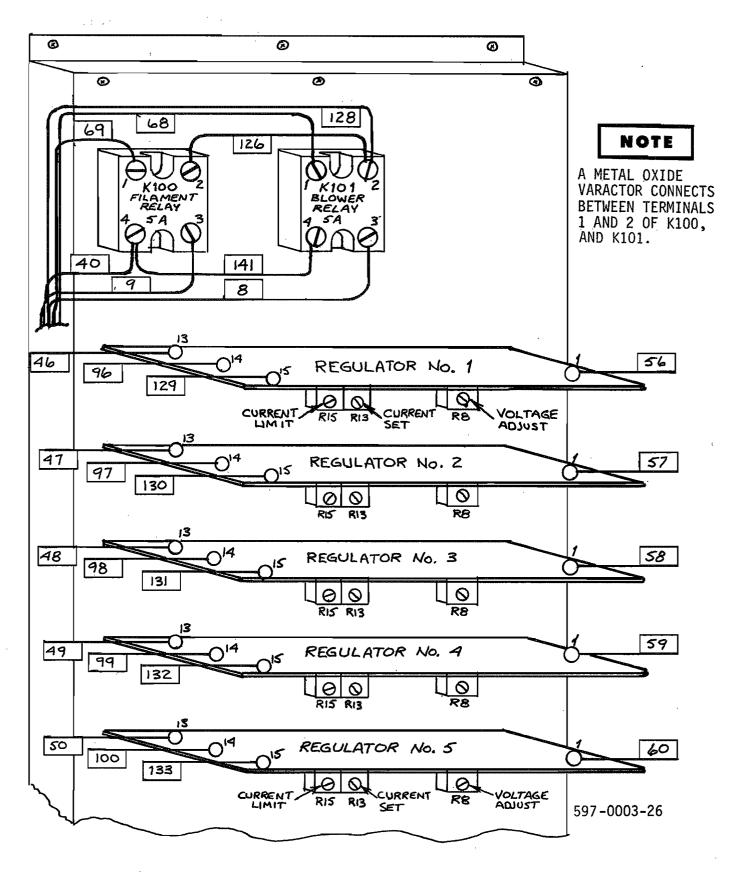


FIGURE 2-1. IPA MODULE REGULATOR WIRING DIAGRAM

2-24. Replace the module(s) in the equipment. Wiring information is shown in Figure 2-1.

2-25. TROUBLESHOOTING



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANSMITTER AND EXCITER PRIMARY POWER IS DISCONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COM-PONENTS AND ALL SURROUNDING COMPONENTS ARE DIS-CHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-26. Most troubleshooting consists of visual checks. Because of the voltages and high currents in the equipment, it is considered hazardous to work with power energized. Therefore, the various transmitter indications (meters, LEDs, fuses, and the digital read-out) should be used to isolate the malfunction to one specific area.

2-27. Once the trouble is isolated and power is totally deenergized, it is suggested that the exact problem be located with resistance checks using the schematic diagrams and theory of operation presented throughout the text.

2-28. If a circuit is diagnosed as faulty, the circuit fault may be isolated and repaired locally or the entire device may be returned to Broadcast Electronics, Inc. for exchange, alignment, or replacement.

WARNING:

DISCONNECT POWER PRIOR TO SERVICING

SECTION III

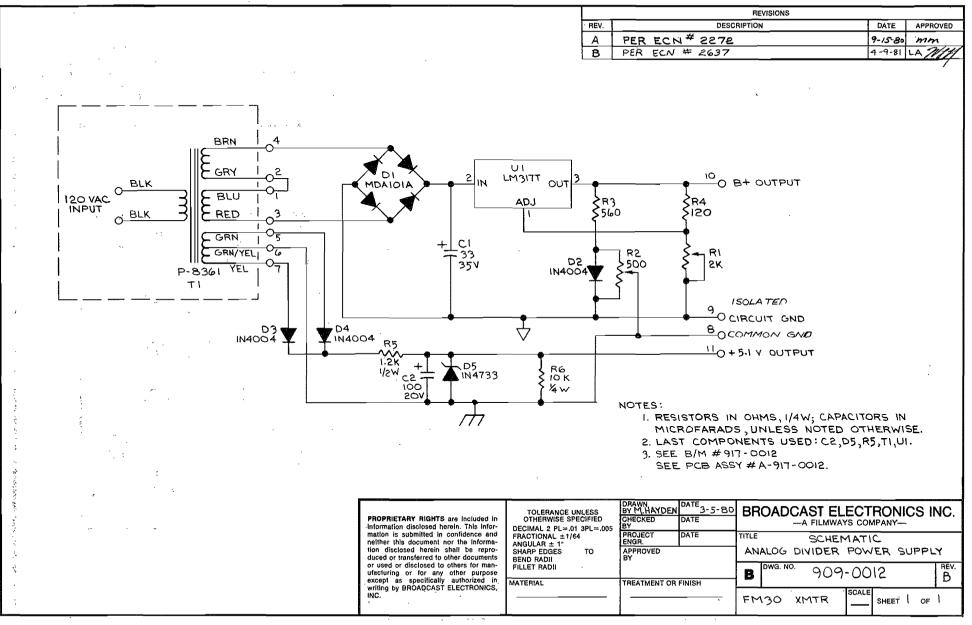
POWER SUPPLY DRAWINGS

3-1. INTRODUCTION

3-2. This section provides assembly drawings, schematic diagrams, and wire lists as indexed below for the FM-30 Transmitter power supplies.

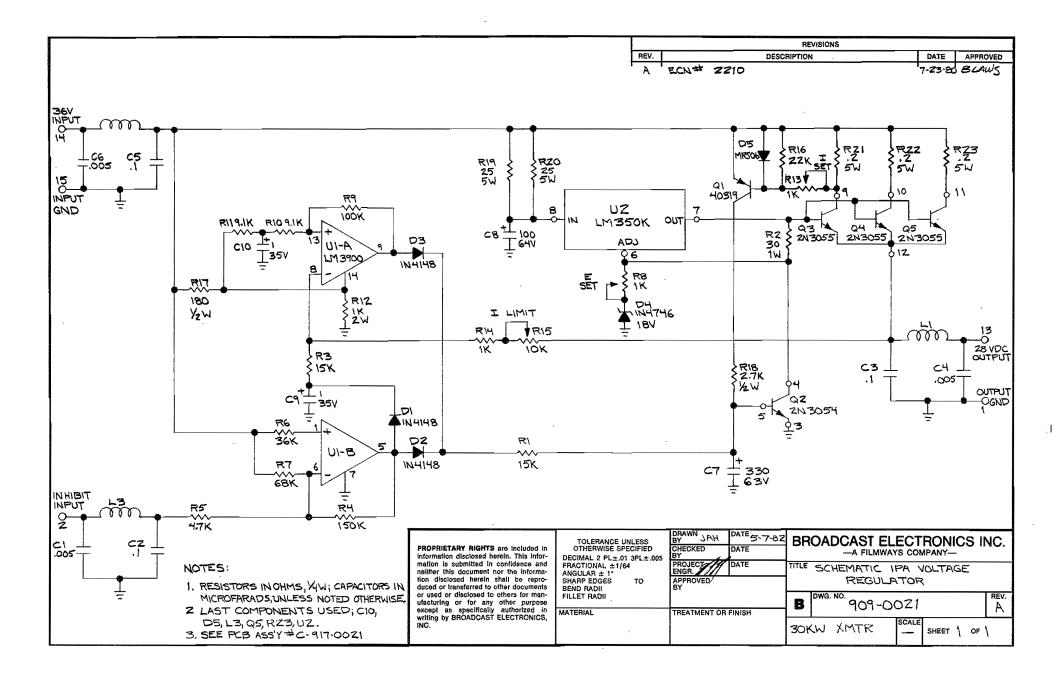
FIGURE	TITLE	NUMBER
3-1	Schematic, IPA Analog Divider Power Supply	B909-0012
3-2	Assembly, IPA Analog Divider Power Supply	A917-0012
3-3	Schematic, IPA Voltage Regulator	B909-0021
3-4	Assembly, IPA Voltage Regulator	C917-0021
3-5	Schematic, Microprocessor Controller Power Supply	C909-0059
3-6	Assembly, Microprocessor Controller Power Supply	C919-0034
3-7	Schematic, Step-Start Circuit	C909-0199
3-8	Assembly, Step-Start Circuit	B919-0199

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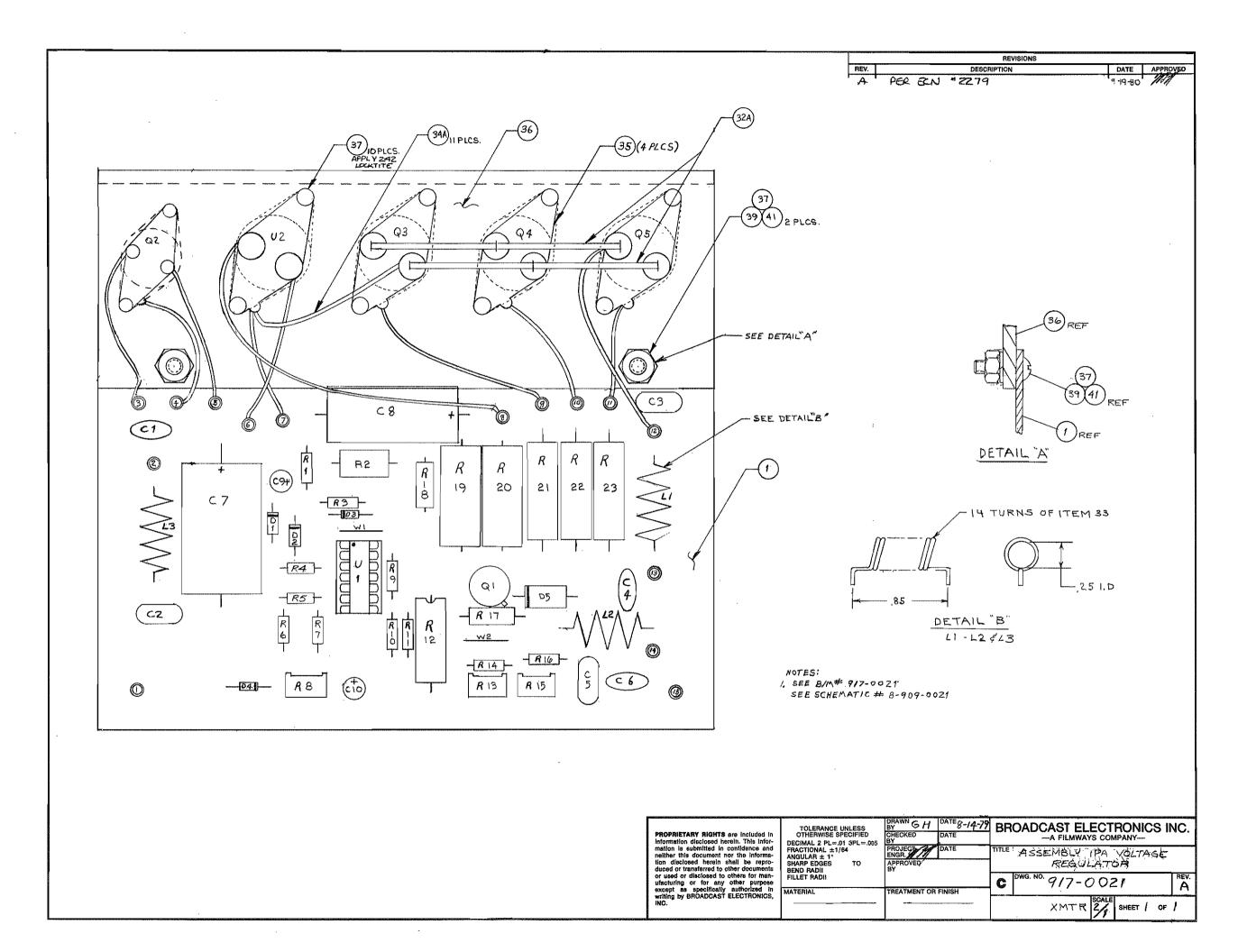


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	'A '	PER ECN#2637		4-16-8	LA CWK
			SEE B/M # 917-0 SEE SCHEMATIC		-0012
PROPRIETARY RIGHTS are included in information disclosed herein. This infor- mation is submitted in confidence and neither this document nor the informa- tion disclosed herein shall be repro- duced or transferred to other documents or used or disclosed to others for man- ufacturing or for any other purpose except as specifically authorized in writing by BROADCAST ELECTRONICS, INC.	TOLERANCE UNLESS OTHERWISE SPECIFIED DECIMAL 2 PL=.01 3PL=.005 FRACTIONAL ±1/64 ANGULAR ± 1° SHARP EDGES TO BEND RADII FILLET RADII MATERIAL	DRAWN BY M.HAYDEN DATE CHECKED DATE BY PROJECT DATE ENGR. APPROVED BY TREATMENT OR FINISH	TITLE A ANALOG DIVIDER DWG. NO. 917-	COMPANY SSEMBLY POWER 0012 CALEI	

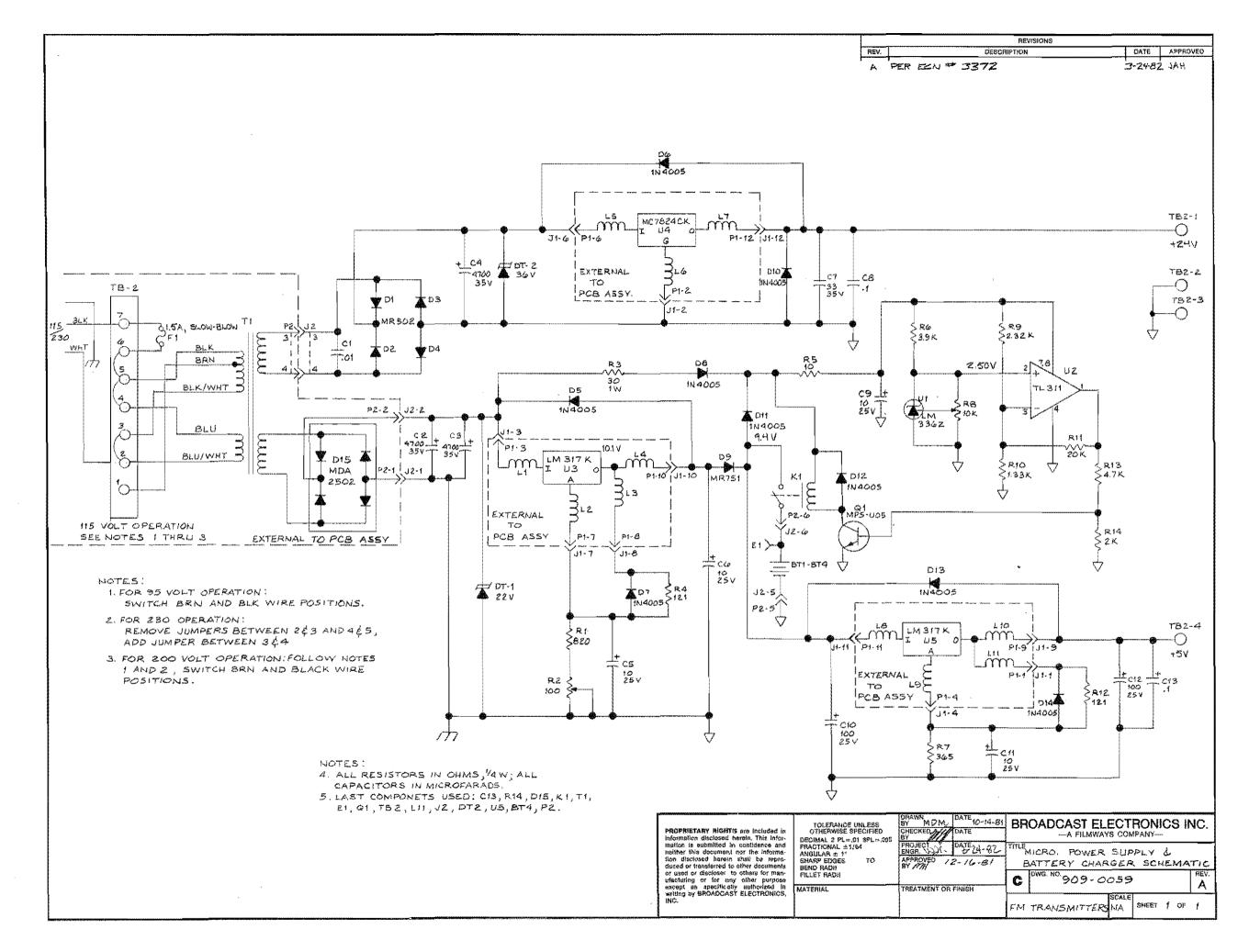


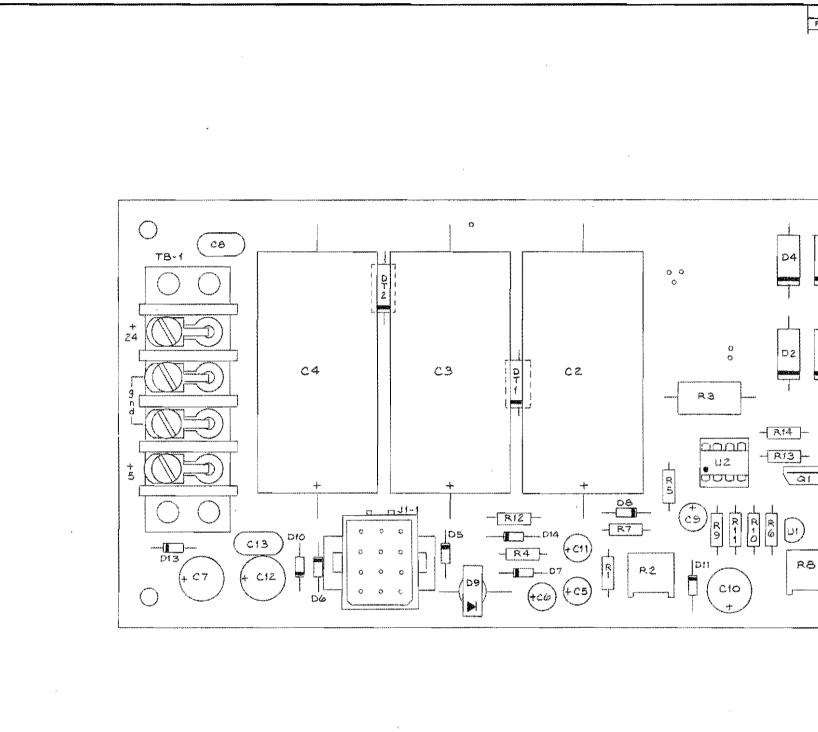
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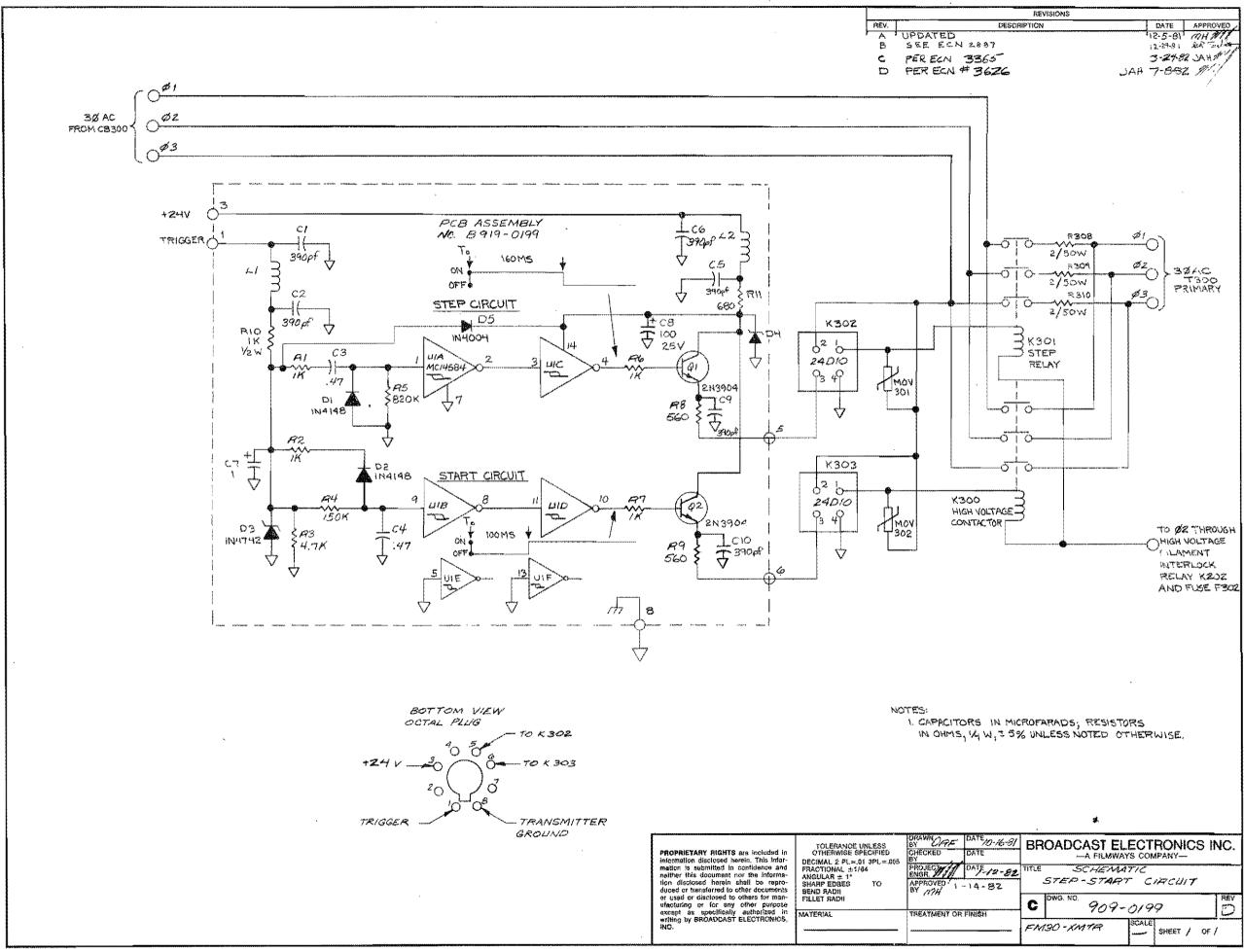


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TOLERANCE UNLE OTHERWISE SPECI DECIMAL 2 PL=-31 3F FRACTIONAL ±1/64 ANGULAR ± 1° SHARP EDGES BEND RADH FRLET RADH

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) JZ-1	PTION					DATE	APPRO	VEO
	see See	B/M#9 SCHEM,	19-0 TIC	0034 #c-	909-	00	59			-
	·									
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CIFIED SPL=.005	CHECKED BY PROJECT ENGR	DATE		OADC						•••
то	APPROVED /:	DATE-15-82	TITLE		ASS				<i>₽</i> 1167	acro
	BY MA	····· ••• •	C.	RO. 51 DWG. NO.	GIG	00	2A17	<u>EKY</u>	CHAI	KGEK
	TREATMENT OR	Finish	<u> </u>		~~~~~		BOALE			
			FM *	FRANS	MITTE	:R5	2/1	SHEET	1 OF	1



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						REVISIONS			
			REV.		DES	CRIPTION	0	ATE API	PROVE
			' A	37	DD D3 C7 & R10. 10 5; 4 T06 ; ANI	.CHGD. CONTACT. 5 5 TO 8.	5 2 TO 3: 12	-4-81 m	H M
			В	Pe	ER ECN #3365		ORF 4-	8 8 2 🖉	1
			C D		ode symeol Co er ecn#3626	RECTED	ORF 6 JAH 7	-2-82/1 • 8-82 /1	NI T
]						
(C8	3+) - <u>1</u> 0-		-519-01	99					
		$\overline{12}$ $\overline{12}$ $\overline{12}$ $\overline{12}$							
			s						
	P	$- \left(\overline{q_1} \right) - \left[\frac{RB}{RB} \right]^{\circ 5}$							
			1						
			_]						
					SEE	SCHEMATIC N	nC909-01	99	
						B/M NO. 919-0		<i>,</i> .	
		PROPRIETARY RIGHTS are included in	TOLERANCE UNLESS OTHERWISE SPECIFIED		HECKED DATE		LECTR	IONICS	IN
		information disclosed herein. This infor- mation is submitted in confidence and	DECIMAL 2 PL=.01 3PL=.0 FRACTIONAL ±1/64	005 81	ROJECT		MWAYS COMP	ANY	
		neither this document nor the informa- tion disclosed herein shall be repro- duced or transferred to other documents	ANGULAR ± 1* SHARP EDGES TO BEND RADII	A	NGR. 11/1/ 1 - 12 - 22 PPROVED (- 14 - 82 Y MH	STEP - STA		UIT	
		or used or disclosed to others for man- ufacturing or for any other purpose	FILLET RADII			B DWG. NO. 91	7-0199		
		except as specifically authorized in writing by BROADCAST ELECTRONICS, INC.		TF	REATMENT OR FINISH	FM30-XMT	SCALE		_

APPENDIX A

POWER SUPPLY MANUFACTURERS DATA

A-1. INTRODUCTION

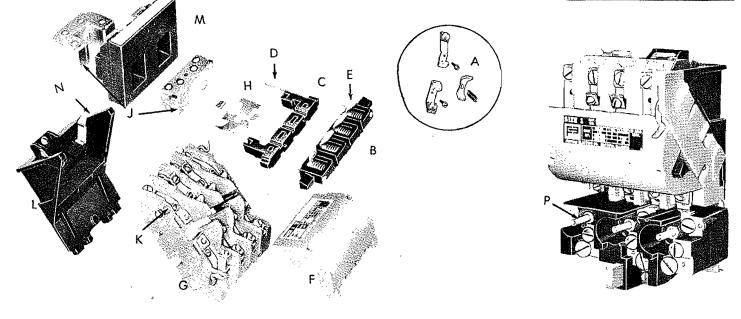
A-2. This appendix provides the following technical data relative to the operation and maintenance of the FM-30 FM transmitter power supplies. Information in the appendix is provided in the following order.

- A. Service Bulletin, Furnas Contactor, Size 1 & 1 3/4
- B. Service Bulletin, Furnas Contactor, Size 4 1/2
- C. Operation and Maintenance Bulletin, Powerstat 21-40 Variable Transformer
- D. Operation and Maintenance Bulletin, Powerstat 10B-12 Variable Transformer
- E. Technical Data Sheet, Opto 22 Solid State Relay
- F. Operating Instructions and Parts List, Cincinnati Fan Company Type PB-14 Pressure Blower
- G. Instructions, Furnas 3 Phase Voltage Monitor, P/N 947PB10AD/AG/AH

Innova/45 Supersedes Issue of January, 1975

REPLACEMENT PARTS MAGNETIC CONTROLS

File No. 14-0	GCF								
Cat. No. or Class Se	ries								
14BF, 14CF, 14DF, 14EF 40BF, 40CF, 40DF, 40EF									
Size 00, 0, 1,	1P, & 134								
SEPTEMB	ER 1975								

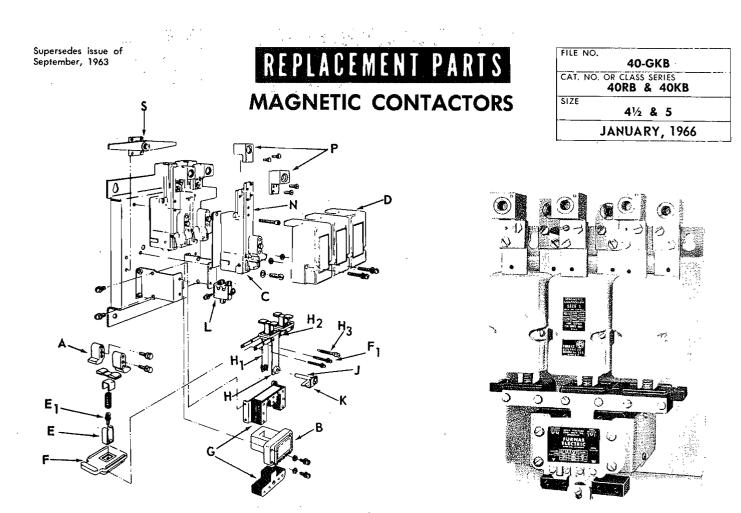


Γ						PART	NUMBER	
-	ITEM		PART NAME		14BF Size OO	14CF Size O	14DF Size 1	14EF Size 1P & 134
	А	Contacta & Envina	, One complete pole –	Power Pole	75BF14	75CF14	75DF14	75EF14
		contacts & spring	, One complete pole –	nterlock Pole	75AF14	75AF14	75AF14	75AF14
	В	Cross Arm (less of	contacts)		D54670-001	D54670-001	D54670-001	D54670-001
	C	Cross Arm Base			D54873-001	D54873-001	D54873-001	D54873-001
	D	Cross Arm Spring	15		D24826-001	D24826-001	D24826-001	D24826-001
1	E	Cross Arm Screw			D25013-001	D25013-001	D25013-001	D25013-001
	F	Contact Board Co	over	1	D73062-001	D73062-001	D73062-001	D73062-001
	G	Contact Board (le	ss contacts)		D73116-022	D73116-021	D73116-021	D73116-021
	н	Armature Spring	Clip		D24817-001	D24817-001	D24817-001	D24817-001
	J	Magnet and Arm	ature		D25551-001	D25551-001	D25551-001	D25551-001
	К	Contact Board Sci	rew		D24827-001	D24827-001	D24827-001	D24827-001
	L	Base			D73060-001	D73060-001	D73060-001	D73060-001
	M	Coil 60 Hz. 110	-120/208-240 Volts 50	Hz. 110 Volts	75D73070A	75D73070A	75D73070A	75D73070A
ſ		208	3-240/440-480 Volts	220 Volts	75D73070C	75D73070C	75D73070C	75D73070C
		550	-600 Volts	550 Volts	75D73070E	75D73070E	75D73070E	75D73070E
	Ν	Coil Spring Clip						
		ť	Atalian allas (and)	1 Pole	48DC11A2	48DC11A2	48DC11A2	48EC11A2
			Melting alloy (std.)	3 Pole	48DC31A2	48DC31A2	48DC31A2	48EC31A2
		Ownstand Dates	Céanaland Dimental	1 Pole	48DC17AA2	48DC17AA2	48DC17AA2	48EC17AA2
	Ρ	Overload Relays	Standard Bimetal	3 Pole	48DC37A2	48DC37A2	48DC37A2	48EC37A2
1			Aunte Commence de la Disse	1 Pole	48DC18AA2	48DC18AA2	48DC18AA2	48EC18AA2
			Amb. Compensated Bim	a Pole	48DC38A2	48DC38A2	48DC38A2	48EC38A2`

NOTE: When ordering replacement parts, give catalog number of control and part name and number.



FURNAS ELECTRIC COMPANY = BATAVIA, ILLINOIS



, -		PARTS NUMBER				
ITEM	PART NAME	40RB SIZE 41/2	40KB SIZE 5			
А	Contacts and Spring	· · · · · · · · · · · · · · · · · · ·				
	One (1) Complete Pole – Specify No. Required	75RB14	75KB14			
. B	Coil* (50/60 Cycle)					
3	110-220 Volts	D72069-31	D72069-31			
	220-440 Volts	D72069-32	D72069-32			
	*Other voltages and frequencies available on request. 550 Volts	D72069-33	D72069-33			
С	Contact Board (Less Hardware) One (1) Pole	D20746-2	D20746-1			
C D E F F	Contact Board Cover with Screws One (1) Pole	D52087-2	D52087-1			
E	Contact Guide	D12101-1	D12101-1			
E,	Contact Guide Screw – Size $\frac{1}{4}$ – 20 x $\frac{1}{2}$ Fil. Hd. Sems	S-227-8	S-227-8			
F	Cross Arm (Less Hardware)	D52051-3	D52051-3			
۴ı	Cross Arm Screw – Size 1/4 – 28 x 2 Rd. Hd.	S-114-32	S-114-32			
G	Magnet and Armature	D18826-1	D18826-1			
н	Front Pusher Assembly	D17066-3	D17066-3			
H ₁	Rear Pusher Assembly	D17066-4	D17066-4			
H_2	Pusher Screw – Size $\frac{1}{4}$ – 28 x 2 $\frac{1}{4}$	S-114-36	S-114-36			
Н₃	Pusher Screw for Reversing	D18945-1	D18945-1			
	Split Locker Washer for F_1 , H_1 , H_2	S-122-6	S-122-6			
J	Armature Pin	D18742-1	D18742-1			
К	Armature Pin Retaining Clip	D18760-1	D18760-1			
L	Switchlets – Interlock – Kit (Max. 2 each side) Left	49L100103	49L100103			
	Right	49L100102	49L100102			
N	Terminal Front	D52118-2	D52118-1			
	Rear	D18756-2	D18756-1			
Р	Terminal Lug Front	D18748-2	D18748-2			
	Rear	D18749-2	D18749-2			
S	Mech. Interlock for Reversing	D18951-1	D18951-1			

NOTE: When ordering replacement parts, give catalog number of control and part number.





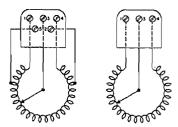
OPERATION and MAINTENANCE

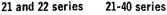


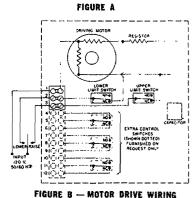
CONNECTIONS AND RATINGS

Connections and ratings given in these instructions are those most commonly used. The individual units in ganged 21-40 Series assemblies are usually wired as electrically independent units according to the single unit connection chart. Ganged 21 and 22 Series assemblies may be wired as independent units, if desired.

Connections are made to the 8-32 screws on the terminal board. Terminal adapters are furnished in the mounting







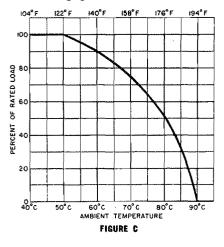
SINGLE UNITS

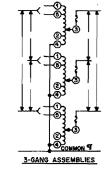
hardware pack to accommodate AMP250 series (or equivalent) female connectors or for soldered connections.

Coil-to-terminal connections for 21, 21-40 and 22 Series POWERSTAT Variable Transformers are shown in Figure A.

MOTOR-DRIVEN UNITS are wired in the same manner as manually-operated units using the connections for CW ROTATION, KNOB ON RADIATOR END. Motor-drive wiring is shown in Figure B.

DERATING OF OUTPUT CURRENT AT AMBIENT TEMPERATURES ABOVE 50°C is shown in Figure C. At ambient temperatures between -20°C and +50°C use the current ratings given in the charts.







2-GANG ASSEMBLIES

	INPUT			(ουτρυτ	•	*	,	TERMINALS							
TYPE				CONS CURI LO	TENT	IMPED	CONSTANT IMPEDANCE LOAD*			KNOB ON BASE END		KNOB ON RADIATOR END				
	VOLTS	HERTZ	VOLTS	MAX. AMPS.	MAX. KVA	MAX. AMPS.	MAX. KVA		INPUT	JUMPER	OUT- PUT	INPUT	JUMPER	OUT- PUT		
					SINC	LE UNIT	rs — sit	IGLE PHA	SE							
21-40 M21-40t	40	60	0-40	18#	0.72	22**	0.88	CW CCW	1-4 1-4		3-4 1-3	1-4 1-4		1-3 3-4		
21	120	50/60	0-120	57	0.54	6.5§	0.78	CW CCW	1-4	1	3-4 1-3	1-4		1-3 3-4		
M21‡	120	50/60	0-140	54	0.63			CW CCW	4-5 1-2		3-4 1-3	1-2 4-5	-	1-3 3-4		
22	240	50/60	0-240	2.25‡‡	0.54	3.25††	0.78	CW CCW	1-4 1-4	-	3-4 1-3	1-4 1-4	-	1-3 3-4		
M22‡	240	30/00	0-280	2.25‡‡	0.63		-	CW CCW	4-5 1-2		3-4 1-3	1-2 4-5		1-3 3-4		
					2-GANG	ASSEMB	LIES -	SINGLE	PHASE							
21-2			0-240	51	1.1	6.5§	1.6	CW CCW	1-1 4-4	4-4 1-1	3-3 3-3	4.4	1-1 4-4	3-3 3-3		
M21-2‡	240	50/60	0-280	54	1.3	-	-	CW CCW	5-5 2-2	4-4 1-1	3-3 3-3	2-2 5-5	1-1 4-4	3-3 3-3		
22-2			0-480	2.25‡‡	1.1	3.25++	1.6	CW CCW	1-1	4-4	3-3 3-3	4-4 1-1	1-1 4-4	3-3 3-3		
M22-2‡	480	50/60	0-560	2.25‡‡	1,3	-		CW CCW	5-5 2-2	4-4 1-1	3-3 3-3	2-2 5-5	1-1 4-4	3-3 3-3		
	•				2-GANG	ASSEM	BLIES -	THREE I	PHASE							
21-2			0-120	51	0.94	6.5§	1.4	CW	1-4-1	4-4	3-4-3 3-1-3	4-1-4	1-1	3-1-3		
M21-2‡	120	50/60	0-140	5†	1.1	-	-	CW CCW	5-4-5	4-4	3-4-3	2-1-2	1-1	3-1-3		
22-2			0-240	2.25‡‡	0.94	3.25††	1.4	CW CCW	1-4-1	4-4	3-4-3 3-1-3	4-1-4	1-1	3-1-3		
M22-2‡	240	50/60	0-280	2.25‡‡	1.1	-	-	CW CCW	5-4-5	4-4 1-1	3-4-3 3-1-3	2-1-2	1-1	3-1-3		
					3-GANO	ASSEM	BLIES -	THREE I	HASE	•						
21-3		50/60	0-240	51	1.9	6.5§	2.7	CW	1-1-1	4-4-4	3-3-3 3-3-3	4-4-4	1-1-1 4-4-4	3-3-3 3-3-3		
21-3 M21-3‡	240	60	0-280	51	2.2	-	-	CW CCW	5-5-5	4-4-4	3-3-3 3-3-3	2-2-2 5-5-5	1-1-1 4-4-4	3-3-3		
22-3		50/60	0-480	2.25‡‡	1.9	3.25++	2.7	CW	1-1-1 4-4-4	4-4-4	3-3-3	4-4-4	1-1-1 4-4-4	3-3-3 3-3-3		
M22-3‡	480	60	0-560	2.25‡‡	2.2	-	_	CW	5-5-5	4-4-4	3-3-3	2-2-2 5-5-5	1-1-1 4-4-4	3-3-3		

gCommon used as third leg in 3-phase open delta or neutral in 3-wire single-phase and 4-wire 3-phase wye connections; not used in

 Wite string of sum we connections,

 For motor-driven units use terminals for CW rotation, KNOB ON RADIATOR END.

 *Loads such as incandescent lamps or resistance heaters in which current drawn is approximately proportional to applied voltage.

 #18 ampere luses recommended, not supplied.

 #24 ampere fuses recommended, not supplied.

 #14 ampere fuses recommended, not supplied.

 #14 ampere fuses recommended, not supplied.

 #25 ampere fuses recommended, not supplied.

MAINTENANCE

With ordinary care, a POWERSTAT Variable Transformer should require no servicing except possible replacement of the brush assembly. The brush should be inspected periodically and replaced if arcing takes place or if it is badly worn. Because the brush must be of a special material, replace only with the Superior Electric brush assembly listed below. The assembly is designed to assure perfect contact of the brush to the radiator regardless of brush position and length of time in use.

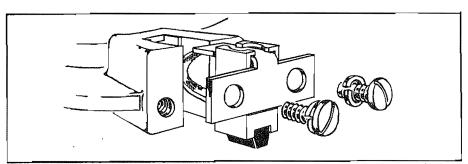
Follow these steps to install a new brush assembly.

- 1. Unfasten the brush assembly anchor screws, remove and discard the old brush assembly.
- 2. Insert the new brush assembly in the radiator slot, replace the anchor screws and tighten to the radiator. Be sure the back end of the brush strap is under the projection at the rear of the radiator brush slot.

- 3. Raise the brush and place a piece of crocus cloth or very fine sandpaper between the brush and the commutator so the smooth side is against the commutator and the abrasive side is toward the brush.
- 4. While holding the cloth or sandpaper in place, rotate the radiator through a short arc. Blow out the excess carbon particles.
- 5. Remove the cloth or sandpaper and rotate the radiator over the full range several times to check for smooth travel of the brush over the commutator surface. The brush should fit flat over the entire commutator range. No space should be visible between the brush and the surface.

REPLACEMENT BRUSH ASSEMBLIES

түре	BRUSH ASSEMBLY NO.
21	RB 21
21-40	RB21-40
22	RB22



POWERSTAT[®] VARIABLE TRANSFORMER INSTRUCTIONS

108. 108-40 AND 12 SERIES

The right to make engineering refinements on all products is reserved. Dimensions and other details are subject to change.

These Devices Manufactured Under One or More Of The Following U.S. Patents: 2,947,959; 3,087,132; 3,126,442; 3,136,967; 3,466,585; 3,529,348. Patented Canada J953. 1000

INSPECTION

Your new POWERSTAT Variable Transformer has been carefully packed for shipment. However, damage may occur in transit. After receiving unit, check all components (brush contact primarily) to satisfy yourself that there is no damage. Also make sure that the dial, knob, lock-washer and mounting nuts are in the package. The "Damage and Shortage" Instructions nacked with the unit outline the proper procedure to follow if any parts are damaged or missing.

INSTALLATION

POWERSTAT Variable Transformers of the 10B, 10B-40 and 12 Series are designed for mounting in the back-of-panel position only.

SINGLE UNITS

The single hole mounting of single units is fast and simple. For keying to the panel, a 1/16 inch projection is provided. To facilitate mounting, a drilling template is supplied as part of these instructions. Actually, the drilling template must be used only when the hole for the 1/16 inch projection is required.

To mount, proceed as follows:

- Using the drilling template, locate the panel holes. In order that the terminals should be on top, the template should be upright. Drill the holes.
- 2. Mount the POWERSTAT variable transformer as shown. Mount the unit flush to the back of the panel and the dial flush to the front. A single nut and lockwasher hold the unit and dial in place. The knob, mounted on the shaft, covers the nut and lockwasher.
- 3. If the unit is not to be keyed to the panel, only the hole for the 3/8 inch center shaft should be drilled. The extra nut provided is placed on the shaft between the unit and the back of the panel. Otherwise the mounting is as explained above.

GANGED UNITS

Ganged units require four panel holes for mounting. Three are needed for the mounting bolts and a clearance hole is necessary for the center shaft.

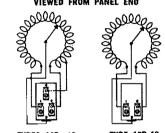
To mount, proceed as follows:

- 1. Using the drilling template locate the four panel holes. If the template is upright, the terminals will not be directly on top. When terminals are required at the top, line marked "T" should be vertical. Drill the holes.
- Mount the unit behind the panel as shown using the three 1/4" 20 mounting bolts provided, Mount the dial on the front of the panel, securing it in place with the 3/8"-32 nut and lockwasher provided. The knob, when mounted on the shaft covers the nut and lockwasher.

CONNECTION AND RATING *

POWERSTAT Variable Transformers of the 10B, 10B-40 and 12 Series may be connected to suit various requirements as shown in the chart. The individual units in types 10B-40-2 and 10B-40-3 are not electrically interconnected but are independently wired following the type 108-40 connections. Under "KNOB ROTATION," rotating the knob in the direction indicated will INCREASE the output voltage. The dial is marked for clockwise rotation only.







			OUTPUT									
				CUR	TANT RENT AD	IMPE	TANT DANCE			700000000		
TYPE	INPUT VOLTAGE	(hertz)	VOLTS	MAX. AMP.	MAX. KVA	MAX. AMP.	MAX. KVA	KNOB Rotation	INPUT	TERMINALS JUMPER*	OUTPUT	
		(nor az)	L		<u> </u>	S SINE		SE				
								C₩	1-2		1-3	
108-40	40	60	0-40	7	0.28	9	0.35	CCW	1.2		2.3	
								CW	1.2		1-3	
108	120	50/60	0-120	2.25†	0.27	3‡	0.36	CCW	1-2		2.3	
	•	60	0-132	2.251	0.30			CW	1.4		1-3	
			• • • •		0.17		0.05	CW	1-2		1.3	
12	240	50/60	0-240	0.7††	0.17	0.9**	0.22	CCW	1-2		2-3	
			0-264	0.5 ∦t	0.13			CW	1-4		1-3	
TWO GANG ASSEMBLIES SINGLE PHASE, SERIES CONNECTED												
		50/60	0.240	2.25†	0.54	31	0.72	CW	2-2	1-1	3.3	
10B-2	B-2 240	30/00	0.240	2.251	0.54		0.72	CCW	1-1	2-2	3.3	
		60	0-264	2.25†	0.59			CW	4.4	1-1	3.3	
		50/60						CW	2-2	1-1	3 -3	
12-2	480		50/60	0-480	0.7††	0.34	0.9**	0.43	CCW	1-1	2-2	3.3
			0-528	0.5()	0.26			CW	4-4	Į-1	3-3	
		TWO GAN	G ASSEN	IBLIES -	- THRE	E PHASE	OPEN	DELTA CONN	ECTED			
	1	50/60			0.47	31	0.62	CW	2-1-2	1-1	3-1-3	
10B-2	120	50/60	0-120	2.25†	0,47	34	0.02	CCW	1-2-1	2-2	3-2-3	
		60	0-132	2.25†	0.51			CW	4-1-4	1-1	3-1-3	
				0.744	0.29	0.9**	0.37	CW	2.1-2	1-1	3-1-3	
12-2	240	50/60	0-240	0.7††	0.23	0.9	0.37	CCW	1-2-1	2-2	3-2-3	
	ľ		0-264	0.5)†	0.23			CW	4-1-4	1-1	3-1-3	
	•	THR	EE GANG	ASSEM	BLIES	- THREE	PHASE,	WYE CONNE	CTED		-	
160.2		60	0-240	2.251	0.94	3t	1.2	cw	2-2-2	1-1-1	3-3-3	
10B-3	240	60	0-240	2.23	0.34	<u> </u>	1	ccw	1-1-1	2-2-2	3-3-3	
		50/60	D-480	0.711	0.58	0.9**	0.75	CW	2-2-2	1-1-1	3-3-3	
12-3	480	50/60	0~460	0.71	0.58	0.3	0.10	ccw	1-1-1	2-2-2	3-3-3	
	l	60	0-528	0.5	0.46			cw	4-4-4	1-1-1	3-3-3	

*Jumper provided in standard common position should be moved or removed as required. fRating when mounted on a metal panel. When mounted on a bracket or nonmetallic panet, derate to 1.75 amperes. fRating when mounted on a metal panel. When mounted on a bracket or nonmetallic panet, derate to 0.5 amperes. 'fRating when mounted on a metal panel. When mounted on a bracket or nonmetallic panet, derate to 0.5 amperes. *Rating when mounted on a metal panel. When mounted on a bracket or nonmetallic panet, derate to 0.5 ampere. 140.7 ampere maximum in range from zero to line voltage when mounted on a metal panel.

PRECAUTIONS

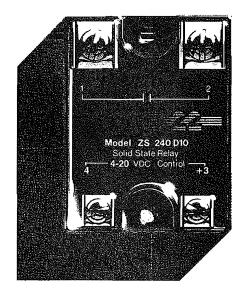
Be absolutely certain that the line voltage, phase and frequency are as noted on the nameplate. Install a fuse in the brush output lead.

MAINTENANCE

With ordinary care and attention to the precautions outlined above, the POWERSTAT Variable Transformer should require no servicing except possible replacement of the brush. The brush should be inspected periodically and replaced if arcing takes place or if it is badly worm. The correct replacement brush is RB10B for 108 Series units, RB10B-40 for 108-40 Series units and RB12 for 12 Series units. Because the brushes must be of a special material, only the specified replacement should be used.

Whenever electrical or mechanical difficulties arise in installing or operating the POWER-STAT Variable Transformer, contact the factory or the nearest Superior Electric field office.

THE SUPERIOR ELECTRIC COMPANY, Bristol, Connecticut, U.S.A.



MODELS

10 AMP

PEAK

AMPS

110

85

70

60

50

40

36

33

32

31

30

5 AMP

PEAK

AMPS

85

70

65

55

48

40

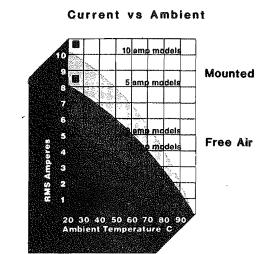
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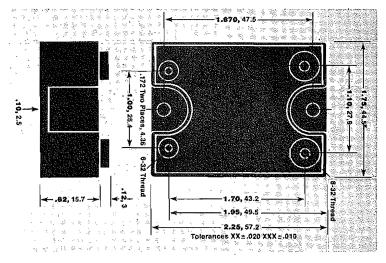
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-31

30

28





Detail Electrical Specifications

Surge Current Data

TIME

(CYCLES)

È

3

6

12

30

60

120

180

240

300

600

£

TIME

.017

.050

.100

.200

.500

1

3 16

4

5 🐇

10

2 🖉

SECONDS

Detail	Elect	rical	Speci	ficatio	ms	i na			<u> </u>		1.2.6.9.冬	€ <i>€ № %</i>	an sa hari	
Model Number	Nominal AC Line Voltage	Nominat Current Rating Amps	1 Cycle Surge (Amps) Peak	Signal 🚽	Signal Pick-up Voltage	Signa) Drop-out Voltage	Peak Repatitive Voltage Minimum	Maximum Contact Voltage Drop	Off State Leakage ma Maximum	Operating Voltage Range Volts AC	I ² t Rating t=8,3 Milli- Seconds	Standard Isolation Voltage	⊖jc ℃/Watt	Dissipation Watts/Amp
Z 120 D5 or ZS 120 D5	120	5 5 6 5	85 · · ·	500	4 VDC (20 V allowed)	1 VDC	250	1.6 V	8 ma	12-140	30	2500 V RMS	5	1:3
Z 120 D10 or ZS120 D10		10	110		en e				15 ma	12-140	30 × 1			1
Z 240 D5 of ZS 240 D5	240	5	85 ***				500 1		8 ma	24-280	50		5	1:3
Z240 D10 or ZS240 D10		10	110	× ∀ ,>≊, 	· · · ·		ł		15 ma	24-280	50		4	4
			1997 - 1997 1997 - 1997 - 1997 - 1997 1997 - 1997 - 1997 - 1997 1997 - 19	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·				2013年1月1日 1月1日 1月1日 1月1日 1月1日 1月1日 1月1日 1月111日 1月111日 1月111日 1月111日 1月1111 1月1111 1月1111 1月11111 1月11111 1月11111 1月111111					
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Additional Specifications (All Models) Isolation: Input-to-output and input-to-base: 2500 VAC 10¹⁰ ohms DC. Coupling capacitance input to output 8 PF max. Operating temp: -40°C to 100°C Operating Freq: 25-65 HZ

Turn-On-Time: ½ cycle maximum zero voltage Turn-Off-Time: ½ cycle maximum zero current DV/DT-Off State: 200 V/microsecond DV/DT-Commutating: Snubbed for rated current at .5 power factor Note: —4 to Part No, for 4000 V. isolation, 600 volt PRV available any model. Add -6 to Part No.

Ojc = Thermal resistance junction to base. Maximum junction temperature = 110°C

OPERATING INSTRUCTIONS AND PARTS LIST

For

"PB" Pressure Blowers "HP" Pressure Blowers "LM" Volume Blowers "ORB" Industrial Exhausters Series FC and BI Utility Sets

WARNING

Rotating Equipment must be properly guarded to prevent personal injury.

By acceptance of this merchandise, the purchaser and user assume complete responsibility for the safe operation of this equipment. The manufacturer disclaims any and all responsibility unless this unit is operated in compliance with all federal and local laws and regulations.

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Receiving and Start-up Instructions	Page 2
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Bearing Maintenance	Page 3
Warranty	Page 3
Ordering Replacement Parts	Page 3



5345 Creek Road, Cincinnati, Ohio 45242, Area Code 513-984-0600

RECEIVING & START-UP

Receiving Inspection

When unit is received, inspect immediately for damaged or missing parts. Even though all units are carefully inspected. and prepared for shipment at the factory, rough handling enroute may cause concealed damage or cause nuts, bolts or locking collars to work loose. Check wheel to see that it rotates freely and that there are no obstructions. Be certain all bolts and locking collars are tightened securley.

If concealed damage is found, call the carrier and ask for their Inspection Department. Then fill out a concealed damage inspection report.

Operation

Before Start Up

- 1. Inspect all fasteners to make sure they are secure.
 - a. Foundation bolts
 - b. Set screws in fan wheel and V-belt drive
 - c. Housing, bearing and motor mounting bolts
- 2. Access Doors should be tight and sealed.
- 3. Bearings should be checked for alignment and lubrication.
- 4. Turn rotating assembly by hand to insure that it does not strike housing. If the wheel strikes the housing, the wheel may have moved on the shaft or the bearings may have shifted in transit. Correction must be made prior to start up.
- 5. Check motor to insure proper speed and electrical characteristics.
- 6. Check V-belt drive for alignment.

GENERAL MAINTENANCE

CAUTION –Before any maintenance or service is performed, be sure that unit is disconnected from power source to prevent accidental starting.

Cast Aluminum & Metal Parts

The cast aluminum bearing housings and impellers, as well as all metal parts, are maintenance free and should not require any maintenance during the life of the unit.* In a severe dirty operation, the wheel should be cleaned with a wire brush to prevent an accumulation of foreign matter that could result in fan unbalance. After cleaning impeller, inspect for possible cracks or excessive wear, which can cause unbalance. Belts on V-belt drive units require periodic inspection and replacement when worn.

Motor Maintenance

- 1. Removing dust and dirt: Blow out open type motor windings with low pressure air to remove dust or dirt. Air pressure above 50 P.S.I. should not be used as high pressure may damage insulation and blow dirt under loosened tape. Dust can cause excessive insulation temperatures.
- 2. Lubrication: Under normal conditions, ball bearing motors will operate for five years without relubrication. Under continuous operation at higher temperatures (exceeding 104 degrees F. ambient) or dusty atmosphere re-lubricate after one year. To re-lubricate motor bearings, disassemble motor and housings thoroughly. Bearings are located in the end shields of the motor. Repack each bearing and fill cavity in back of bearings 1/3 full with Alvania Grease No. 2 (Shell Oil Company) or equivalent.

V-BELT DRIVES

CAUTION-Care should be taken not to over tighten V-belt drives. Excessive belt tension overloads fan and motor bearings. It is much less expensive to replace belts worn from slippage than to replace bearings damaged from excessive loading.

Fans shipped completely assembled have had V-belt drive aligned at Cincinnati Fan. Alignment should be re-checked before operation as a precaution due to handling during shipment.

- 1. Be sure sheaves are locked in position.
- 2. Key should be seated firmly in keyway.
- 3. Place straight edge or taut cord across faces of driving and driven sheaves to check alignment. The motor and fan shafts must be parallel; with V-belts at right angles to the shafts.
- 4. Start the fan. Check for proper rotation. Run fan at full speed. A slight bow should appear on slack side. Adjust belt tension by adjusting motor on its sliding base. All belts must have slack on one side.
- 5. If belts squeal at start-up, they are too loose and should be tightened.
- 6. When belts have had time to seat in the sheave grooves, then readjust belt tension.

V-belt drive assembly can be mounted as follows:

- 1. Clean motor and fan shafts. Be sure they are free from corrosive material. Clean bore of sheaves and coat with white lead or heavy oil for ease of shaft entry. Remove oil, grease, rust or burrs from sheaves.
- 2. Place fan sheave on fan shaft and motor sheave on its shaft. DO NOT POUND SHEAVES ON as this may damage bearings. Tighten sheaves in place.

^{*}Painted metal surfaces may require periodic repainting,

- 3. Move motor on slide base so belts can be placed in grooves of both sheaves without forcing. Do not roll belts or use a tool to force belts over the grooves.
- 4. Align fan and motor shafts so they are parallel. The belts should be at right angles to the shafts. A straight edge or taut cord placed across the face of sheaves will aid in alignment.
- 5. Tighten belts by adjusting motor base. Correct tension gives the best drive efficiency. Excessive tension causes undue bearing pressure.
- 6. Start the fan and run it at full speed. Adjust belt tension until only a slight bow appears on the slack side of the belts. If slippage occurs, a squeal will be heard at start-up. Eliminate this squeal by tightening up the belts.
- 7. Give belts a few days running time to become seated in sheave grooves then readjust belt tension.

If the shafts become scratched or marked, carefully remove sharp edges and high spots such as burrs with fine emery cloth or honing stone. Avoid getting emery dust in the bearings.

Do not apply any belt dressing unless it is recommended by the drive manufacturer. V-belts are designed for frictional contact between the grooves and sides of the belts. Dressing will reduce this friction.

Belt tension on an adjustable pitch drive is obtained by moving the motor - not by changing the pitch diameter of the adjustable sheave.

BEARING MAINTENANCE

Sealed Bearings

Sealed for life bearings are pre-lubricated with the correct amount of manufacturer-approved ball bearing grease, and are designed for application where re-lubrication is not required,

Units feature two single row deep groove bearings in a rugged cast aluminum or cast iron bearing bracket. Dirt and grease guard seals are an integral part of the assembly. For high temperature applications the bearings are prelubricated with a high temperature grease.

Relubricatable Bearing

For grease lubricated ball or roller bearings, or pillow blocks, a good grade of soda soap grease free from chemically or mechanically active material should be used.

This grease is a mixture of lubricating oil and a soap base to keep the oil in suspension. They have an upper temperature limit where the oil and soap base oxidize and thermally decompose into a gummy sludge.

Grease listed (or equivalents) are satisfactory for normal operating conditions. Regreasing will vary from 3 months to a year depending upon hours of operation, temperature and surrounding conditions. Special grease may be required for dirty or wet atmospheres (consult your lubricant supplier).

The pillow block should be filled with a low pressure gun until 1/3 full as excess grease may cause over heating.

Recommended grease for temperatures ranging from -40 degrees F to 250 degrees F are: Sinclair Refining Co.-AF No. 2, Scony Mobile Oil Co.-Mobilplex EP No. 1, Sun Oil Co.-Sun 72XMP grease, Esso Standard Oil Co.-ANDOK "C", Texas Co.-Texaco Regal Starfak No. 2.

WARRANTY

Cincinnati Fan & Ventilator Company warrants products of its own manufacture, against defects of material and workmanship under normal use and service for a period of eighteen (18) months from date of shipment or twelve (12) months from date of installation whichever occurs first. This warranty does not cover ordinary wear and tear, abuse, misuse, overloading, altered products, systems or materials not of Seller's manufacture. Expenses incurred by Buyer(s) in repairing or replacing any defective product will not be allowed except where authorized in writing and signed by an officer of the Seller.

The obligation of Seller under this warranty shall be limited to repairing or replacing F.O.B. Seller's plant, or allowing credit at Seller's option.

On equipment furnished by Seller, but manufactured by others, such as motors, Seller extends the same warranty as Seller receives from the manufacturer thereof.

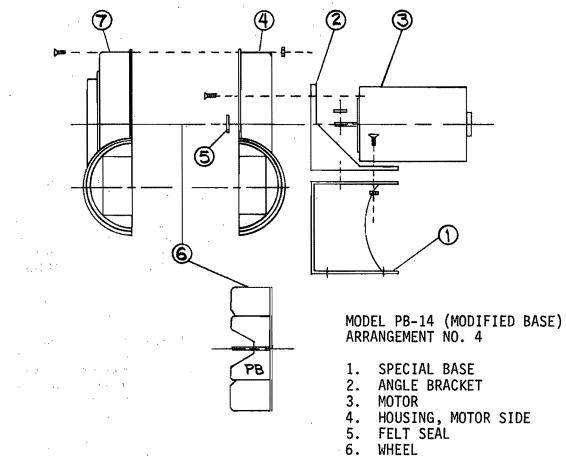
Cincinnati Fan & Ventilator Company assumes no responsibility for material returned to our plant without our written permission.

ORDERING REPLACEMENT PARTS

Replacement or spare parts may be ordered through your local Cincinnati representative.

The following information should accompany parts orders.

- 1. Motor horsepower, frame size and motor speed.
- 2. Fan Speed (if V-belt driven).
- 3. Fan arrangement and model number.
- 4. Serial number, model number and a complete description of the part.



7. HOUSING, INLET SIDE



INSTRUCTIONS

3 PHASE VOLTAGE MONITORS

UNDER VOLTAGE – PHASE PROTECTION RELAY

File No.	
	947-HPB
	, or Class Series BIOAD, AG & AH
Size	
Date	JUNE, 1977

THREE PHASE RATING

Specification	208V		24	ov		480V	
Operating Voltage 60 Hz. (Neutral Not Required)	190-225	v		265∨	430-520V		
Trip Voltage Range	175-208	V	200-	235V	4	100-470V	
Pick Up Sequence L1 - L2 - L3	A-B-C		A - B	- C	A	-В-С	
Pick Up - Trip Out Differential	15V		15V		-	νo	
Pick Up Delay (Typ.)	12 sec.		12 \$	ec.	1	2 sec.	
Trip Out Delay (Typ.)	6.5 sec.	6.5 sec.			6	6.5 sec.	
Set Point Repeatability @ 25°C	2%	2%		2	%		
Dial Calibration	5%	5%			5	%	
Transient Protection	10,000		10,0	00V	10,000∨		
Operating Temperature	0 to +7	0C	0 to	+70C	0	to +70C	
Trip Indicator Light (Solid State) Relay Output Contact	L.E.D. SPDT		L.E.D SPD1	-	-	.E,D. PDT	
	Max.	Amp	5	Max.	٧o	It Amps	
Contact Rating	Make	B	ireak	Make		Break	
120 Volts	15	15 1.		1800		180	
240 Volts	7.5		0.75	1800		180	
480 Volts	3.75) c	.375	1800		180	

GENERAL OPERATION

The voltage monitor is a voltage and phase sensing relay which helps protect machinery and equipment against low voltage, voltage unbalance, loss of phase, and phase reversal. The voltage monitor will not pick up if any of the above fault conditions exists or if they occur during operation, the voltage monitor will trip out. It will automatically pick up (reset) after it has tripped out provided the fault condition is corrected and all other requirements for pick up are met.

LOW VOLTAGE

The voltage monitor will pick up after a time delay if all three phase voltages are at least 15 volts higher than the dial set trip voltage for either the 208 V or 240 V unit and 30 volts higher for the 480 V unit. The voltage monitor will trip out after a time delay when all three phase voltages drop below the dial set trip voltage.

The voltage monitor will trip out in the same manner as previously described if all three phase voltages drop just below the dial set trip voltage for longer than 4 seconds and then return to their original value. The unit will trip out instantaneously if all three phase voltages are momentarily interrupted or turned off.

The pick up-trip out voltage differential and time delays have been designed into the voltage monitor to prevent chattering, rapid recycling, and nuisance trip outs caused by momentary transient voltage drops that can occur during motor starting. (See increased protection adjustment.)



VOLTAGE UNBALANCE

The voltage monitor will trip out in cases where the voltage unbalance is created by a phase voltage drop. The voltage monitor will trip out after a time delay when the system operating voltage is the same as the just pick up voltage and any one of the phase voltages drops 9% below the system operating voltage. (See increased protection adjustment.)

LOSS OF PHASE

The voltage monitor will not pick up if all three phases are not present or it will trip out after a time delay if a phase loss occurs during operation. The voltage monitor senses a lost phase by monitoring the voltage drop on the lost phase. In some applications a lightly loaded motor may regenerate the voltage drop on the lost phase enough to keep the voltage monitor from tripping out. (See increased protection adjustment.)

PHASE REVERSAL

The voltage monitor will pick up after a time delay only if it senses the proper phase sequence: A-B-C to L1-L2-L3. The voltage monitor will trip out after a time delay if a phase reversal occurs during operation.

INCREASED PROTECTION ADJUSTMENT

To increase the amount of protection afforded by the voltage monitor the dial set trip voltage can be adjusted closer to the system operating voltage once the unit has picked



44-3-863 -34 4 5 5

FURNAS ELECTRIC COMPANY . BATAVIA, ILLINOIS

3 PHASE VOLTAGE MONITORS

UNDER VOLTAGE - PHASE PROTECTION RELAY

TYPICAL DIAGRAM

up. This in effect reduces the amount of voltage drop required to trip out the voltage monitor due to low voltage, voltage unbalance and loss of phase during operation. The amount of the reduction is governed by the system voltage fluctuation. This adjustment may require that the voltage monitor be reset manually for pick-up if the system voltage-trip out voltage differential is less than the pick up - trip out voltage differential.

The voltage monitor can be manually reset for pick up by turning the dial set trip voltage to the minimum trip voltage value and then after the unit has picked up, returning it to its original dial set trip voltage.

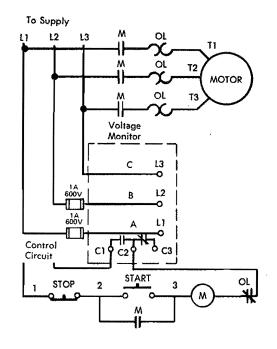
TRIP INDICATOR

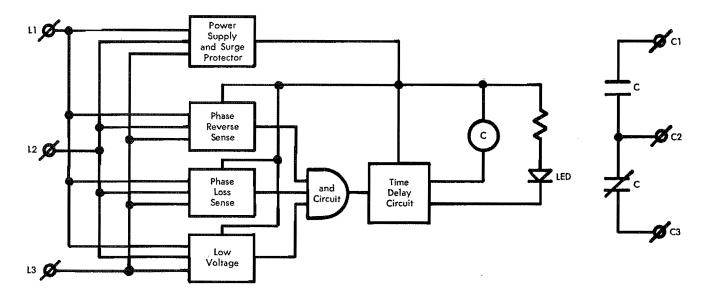
The voltage monitor incorporates in its design a light emitting diode to indicate the operational status of the unit and is operational only when the applied voltage is at least 25% of the system voltage. LED on, unit has tripped out; LED off, unit has, picked up.

OUTPUT

The voltage monitor incorporates in its design a set of single pole double throw relay contacts for the output circuit. The normally closed portion of this contact arrangement can be used to initiate an alarm to warn of improper conditions when the unit is tripped out.

CAUTION: Automatic resetting of the voltage monitor can occur on two wire control. When not desired, three wire control should be used.





BLOCK DIAGRAM

RF CIRCUITRY

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SECTION I

RF CIRCUIT THEORY OF OPERATION

1-1. INTRODUCTION

1-2. The following text provides detailed theory of operation with supporting diagrams for the FM-30 FM transmitter RF circuitry. For purposes of definition, the text is divided into functional circuits (see Figure 1-1).

1-3. FUNCTIONAL DESCRIPTION

1-4. FM EXCITER

1-5. A complete technical description of the FM exciter circuitry is contained in publication 597-0002, FX-30 FM Exciter.

1-6. RF AMPLIFIER

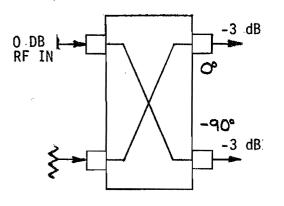
1-7. IPA STAGE. The RF output from the FM exciter is applied to the FM-30 driver amplifier. Five identical amplifiers comprise the IPA section of the FM-30 transmitter. One amplifier is used as a driver for the remaining four. The RF driver may be interchanged with any of four other RF amplifiers in the IPA stage, its only distinction being the physical placement of the amplifier in the MODULE 1 position within the configuration.

1-8. Each amplifier module employs two RF transistors conservatively operated class C in parallel with tuned input and output circuits. The amplifiers employ micro-stripline tuned sections etched into the circuit board. When combined with associated capacitors in the circuit, the micro-stripline sections offer the required impedance transformation from RF input to base circuit impedance and collector circuit impedance to RF output. Normally, amplifier tuning will not be required unless a component fails on an amplifier circuit board and requires replacement. Bandwidth of each amplifier is approximately 6 MHz at 3 dB points.

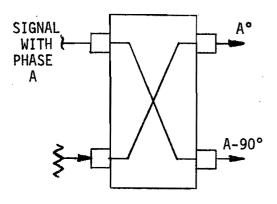
1-9. <u>Hybrid Combiner/Splitter Operation</u>. A hybrid combiner/splitter is a four-port device. When fed by an RF source into one port, the device will split the applied input equally between the two opposite ports (see Figure 1-2).

1-10. Assuming the same input conditions, the phase of the two outputs will be 90 degrees out-of-phase with respect to each other. The port directly opposite the input port will be in phase with the input port.

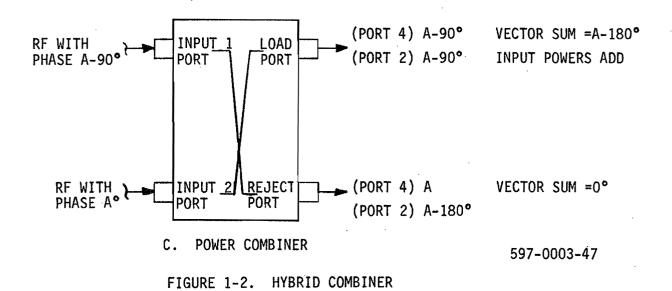
1-11. If two RF signals of the same amplitude and frequency, but 90 degrees out-of-phase are fed into two ports of a hybrid combiner, the two signals will completely combine at the output port and no power will appear at the reject port. Any difference in input phase (other than 90 degrees) or any difference in amplitude between the two inputs will appear as power at the reject port.



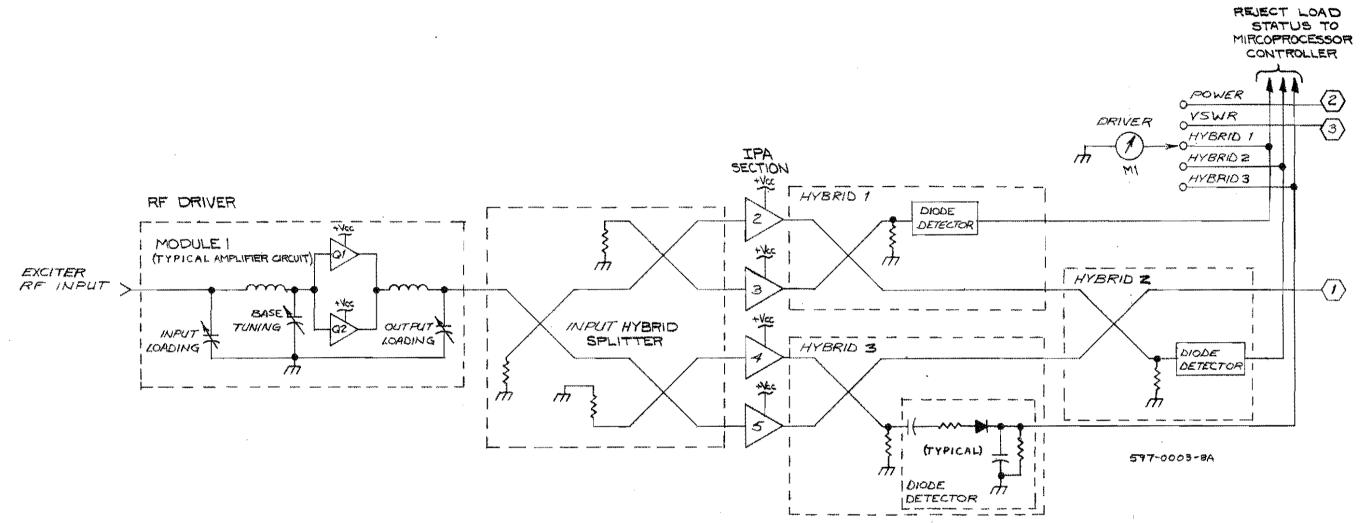
A. POWER RELATIONSHIP



B. PHASE RELATIONSHIP



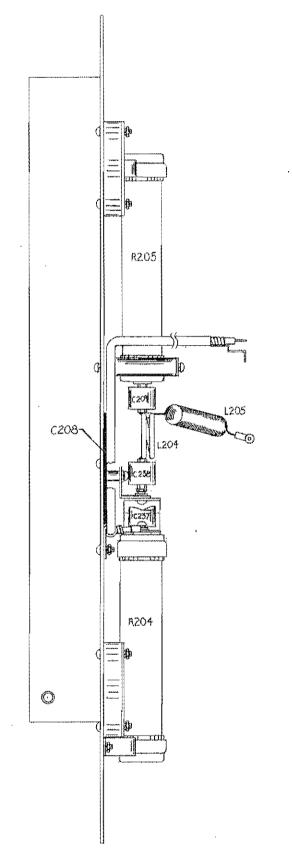
1-12. <u>FM-30 Hybrid RF Circuit</u>. The output of the RF driver is connected to the input of a triple section hybrid splitter which offers four outputs, each output 90° shifted in phase from one output to each adjacent output. The outputs from this hybrid splitter feed the inputs of the four IPA amplifiers. Each amplifier is identical and may be interchanged.



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FIGURE 1-1. RF CIRCUIT SIMPLIFIED SCHEMATIC (SHEET 1 OF 2)

1-3/1-4

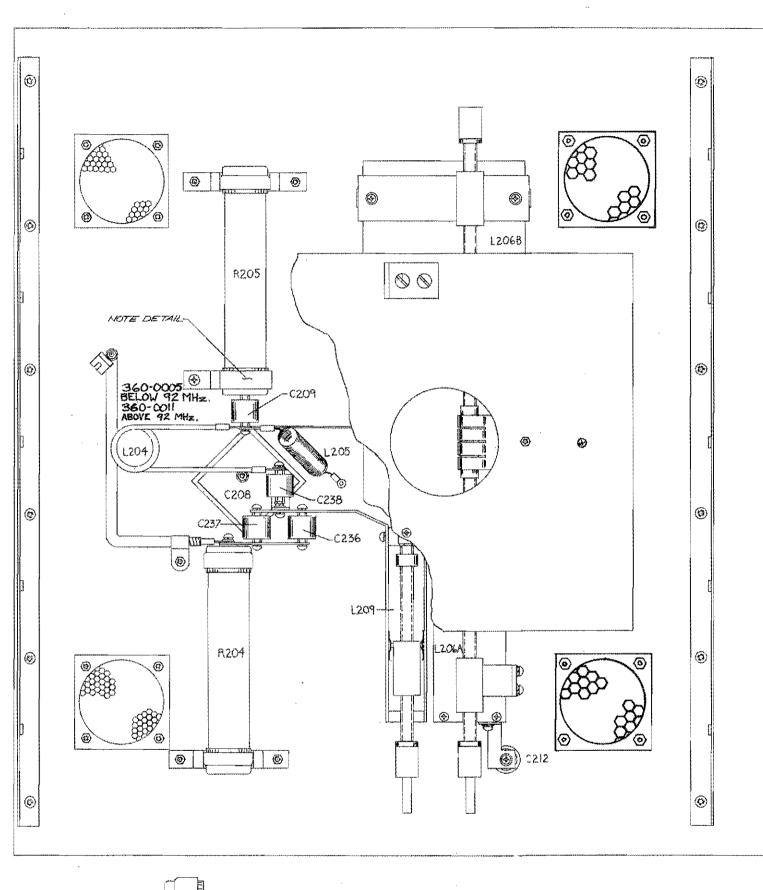


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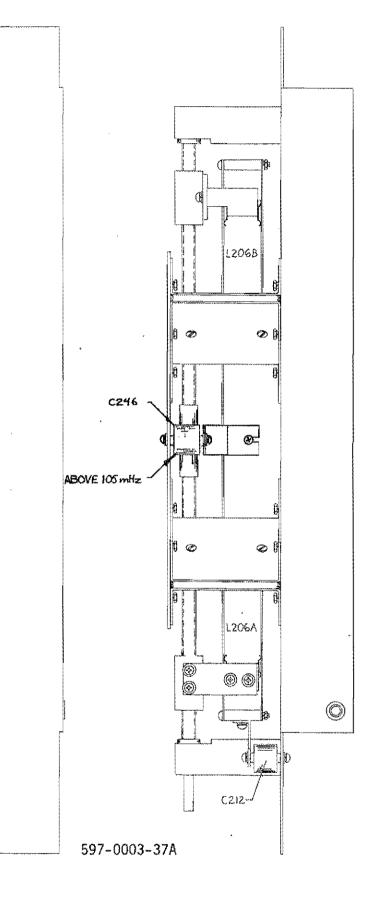
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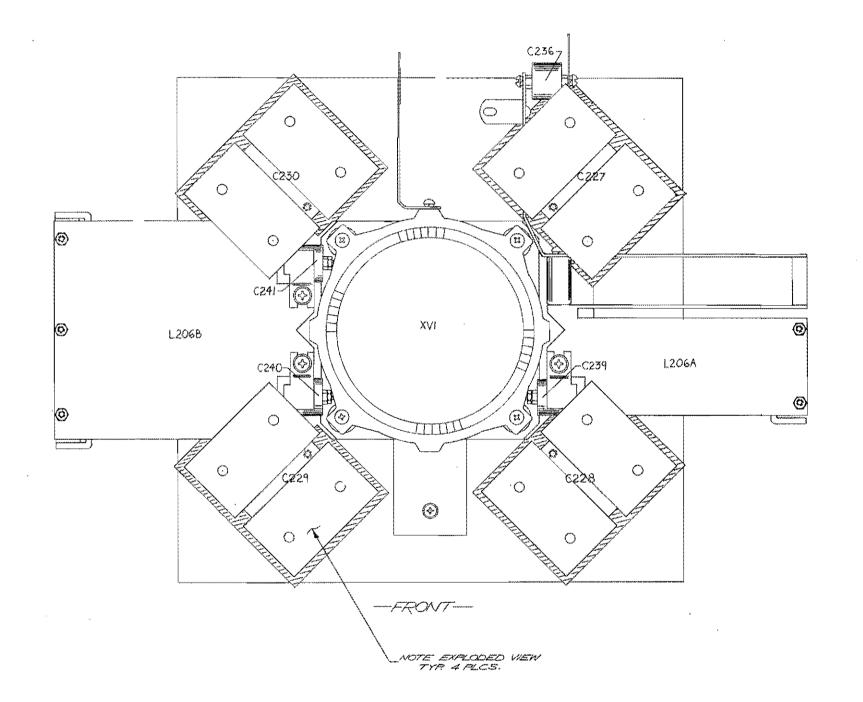


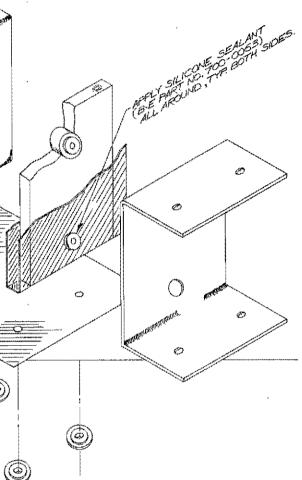
DETAIL

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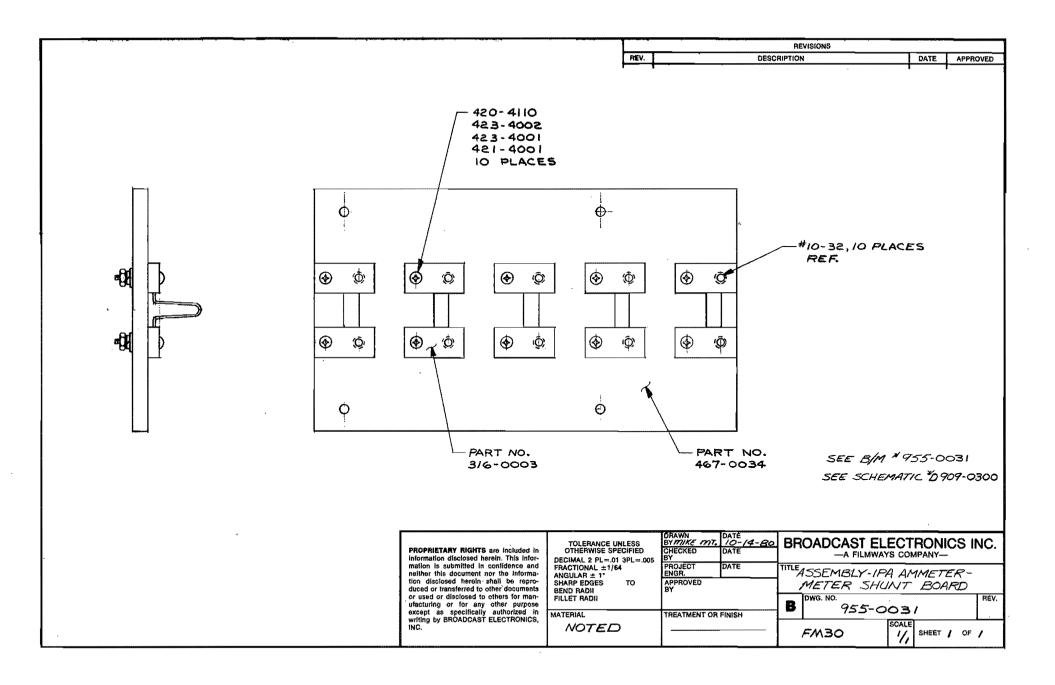
FM-30 GRID INPUT CIRCUIT ASSEMBLY (SHEET 1 OF 2)





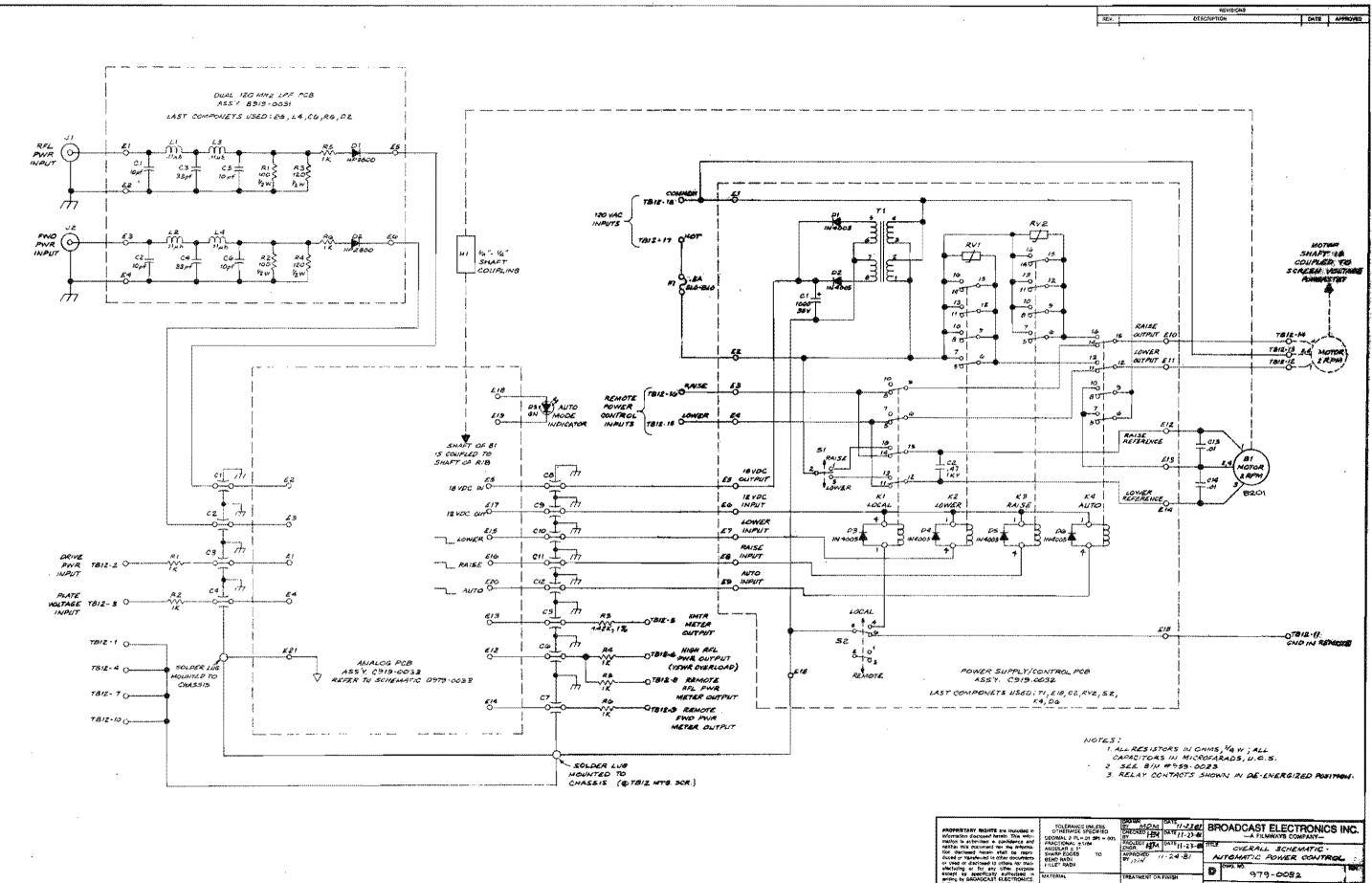
597-0003-37B

FM-30 GRID INPUT CIRCUIT ASSEMBLY (SHEET 2 OF 2)



				REVISIONS		
			REV.	DESCRIPTION	DATE	APPROVED
			A	PER ECN #1935	3-3-80	M
			В	PER ECN # 1965	3-19-80	
			C	PER ECN 2542	2-5-81	<i>m 1</i> n
REJECT LOAD #20 4.7K REJECT LOAD #306 4.7K REJECT LOAD #104 A.7K FORWARD POWER 0 K	90 R7 100 GND 2K 70 R5 2K 50 R3 2K 50 R3 2K 2K 50 R3 2K 2K 50 R3 2K 70 R3 2K 70 R5 2K 50 R3 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R5 2K 70 R3 2K 70 R3 2K 70 R3 2K 70 R3 2K 70 8 8 8 8 8 8 8 8 8 8 8 8 8			12 VSWR METER OUT		
			+ MI			
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/		PROPRIETARY RIGHTS are included in information disclosed herein. This infor- mation is submitted in confidence and neither this document nor the informa- tion disclosed herein shall be repro- duced or transterred to other documents or used or disclosed to others for man- ufacturing or for any other purpose except as specifically authorized in writing by BROADCAST ELECTRONICS, INC.	TOLERANCE UNLESS OTHERWISE SPECIFIED DECIMAL 2 PL=.01 3PL=.003 FRACTIONAL ±1164 ANGULAR ± 1* SHARP EDGES TO BEND RADII FILLET RADII MATERIAL	BY DATE A FII PROJECT DATE TiTLE ENGR. IPA MULTI BY IPA MULTI	ELECTRONIC MWAYS COMPANY- CHEMATIC METER BOAR	

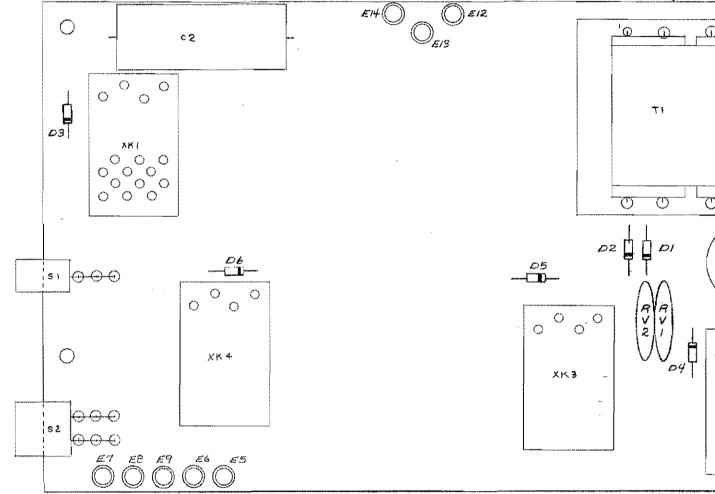
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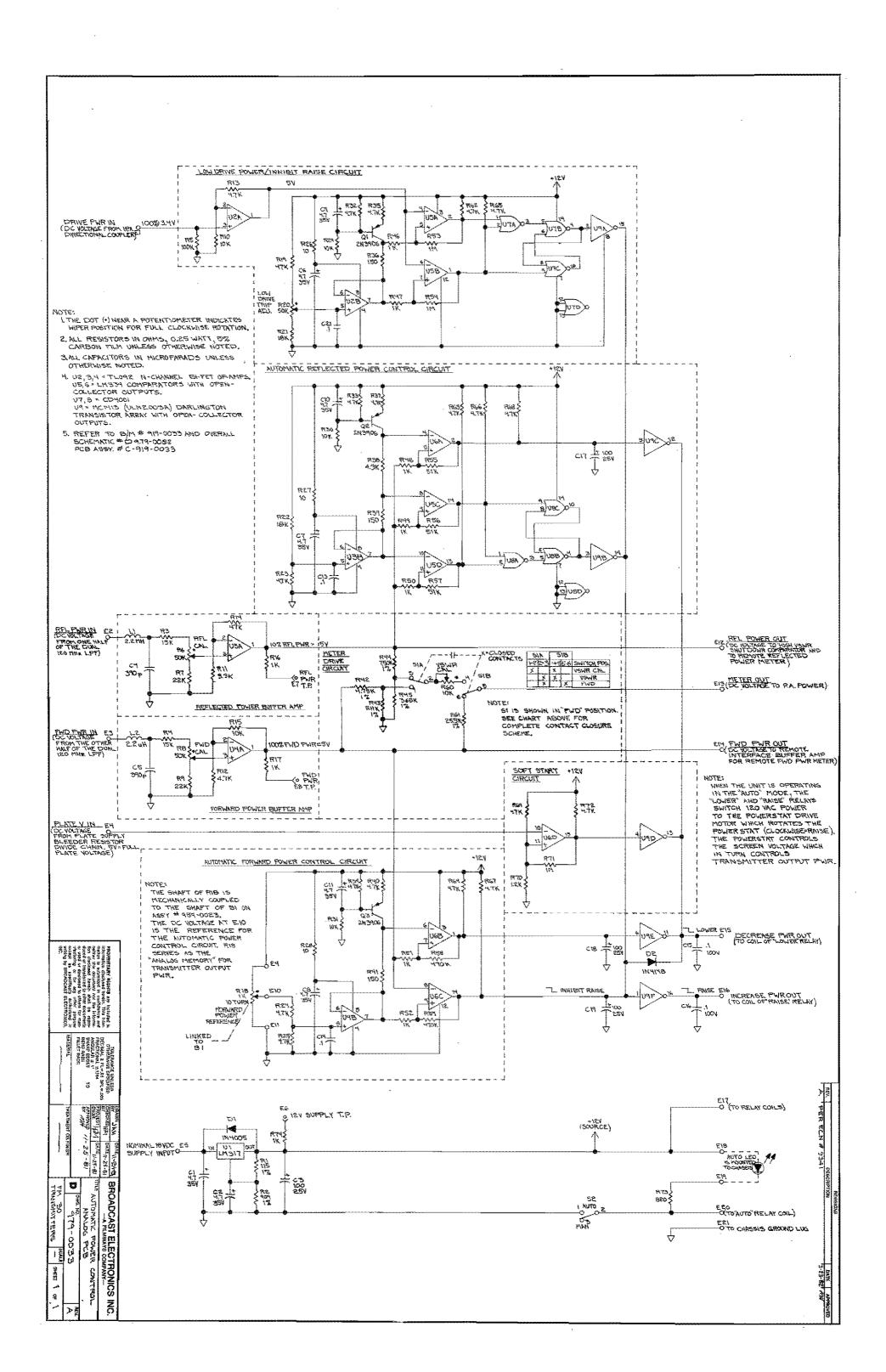
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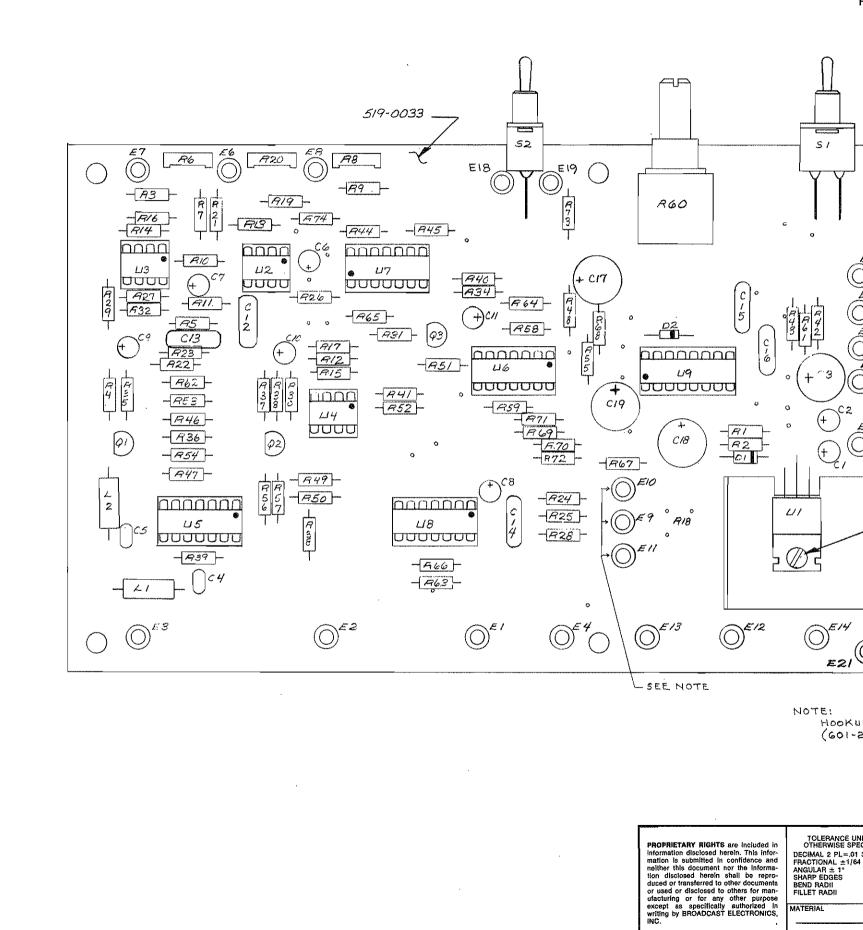
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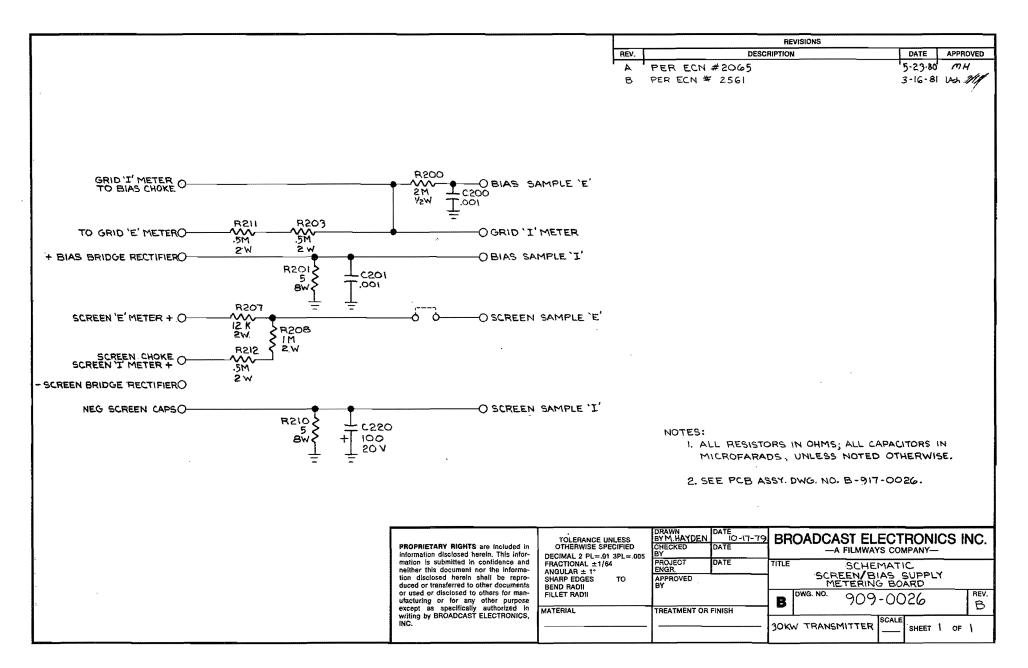




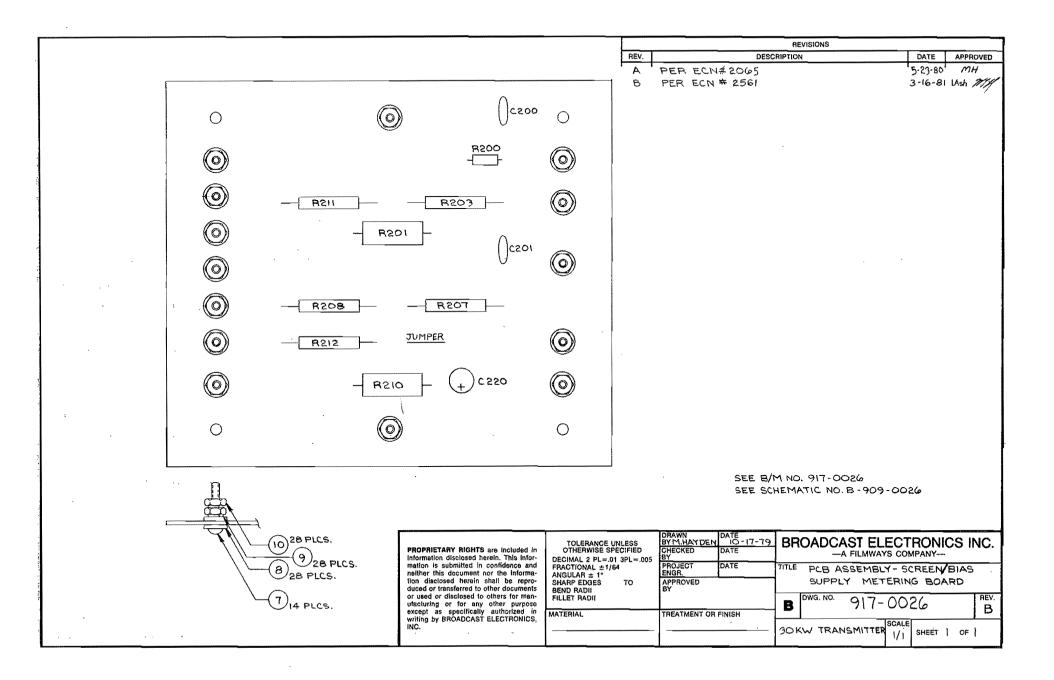
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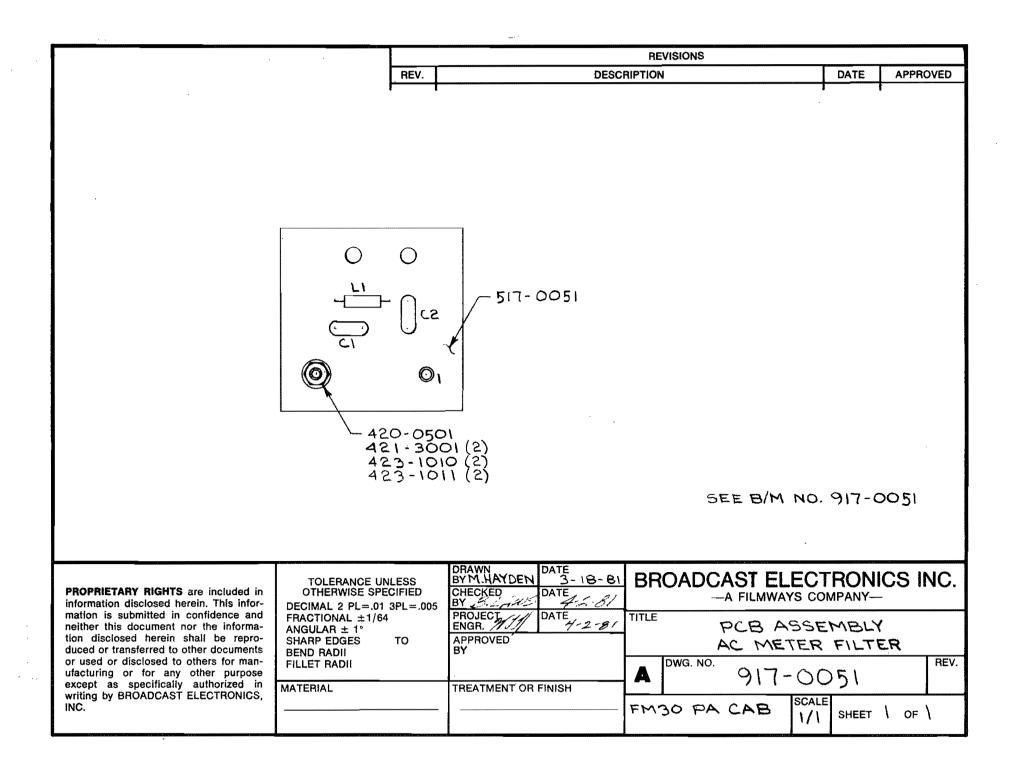
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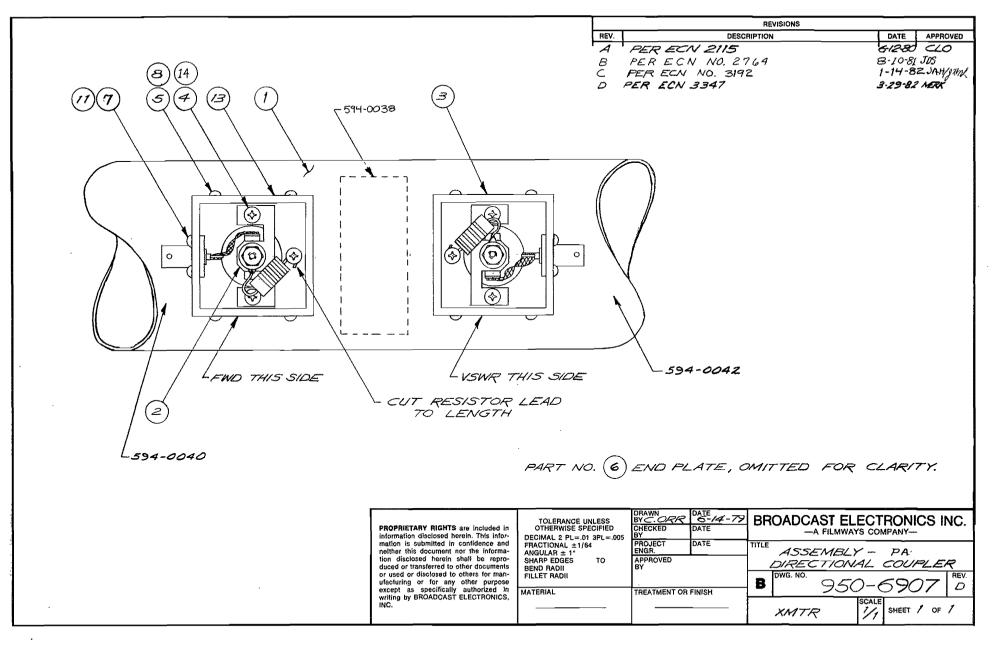
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2 .75 REF. SOLDER IN PLACE 6	SOLDER IN PLACE	7 420-0068 #6-32 × 1/2 STUD (BRASS)	QTY 1 1 1 1 1 1 1
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APPENDIX A

RF CIRCUIT MANUFACTURERS DATA

A-1. INTRODUCTION

A-2. This appendix provides the following technical data relative to the operation and maintenance of the FM-30 FM Transmitter RF circuitry. Information in the appendix is provided in the following order.

A. Technical Data Sheet, Communications Transistor Corporation BM100-28 Transistor.

B. Technical Data Sheet, Eimac 8990 (4CX20000A Tetrode).

C. Engineering News Letter, Eimac, Life VS Filament Voltage.



GENERAL DESCRIPTION The BM100-28 is a matched, 100 watt VHF device. The single matching section allows improved performance for operation to 220 MHz. The BM100-28 offers improved saturated power and ruggedness at the same gain as the 2N6369 (BM80-28). Input match has been designed to be similar to that of the BM80-28.

Maximum Power Dissipation (Note 1) Total Power Dissipation at 25 °C Case Temperature

Maximum Voltage and Current

LA CELEVITE	antraño ana mariare
BVCES	Collector to Emitter Voltage
BVERO	Emitter to Base Voltage
BV _{CES} BV _{EBO}	Collector Current

ELECTRICAL CHARACTERISTICS (25°C unless otherwise specified)

PACKAGE

SYMBOL	CHARACTERISTIC	MIN.	TYP.	MAX.	UNITS	TEST CONDITIONS
POUT	Power Output	100			WATTS	f = 175 MHz, Vcc = 28 Volts
P IN	Power Input (At rated Power Out)			20	WATTS	f = 175 MHz, Vcc = 28 Volts
η	Collector Efficiency (At rated Power Out)		60		%	f = 175 MHz, Vcc = 28 Volts
ZIN	Series Input Impedance		1 + j 2.2		OHMS	At rated output power and frequency
Ссв	Collector to Base Capacitance(f=1.0 MHz)		250		pF	V CB = 28 V, I E = 0
BV EBO	Emitter to Base Voltage	4			VOLTS	IE = 5 mA
BV CES	Collector to Emitter Voltage	70			VOLTS	$I_{C} = 100 \text{ mA}$
8V ceo	Collector to Emitter Voltage	33			VOLTS	I _C =50 mA
HFE	DC Current Gain	20		100		I _C =1A, Vce=5 Volts
VSWR	Output VSWR Capability	∞				POUT= 100W, Vcc=28V f=175MHz

270

70 4 20

NOTES:

1. This rating gives a maximum junction temperature of 200°C with junction to case thermal resistance of .65 °C/watt.

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OUTPUT-WATTS

POUT = POWER

90

60

30

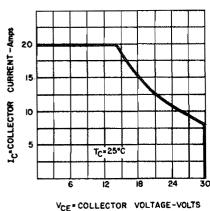
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PIN POWER INPUT-WATTS

D.C. SAFE OPERATING AREA



POWER OUTPUT VS POWER INPUT (TYPICAL)

BMI00-28

f+175 MHz

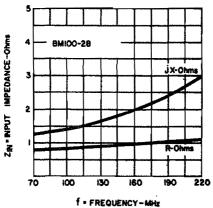
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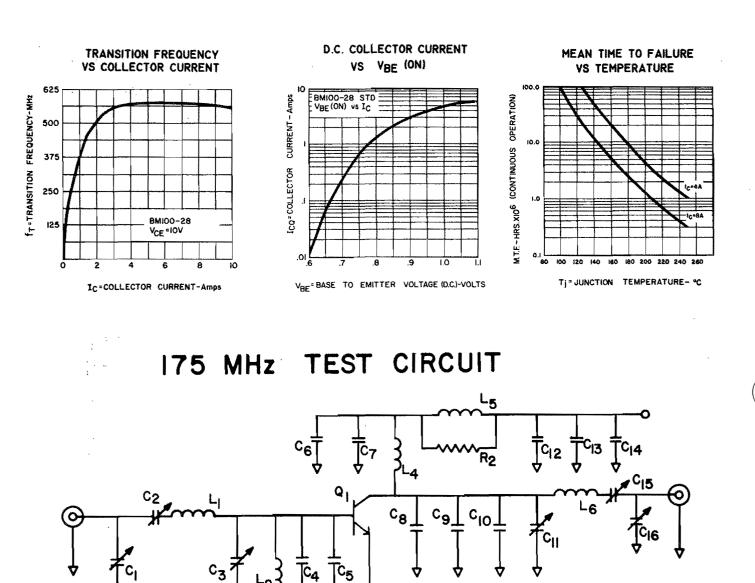




CT 8M100-28 July, 1976 (2.2.8.5L)

COMMUNICATIONS TRANSISTOR CORPORATION 301 Industrial Way, San Carlos, California 94070

A Subsidiary of Varian Associates (415) 592-9390 TWX 910-376-4893 COMMUNICATIONS TRANSISTOR CORPORATION BM100-28



	\bot	
01	BM100-28 V	C14
C1, C2, C3	ARCO 5-70pF	L1
C11, C16	ARCO 5 - 70pF	L2
C4, C5	100pF UNDERWOOD	L3
C6, C12	300pF UNDERWOOD	L4
C7	$.01 \mu$ F disc ceramic	L5
C8, C9	15pF UNDERWOOD	
C10,	4 ea, 33pF ATC .10'' cube	L6
C13	100pF UNDERWOOD	R1
010		R2

RI

50 μ F, 100 V electrolytic 2 turns #16 wire, ½'' I.D. .33 μ H, molded inductor 5.6 μ H, molded inductor 3 turns #16 wire, ½'' I.D. 6 turns #18 wire, wound on Indiana General F627 - 8, H material 2 turns #16 wire, ½'' I.D. 15 Ω ½ watt carbon comp. 15 Ω ½ watt carbon comp.

5K Printed in U.S.A.

TECHNICAL DATA

The EIMAC 8990/4CX20,000A is a ceramic/metal power tetrode intended for use in audio or radio-frequency applications. It features a type of internal mechanical structure which results in high rf operating efficiency. Low rf losses in this structure permit operation at full ratings up to 110 MHz.

The 8990/4CX20,000A has a gain of over 18 dB in FM broadcast service, and is also recommended for radio-frequency linear power amplifier service, and for VHF television linear amplifier service. The anode is rated for 20 kW of dissipation with forced-air cooling and incorporates a highly efficient cooler of new design.

The 8990A is recommended for high-level, plate modulated amplifier service.

GENERAL CHARACTERISTICS¹

ELECTRICAL

Filament: Thoriated Tungsten Voltage:	
Grid to Screen	
Direct Interelectrode Capacitances (cathode grounded): ²	
Cin	190 pF
Cout	
Cgp	1.5 pF
Direct Interelectrode Capacitances (grid and screen grounded): ²	
Cin	83 pF
Cout	24.5 pF
Cpk	0.2 pF
Frequency of Maximum Ratings (CW)	110 MHz

- 1. Characteristics and operating values are based on performance tests. These figures may change without notice as the result of additional data or product refinement. EIMAC Division of Varian should be consulted before using this information for final equipment design.
- 2. Capacitance values are for a cold tube as measured in a special shielded fixture in accordance with Electronic Industries Association Standard RS-191.

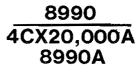
MECHANICAL

Maximum Overall Dimensions:	0.840 in: 04.00 or
Length	
Diameter	
Net Weight (Approximate)	
Operating Position	Axis vertical, base up or down
Cooling	Forced air
Operating Temperature, maximum	
Ceramic/Metal Seals and Anode Core	
Base	
Recommended Air System Socket	SK-320
Recommended Air Chimney	

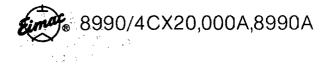
4402 (Effective 20 October 1980)

Printed in U.S.A.





VHF RADIAL BEAM POWER TETRODES



RADIO FREQUENCY POWER AMPLIFIER OR OSCILLATOR

Class C Telegraphy or FM (Key-Down Conditions)

ABSOLUTE MAXIMUM RATINGS

DC PLATE VOLTAGE	10,000	VOLTS
DC SCREEN VOLTAGE	2,000	VOLTS
DC PLATE CURRENT	5.0	AMPERES
PLATE DISSIPATION	20,000	WATTS
SCREEN DISSIPATION	450	WATTS
GRID DISSIPATION	200	WATTS

TYPICAL OPERATION (frequencies to 30 MHz)

	Plate Voltage	7.5	9.0	kVdc
	Screen Voltage	750	900	Vdc
	Grid Voltage	-200	-250	Vdc
	Plate Current	3.68	4.01	Adc
	Screen Current ¹	208	222	mAdc
	Grid Current ¹	91	88	mAdc
	Peak rf Grid Voltage ¹	265	300	v
	Calculated Drive Power	24.1	26.4	W
ES	Plate Dissipation ¹	5.84	7.93	kW
-0	Plate Output Power ¹	21.8	28.2	kW
	Load Impedance	1062	1136	Ω
	¹ Approximate value			

TYPICAL OPERATION, COMMERCIAL FM SERVICE (measured values at frequency shown, in EIMAC CV-2200 cavity amplifier)

Frequency of Operation	88.3	107.7	MHz
Plate Voltage	9.0	9.0	kVdc
Screen Voltage	800	800	Vdc
Grid Voltage	-400	-300	Vdc
Plate Current	4.08	4.15	Adc
Screen Current	200	200	mAdc
Grid Current	40	38	mAdc
Drive Power	325	360	W
Useful Power Output ¹	28.75	28.9	kW
Efficiency	80.5	77.4	%
Gain	19.5	19.0	dB
1. Double and the step is a set			

¹ Delivered to the load

PLATE MODULATED RADIO FREQUENCY POWER AMPLIFIER 8990A RECOMMENDED

GRID DRIVEN Class C Telephony (Carrier Conditions)

ABSOLUTE MAXIMUM RATINGS

DC PLATE VOLTAGE	8,000	VOLTS
DC SCREEN VOLTAGE	2,000	VOLTS
DC GRID VOLTAGE	-1,000	VOLTS
DC PLATE CURRENT	5	AMPERES
PLATE DISSIPATION	13.5	KILOWATTS
SCREEN DISSIPATION	450	WATTS
GRID DISSIPATION	200	WATTS

AUDIO FREQUENCY POWER AMPLIFIER OR MODULATOR

GRID DRIVEN, Class AB1 (sinusoidal wave)

ABSOLUTE MAXIMUM RATINGS (per tube)

DC PLATE VOLTAGE		VOLTS
DC SCREEN VOLTAGE	2,500	VOLTS
DC PLATE CURRENT	6	AMPERES
PLATE DISSIPATION	20	KILOWATTS
SCREEN DISSIPATION	450	WATTS
GRID DISSIPATION	200	WATTS

TYPICAL OPERATION

Plate Voltage Screen Voltage Grid Voltage	7,800 750 300	Vdc
Peak af screen voltage	750	v
Plate Current	4.6	Adc
Screen Current ¹	220	mAdc
Grid Current ¹	108	mAdc
Calculated Driving Power	35	W
Plate Impedance	845	Ω
Plate Output Power	29	kW
Plate Dissipation	6880	W
¹ Approximate		

TYPICAL OPERATION (2 tubes)

	Plate Voltage	7,800	7,800	7800	Vdc
	Screen Voltage	500	750	1500	Vdc
	Grid Voltage ¹	-70	-125	-250	Vdc
	Zero Signal Plate Current	0.75	0.75	1.0	Adc
	Max. Signal Plate Current	3.4	5.2	9.2	Adc
	Max. Signal Screen Current ²	90	220	600	mAdc
	Peak Grid Voltage ²	65	115	200	v
	Max Signal Plate Dissipation ³	6	7	13.5	kW
	Plate Output Power	14.5	26	44	kW
	Load Impedance p/p	6,300	3,500	1600	Ω
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¹ Adjust for specified zero-signal plate current.

² Approximate value

³ Per tube

8990/4CX20,000A,8990A

TYPICAL OPERATION values are obtained by calculations from published characteristic curves. To obtain the specified plate current at the specified bias, screen, and plate voltages, adjustment of the rf grid voltage is assumed. If this procedure is followed, there will be little variation in output power when the tube is replaced, even though there may be some variation in grid and screen currents. The grid and screen currents which occur when the desired plate current is obtained are incidental and vary from tube to tube. These current variations cause no performance degradation providing the circuit maintains the correct voltage in the presence of the current variations. If grid bias is obtained principally by means of a grid resistor, the resistor must be adjustable to produce the required bias voltage when the correct rf grid voltage is applied.

APPLICATION

MOUNTING – The 8990 must be operated with its axis vertical. The base of the tube may be up or down at the convenience of the circuit designer.

SOCKET & CHIMNEY – The EIMAC air-system socket SK-320 and air chimney SK-326 are designed especially for use with the 8990. The use of the recommended air flow through this socket provides effective forced-air cooling of the base, with air then guided through the anode cooling fins by the air chimney.

COOLING – The maximum temperature rating for the external surfaces of the tube is 250°C, and sufficient forced-air cooling must be used in all applications to keep the temperature of the anode (at the base of the cooling fins) and the temperature of the ceramic/metal seals comfortably below the rated maximum.

The cooling characteristics of the anode are shown in the attached graph, for power levels from 7.5 kW to 20 kW dissipation. The designer is cautioned to keep in mind that is ABSOLUTE data, with pure dc power, with no safety factors added, and the pressure drop figures make no allowance for losses in filters, ducting, and the like.

It is considered good engineering practice to design for a maximum anode core temperature of 225°C, and temperature sensitive paints are available for checking base and seal temperatures before any design is finalized. It is also considered good practice to add a 15% safety factor to the indicated airflow, and allow for variables such as dirty air filters, rf seal heating at VHF, and the fact that the anode coolings fins may not be clean if the tube has been in service for some length of time. Special attention is required in cooling the center of the stem (base), by means of special directors or some other provision. An air interlock system should be incorporated into the design to automatically remove all voltages from the tube in case of even partial failure of the tube cooling air.

Air flow must be applied before or simultaneously with the application of power, including the tube filament, and should normally be maintained for a short period of time after all power is removed to allowed for tube cooldown.

FILAMENT OPERATION – The rated nominal filament voltage for the 8990 is 10.0 volts, as measured at the socket or tube base. Variation in voltage should be maintained within plus or minus five percent. During application of filament voltage the inrush current should be limited to no more than twice normal current.

The peak emission capability at nominal filament voltage is normally more than that required for communication service. A small decrease in filament temperature due to reduction in filament voltage can increase tube life by a substantial percentage. It is good practice to determine the nominal filament voltage for a particular application that will not adversely affect equipment operation. This is done by measuring some important parameter of performance (such as plate current, power output, or distortion) while filament voltage is reduced. At some point in filament voltage there will be a noticeable change in the operating parameter being monitored, and the operating filament voltage must be slightly higher than the level at which deterioration was noted. When filament voltage is to be reduced in this manner it should be regulated and held to plus or minus one percent, and the actual operating value should be checked periodically to maintain proper operation.

ELECTRODE DISSIPATION RATINGS – The maximum dissipation ratings for the 8990 must be respected to avoid damage to the tube. An exception is the plate dissipation which may be permitted to rise above the rated maximum during brief periods (10 seconds maximum) such as may occur during tuning.

GRID OPERATION – The 8990 control grid has a maximum dissipation rating of 200 watts. Precautions should be observed to avoid exceeding this rating. The grid bias and driving power should normally be kept near the values shown in the TYPICAL OPERATION section of the data sheet whenever possible.

SCREEN OPERATION – The power dissipated by the screen of the 8990 must not exceed 450 watts. Screen dissipation, in cases where there is no ac applied to the screen, is the simple product of the screen voltage and the screen current. If the screen voltage is modulated, the screen dissipation will depend upon loading, driving power, and carrier screen voltage.

Screen dissipation is likely to rise to excessive values when the plate voltage, bias voltage, or plate load are removed with the filament and screen voltages applied. Suitable protective means must be provided to limit the screen dissipation to 450 watts in the event of circuit failure. Energy limiting circuitry (which will activate if there is a fault condition) and spark gap over-voltage protection are recommended as good engineering practice.

The 8990 may exhibit reversed (negative) screen current under some operating conditions.

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8990/4CX20,000A,8990A

The screen supply voltage must be maintained constant for any values of negative and positive screen current which may be encountered. Dangerously high plate current may flow if the screen power supply exhibits a rising voltage characteristic with negative screen current. Stabilization may be accomplished with a bleeder resistor connected from screen to cathode, to assure that net screen supply current is always positive. This is absolutely essential if a series electronic regulator is employed.

FAULT PROTECTION – In addition to normal plate overcurrent interlock and screen current interlock it is good practice to protect the tube from internal damage which could result from a plate arc at high voltage. In all cases some protective resistance, 10 to 50 ohms, should be used in series with the tube anode to absorb power supply stored energy in case a tube arc should occur. If power supply stored energy is high some form of electronic crowbar which will discharge power supply capacitors in a few microseconds following indication of start of a tube arc is recommended.

HIGH VOLTAGE – Normal operating voltages used with the 8990 are deadly and the equipment must be designed properly and operating precautions must be followed. All equipment must be designed so that no one can come into contact with high voltages. All equipment must include safety enclosures for high-voltage circuits and terminals, with interlock switches to open primary circuits of the power supply and to discharge high-voltage capacitors whenever access doors are opened. Interlock switches must not be bypassed or "cheated" to allow operation with access doors open. Always remember that HIGH VOLTAGE CAN KILL.

INTERELECTRODE CAPACITANCE - The actual internal interelectrode capacitance of a tube is influenced by many variables in most applications, such as stray capacitance to the chassis, capacitance added by the socket used, stray capacitance between tube terminals, and wiring effects. To control the actual capacitance values within the tube, as the key component involved, the industry and Military Services use a standard test procedure as described in Electronic Industries Association Standard RS-191. This requires the use of specially constructed test fixtures which effectively shield all external tube leads from each other and eliminate any capacitance reading to "ground". The test is performed on a cold tube. Other factors being equal, controlling internal tube capacitance in this way normally assures good interchangeability of tubes over a period of time, even when the tube may be made by different manufacturers. The capacitance values shown in the manufacturer's technical data, or test specifications, normally are taken in accordance with Standard RS-191.

The equipment designer is therefore cautioned to make allowance for the actual capacitance values which will exist in any normal application. Measurements should be taken with the socket and mounting which represent approximate final layout if capacitance values are highly significant in the design.

SPECIAL APPLICATIONS – If it is desired to operate this tube under conditions widely different from those listed here, write to Application Engineering, Power Grid Tube Division, EIMAC Division of Varian, 301 Industrial Way, San Carlos, CA 94070 for recommendations.

OPERATING HAZARDS

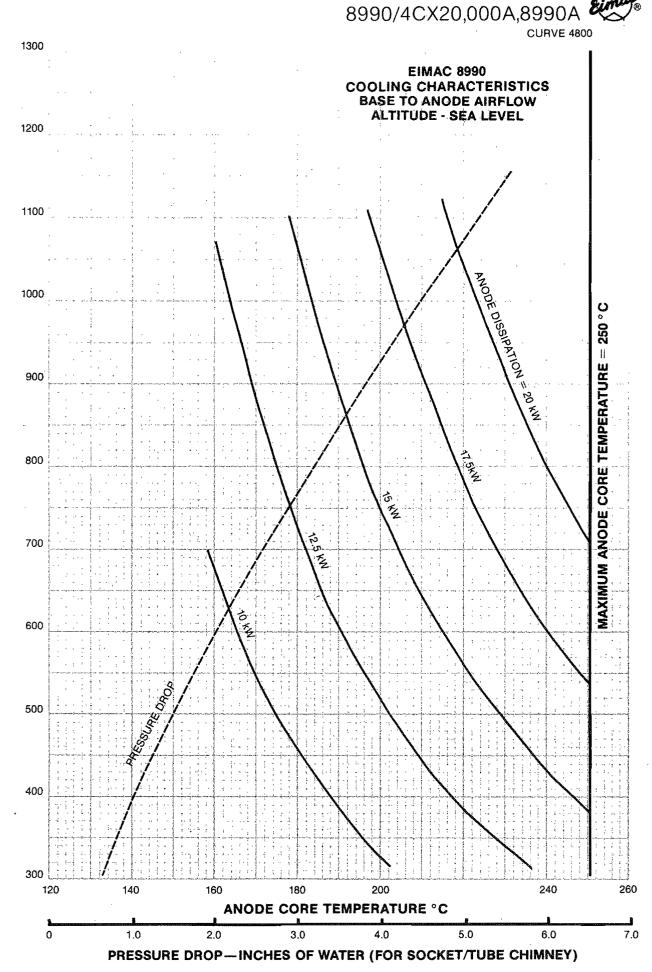
PROPER USE AND SAFE OPERATING PRAC-TICES WITH RESPECT TO POWER TUBES ARE THE RESPONSIBILITY OF EQUIPMENT MANUFAC-TURERS AND USERS OF SUCH TUBES. ALL PERSONS WHO WORK WITH OR ARE EXPOSED TO POWER TUBES OR EQUIPMENT WHICH UTI-LIZES SUCH TUBES MUST TAKE PRECAUTIONS TO PROTECT THEMSELVES AGAINST POSSIBLE SERIOUS BODILY INJURY. DO NOT BE CARE-LESS AROUND SUCH PRODUCTS.

The operation of power tubes involves one or more of the following hazards, any one of which, in the absence of safe operating practices and precautions, could result in serious harm to personnel:

- a. HIGH VOLTAGE Normal operating voltages can be deadly.
- b. RF RADIATION Exposure to strong rf fields should be avoided, even at relatively low frequencies. The dangers of rf radiation are more severe at UHF and microwave frequencies and can cause serious bodily and eye injuries. CARDIAC PACEMAKERS MAY BE AFFECTED.

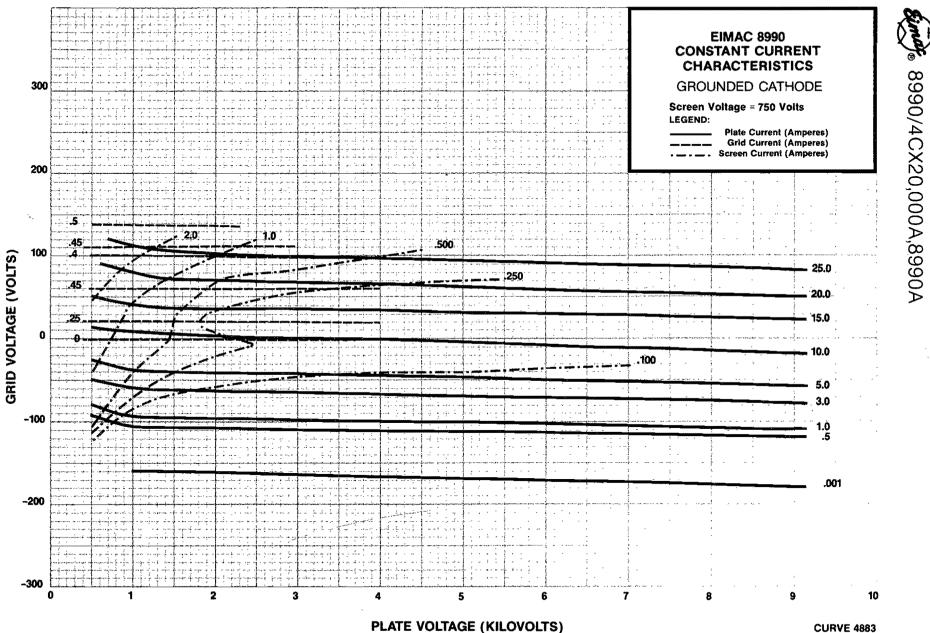
- c. X-RAY RADIATION High voltage tubes can produce dangerous and possibly fatal x-rays.
- d. BERYLLIUM OXIDE POISONING Dust or fumes from BeO ceramics used as thermal links with some conduction-cooled power tubes are highly toxic and can cause serious injury or death.
- GLASS EXPLOSION Many electron tubes have glass envelopes. Breaking the glass can cause an implosion, which will result in an explosive scattering of glass particles. Handle glass tubes carefully.
- f. HOT WATER Water used to cool tubes may reach scalding temperatures. Touching or rupture of the cooling system can cause serious burns.
- g. HOT SURFACES Surfaces of air-cooled radiators and other parts of tubes can reach temperatures of several hundred degrees centigrade and cause serious burns if touched.

Please review the detailed operating hazards sheet enclosed with each tube or request a copy from the address shown below: Power Grid Tube Division, Varian, EIMAC division, 301 Industrial Way, San Carlos, California 94070.



AIRFLOW - CUBIC FEET PER MINUTES

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CURVE 4883

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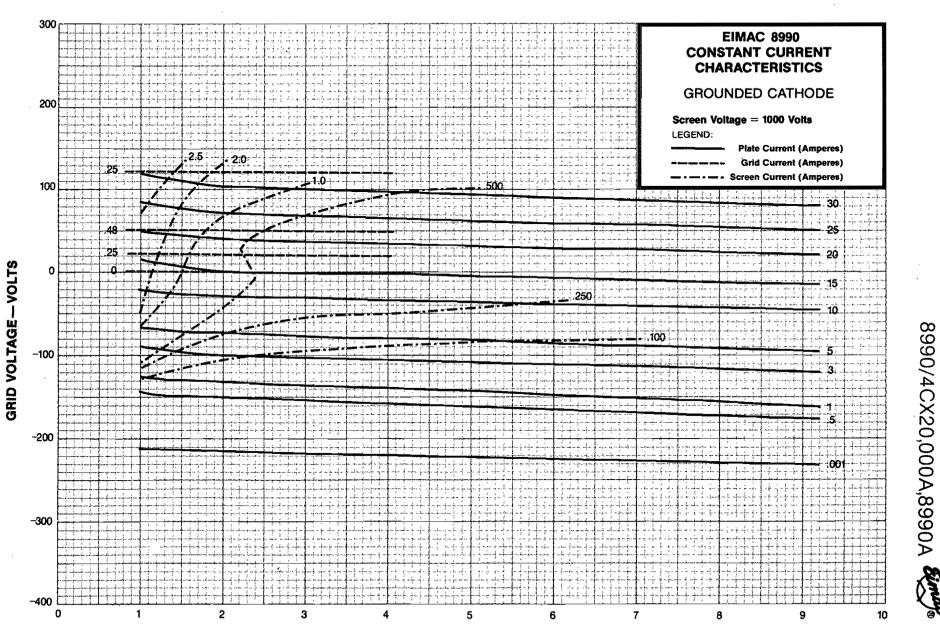


PLATE VOLTAGE-KILOVOLTS

CURVE 4884

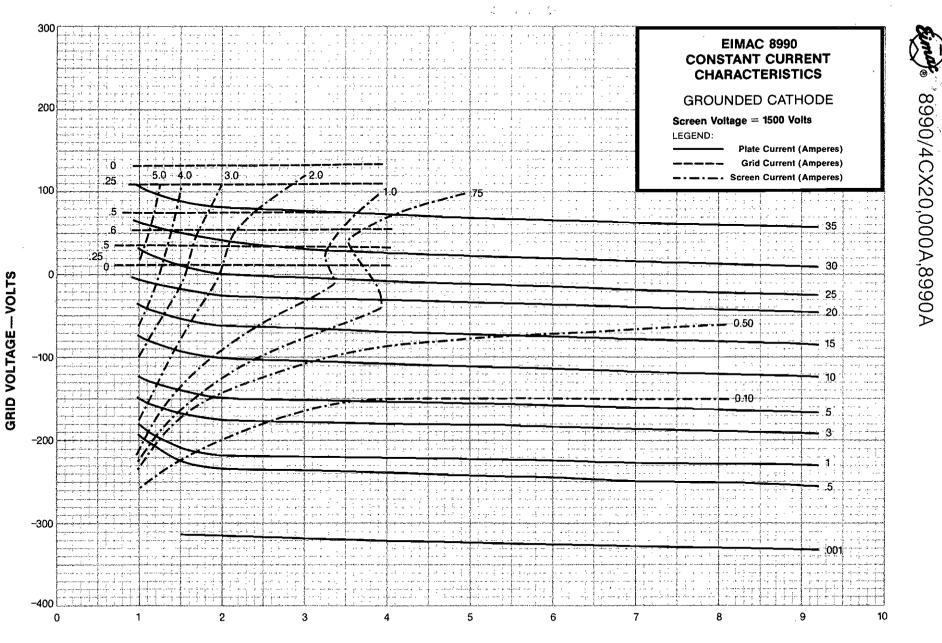
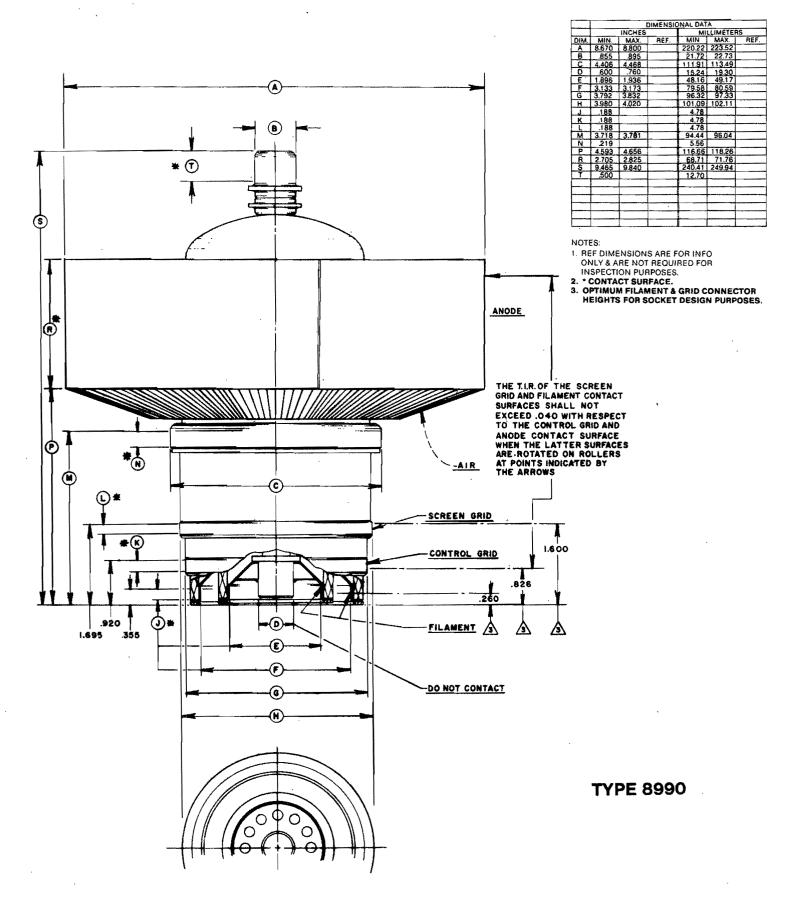


PLATE VOLTAGE-KILOVOLTS

CURVE 4886

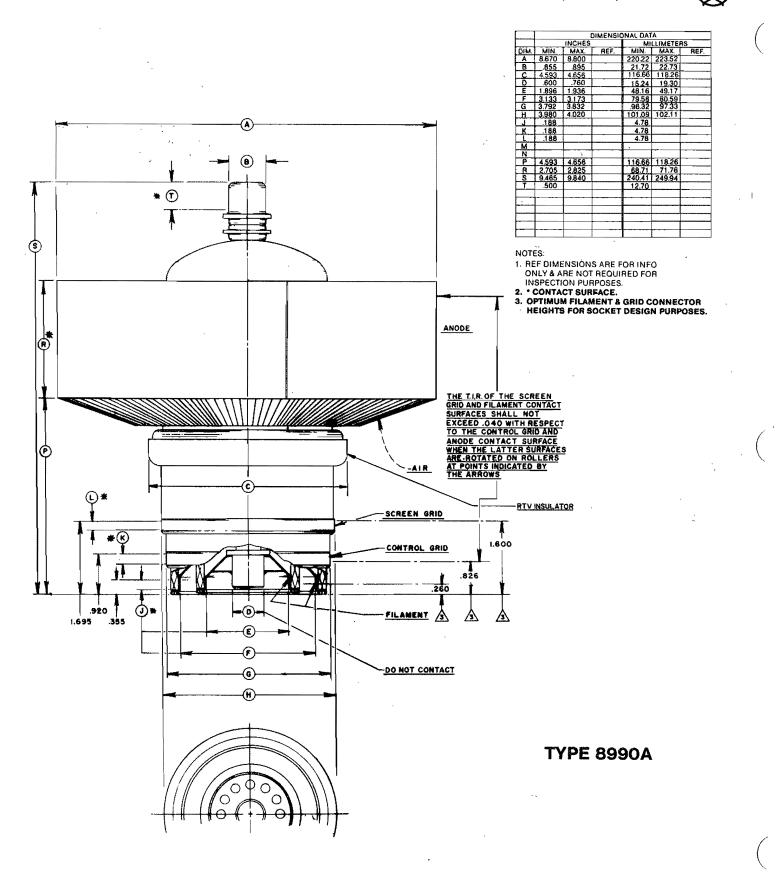
8990/4CX20,000A,8990A





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8990/4CX20,000A,8990A



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LIFE VS. FILAMENT VOLTAGE

TUBE TYPES WITH THORIATED-TUNGSTEN FILAMENTS OR CATHODES.

Power tube users and equipment manufacturers are naturally interested in extending the life of these tubes. A very large factor in tube life is the temperature of the thoriated-tungsten cathode.

engineering newsletter

The equipment manufacturer and the end user of the equipment have more control over tube life through proper adjustment of filament voltage (filament power) than is generally realized. This is true because tube ratings and most equipment designs are conservative in peak cathode emission required of the tube compared with peak cathode emission available at nominal rated filament voltage.

It is good practice to determine in the field for each particular combination of equipment and operating power level, the nominal filament voltage for best life. This is best done in the field by measuring some important parameter of performance such as plate current, power output, or distortion while filament voltage on the power tube is reduced. At some point in filament voltage there will be a noticeable reduction in plate current, or power output, or an increase in distortion. Operation may safely be at a filament voltage slightly higher than that point at which performance appeared to deteriorate. A recheck should be made in 12 to 24 hours to make certain that emission is stable.

The thoriated-tungsten filament or cathode is processed in a hydrocarbon atmosphere to form a deep layer of di-tungsten carbide on the surface. Stable emission is not possible without the carbide. If the carbide layer is too deep the filament becomes too brittle to withstand shipping and handling. The end of useful life for this type of filament occurs when most of the carbon has evaporated or combined with residual gas, depleting the carbide surface layer.

Theoretically it is estimated that a 3% increase in filament voltage will result in a 20°K increase in temperature, a 20% increase in peak emission, and a 50% decrease in life due to carbon loss. This, of course, works the other way, too. For a small decrease in temperature and peak emission, life of the carbide layer and hence tube life can be increased by a substantial percentage. Peak emission as meant here is the emission obtained in the test for emission described in the Test Specification. This is normally many times the peak emission required in communication service.

Continued.....

an application engineering service - eimac, division of varian

Obviously, if small percentage variations in filament voltage are to have a large percentage effect on tube life, it is important to be able to measure and adjust filament voltage measured at the tube terminals with accuracy of about 1%.

The common rectifier type of multimeter which is used for almost every measurement in electronic gear, should not be relied on for AC filament voltage measurement. A simple iron-vane AC meter which has recently been checked against a reliable standard is the best inexpensive instrument for this measurement because it responds to the RMS, or heating value, of the voltage wave form.

As a guide for use with most communications, and broadcast equipment, to get the best life service from your EIMAC power tubes, the following table has been prepared. It is not meant to imply that lower filament voltage will not be satisfactory in some instances.

SUGGESTED NOMINAL FILAMENT VOLTAGE

FOR

EXTENDED LIFE IN BROADCAST AND COMMUNICATION SERVICE

TUBE TYPE

3X2500A3 and F3 3X3000A1 and A7 3CX2500A3 and F3 3CX3000A1 and A7 3CX10,000A3, A1 and A7 3CX15,000A3 6697A 4-125A 4-400A 4-1000A 4w20,000A 4w20,000A 4CX3000A 4CX3000A 4CX10,000D 4CX15,000A 4CX15,000A 4CX15,000A 4CX15,000A 4CX15,000A 4CX35,000C 4E27A 5-500A	7.2 volts 7.2 7.2 7.2 7.2 6.0 12.3 4.8 4.8 7.2 (2300 watts cathode heating power) 8.6 volts 7.2 7.2 7.2 6.0 9.0 9.0 4.8 9.5 (200)
5-500A 5CX1500A	9.5 4.8
5CX3000A	8.6

Credit is due the paper, High Power Transmitting Valves ---, by Walker, Aldous, Roach, Webb and Goodchild, IEE Paper No. 3200E March, 1960, also the paper Life Expectancy Tubes ---, Eitel-McCullough, October 6, 1963, by Paul Williams.

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MICROPROCESSOR CONTROL CIRCUIT

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3

SECTION I

MICROPROCESSOR CONTROLLER THEORY OF OPERATION

1–1. INTRODUCTION

1-2. The following text provides theory of operation with supporting diagrams for the FM-30 transmitter microprocessor controller.

1-3. FUNCTIONAL DESCRIPTION

1-4. Two levels of discussion are provided. A general discussion of microprocessor controller principles at block diagram level is followed by a detailed discussion of circuit operation for each circuit board.

1-5. GENERAL DESCRIPTION

1-6. All status functions and most control functions in the FM-30 transmitter are implemented through use of a microprocessor controller that monitors transmitter operation (see Figure 1-1). Using information collected throughout the transmitter, the microprocessor controller will determine what control actions are required. Some control actions such as timed functions, overloads, or interlocks will be accomplished without delay by the controller. Information concerning faults, overloads, or a power outage will be stored by a non-volatile memory for analysis after the problem has occurred to aid in problem resolution.

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1-7. In the case of out-of-tolerance status samples, the controller will advise the operator of the status of each sample according to a preset priority. The controller provides 123 status indications on a twosegment digital readout, four LED indicators, and three incandescent lights for diagnostic purposes.

1-8. The transmitter control logic will interface with most modern remote control devices and ATS units. Two parallel four bit binary coded decimal outputs from the microprocessor controller allow remote indications of the two transmitter status display digits.

1-9. OPERATION. The microprocessor controller is implemented using a Motorola MC14500B Industrial Control Unit integrated circuit. Throughout the following discussions, this integrated circuit will be referred to as "the processor".

1-10. A system reset generated at power application starts the program counter incrementing from zero. Once started, this program loops continuously. At the maximum count, the program counter "rolls over" to zero and continues incrementing. Processor instructions and I/O addresses are stored in a programmable read only memory addressed by the program counter. Interlaced clock is used to differentiate between these instructions and the I/O addresses as the system scans through the read only memory. Data from the various input and output locations is carried to and from the processor by a single one-bit bidirectional data bus.

1-1

1-11. Eight bit addressable latches with tri-state data ports are used on each circuit board to prevent loading of the data bus. Unless a specific chip is addressed, all data bus connections exhibit a high impedance. Whenever a chip is addressed, the chip output can be HIGH or LOW, depending upon the inputs to the chip.

1-12. Commands such as "filament on" and "high voltage on" are initiated by a momentary ground applied to the control/timer board input circuitry. When the switches are depressed, the associated switch/indicators will illuminate to indicate that the selected commands have been received and stored.

1-13. As directed by the program, the processor will address each addressable chip on each circuit board to determine all status inputs. When the processor addresses the correct chip on the control/timer board, the "filament on command" will be output over the data bus to the processor board. The "filament on command" is assigned a higher priority than the "high voltage on command" by the program and will therefore be output first.

1-14. The processor board will momentarily raise the write line, address the output board, and output an instruction on the data bus to apply drive to the blower control relay. The associated BLOWER indicator on the primary function indicator board will illuminate to indicate that a "blower on command" has been output from the microprocessor controller.

1-15. After the PA air switch closes, this information will be applied as a status input to input board 1. When the processor addresses the correct chip on input board 1, the "air switch closed" information will be output to the processor over the data bus.

1-16. After the "air switch closed" information has been received by the processor, the processor board will momentarily raise the write bus, address the output board, and output a command on the data bus to apply drive to the filament control relay. The associated FILAMENT indicator on the primary function indicator board will illuminate to indicate that a "filament on command" has been output from the microprocessor controller. At the same time, the processor will initiate a filament timing sequence by addressing the correct circuitry on the control/timer board.

1-17. After the filament heating delay has expired, the processor board will accept the "high voltage on command" from the control/timer board via the data bus. If no overloads exist, all interlocks remain closed, the air switch remains closed, and the FM exciter is operational, the processor board will momentarily raise the write bus, address the output board, and output commands on the data bus to apply drive to the high voltage step-start circuitry and remove the mute from the FM exciter. The associated HIGH VOLTAGE indicator on the primary function indicator board will illuminate to indicate that a "high voltage command" has been output from the microprocessor controller.

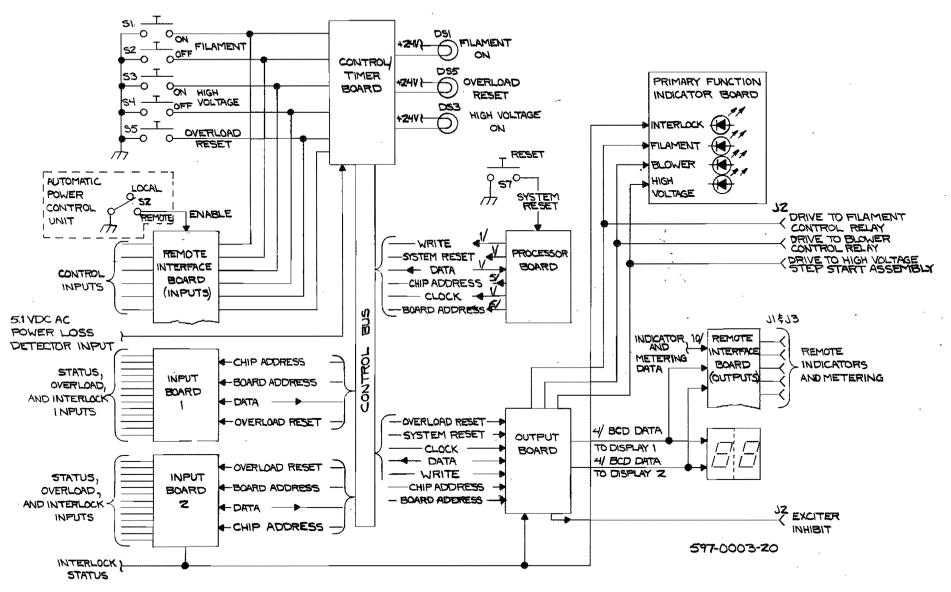


FIGURE 1-1. MICROPROCESSOR CONTROLLER BLOCK DIAGRAM



1-3

1-18. If the FILAMENT OFF switch is depressed, a momentary ground applied to the control/timer board input circuitry will initiate a control sequence similar to the preceeding examples. The processor will receive the command via the data bus, deenergize the high voltage and filament supplies, and start a filament cool-down interval timer on the control/ timer board. When the timed interval expires, the processor will command the output board to deenergize the blower.

1-19. <u>Remote Control</u>. Remote interface is accomplished by circuitry on the remote interface board. The remote control inputs are enabled by a ground applied to the remote interface board by the LOCAL/REMOTE switch. However, outputs to the remote indicators and metering are active at all times. When a high is input to the interface, a ground is output to simulate the transmitter switch-selectable commands. A "one button start" provision is incorporated as a remote control feature.

1-20. Interlocks. Interlocks and overloads are treated to the same priority. If an interlock opens, the transmitter will deenergize immediately. The INTERLOCK indicator on the primary function indicator board will go out to indicate an open interlock. The transmitter must then be manually restored to operation with a new start sequence initiated by depressing the FILAMENT ON and HIGH VOLTAGE ON switch/indicators.

1-21. <u>Overloads</u>. If an overload occurs, this information will be output to the processor board via the data bus when the proper chip is addressed. The processor board will then enable the write bus, initiate two timed intervals on the control/timer board, and illuminate the OVERLOAD indicator. One timer monitors the number of times an overload occurs during a timed interval and the second timer delays restoration of the equipment to operation to allow the condition that produced the overload to dissipate.

1-22. When the timed interval delaying restoration of the equipment has expired, the processor will recycle the equipment back into operation. If no further overloads occur during the recycle timed interval, the recycle timer interval will expire to await another overload. If two overloads occur during the period of the recycle interval timer, the equipment will deenergize and must be manually reset. This can be done from the front panel OVERLOAD reset switch or from remote control, if enabled by the LOCAL/REMOTE switch.

1-23. The manual overload reset sequence after overload lock-out is initiated by a ground applied to the control/timer board input circuitry. The OVERLOAD indicator will go out to indicate that the overload reset command has been received and stored. When the processor addresses the correct chip on the control/timer board, the overload reset command will be output over the data bus to the processor board. The processor will momentarily raise the write bus, address the output board, and output a command on the data bus to generate an overload reset pulse. The overload reset pulse is simultaneously applied to both input boards to reset the overload latches.

1-24. DETAILED DESCRIPTION

1-25. INPUT BOARDS. All status information to the microprocessor controller is input through input boards 1 and 2 (see Figures 1-2 and 1-3). The first nine inputs to each board provide the controller with diagnostic information. These inputs are priority encoded with hardware before they are scanned by the processor. The remaining four inputs are used to signal critical parameters out-of-tolerance which will result in immediate transmitter shut-down.

1-26. All inputs are isolated through series resistors and amplitude protected by shunt zener diodes. The zener diodes are returned to ground through a bus which is slightly positive. This limits negative over voltage excursions so that the forward biased zener voltage drop is compensated by the positive return bus voltage which results in zero voltage at the level detector input.

1-27. Each input has resistive strapping options to divide the input down to a nominal level. Negative polarity inputs are connected to the end of a positive polarity voltage divider to convert the signal into a positive sample. A reference voltage divider establishes the comparison level for each level detector, which outputs a binary state according to the comparison of its inputs. The level detector may be followed by an inverter, depending upon the normal state of the input signal.

1-28. Some inputs have adjustments which depend upon the transmitter operating power level and therefore contain potentiometers in the reference voltage dividers. These more critical adjustments are preset at the factory during actual operation and should not be readjusted in the field unless absolutely necessary.

1-29. Overloads and interlocks are processed by the input circuitry identical to the diagnostic inputs. However, the outputs from the overload level detectors are applied to bistable flip-flops which function as storage devices. These flip-flops can only be reset by a +5 volt pulse from the output board which is generated by the processor responding to the OVERLOAD reset switch.

1-30. Diagnostic information from each level detector is applied to a priority encoder which reduces the information to a single BCD word for the highest priority input which as an abnormal level. This code is applied to an eight channel data selector. Outputs from the overload and interlock circuits are applied directly to the same eight-channel data selector. These inputs share equal priority in the controller.

1-31. As a matter of routine, the controller will address each input board through a three-input NAND gate. After a board has been addressed, activity on the chip input select lines will determine what information will be output on the bidirectional data line to the processor board. All information is output in serial binary form. Whenever an input board is not addressed, the respective eight-channel data selector remains disconnected from the data bus.

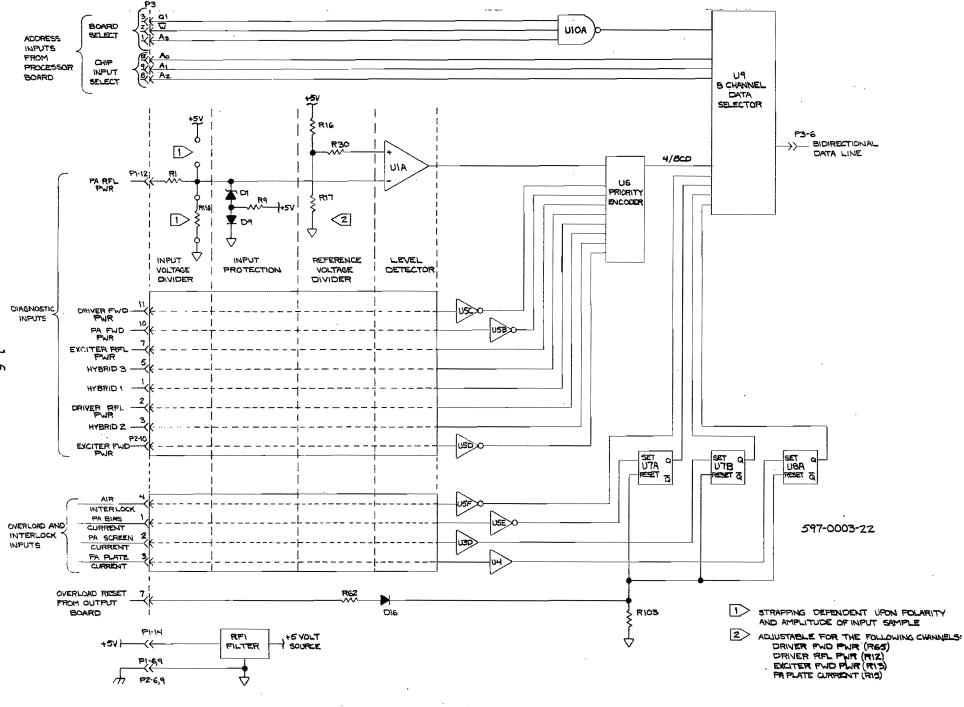


FIGURE 1-2. INPUT BOARD 1 SIMPLIFIED SCHEMATIC

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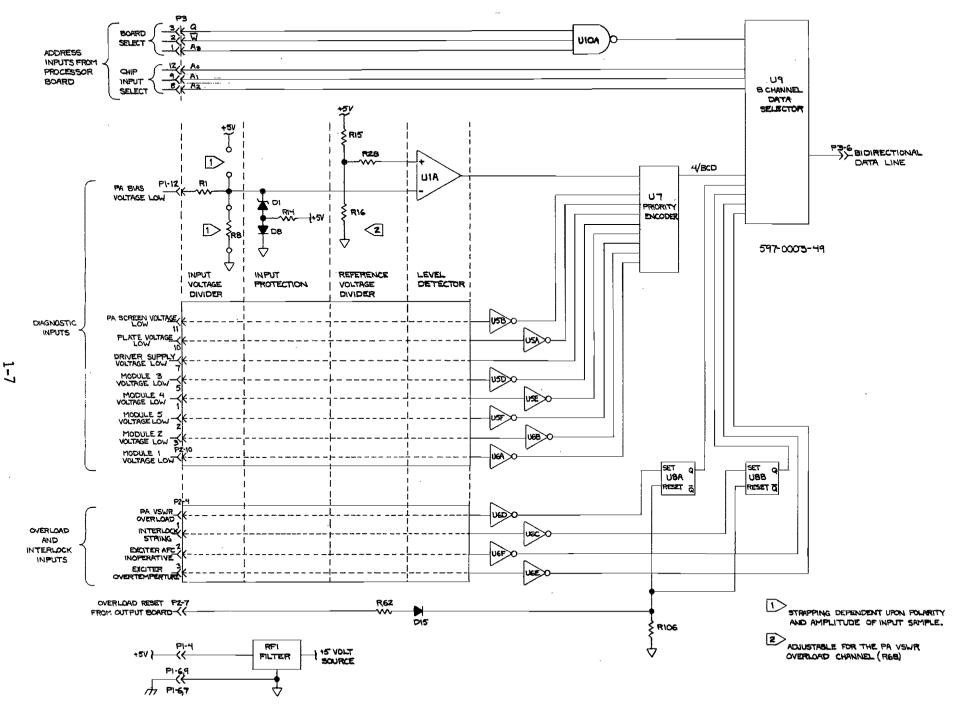


FIGURE 1-3. INPUT BOARD 2 SIMPLIFIED SCHEMATIC

1-32. CONTROL/TIMER BOARD. The control/timer board interfaces control commands and provides turn-on, turn-off, time-up and time-down functions to operate the transmitter. One status input allows the processor to monitor the 230 volt ac power status (+5.1V dc sample) and one status input allows the processor to check the contents of the processor result register (RR) (see Figure 1-4). This is a temporary storage register for one-bit data.

1-33. The input latches store contact closures for commands. When the FILAMENT ON and HIGH VOLTAGE ON switches are depressed, grounds applied to U7 A/B and U8 A/B will force each latch to the HIGH state. Line driver U9 will illuminate the FILAMENT ON and HIGH VOLTAGE ON indicators to signify that the commands have been received and stored. Resistors R20, R21, and R22 allow the lamp bulbs to draw standby current to keep the filaments warm and thereby reduce inrush current when illuminated, prolonging lamp life. An RC circuit connected to the input of each latch provides noise immunity.

1-34. The transmitter can be controlled by positive dc inputs to the remote interface board. Inverters on the remote interface board provide a ground output to simulate the switch selectable commands. Additionally, a one-button start provision is available as a remote control feature by diodes connected to the FILAMENT ON and HIGH VOLTAGE ON switches.

1-35. As directed by the program, the processor will address the control/timer board. When the processor addresses eight-channel data selector U5, the "filament on command" will be output over the data bus to the processor board. The "filament on command" is assigned a higher priority than the "high voltage on command" by the program and will therefore be output first.

1-36. First a "blower on" control action will be initiated and when complete, the "filament on" sequence will be initiated. The processor will again address the control/timer board, address latch U4, raise the write enable bus, and output a command on the bidirectional data bus to initiate a "filament on" timing sequence by timer U1 via U6F.

1-37. After a filament heating delay has expired and this information has been received by the processor, the processor will accept the "high voltage on command". If all parameters are within tolerance, the processor will complete the "high voltage on" sequence and the transmitter will be operational.

1-38. When the FILAMENT OFF switch is depressed, a momentary ground applied to the control/timer board will reset latch U7 A/B. The FILAMENT ON indicator will extinguish to signify that the "filament off command" has been received and stored. The processor will receive the "filament off command" via the data bus and deenergize high voltage. The controller will address the control/timer board, raise the write bus, address latch U4 via the data bus, and reset the "high voltage on" latch (U8 A/B) and deenergize the HIGH VOLTAGE ON indicator via U6B. Instructions will also initiate a "blower off" timing sequence by U1 via U6F. When the timed interval expires, the processor will output a command to open the blower relay and the transmitter will be deenergized.

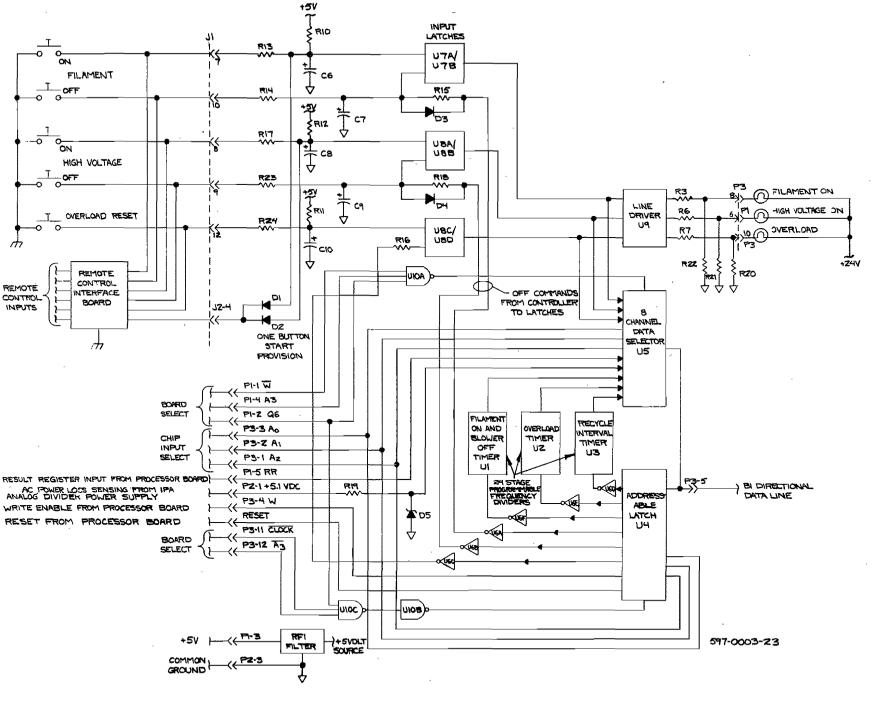


FIGURE 1-4. CONTROL/TIMER BOARD SIMPLIFIED SCHEMATIC DIAGRAM

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1-39. After an overload has occured and the overload information has been received by the processor, the processor will address the control/ timer board, raise the write bus, address latch U4, and output commands via the data bus to simultaneously start timers U2 via U6E and timer U3 via U6D. Additional instructions will set latch U8 C/D by way of U6C to illuminate the OVERLOAD indicator.

1-40. Timer U2 determines the length of time the transmitter remains off-the-air after an overload to allow the conditions that prompted the overload to dissipate. Timer U3 determines the time interval between overload recycle attempts.

1-41. When the interval timed by U2 expires, the processor will cycle the high voltage relay back into operation. If no further overloads occur during the timing cycle of U3, the interval timed by U3 will expire to await another overload. If two overloads occur during the timing cycle of U3, the transmitter will deenergize and must be manually reset.

1-42. The overload reset sequence is initiated by a ground applied to the control/timer board input circuitry that resets latch U8 C/D. The OVERLOAD indicator will go out to indicate that the overload reset command has been received and stored. The "reset" command will be output to the processor via the data bus to initiate a reset pulse sequence. The processor will then output an overload reset pulse from the output board to reset the overload latches on the input boards.

1-43. PROCESSOR BOARD. The entire transmitter system is synchronized and controlled by logic circuitry along with the program stored on the processor board (see Figure 1-5). The program begins cycling when power is applied to the processor and a reset is initiated by R2 and C3 or manually with switch S7. Control actions will begin only when a command such as "filament on" is received by the processor as it scans the inputs on the control/timer board.

1-44. <u>Processor Chip</u>. The MC14500B Industrial Control Unit is the microprocessor integrated circuit used in the FM-30 system. The chip controls the flow of data between its internal register and the one-bit bidirectional data bus, performs logical operations between data in its result register and data on the one-bit bidirectional data bus, and controls all system components with the write line, reset line, and the clock line (which assures synchronized system operation). The system clock is generated internally to the processor chip. The clock frequency is determined by the value of R4 and is approximately 55 kHz ± 15 kHz.

1-45. The MC14500B operates synchronously with single phase clock which divides the processor machine cycle into two phases. The first phase (CLOCK HIGH) is the "fetch" phase when the processor fetches an instruction from memory. When the clock signal falls low, the instruction is latched into the processor's instruction register. During the second phase (CLOCK LOW) the instruction is executed.

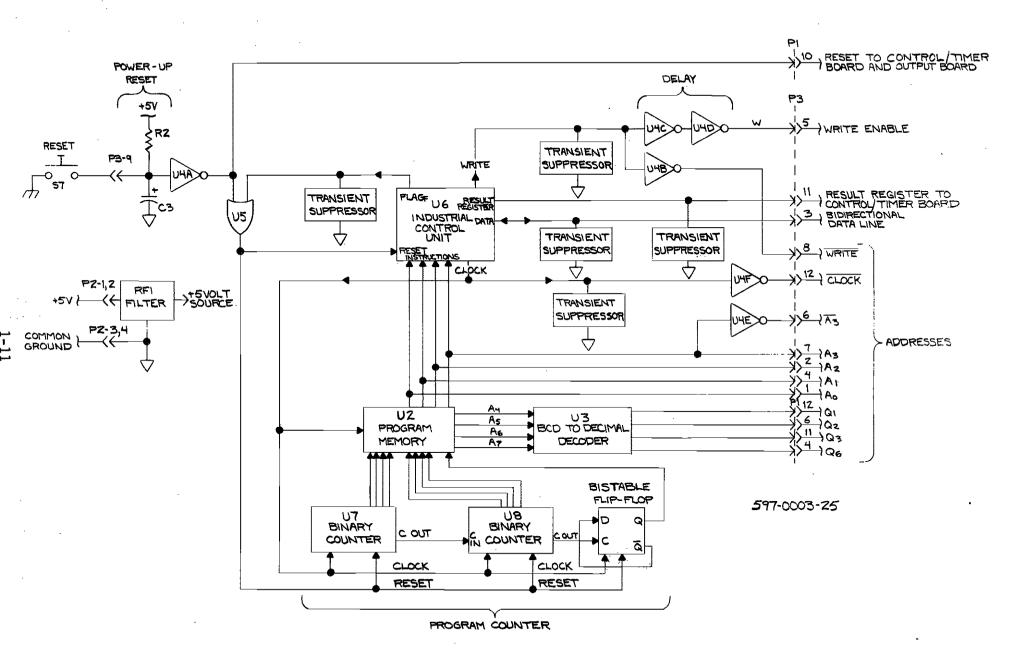


FIGURE 1-5. PROCESSOR SIMPLIFIED SCHEMATIC DIAGRAM



1-46. Three types of I/O related instructions are used: logical, input, and output. During the execution phase of input or logical instructions, the operand of the instruction is demultiplexed onto the processor's data bus by the input data selectors. The memory supplies the input selectors with the address of the bit to be used in the operation. During the execution phase of an output instruction, the processor puts the data (or the data complement) in the result register on its data bus and raises the write control line. The data bit is then multiplexed to an output line where the data is read into an output latch on the rising edge of the clock signal. The memory supplies the address of the output latch to which the data is to be routed.

1-47. <u>Program Memory</u>. The processor chip data output is wired to the one-bit bidirectional data bus. To prevent loading of this bus, tri-state logic is used on all circuit boards connected to this bus. Unless a specific chip on a board is addressed, all data connections to the bus exhibit a high impedance. When a chip is addressed, the chip output can be high or low, depending upon the inputs to the chip.

1-48. The controller program is contained in programmable read-only memory U2 which is factory programmed. The program consists of 4-bit processor instruction codes interlaced with 8-bit I/O addresses. The low order bits contain the instruction codes and are output from the program memory when the clock is high (the clock forms the least significant bit of the memory address). When the clock is low, the program memory sends out four high order bits, which are further decoded to generate board address signals by U3, and four low order bits which are routed directly to all input selectors and output latches in the system. These signals (called chip selects) are decoded by each data selector or addressable latch to select the appropriate input or output line to be connected to the bidirectional data bus.

1-49. <u>Program Counter</u>. The 8-bit program counter formed by U7 and U8 supplies the processor system memory with the address of the command to be executed. Stepped by clock obtained from the processor chip, the counter counts up sequentially in binary to its highest value. After an entire program has cycled, U6 will output a FLAGF pulse that resets the program counter and the processor chip to initiate a new program cycle. This is a looping control structure.

1-50. OUTPUT BOARD. Controller actions are interfaced with all external devices through the output board. Discrete drivers on the output board drive solid-state relays which control operation of the transmitter contactors. The board also mutes the exciter whenever the transmitter is not fully operational, provides a +5 volt pulse to reset the overload circuitry on the input boards in response to a command input from the processor, and supplies information to operate the transmitter front-panel digital display (see Figure 1-6).

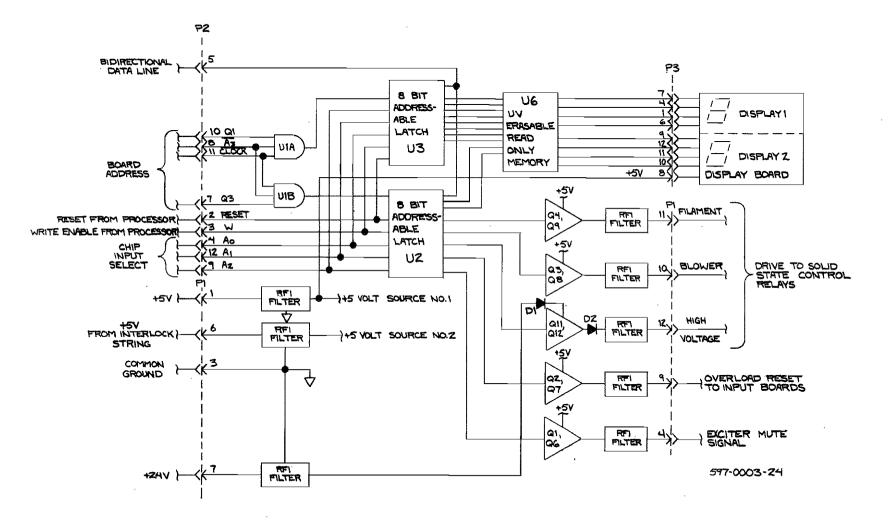


FIGURE 1-6. OUTPUT BOARD SIMPLIFIED SCHEMATIC DIAGRAM

1-51. After a command sequence such as "filament on" is initiated, the processor will address the output board as directed by the program. The first interface action required in the "filament on" sequence is the "blower on" action. After the board has been addressed, the processor will address U2, raise the write bus, and output a command on the data bus to switch Q8 via Q3 to output a +5 volt pulse to activate the blower control relay. The remaining interface provisions function in the same manner in sequence as directed by the program. The high voltage driver operates at +18 volts to provide noise immunity for the control line to the step start assembly in the high voltage power supply cabinet.

1-52. The two digit numeric display provides three types of information.

- A. During turn on or turn off sequences, it displays a single digit control status code. This code changes to indicate each step in the sequence.
- B. PA current overloads and output reflected power overloads will cause a two digit code to be displayed along with illumination of the yellow OVERLOAD indicator. Up to four overloads can be displayed simultaneously.
- C. Minor faults which are not serious enough to warrant shutdown are displayed with a two digit code. Two faults can be displayed simultaneously. The priority system is structured so that a fault can be diagnosed to the lowest component or subsystem.

1-53. When information displayed is to be changed, the processor will address the output board, address U3, raise the write bus, and output a command on the data bus containing information to be displayed. Factory programmed read only memory U4 is programmed with a table to convert information bits from U3 into BCD to drive the decoders in the transmitter front panel display.

1-54. If an overload occurs, the display will change to indicate the overload. This information will be retained by the indicator until the overload sensing circuitry on the input boards is reset by depressing the OVERLOAD switch/indicator. If a safety interlock is opened, the display will indicate the open interlock information until the interlock is closed.

1-55. Safety interlocks have the highest priority in the transmitter controller system. Overloads have a secondary priority followed by the remaining parameters. The display will change from a lower priority display to indicate a higher priority parameter, but will not switch between parameters sharing the same priority.

1-56. REMOTE CONTROL INTERFACE BOARD. The FM-30 remote control interface permits remote control of transmitter basic control functions and allows remote indications of critical displays when associated with the correct extended control panel or remote control unit (see Figure 1-7). The amplifiers on the remote control interface board are intended as signal buffers to prevent external devices from interferring with local transmitter operation and should not be considered as line amplifiers. All circuits may be accessed on the remote interface terminal strips in the driver cabinet (TB8 and TB9).

1-57. <u>Display Drivers</u>. Drive obtained from the output board is applied to buffers which provide isolation to operate a remote digital display. Each buffer output TTL levels. The remote display outputs are enabled whenever the transmitter front panel display is operational.

1-58. <u>Remote Metering</u>. Plate current, Plate voltage, and PA forward power are available as remote metering outputs from the FM-30. All three outputs are active whenever the transmitter is operational.

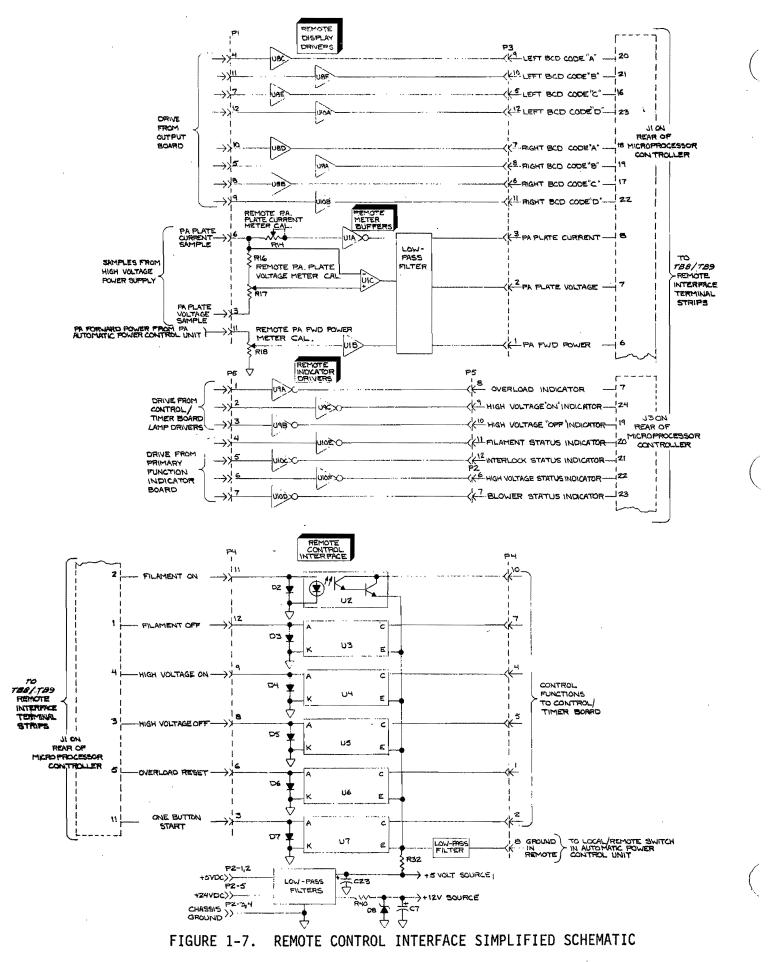
A. Plate current is sampled across the negative return resistor in the high voltage power supply. U1A is configured as an inverting amplifier to provide +5 volts at nominal plate current. R14 adjusts the sample level to U1A.

B. Plate voltage is sampled across the low voltage end of the bleeder resistor chain in the high voltage power supply. This resistor is not connected to ground, but to the negative return resistor. Therefore a differential amplifier (U1C) is used to negate common mode voltage from the plate current sample. R17 adjusts the sample level to U1C.

C. PA forward power is derived from the rectifier and buffer amplifier in the automatic power control unit and is buffered by U1B. The level is adjusted by R18.

1-59. <u>Remote Indicators</u>. Signals representative of the three transmitter front panel incandescent indicators and the four LED indicators are applied to buffers and available as +5 volt outputs on the remote interface terminal strips. These indicators are enabled whenever the associated transmitter front panel indicators are illuminated.

1-60. <u>Remote Control</u>. Remote control of the five basic transmitter control functions is provided by optical isolators. A one button start feature is provided as a remote provision. A low voltage positive dc input to each photo diode will enable the associated photo darlington transistor to simulate one of the basic switch selectable commands. Remote control is enabled by a ground from the REMOTE/LOCAL switch in the automatic power control unit. Removing the ground connection "floats" the darlington transistor emitters in the optical couplers which prevents their collectors from pulling down the command lines.



¹⁻¹⁶

1-61. MICROPROCESSOR CONTROLLER BYPASS ASSEMBLY

1-62. The microprocessor controller bypass assembly is a maintenance tool which allows basic control of the transmitter in event of a microprocessor controller failure. The assembly is interfaced to inline receptacle J2 which connects to plug P2 attached to the transmitter wiring harness. The microprocessor controller may then be removed from maintenance. No timed intervals, remote features, or automatic power control features are provided, only on/off functions and PA stage overloads (see Figure 1-8).

1-63. The bypass assembly is powered by a five volt input from the safety interlock circuit. Presence of the +5 volt input is signified by illumination of the INT/LCK indicator. If a safety interlock is opened, all power to the bypass assembly will be lost and the transmitter will completely shut down.

1-64. The five volt "blower air switch closed" potential is applied to transistor switch Q1. This potential turns on Q1 which illuminates the BLO indicator and provides drive to the filament control relay to signify that the air flow in the transmitter has reached adequate levels for PA stage operation.

1-65. The basic on and off functions are implemented with NAND gates configured as two bistable flip-flops.

1-66. If the FIL START switch is depressed, a ground applied to the filament control flip-flop causes the output of UIA to go HIGH which illuminates the FILL START indicator and provides drive to the blower control relay through transistor switch Q2.

1-67. If the H.V. START switch is depressed, a ground applied to the high voltage control flip-flop causes the output of U1C to go HIGH. This HIGH will enable the exciter. Additionally, drive from transistor switch Q3 will enable U4 which illuminates the H.V. START indicator and provides drive to the plate control relay.

1-68. If the H.V. STOP switch is depressed, U1C will output a LOW which inhibits exciter operation, turns off the H.V. START indicator, and removes drive from the plate control relay.

1-69. If the FIL STOP switch is depressed, U1A will output a LOW which turns off the FIL START indicator and removes drive from the blower control relay. In this configuration, the HIGH output by U1B is inverted by U3B and applied to U1D assures the plate potential is deenergized.

1-70. PA stage plate current, screen grid current, control grid current, and PA output VSWR are monitored as overloads by four level detectors (U2A through U2D). The threshold of each level detector is preset by a potentiometer to a level relative to the parameter being sensed. The output of each level detector is applied to an inverter and is used to deenergize the plate supply automatically if an overload is sensed. Steering diodes connected to each inverter prevents interaction between overload detectors.

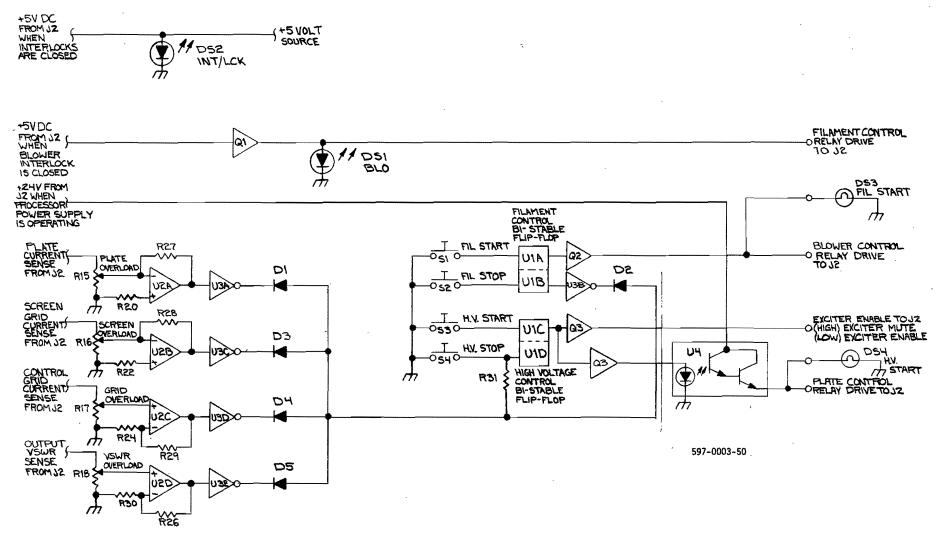


FIGURE 1-8. MICROPROCESSOR CONTROLLER BYPASS ASSEMBLY SIMPLIFIED SCHEMATIC DIAGRAM

1-18

SECTION II

MICROPROCESSOR CONTROLLER MAINTENANCE

2-1. INTRODUCTION

2-2. This section provides maintenance information for the FM-30 FM transmitter microprocessor controller.

2-3. SAFETY CONSIDERATIONS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-4. The FM-30 transmitter contains high voltages and currents which, if regarded carelessly, could be fatal. The transmitter has many built-in safety features. However, good judgement, care, and common sense are the best accident preventives. The maintenance information contained in this section should be performed only by trained and experienced maintenance personnel.

2-5. It is very dangerous to attempt to make measurements or replace components with power energized, therefore such actions are not recommended. The design of the equipment provides safety features such that when a door or access panel is opened, interlock switches will deenergize the plate and screen power supplies. Do not short out or bypass interlock switches as a maintenance short cut.

2-6. The power supply cabinet and the PA cabinet contain switches which discharge the PA plate potential directly to ground whenever either cabinet is opened.

2-7. Grounding sticks are provided as safety features. Each grounding stick consists of a metal rod with a phenolic handle. The metal end is connected to chassis ground. Use a grounding stick to touch every part in the area or circuit on which maintenance is to be performed before attempting maintenance.

2-8. The grounding stick in the high voltage power supply cabinet and the grounding stick in the PA cabinet both rest on hook switches. When either of these grounding sticks is removed, the associated hook switch opens the transmitter interlock string and deenergizes the transmitter PA and screen potentials until each grounding stick is replaced on its respective hook switch.

2–9. MAINTENANCE



ENSURE THE REMOTE/LOCAL SWITCH IS SET TO LOCAL BEFORE ATTEMPTING ANY MAINTENANCE.



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-10. The FM-30 maintenance philosophy consists of preventative maintenance such as cleaning applied to the equipment to forestall future failures and second level maintenance consisting of procedures required to restore the equipment to operation after a fault.

2-11. ADJUSTMENTS



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-12. INPUT BOARD AND MICROPROCESSOR BYPASS ASSEMBLY LEVEL CONTROLS. The input level controls are all preset during factory final test and will not normally require readjustment in the field. Replacement of an associated level detector will not require control readjustment. Adjustment will only be required if a control is replaced or the PA power output level is changed. The microprocessor bypass assembly level controls are adjusted in a manner similar to the procedure stated in Paragraph 2-16 except that the transmitter must be restored to operation by depressing the H.V. START switch/indicator. To adjust the input level controls, proceed as follows.

2-13. <u>Required Equipment</u>. The following equipment is required to complete adjustment of the input board level controls.

A. Insulated adjustment tool, flat screwdriver tip (BE P/N 710-0001).

B. Flat tip screwdriver, 4 inch (10.16 cm) blade and 1/4 inch (0.635 cm) tip.

2-14. <u>Procedure</u>. To adjust the input board level controls, proceed as follows:

2-15. Operate the transmitter within specifications at the rated RF output power into a proper 50 Ohm load in the manual power control mode.

2-16. If a control associated with an overload is to be adjusted, complete the following steps:

A. Refer to Figure 2-1 and locate the control to be adjusted.



THE MAXIMUM POTENTIAL AT ANY POINT WITHIN THE MICROPROCESSOR DRAWER IS 24V DC TO GROUND.

B. Open the microprocessor controller drawer.

CAUTION

ADJUSTMENT OF THE INPUT BOARD OVERLOAD LEVEL CONTROLS DETERMINES AT WHAT POINT THE PROCES-SOR WILL INITIATE ACTION. IF A CONTROL IS INCORRECTLY ADJUSTED, THE PROCESSOR MAY NOT SENSE A FAULT AND DAMAGE TO THE EQUIPMENT MAY RESULT.

C. Adjust the control until the transmitter deenergizes, then back the control off slightly, noting the direction of rotation.

D. Wait approximately three seconds and depress the OVERLOAD RESET and the HIGH VOLTAGE ON switch/indicators.

E. If the equipment does not return to operation, adjust the control a bit more in the direction of rotation noted in step C.

F. Wait approximately three seconds and depress the OVERLOAD RESET and the HIGH VOLTAGE ON switch/indicators.

G. If the equipment does not return to operation, repeat steps E and F until the control is adjusted to the point where the transmitter will just return to operation.

2-17. If a control associated with a diagnostic input is to be adjusted, complete the following steps:

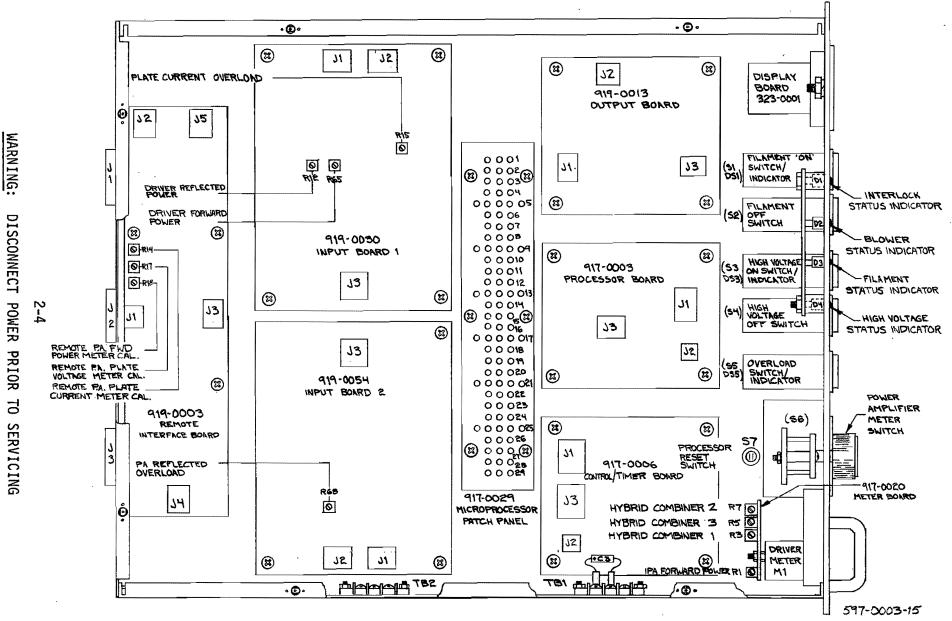


FIGURE 2-1. MICROPROCESSOR_CONTROLLER ASSEMBLY

DISCONNECT POWER PRIOR Ч SERVICING

A. Refer to Figure 2-1 and locate the control to be adjusted.

NOTE

THE MAXIMUM POTENTIAL AT ANY POINT WITHIN THE MICROPROCESSOR DRAWER IS 24V DC TO GROUND.

B. Open the microprocessor controller drawer.



ADJUSTMENT OF THE INPUT BOARD DIAGNOSTIC LEVEL CONTROLS DETERMINES WHAT DIAGNOSTIC INFORMATION WILL BE DISPLAYED. IF A CONTROL IS INCORRECTLY ADJUSTED, THE PROCESSOR MAY NOT SENSE AN OUT-OF-TOLERANCE PARAMETER AND THEREFORE THAT PARA-METER MAY NOT BE DISPLAYED.

C. Adjust the control until the display indicates |0|0|.

2-18.

TROUBLESHOOTING



NEVER OPEN THE EQUIPMENT UNLESS ALL TRANS-MITTER AND EXCITER PRIMARY POWER IS DIS-CONNECTED. USE THE GROUNDING STICKS PROVIDED TO ENSURE ALL COMPONENTS AND ALL SURROUNDING COMPONENTS ARE DISCHARGED BEFORE ATTEMPTING ANY MAINTENANCE.

2-19. Most troubleshooting consists of visual checks. Because of the voltages and high currents in the equipment, it is considered hazardous to work with power energized. Therefore, the various transmitter indications (meters, LEDs, fuses, and the digital read-out) should be used to isolate the malfunction to one specific area.



THE MAXIMUM POTENTIAL AT ANY POINT WITHIN THE MICROPROCESSOR DRAWER IS 24V DC TO GROUND.

2-20. Troubleshooting within the controller drawer is not considered hazardous due to the low potentials and currents involved. If trouble-shooting in the controller drawer is required to isolate problems, an oscilloscope with a 5 MHz bandwidth and 1 volt per centimeter sensitivity and a 20 k Ohm/volt multimeter is required. Microprocessor controller waveform patterns are presented in Figure 2-2 as aids to maintenance.

2-21. Once the trouble is isolated and power is totally deenergized, it is suggested that the exact problem be located with resistance checks using the schematic diagrams and theory of operation presented throughout the text.

2-22. If a circuit is diagnosed as faulty, the circuit fault may be isolated and repaired locally or the entire device may be returned to Broadcast Electronics, Inc. for exchange, alignment, or replacement.

2-23. MICROPROCESSOR BYPASS ASSEMBLY USE. Basic on and off functions and PA stage overloads may be controlled with the bypass assembly which derives its power from the five volt interlock circuit. As the unit is intended as a temporary maintenance back-up device, no timed intervals, remote features, or automatic power control features are provided.



DISCONNECT ALL TRANSMITTER PRIMARY POWER BEFORE PROCEEDING.

2-24. Disconnect all transmitter primary power, then extend the microprocessor controller forward, out of the rack on its slides.

2-25. Unplug P2 from J2 on the rear of the microprocessor controller.

2-26. Plug P2 into J2 of the microprocessor controller bypass assembly and latch the two connectors together.

2-27. The microprocessor controller may now be removed from the transmitter for maintenance if the remaining connectors are unplugged. Ensure all plugs and wiring are taped or tied securely in a safe area within the transmitter.



DO NOT TOUCH ANYTHING WITHIN THE TRANS-MITTER IF THE TRANSMITTER IS OPERATED WITH THE MICROPROCESSOR CONTROLLER REMOVED. IT IS SUGGESTED THAT A TEMPORARY GUARD BE LOCALLY FABRICATED TO COVER THE AREA IN WHICH THE MICROPROCESSOR CONTROLLER IS NORMALLY MOUNTED.

2-28. <u>Turn On</u>. Assure the INT/LCK indicator is illuminated. If not, the open safety interlock must be located and closed.

2-29. Depress the FIL START switch/indicator. The FIL START indicator will illuminate.

2-30. At least ten seconds after the BLO indicator illuminates to indicate the blower is up to speed, the H.V. START switch/indicator may be depressed. The H.V. START indicator will illuminate.

2-31. A PA stage overload will deenergize the PA plate supply. The transmitter may be restored to operation by depressing the H.V. START switch/indicator.

2-32. Turn Off. Depress the H.V. STOP switch.

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2-33. After a ten second minimum delay to allow the PA tube filament to cool, depress the FIL STOP switch.

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CHANNEL A:	TYPICAL	PROGRAM	PATTERN
	(3.3 ms	Long)	

<u>CHANNEL B</u>: FLAG_o PULSE (Signals Program Start)

MICROPROCESSOR INDICATOR:

- TEST POINT: A PATCH PANEL PIN 4 B U6 PIN 10 ON PROCESSOR BOARD
- SYNC: U6 PIN 10 ON PROCESSOR BOARD

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<u>CHANNEL A</u> : TYPICAL PROGRAM PATTERN, FIRST HALF (Control Pulse Portion)								
<u>CHANNEL B</u> : FLAG _o PULSE (Signals Program Start)								
MICROPROCESSOR INDICATOR:								
TEST POINT:A PATCH PANEL PIN 4 B U6 PIN 10 ON PROCESSOR BOARD								
SYNC: U6 PIN 10 ON PROCESSOR BOARD								

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<u>CHANNEL A</u> :	TYPICAL PROGRAM PATTERN, FIRST HALF (Control Pulse Portion)						
CHANNEL B:	FLAG, PULSE (Signals Program Start)						
MICROPROCES	SOR INDICATOR: 98						
TEST POINT:	A PATCH PANEL PIN 4 B UG PIN 10 ON PROCESSOR BOARD						
<u>SYNC</u> : UG P	IN 10 ON PROCESSOR BOARD 597-0003-35A						

FIGURE 2-2. MICROPROCESSOR CONTROLLER TYPICAL WAVEFORMS (Sheet 1 of 3)

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- <u>CHANNEL A</u>: TYPICAL PROGRAM PATTERN, FIRST HALF (Control Pulse Portion)
- CHANNEL B: FLAG_o PULSE (Signals Program Start)

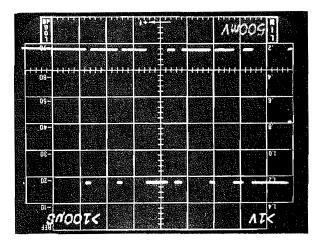
MICROPROCESSOR INDICATOR: 00

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TEST POINT: A PATCH PANEL PIN 4 B U6 PIN 10 ON PROCESSOR BOARD SYNC: U6 PIN 10 ON PROCESSOR BOARD

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<u>CHANNEL A:</u> CLOCK PATTERN (15us - 66kHz)							
MICROPROCESSOR INDICATOR:							
TEST POINT: U6 PIN 14 ON PROCESSOR BOARD							
SYNC: SCOPE							



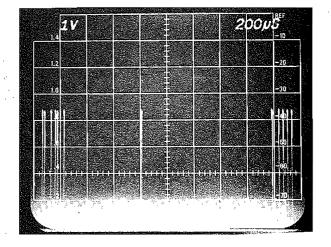
CHANNEL A: DATA BUS PATTERN
MICROPROCESSOR INDICATOR: 00
TEST POINT: PATCH PANEL PIN 17
SYNC: U6 PIN 10 ON PROCESSOR BOARD
597-0003-35B

FIGURE 2-2. MICROPROCESSOR CONTROLLER TYPICAL WAVEFORMS (Sheet 2 of 3)

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SYNC: U	6 PIN 10	ON PROCE	SSOR BOARD



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8b						P

CHANNEL A:	BLOWER TIMER PATTERN
MICROPROCESS	OR INDICATOR: 00
TEST POINT:	U1 PINS 6 AND 7 ON CONTROL/TIMER BOARD
SYNC: SCOPE	

597-0003-350

FIGURE 2-2. MICROPROCESSOR CONTROLLER TYPICAL WAVEFORMS (Sheet 3 of 3)

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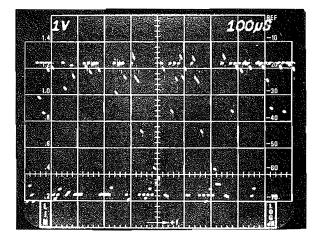
- CHANNEL A: TYPICAL PROGRAM PATTERN, FIRST HALF (Control Pulse Portion)
- <u>CHANNEL B</u>: FLAG_O PULSE (Signals Program Start)

MICROPROCESSOR INDICATOR: 00

TEST POINT: A PATCH PANEL PIN 4 B U6 PIN 10 ON PROCESSOR BOARD SYNC: U6 PIN 10 ON PROCESSOR BOARD

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.8							~50
.4			 				-60
.2							

CHANNEL A:	CLOCK PATTERN (15us – 66kHz)
MICROPROCESS	OR INDICATOR: 00
TEST POINT:	U6 PIN 14 ON PROCESSOR BOARD
SYNC: SCOPE	



CHANNEL A: DATA BUS PATTERN
MICROPROCESSOR INDICATOR: 00
TEST POINT: PATCH PANEL PIN 17
SYNC: U6 PIN 10 ON PROCESSOR BOARD
597-0003-35B

FIGURE 2-2. MICROPROCESSOR CONTROLLER TYPICAL WAVEFORMS (Sheet 2 of 3)

2-9

WARNING: DISCONNECT POWER PRIOR TO SERVICING

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CHANNEL A:	TYPICAL ADDRESS BUS PATTERN (A _O BUS)
MICROPROCESS	SOR INDICATOR: 00
TEST POINT:	PATCH PANEL PIN 13
SYNC: U6 P	IN 10 ON PROCESSOR BOARD

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597-0003-35C

FIGURE 2-2. MICROPROCESSOR CONTROLLER TYPICAL WAVEFORMS (Sheet 3 of 3)

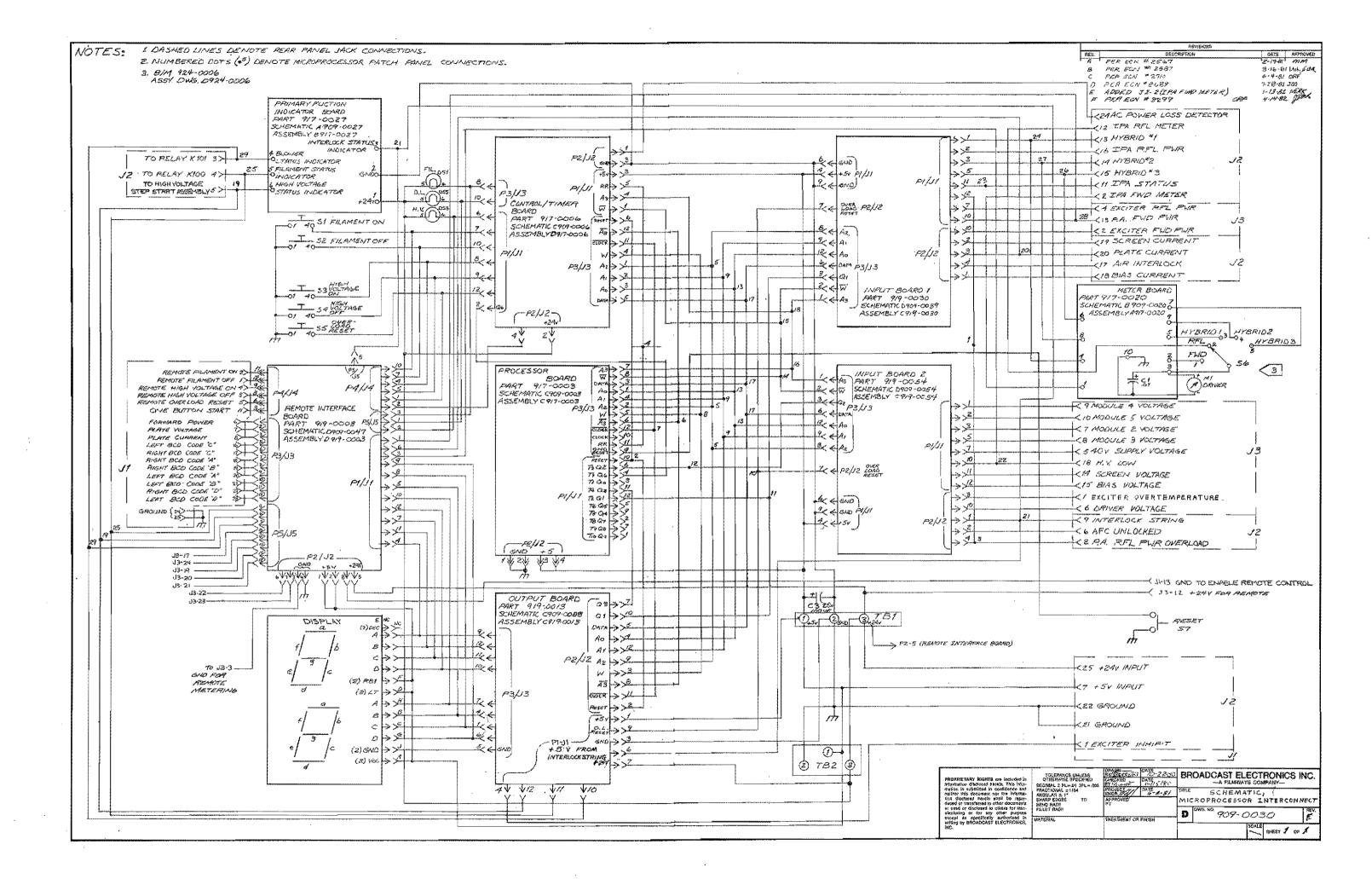
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SECTION III MICROPROCESSOR CONTROLLER DRAWINGS

3-1. INTRODUCTION

3-2. This section provides assembly drawings, schematic diagrams, and wire lists as indexed below for the FM-30 Transmitter Microprocessor controller.

FIGURE	TITLE	NUMBER
3-1	Schematic, Microprocessor Interconnect	D909-0030
3-2	Schematic, Processor Board	C909-0003
3-3	Assembly, Processor Board	C917-0003
3-4	Schematic, Output Board	C909-0088
3-5	Assembly, Output Board	C919-0013
3-6	Schematic, Control/Timer Board	D909-0006
3-7	Assembly, Control/Timer Board	C917-0006
3-8	Schematic, Remote Control Interface	D909-0047
3-9	Assembly, Remote Control Interface	D919-0003
3-10	Schematic, Input Board 1	D909-0039
3-11	Assembly, Input Board 1	C919-0030
3-12	Schematic, Input Board 2	D909-0054
3-13	Assembly, Input Board 2	C919-0054
3-14	Schematic, Primary Function Indicator	A909-0027
3-15	Assembly, Primary Function Indicator	B917-0027
3-16	Schematic, Microprocessor Bypass Assembly	B909-0056
3-17	Schematic, Microprocessor Bypass Circuit Board	C909-0057
3-18	Assembly, Microprocessor Bypass Circuit Board	B919-0009



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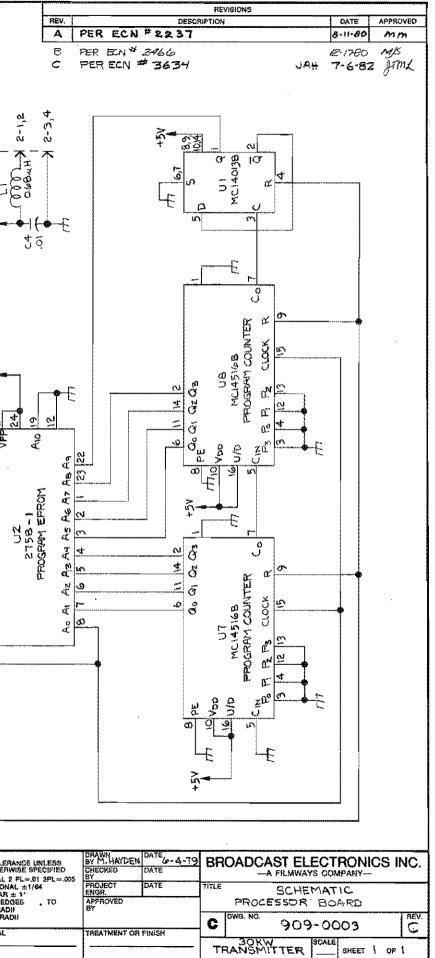
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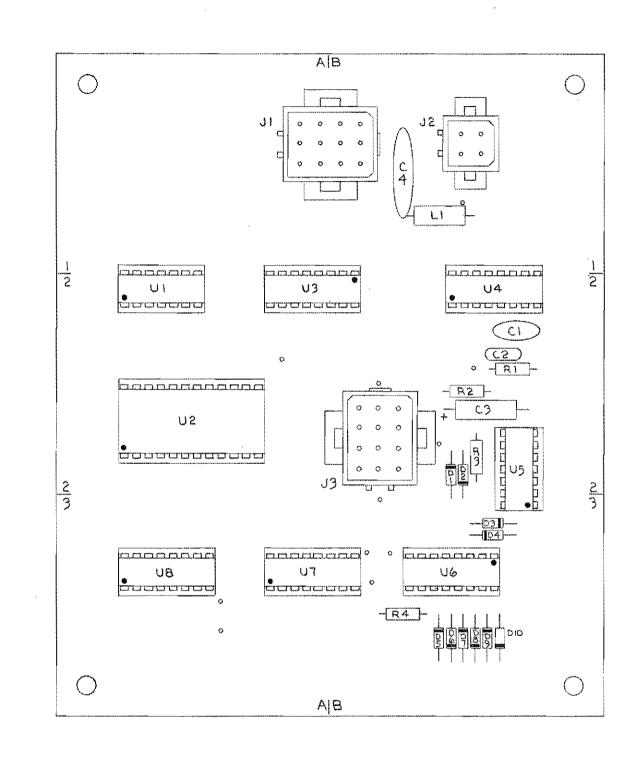
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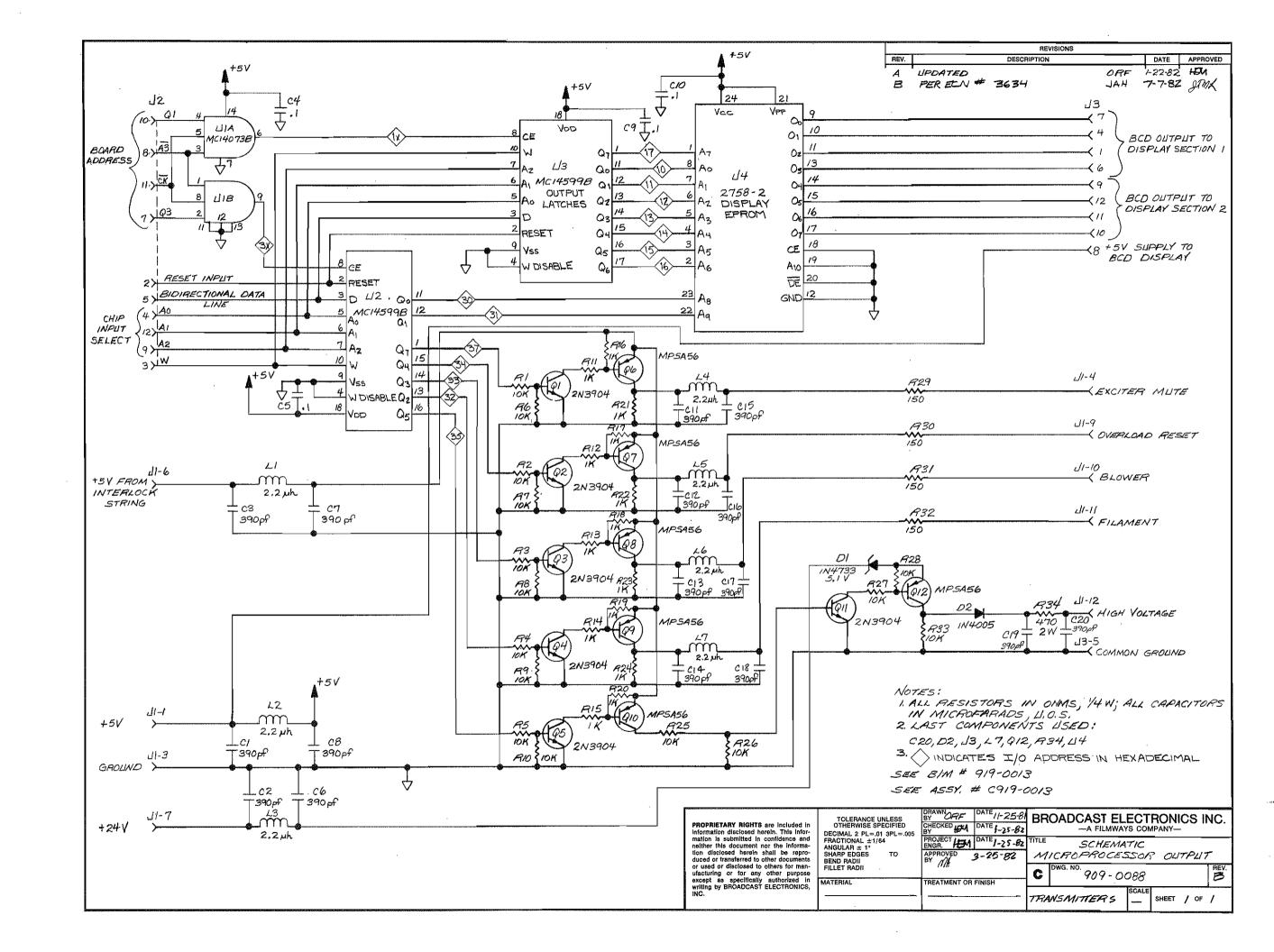
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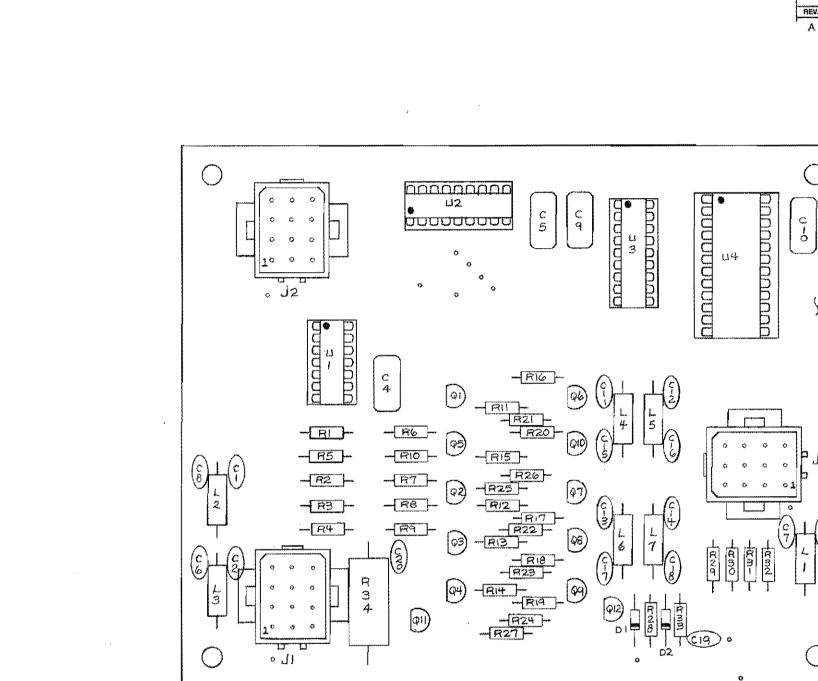
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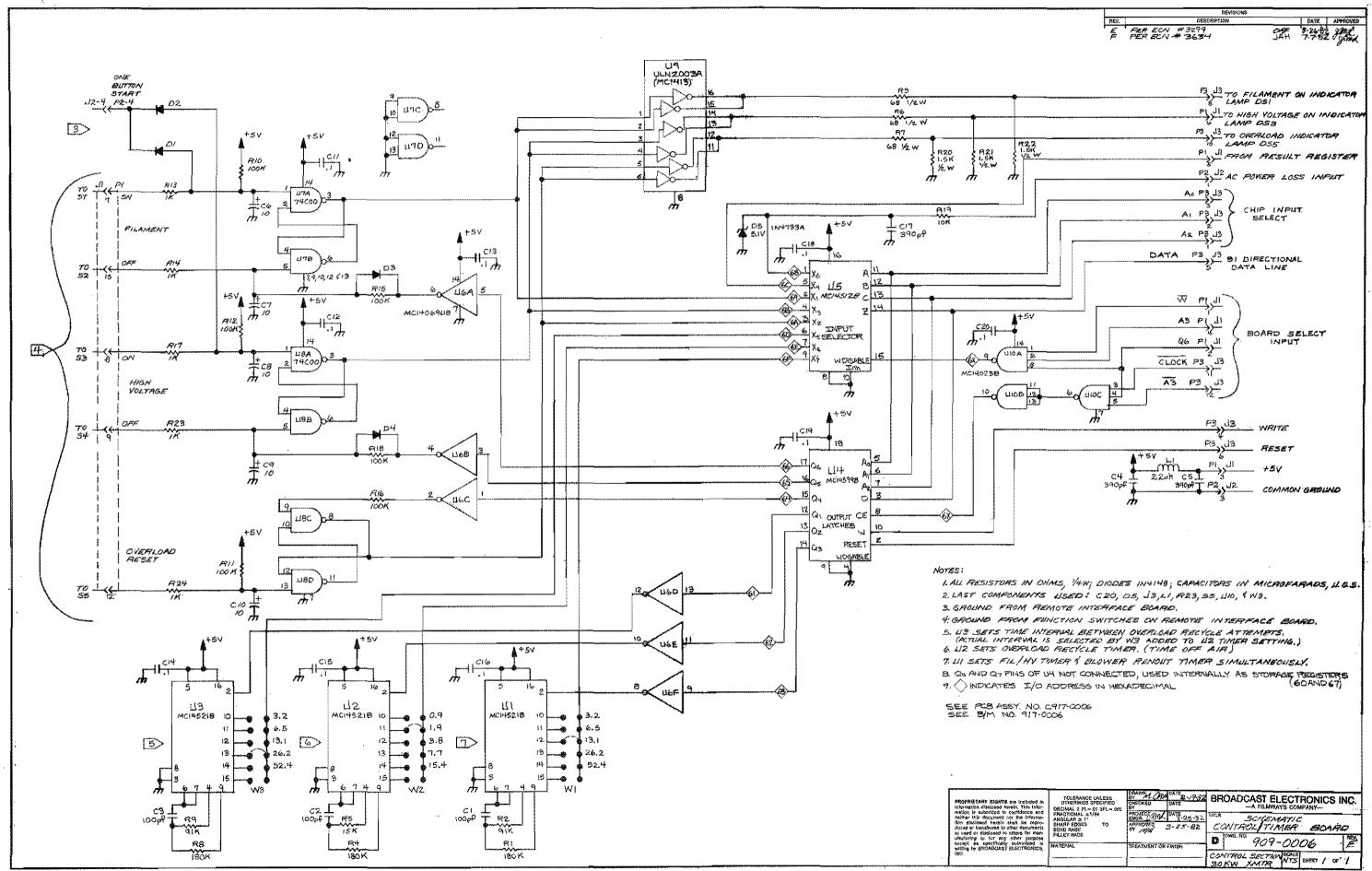
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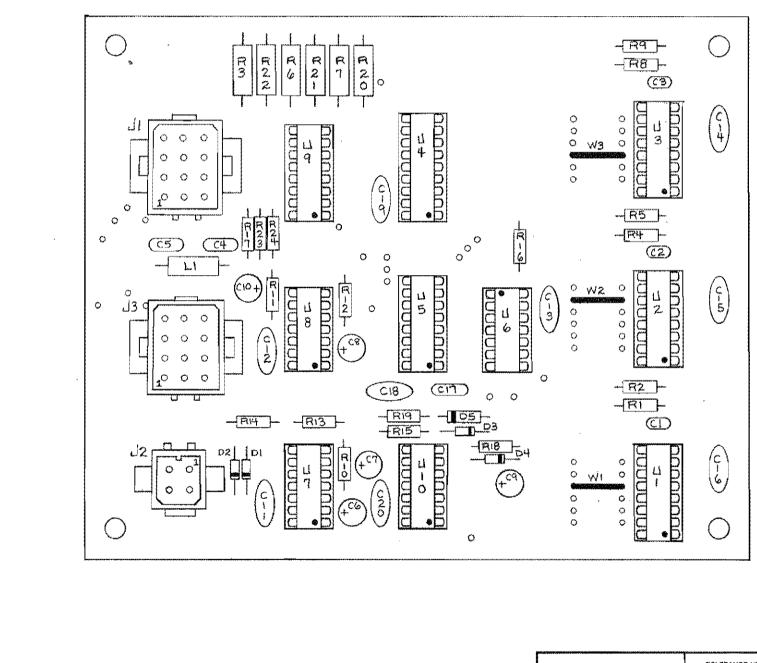
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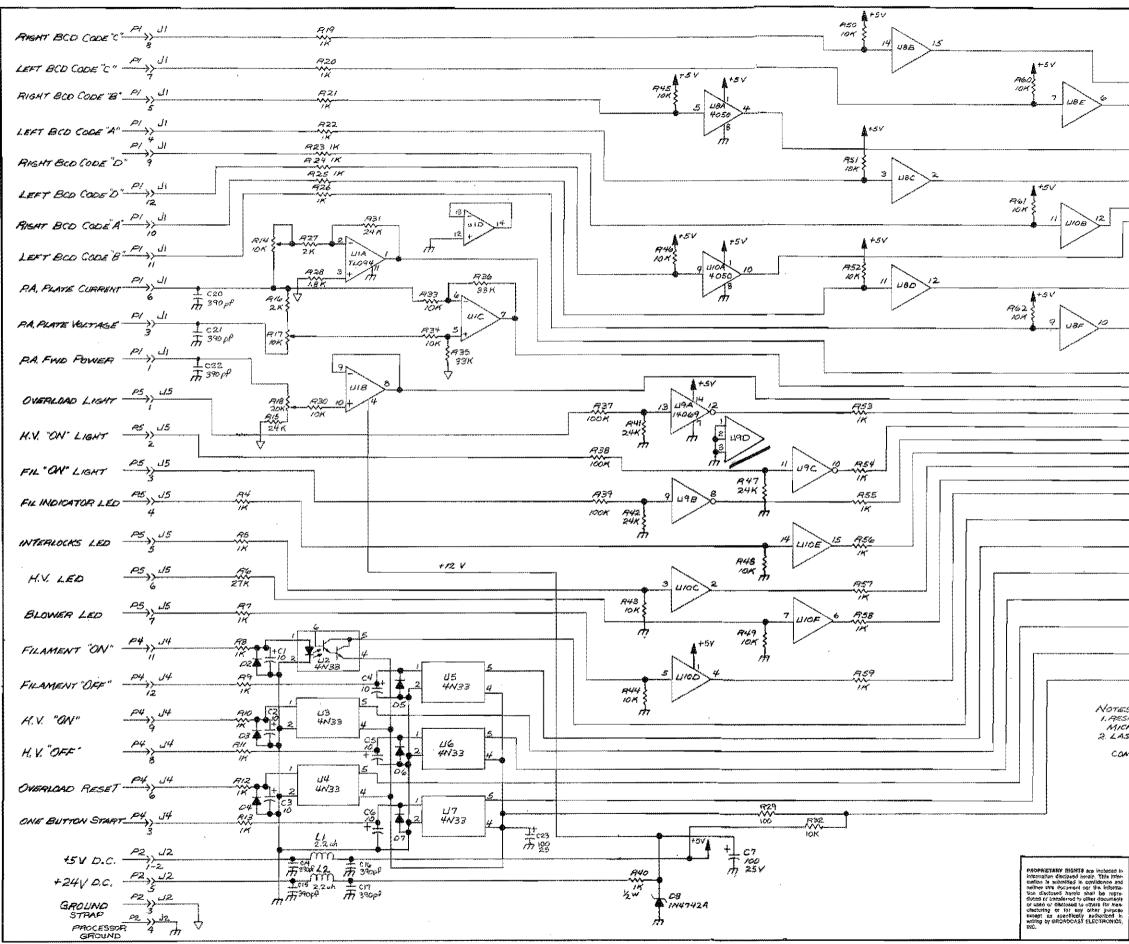
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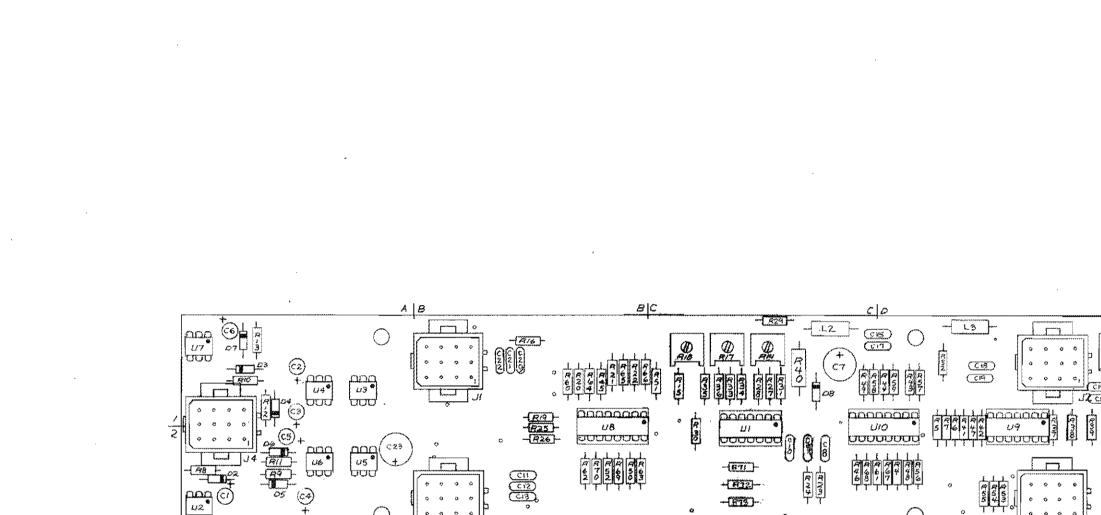
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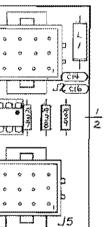
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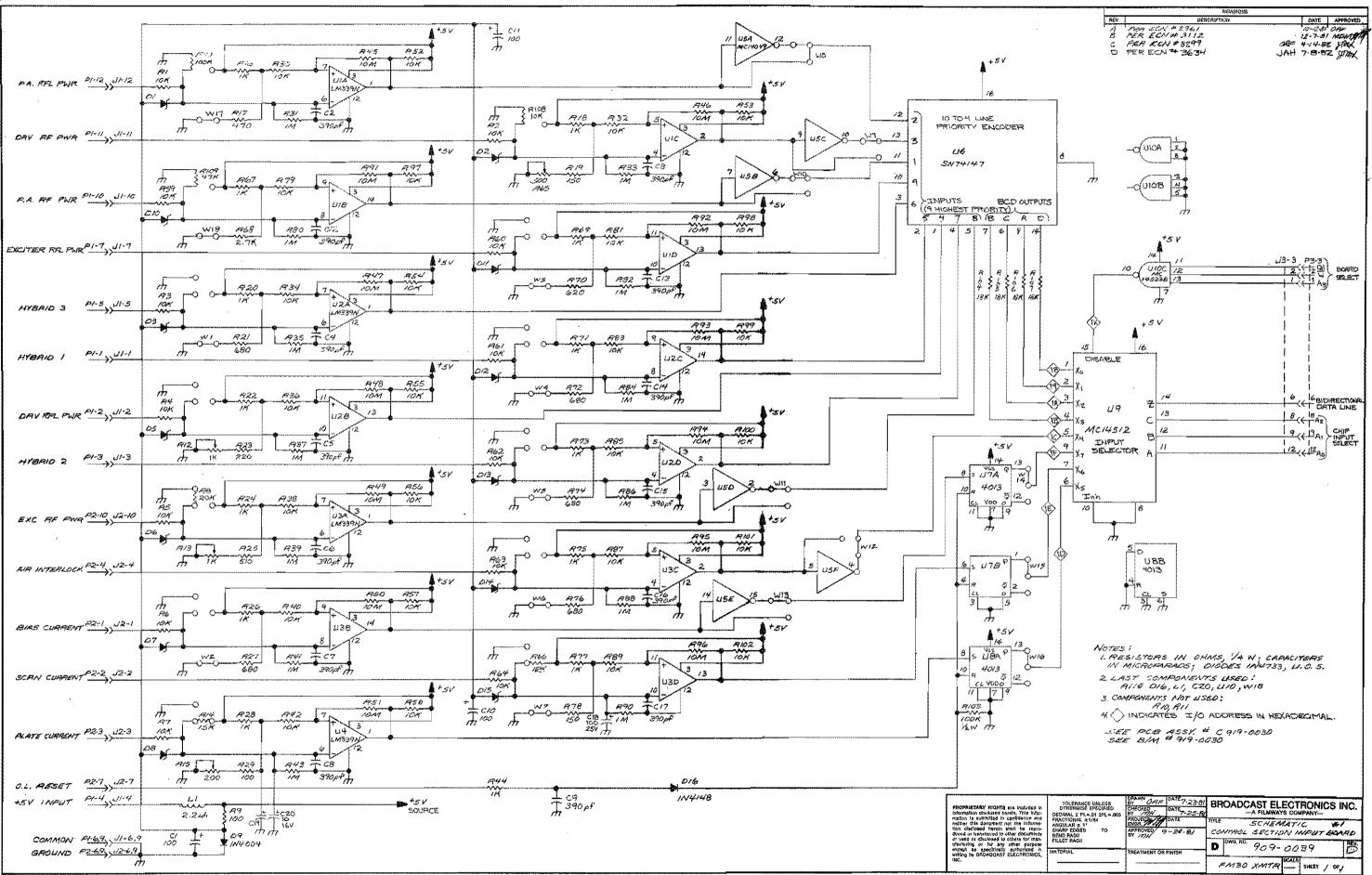
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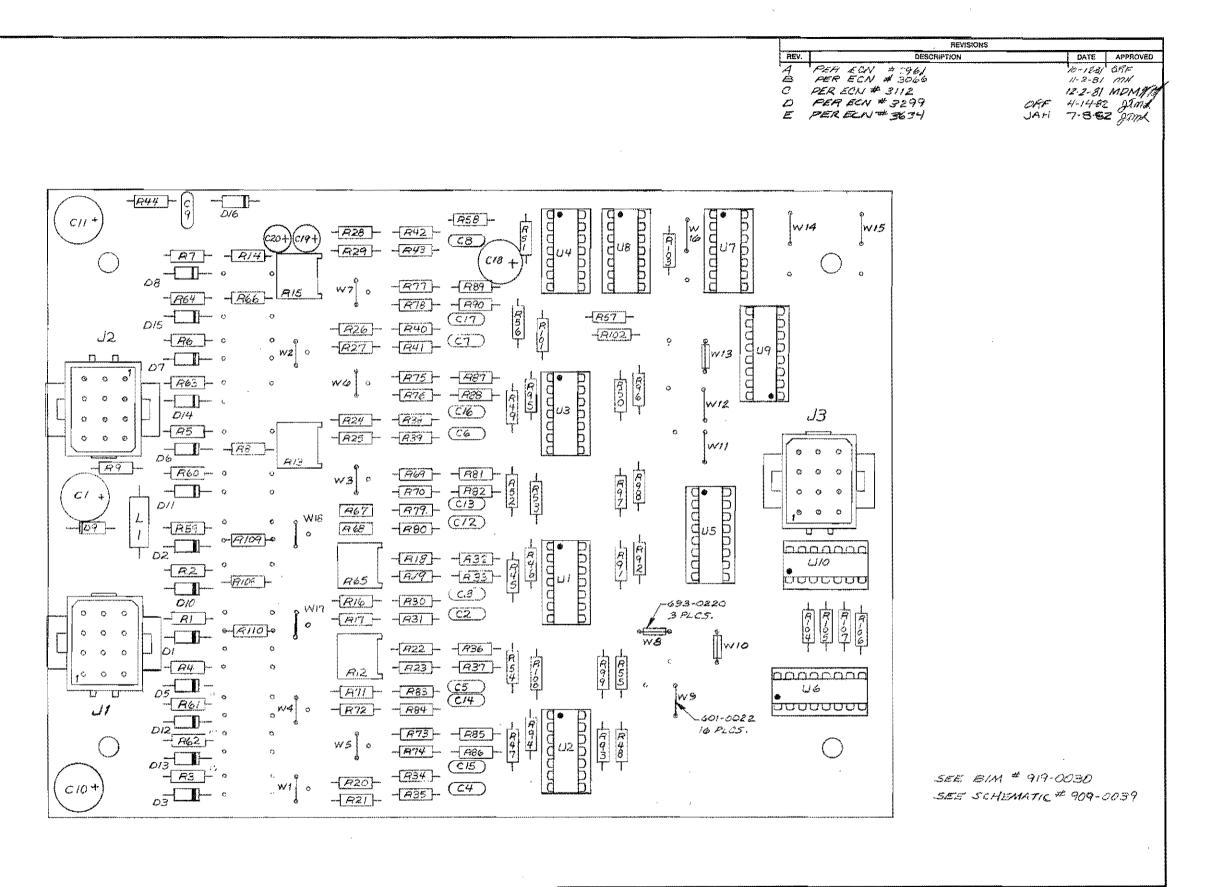
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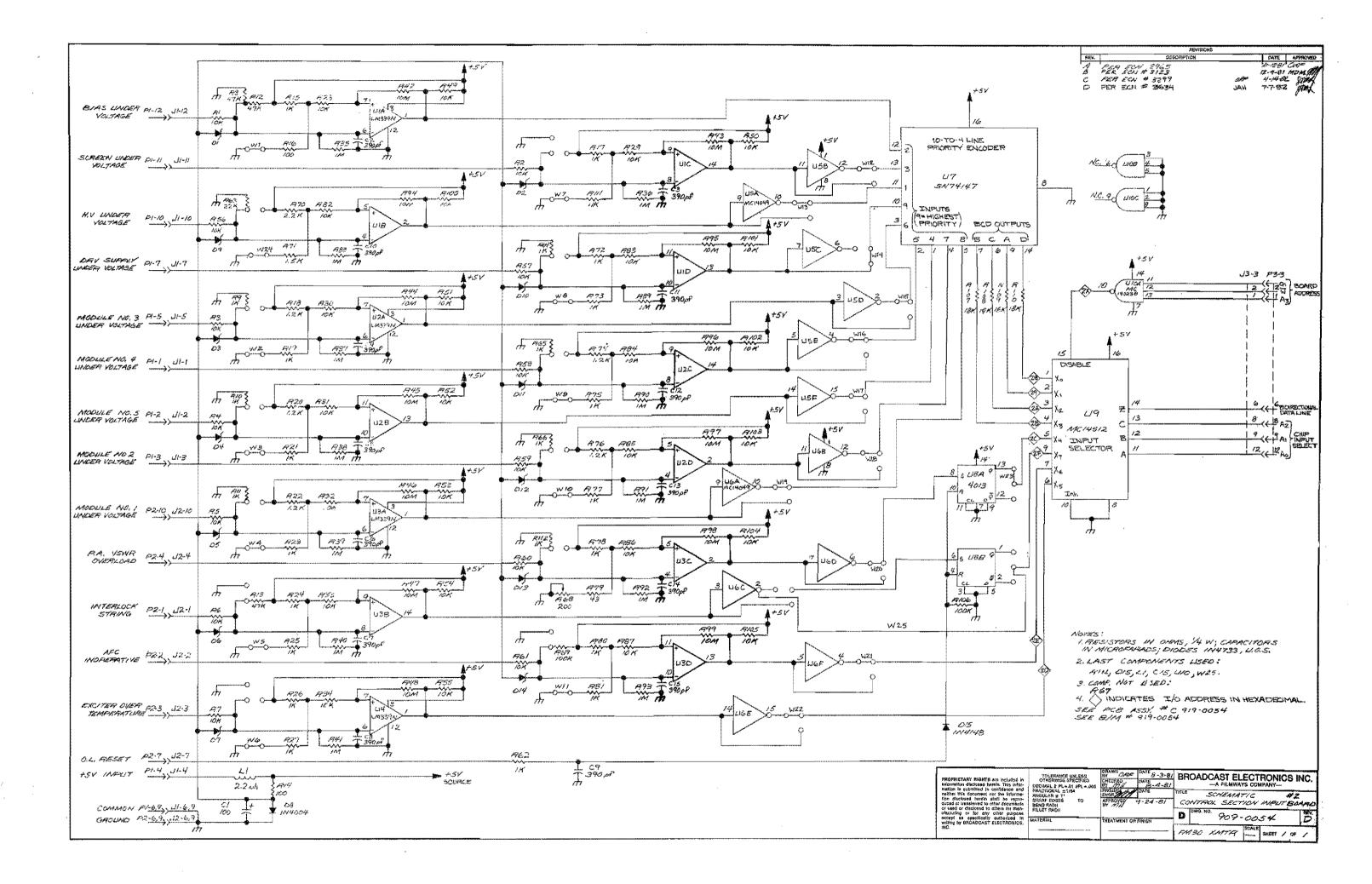
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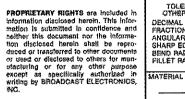
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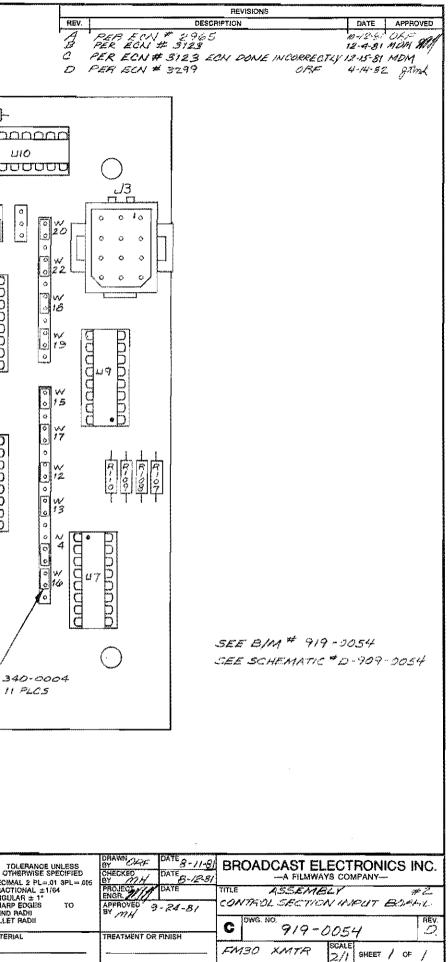
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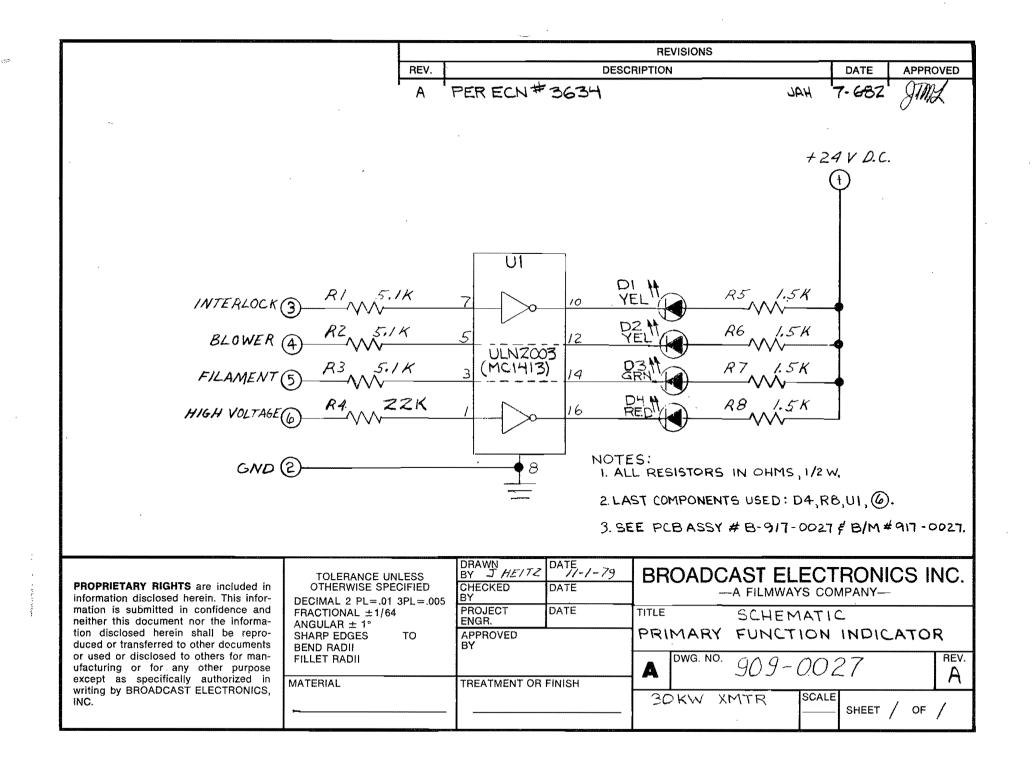


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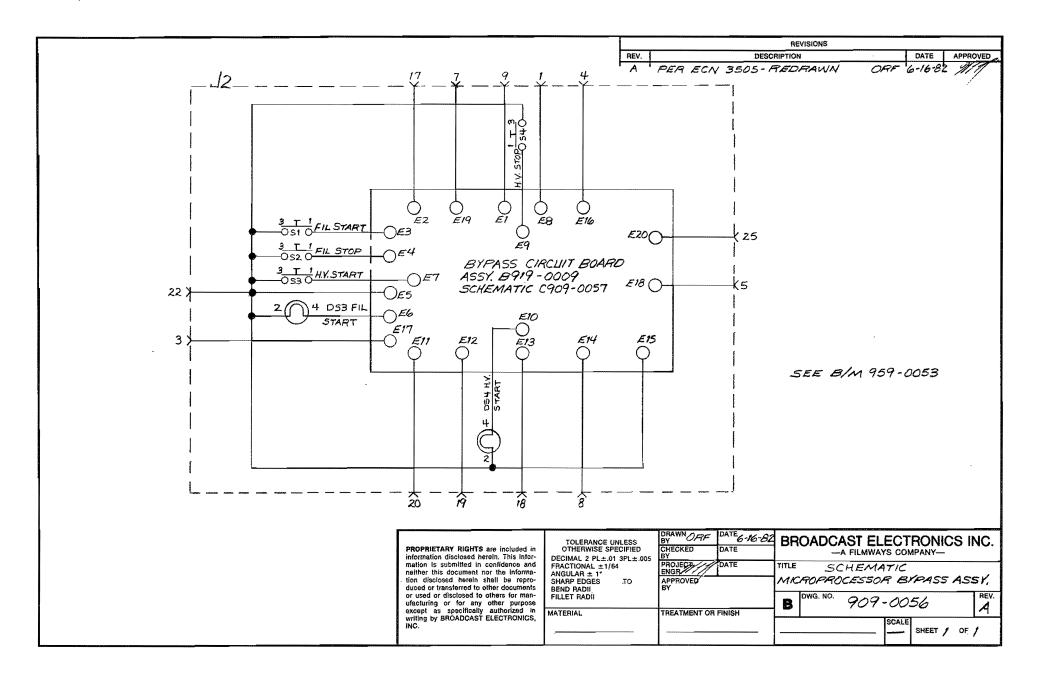


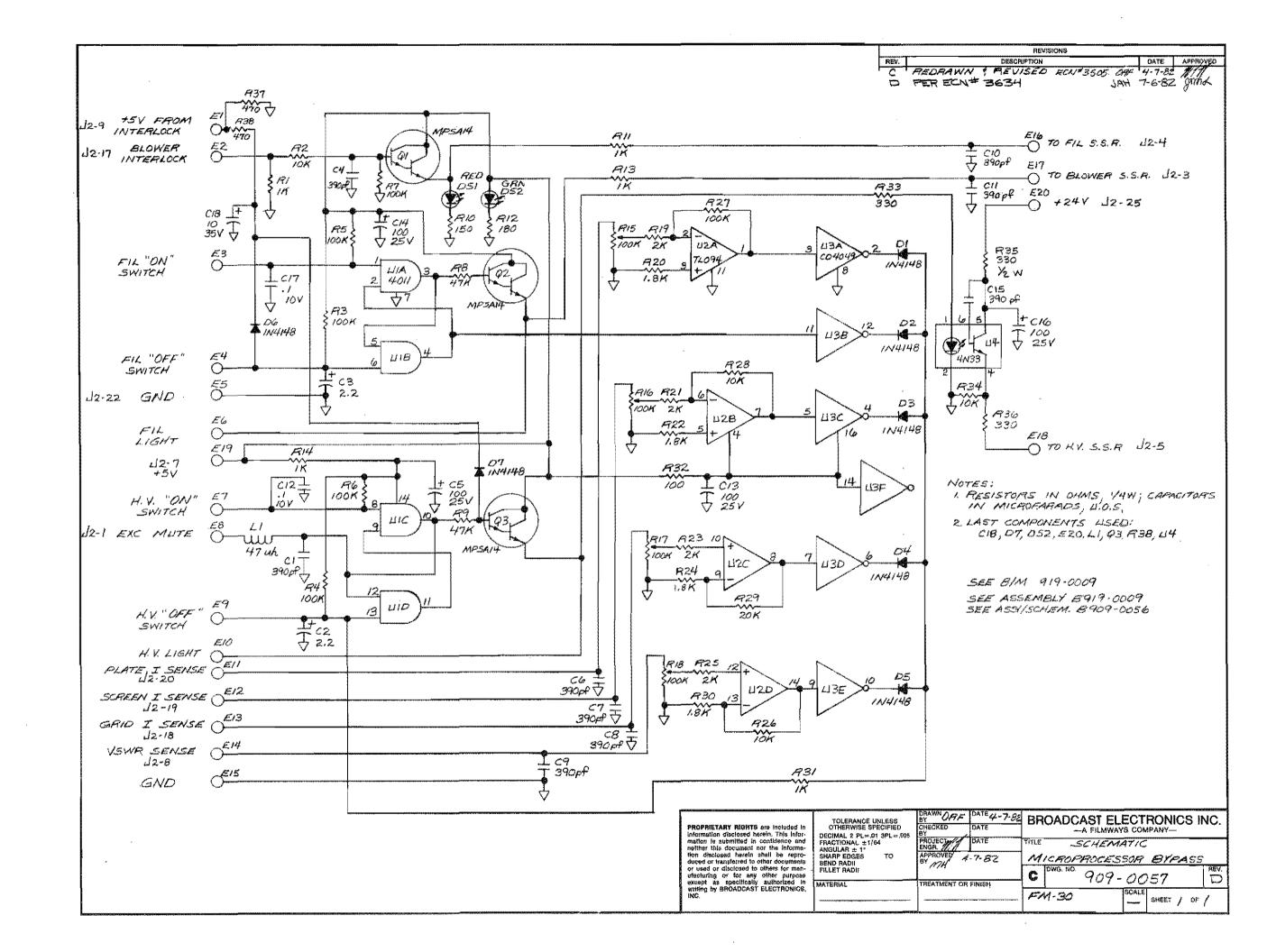
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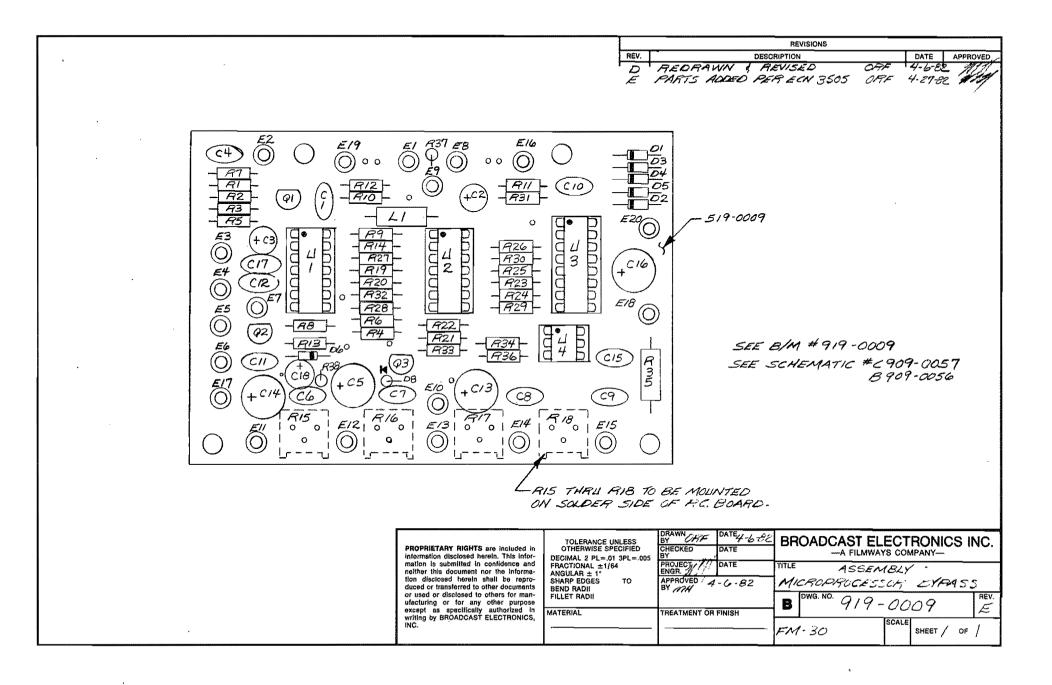




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APPENDIX A

MICROPROCESSOR CONTROLLER MANUFACTURERS DATA

A-1. INTRODUCTION

A-2. This appendix provides the following technical data relative to the operation and maintenance of the FM-30 FM transmitter micro-processor controller. Information contained in this appendix is listed in the following order.

A. Technical Data Sheet, Motorola MC 14500B Industrial Control Unit.

B. Technical Data Sheet, Motorola MC 14599B, 8-Bit Addressable Latch.

C. Technical Data Sheet, Intel 2758 8K UV Erasable Low Power PROM

D. Instruction Sheet, Dialight 7 Segment Numeric Display, No. 730-6007.

E. Operating Specifications, Dialight 7 Segment Numeric Display (730-6001) and Decoder (704-1549).

) MOTOROLA SEMICONDUCTORS

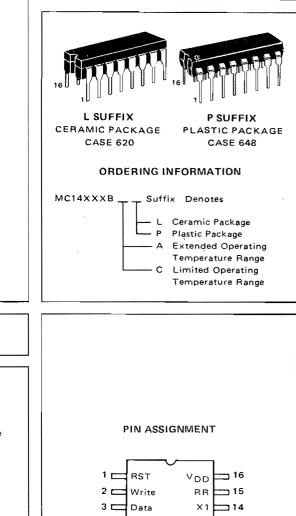
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MC14500B

CMOS LSI

(LOW-POWER COMPLEMENTARY MOS)

INDUSTRIAL CONTROL UNIT

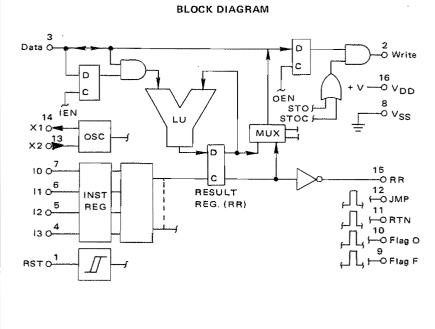


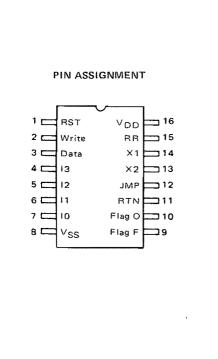
INDUSTRIAL CONTROL UNIT

The MC14500B Industrial Control Unit (ICU) is a single bit CMOS processor. The ICU is designed for use in systems requiring decisions based on successive single bit information. An external ROM stores the control program. With a program counter (and output latches and input multiplexers, if required) the ICU in a system forms a stored program controller that replaces combinatorial logic. Applications include relay logic processing, serial data manipulation and control. The ICU also may control an MPU or be controlled by an MPU.

- 16 Instructions
- DC to 1.0 MHz Operation at VDD = 5 V
- On Chip Clock (Oscillator)
- Executes One Instruction per Clock Cycle
- 3 V to 18 V Operation
- Noise Immunity Typically 45% of VDD
- Quiescent Current 5.0 μ Adc Typical at VDD = 5 V
- Capable of Driving One Low-Power Schottky Load or Two Low-Power TTL Loads over Full Temperature Range

Detailed operation and applications are given in the "MC14500B Industrial Control Unit" handbook.





Rating	Symbol	Value	Unit
DC Supply Voltage	VDD	-0.5 to +18	Vdc
Input Voltage, All Inputs	Vin	-0.5 to V _{DD} + 0.5	Vdc
DC Current Drain per Pin	1.	10	mAdc
Operating Temperature Range – AL Device CL/CP Device	TA	-55 to +125 -40 to +85	°C
Storage Temperature Range	T _{stg}	-65 to +150	°C

This device contains circuitry to protect the inputs against damage due to high static voltages or electric fields; however, it is advised that normal precautions be taken to avoid application of any voltage higher than maximum rated voltages to this high impedance circuit. For proper operation it is recommended that V_{in} and V_{out} be constrained to the range V_{SS} \leq (V_{in} or V_{out}) \leq V_{DD}.

ELECTRICAL CHARACTERISTICS

			VDD	110	w*		25 ⁰ C		1 h	igh [*]	4
Characteristic		Symbol	Vdc	Min	Max	Min	Тур	Max	Min	Max	Unit
Output Voltage	"0" Level	VOL	5.0		0.05		0	0.05	-	0.05	Vdc
V _{in} = V _{DD} or 0			10	-	0.05		0	0.05		0.05	
			15		0.05	-	0	0.05	-	0.05	
	"1" Level	∨он	5.0	4.95	-	4.95	5.0		4.95		Vdc
V _{in} = 0 or V _{DD}			10	9.95	-	9.95	10	÷	9.95		
			15	14.95	-	14.95	15		14.95		
Input Voltage #	"O Level"	VIL									Vdc
RST, D, X2											
(V _O = 4.5 or 0.5 Vdc)			5.0		1.5		2.25	1,5	-	1,5	
(V _O = 9.0 or 1.0 Vdc)			10	-	3.0	-	4.50	3.0		3.0	
(V _O = 13.5 or 1.5 Vdc)			15		4.0		6.75	4.0		4.0	
	"1" Level	VIH									Vdc
(Vo = 0.5 or 4.5 Vdc)			5.0	3.5		3.5	2.75		3.5		
$(V_0 = 1.0 \text{ or } 9.0 \text{ Vdc})$			10	7.0		7.0	5.50	-	7.0		
(V _O = 1.5 or 13.5 Vdc)			15	11.0		11.0 -	8.25	-	11.0		
Input Voltage #	"O" Level	VIL									Vdc
10, 11, 12, 13											
$(V_0 = 4.5 \text{ or } 0.5 \text{ Vdc})$			5.0		0.8	-	1.1	0.8	-	0.8	
$(V_0 = 9.0 \text{ or } 1.0 \text{ Vdc})$			10	-	1.6	-	2.2	1.6	-	1.6	
(V _O = 13.5 or 1.5 Vdc)			15		2.4		3.4	2.4		2.4	
	"1" Level	VIH									Vdd
$(V_0 = 0.5 \text{ or } 4.5 \text{ Vdc})$			5.0	2.0	-	2.0	1.9		2.0		
$(V_0 = 1.0 \text{ or } 9.0 \text{ Vdc})$			10	6.0		6.0	3.1		6.0		
(V _O = 1.5 or 13.5 Vdc)			15	10	-	10	4.3		10		
Output Drive Current	Source	юн									mAd
Data, Write (AL/CL/CP Device)											
$(V_{OH} = 4.6 \text{ Vdc})$			5.0	-1.0	-	-1,0	-2.0		-1.0		
$(V_{OH} = 9.5 Vdc)$			10				-6.0			-	
(V _{OH} = 13.5 Vdc)			15				-12				
$(V_{OL} = 0.4 Vdc)$	Sink	IOL	5.0	1.6	-	1.6	3.2		1.6		mAd
$(V_{OL} = 0.5 Vdc)$			10	-			6.0			• ••••	
(V _{OL} = 1.5 Vdc)			15				12				
Output Drive Current	Source	юн									mAd
Other Outputs (AL Device)) I		
(V _{OH} = 2.5 Vdc)	•		5.0	-3.0		-2.4	-4.2	-	-1.7		
(V _{OH} = 4.6 Vdc)			5.0	-0.64	_	-0.51	-0.88	~	-0.36		
(V _{OH} = 9.5 Vdc)			10	-1.6	_	-1.3	-2.25		-0.9		
(V _{OH} = 13.5 Vdc)			15	-4.2	-	-3.4	8.8		-2.4	-	
(V _{OL} = 0.4 Vdc)	Sink	10L	5.0	0.64		0.51	0.88	-	0.36		mAd
(VOL = 0.5 Vdc)			10	1.6		1.3	2.25		0.9		
$(V_{OL} = 1.5 V_{dc})$			15	4.2	-	3.4	8.8		2.4	-	
Output Drive Current	Source	ЮН									mAd
Other Outputs (CL/CP Device)		_									
(V _{OH} = 2.5 Vdc)			5.0	-2.5	-	-2.1	-4.2		-1.7	-	
$(V_{OH} = 4.6 \text{ Vdc})$			5.0	-0.52		-0.44	-0.88		-0,36		
(V _{OH} = 9.5 Vdc)			10	-1.3		-1.1	-2.25	_	-0.9	-	
(V _{OH} = 13.5 Vdc)			15	-3.6		-3.0	-8.8		-2.4		
(V _{OL} = 0.4 Vdc)	Sink	IOL	5.0	0.52	****	0,44	0.88		0.36		mAd
(VOL = 0.5 Vdc)			10	1.3	_	1.1	2.25		0.9		
$(V_{OL} = 1.5 Vdc)$			15	3.6		3.0	8.8		2.4		

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1001 20 1		

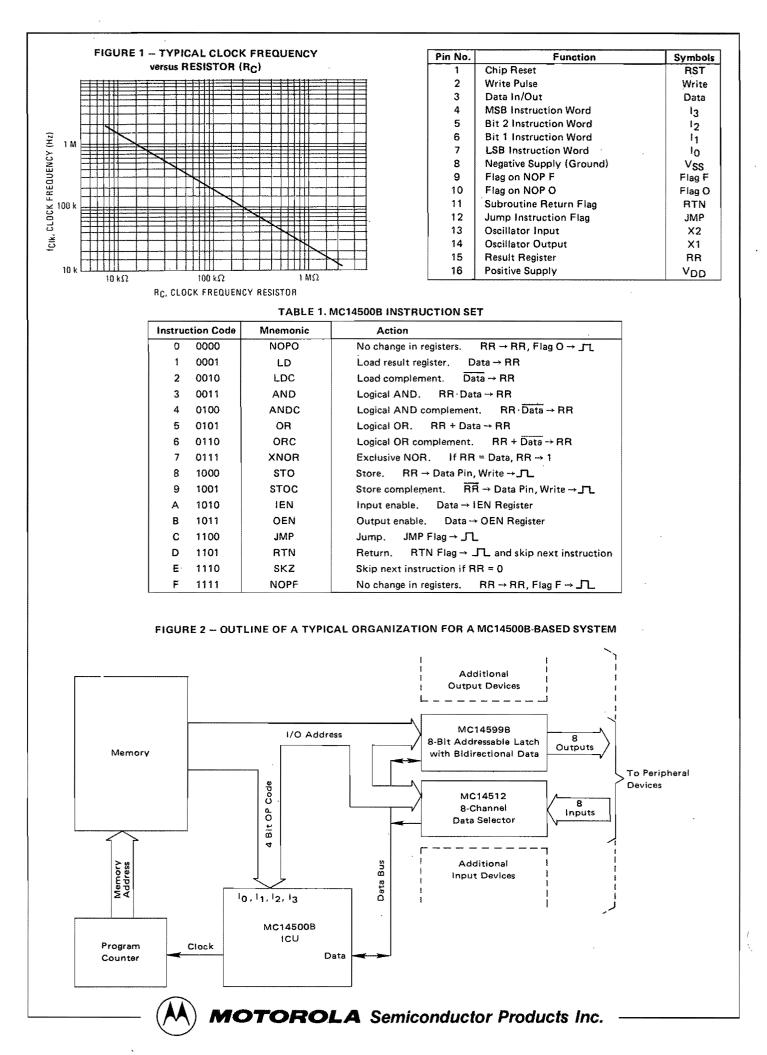
Characteristic	Symbol	V _{DD} Vdc	Tlow*		25°C			Thigh*		
			Min	Max	Min	Тур	Max	Min	Max	Unit
Input Current, RST (AL/CL/CP Device)	lin	15	25	~~~		150		-	250	#Adc
Input Current (AL Device)	l _{in}	15	-	±0.1		±0,00001	±0.1		±1.0	μAdc
Input Current (CL/CP Device)	lin	15		±0.3		±0.00001	±0.3		± 1.0	μAdc
Input Capacitance (Data)	Cin		_		_	15	***		_	pF
Input Capacitance (All Other Inputs) (Vin = 0)	C _{in}		-	unter,		5.0	7.5		juëzy:	pF
Quiescent Current (AL Device)	IDD	5.0		5.0	-	0.005	5.0		150	μAdc
(Per Package)		10	-	10	-	0.010	10	-	300	
		15	-	20	-	0.015	20		600	
Quiescent Current (CL/CP Device)	IDD	5.0	-	20	-	0.005	20	-	150	μÅdc
(Per Package)		10	-	40	-	0.010	40	-	300	
		15		80	-	0.015	80	-	600	
**Total Supply Current at an External Load Capacitance (CL) on All Outputs	١T	_	$I_{T} = (1.5 \ \mu A/kHz) \ f + I_{DD}$ $I_{T} = (3.0 \ \mu A/kHz) \ f + I_{DD}$ $I_{T} = (4.5 \ \mu A/kHz) \ f + I_{DD}$						µAdc	

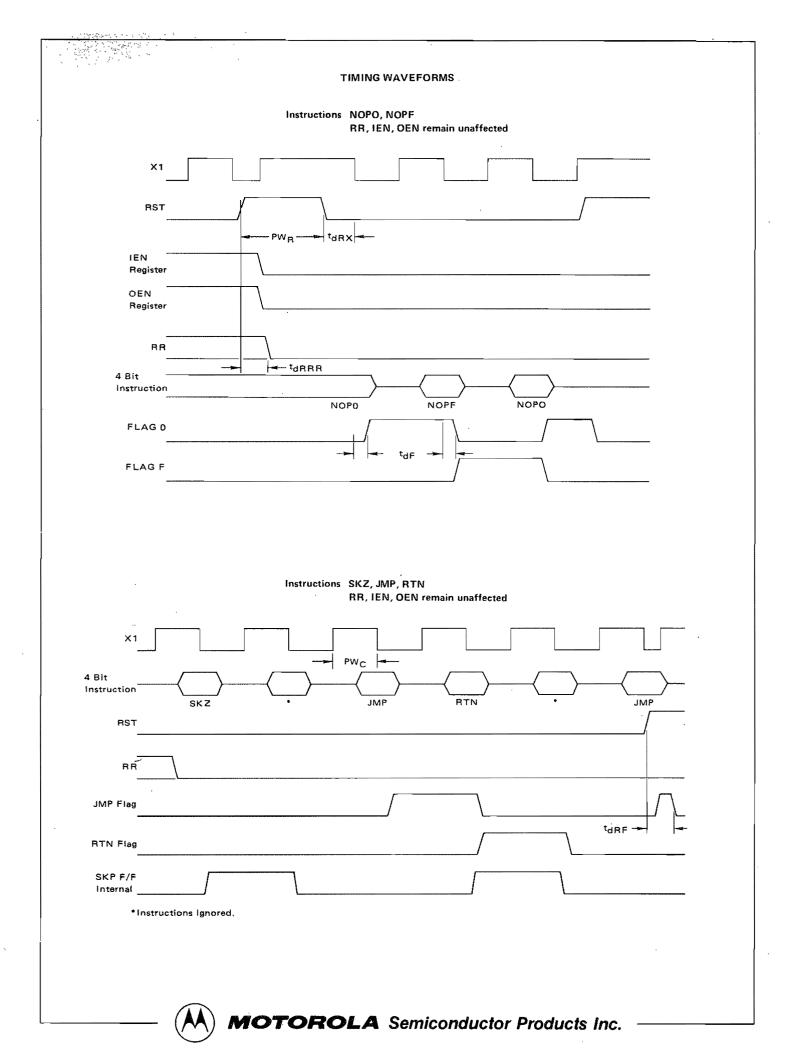
* $T_{1ow} = -55^{\circ}C$ for AL Device, $-40^{\circ}C$ for CL/CP Device. Thigh = $+125^{\circ}C$ for AL Device, $+85^{\circ}C$ for CL/CP Device. ** The formulas given are for the typical characteristics only at $25^{\circ}C$.

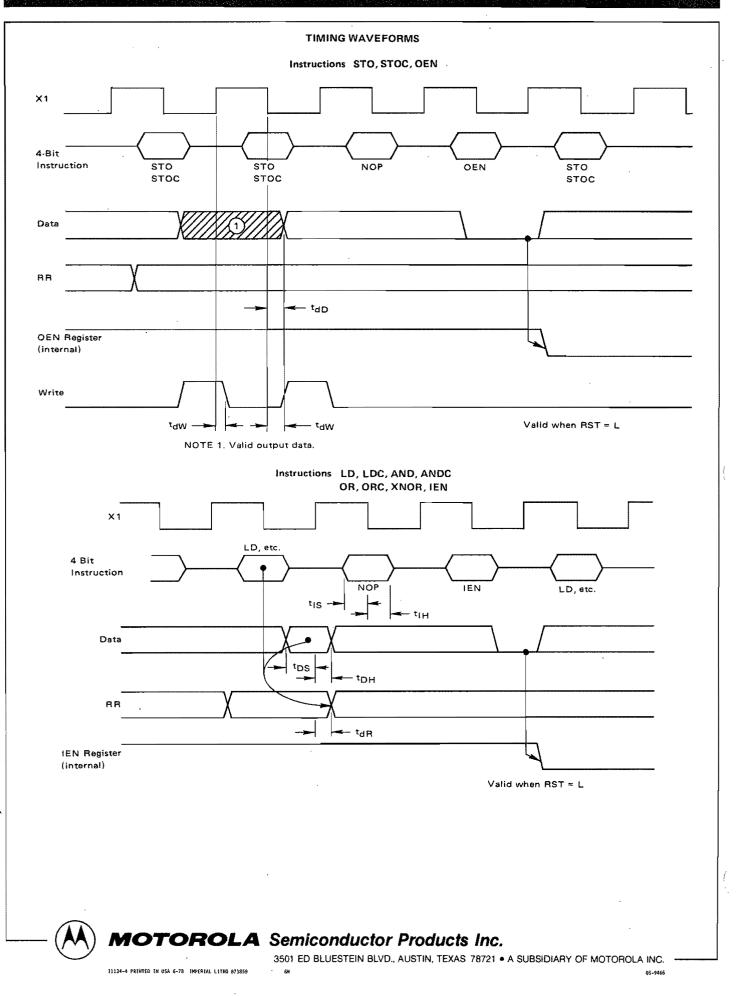
Noise immunity specified for worst-case input combination.

SWITCHING CHARACTERISTICS ($T_A = 25^{\circ}C$; $t_f = t_f = 20$ ns for X and I inputs; $C_L = 50$ pF for JMP, X1, RR, Flag O, Flag F; $C_L = 130$ pF + ITTL load for Data and Write.)

Characteristic	Symbol	V _{DD} Vdc				
			Min	Тур	Max	Unit
Propagation Delay Time X1 to RR	tdR	5.0		250	500	ns
		10	— .	125	250	
		15		100	200	
X1 to Flag F, Flag O, RTN, JMP	tdF	5.0		200	400	ns
	0.	10		100	200	
		15	· · · ·	85	170	
X1 to Write	tdW	5.0		225	450	ns
	un	10		125	250	
		15		100	200	
X1 to Data	tdD	5.0		250	500	ns
	-0.0	10		120	240	
		15		100	200	
RST to RR	tdRRR	5.0		250	500	ns
	-unnn	10		125	250	
		15		100	200	
RST to X1	tdRX	5.0		450	Note 1	ns
	'un X	10		200	Note 1	
		15		150		
RST to Flag F, Flag O, RTN, JMP	tdRF	5,0	_	400	800	ns
	'orr	10		200	400	113
		15		150	300	
RST to Write, Data	+ 15.44	5,0		450	900	ns
	tdRW	10	_	225	450	112
		15	_	175	350	
Minimum Clock Pulse Width, X1 Minimum Reset Pulse Width, RST	PWC	5.0		200	400	
	L MC	10		100	200	ns
		15	_	90	180	
	D141					
Minimum Reset Pulse Width, RS I	PWR	5.0	-	250 125	500 250	ns
		10		100	200	
Contra Instantia						
Setup Time - Instruction	tis	5.0	400	200		ns
		10 15	250 180	125 90	_	
Data						
	tDS	5.0	200	100		ns
		10	100 80	50		
		15		40	WELLA	
Hold Time – Instruction Data	tiH	5.0	100	0	—	ns
		10	50	0		
		15	50	0	······································	
	^t DH	5.0	200 .	100		ns
		10	100	50		
		15	100	50		







MOTOROLA SEMICONDUCTORS

3501 ED BLUESTEIN BLVD., AUSTIN, TEXAS 78721

MC14099B MC14599B

8-BIT ADDRESSABLE LATCHES

The MC14099B and MC14599B are 8-bit addressable latches. Data is entered in serial form when the appropriate latch is addressed (via address pins A0, A1, A2) and write disable is in the low state. Chip enable must be high for writing into MC14599B. For the MC14599B the data pin is a bidirectional data port and for the MC14099B the input is a unidirectional write only port. The Write/Read line controls this port in the MC14599B.

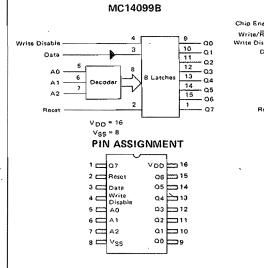
The data is presented in parallel at the output of the eight latches independently of the state of Write Disable, Write/Read or Chip Enable.

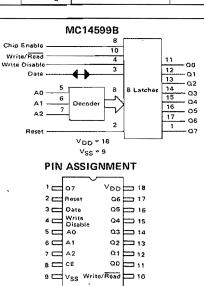
A Master Reset capability is available on both parts.

- Serial Data Input
- Parallel Output
- Low Input Capacitance 5.0 pF typical
- Master Reset
- Noise Immunity 45% of VDD typical
- Supply Voltage Range = 3.0 Vdc to 18 Vdc
- Capable of Driving Two Low-Power TTL Loads, One Low-Power Schottky TTL Load or Two HTL Loads over the Rated Temperature Range
- MC14099B pin for pin compatible with CD4099B

MAXIMUM RATINGS (Voltages referenced to VSS)

Rating	Symbol	Value	Unit
DC Supply Voltage	VDD	-0.5 to +18	Vdc
Input Voltage, All Inputs	Vin	-0.5 to V _{DD} + 0.5	Vdc
DC Current Drain per Pin	1	10	mAdc.
Operating Temperature Range – AL Device CL/CP Device	TA	-55 to +125 -40 to +85	°C
Storage Temperature Range	T _{stg}	-65 to +150	°C



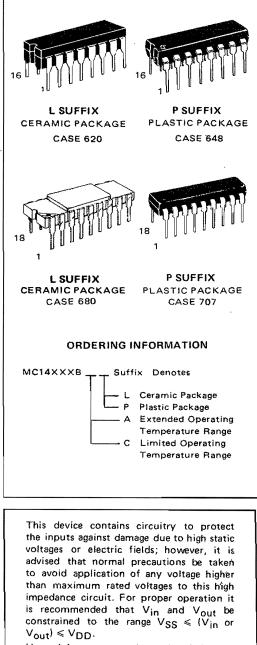


CMOS MSI

(LOW-POWER COMPLEMENTARY MOS)

8-BIT ADDRESSABLE LATCH

MC14599B WITH BIDIRECTIONAL PORT



Unused inputs must always be tied to an appropriate logic voltage level (e.g., either $V_{SS} \mbox{ or } V_{DD}).$

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ELECTRICAL CHARACTERISTICS

			VDD	'Tla				'Tiow* 25°C		25°C			gh*]
Characteristic		Symbol	Vdc	Min	Max	Min	Тур	Max	Min	Max	Unit			
Output Voltage	"O" Level	VOL	5.0		0.05		0	0.05	-	0,05	Vdc			
V _{in} = V _{DD} or 0		•-	10		0.05	_	0	0.05	-	0.05				
			15		0.05	-	0	0.05		0.05				
	"1" Level	∨он	5.0	4.95		4.95	5.0	_	4.95		Vdc			
$V_{in} = 0 \text{ or } V_{DD}$		ЧŲП	10	9.95		9.95	10	****	9.95	_				
			15	14.95		14.95	15		14,95	_				
Input Voltage#	"0" Level	VIL									Vdc			
(Vo = 4.5 or 0.5 Vdc)	O Lever	*1C	5.0	-	1.5	_	2.25	1.5		1.5	1 000			
$(V_0 = 9.0 \text{ or } 1.0 \text{ Vdc})$			10		3.0	_	4.50	3.0	_	3.0				
$(V_0 = 13.5 \text{ or } 1.5 \text{ Vdc})$			15	_	4.0	_	6.75	4.0		4.0				
	"1" Level	N/			4.0		0.70			-7.0	Vdc			
(Vo = 0.5 or 4.5 Vdc)	i Levei	VIH	5.0	3.5		25	2.75		25		vac			
÷.				7.0		3.5 7.0	5.50		3.5	-				
$(V_0 = 1.0 \text{ or } 9.0 \text{ Vdc})$			10						1	-				
$(V_0 = 1.5 \text{ or } 13.5 \text{ Vdc})$			15	11.0		11.0	8.25		11.0					
Output Drive Current (AL De	-	юн									mAd			
$(V_{OH} = 2.5 \text{ Vdc})$	Source		5.0	-3.0		-2.4	-4.2		-1.7					
(V _{OH} = 4.6 Vdc)			5.0	-0.64	-	-0.51	-0.88		-0.36					
(V _{OH} = 9.5 Vdc)			10	-1.6	-	-1.3	-2.25		~0.9					
(V _{OH} = 13.5 Vdc)			15	-4.2		-3.4	-8.8	·	-2.4					
(V _{OL} = 0.4 Vdc)	Sink	IOL	5.0	0.64		0.51	0.88	-	0.36	_	mAd			
(V _{OL} = 0.5 Vdc)			10	1.6	- 1	1.3	2.25		0.9	-				
$(V_{OL} = 1.5 Vdc)$			15	4.2	-	3.4	8.8		2.4					
Output Drive Current (CL/CF	Povice)	юн									mAd			
(VOH = 2.5 Vdc)	Source	-	5.0	-2.5		-2.1	-4.2		~1.7	·				
$(V_{OH} = 4.6 \text{ Vdc})$			5.0	-0.52		-0.44	-0.88		-0.36	_				
(V _{OH} = 9.5 Vdc)			10	-1.3	-	-1.1	-2.25		-0.9					
$(V_{OH} = 13.5 V_{dc})$			15	-3.6	-	~3.0	-8.8	_	-2.4	_				
(VOL = 0.4 Vdc)	Sink.	IOL	5.0	0.52		0.44	0.88		0.36		mAd			
$(V_{OL}^{OL} = 0.5 V dc)$		0	10	1.3		1.1	2.25		0.9	_				
(VOL = 1.5 Vdc)			15	3.6	_	3.0	8.8		2.4					
Input Current (AL Device)		lin	15		±0.1		±0.00001	±0,1	–	±1.0	μAde			
Input Current (CL/CP Device	1	lin	15		±0.3		±0.00001	±0.3		±1.0	μAde			
Input Capacitance	,						5.0	7.5			pF			
(V _{in} = 0)		Cin		-	_	-	5.0	7.5	-		pr			
Input Capacitance		Cin	_	_			15.0	22.5			pF			
MC145998-Data (pin 3)														
(V _{in} = 0)														
Quiescent Current (AL Device	e)	IDD	5.0	<u> </u>	5.0		0.005	5.0		150	μAd			
(Per Package)			10	_	10	_	0.010	10	_	300				
			15	_	20	_	0.015	20	_	600				
Quiescent Current (CL/CP De	vice)	IDD	5.0		20	-	0.005	20		150	μAd			
(Per Package)		טטי	10		40		0.000	40		300	μ Λ Ο			
h of i dokaget			15		80		0.015	80		600				
Total Supply Current**†		1_												
Dynamic plus Quiescent,		١T	5.0				5 μA/kHz)				μAd			
Per Package)			10				$0 \mu A/kHz$							
3			15			'T ⁼ (4,	.5 μΑ/kHz)	DD ידי						
(CL = 50 pF on all output	5,				,									
all buffers switching)														

 $T_{low} = -55^{\circ}C$ for AL Device, $-40^{\circ}C$ for CL/CP Device.

 $T_{high} = +125^{\circ}C$ for AL Device, +85°C for CL/CP Device.

#Noise immunity specified for worst-case input combination. Noise Margin for both "1" and "0" level =

1.0 Vdc min @ V_{DD} = 5.0 Vdc 2.0 Vdc min @ V_{DD} = 10 Vdc 2.5 Vdc min @ V_{DD} = 15 Vdc $\ensuremath{^{+}\text{To}}$ calculate total supply current at loads other than 50 pF:

 $I_T (C_L) = I_T (50 \text{ pF}) + 4 \times 10^{-3} (C_L - 50) \text{ V}_{DD} \text{f}$

where: IT is in μ A (per package), CL in pF, VDD in Vdc, and f in kHz is input frequency.

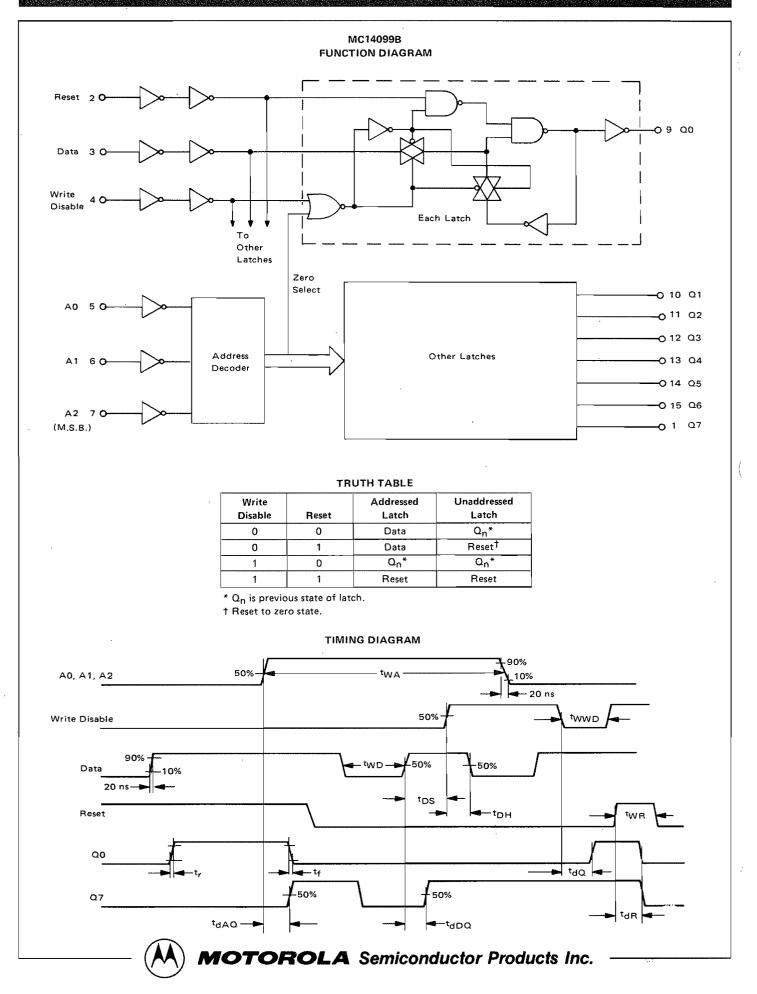
**The formulas given are for the typical characteristics only at 25° C.

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SWITCHING CHARACTERISTICS (C $_{L}$ = 50 pF, T $_{A}$ = 25°C)

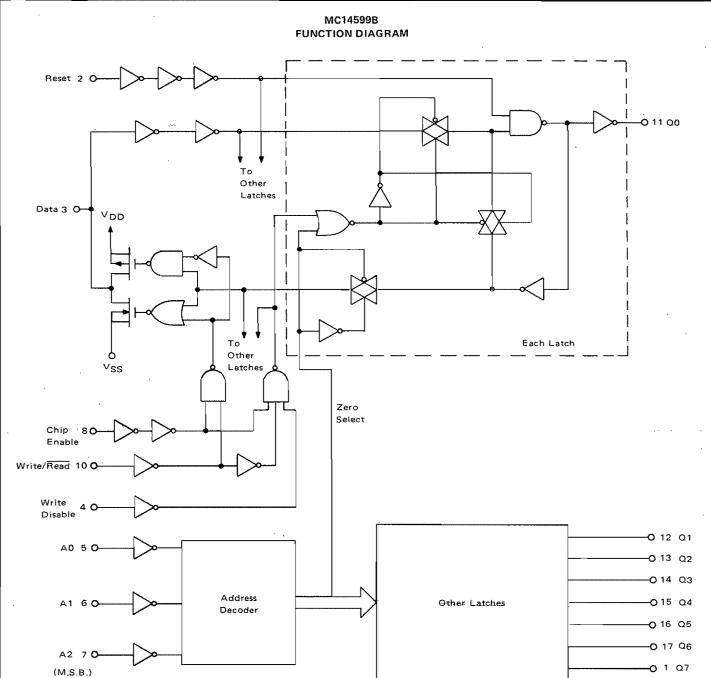
Characteristic	Symbol	V _{DD} Vdc	Min	Тур	Max	Unit
Output Rise and Fall Time	t _r , t _f					ns
t_r , $t_f = (1.35 \text{ ns/pF}) C_L + 32 \text{ ns}$		5.0		100	200	
$t_r, t_f = (0.6 \text{ ns/pF}) C_L + 20 \text{ ns}$		10	_	50	100	
$t_r, t_f = (0.4 \text{ ns/pF}) \text{ CL} + 20 \text{ ns}$		15	-	40	80	
Propagation Delay Time	DCDt					ns
Data to Output		5.0		200	400	
		10	-	75	. 150	
		15		50	100	
Write Disable to Output	t _d Q	5.0	_	200	450	ns
		10	-	80	200	
		15	-	60	150	
Reset to Output	tdR	5.0		175	350	ns
		10	_	80	160	
		15		65	130	
Address, CE to Output	^t dAQ	5.0		225	500	ns
	ur tu	10		100	230	
· · · · · · · · · · · · · · · · · · ·		15	_	75	160	
Propagation Delay Time, MC14599B only	tdED					ns
Chip Enable, Write/Read to Data	0.00	5.0	_	200	400	
		10		80	160 -	
		15	_	65	130	
Address to Data	tdAD	5.0		200	400	ns
	-0,00	10		90	180	
		15		75	150	
Minimum Pulse Widths	twp					ns
Data	-WD	5.0	200	100		
		10	100	50	<u> </u>	
		15	80	40	_	
Address	twa	5.0	400	200		ns
	-0044	10	200	100	_	
		15	125	65	_	
Reset	twr	5.0	150	75		ns
	-4044	10	75	40		
		15	50	25		
Write Disable	twwp	5.0	320	160		ns
	"WWWD	3.0 10	160	80		113
		15	120	60	_	
Set Up Time	tDS					ns
Data	าบร	5.0	100	50		115
		10	. 50	25		
		15	35	20	_	
told Time	tou		+			ns
Data	tDH	5.0	150	75		115
		10	75	40	_	
		15	50	25	_	
			50	20		

R



MC14099B • MC14599B





TRUTH TABLE

Chip Enable	Write/Read	Write Disable	Reset	Addressed Latch	Other Latches	Data Pin
0	×	×	0	*	*	Z
1	1	0	0	Data	*	Input
1	1	1	0	*	¥	Z
1	0	×	0	*	*	· Q _n
x	×	х	1	0	0	Z/0

X = Don't care.

* = No change in state of latch.

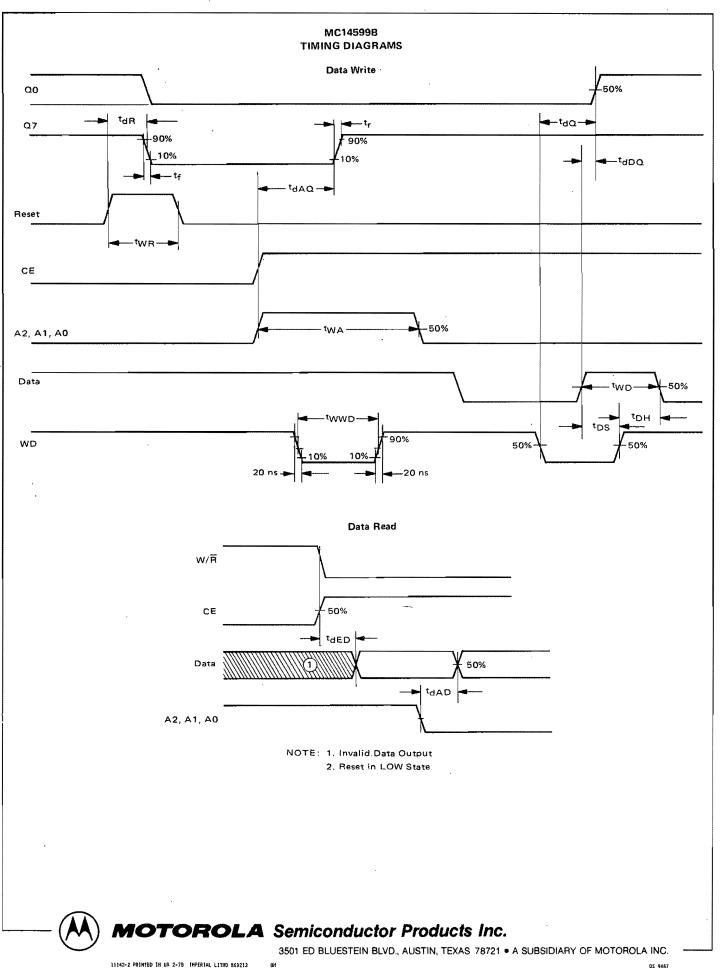
Z = High impedance.

 $Q_n =$ State of addressed latch.



MOTOROLA Semiconductor Products Inc.

MC14099B • MC14599B



11142-2 PRINTED IN UN 2-78 IMPERIAL LITHO 869213

DS 9467

intel

2758 8K (1K × 8) UV ERASABLE LOW POWER PROM

- Single + 5V Power Supply
- Simple Programming Requirements
 Single Location Programming
 Programs with One 50 ms Pulse
- Low Power Dissipation
 525 mW Max. Active Power
 132 mW Max. Standby Power

- Fast Access Time: 450 ns Max. in Active and Standby Power Modes
- Inputs and Outputs TTL Compatible during Read and Program
- Completely Static
- Three-State Outputs for OR-Ties

The Intel[®] 2758 is a 8192-bit ultraviolet erasable and electrically programmable read-only memory (EPROM). The 2758 operates from a single 5-volt power supply, has a static standby mode, and features fast single address location programming. It makes designing with EPROMs faster, easier and more economical. The total programming time for all 8192 bits is 50 seconds.

The 2758 has a static standby mode which reduces the power dissipation without increasing access time. The maximum active power dissipation is 525 mW, while the maximum standby power dissipation is only 132 mW, a 75% savings. Power-down is achieved by applying a TTL-high signal to the \overline{CE} input.

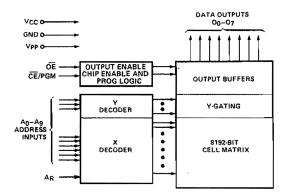
A 2758 system may be designed for total upwards compatibility with Intel's 16K 2716 EPROM (see Applications Note 30). The 2758 maintains the simplest and fastest method yet devised for programming EPROMs — single pulse TTL-level programming. There is no need for high voltage pulsing because all programming controls are handled by TTL signals. Program any location at any time — either individually, sequentially, or at random, with the single address location programming.

PIN CONFIGU	IRATION	MODE SELECTION						
A6 C 2 A5 C 3 A4 C 4 A3 C 5	24 D VCC 23 D A8 22 D A9 21 D VPP 20 D OF	PINS MODE	CE/PGM (18)	A _R (19)	<u>OE</u> (20)	V _{PP} (21)	V _{CC} (24)	OUTPUTS (9-11, 13-17)
A1 0 7		Read	V _{IL} .	VIL	VIL	+5	+5	Dour
AG [8 OG [9 O1 [10	17 D 07 16 D 06 15 D 05	Standby	V _{IH}	VIL	Don't Care	+5	+5	High Z
02 [11	14 04	Program	Pulsed VIL to VIH	VIL	VIH	+25	+5	D _{IN}
GND C 12	13 03	Program Verify	VIL	VIL	VIL	+25	+5	Dout
		Program Inhibit	ViL	VIL	VIH	+25	+5	High Z

PIN NAMES

Ao-Ag	ADDRESSES
CE/PGM	CHIP ENABLE/PROGRAM
ŌĒ	OUTPUT ENABLE
0,-0,	OUTPUTS
AR	SELECT REFERENCE

BLOCK DIAGRAM



PROGRAMMING

The programming specifications are described in the Data Catalog PROM/ROM Programming Instructions section.

Absolute Maximum Ratings*

Temperature Under Bias
Storage Temperature
All Input or Output Voltages with
Respect to Ground
V _{PP} Supply Voltage with Respect
to Ground During Programming +26.5V to -0.3V

*COMMENT: Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

READ OPERATION

D.C. and Operating Characteristics

 $T_A = 0^{\circ}C$ to $70^{\circ}C$, $V_{CC}^{[1,2]} = +5V \pm 5\%$, $V_{PP}^{[2]} = V_{CC}$

			Limits		• • • •		
Symbol	Parameter	Min.	Typ. ^[3]	Max.	Unit	Conditions	
I _{LI}	Input Load Current			10	μA	V _{IN} = 5.25V	
ILO	Output Leakage Current			10	μA	V _{OUT} = 5.25V	
IPP1 [2]	Vpp Current			5	mA	V _{PP} = 5.25V	
I _{CC1} [2]	V _{CC} Current (Standby)		10	25	mA	$\overline{CE} = V_{IH}, \overline{OE} = V_{IL}$	
Icc2 ^[2]	V _{CC} Current (Active)		57	100	mA	$\overline{OE} = \overline{CE} = V_{1L}$	
A _R ^[4]	Select Reference Input Level	-0.1		0.8	V	I _{IN} = 10 μA	
VIL	Input Low Voltage	-0.1		0.8	V	* * * * *******************************	
VIH	Input High Voltage	2.0		V _{CC} + 1	V		
VOL	Output Low Voltage			0.45	V	I _{OL} = 2.1 mA	
V _{OH}	Output High Voltage	2.4			v	I _{OH} = -400 μA	

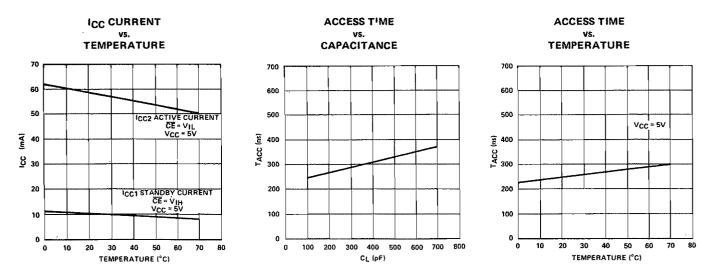
NOTES: 1. V_{CC} must be applied simultaneously or before V_{PP} and removed simultaneously or after V_{PP}.

2. Vpp may be connected directly to V_{CC} except during programming. The supply current would then be the sum of I_{CC} and Ipp1.

3. Typical values are for $T_A = 25 \,^{\circ}$ C and nominal supply voltages.

4. A_R is a reference voltage level which requires an input current of only 10 μA. The 2758 S1865 is also available which has a reference voltage level of V_{IH} instead of V_{IL}.

Typical Characteristics



A.C. Characteristics

Symbol	-		Limits			
	Parameter	Min.	Typ. ^[3]	Max.	Unit	Test Conditions
tACC	Address to Output Delay		250	450	ns	$\overline{CE} = \overline{OE} = V_{1L}$
tCE	CE to Output Delay		280	450	ns	OE = VIL
t _{OE}	Output Enable to Output Delay			120	ns	$\overline{CE} = V_{IL}$
t _{DF} '	Output Enable High to Output Float	0		100	ns	CE = VIL
t _{OH}	Output Hold From Addresses, CE or OE Whichever Occurred First	0			ns	$\overline{CE} = \overline{OE} = V_{IL}$

 $T_A = 0^{\circ}C$ to $70^{\circ}C$, $V_{CC}^{[1]} = +5V \pm 5\%$, $V_{PP}^{[2]} = V_{CC}$

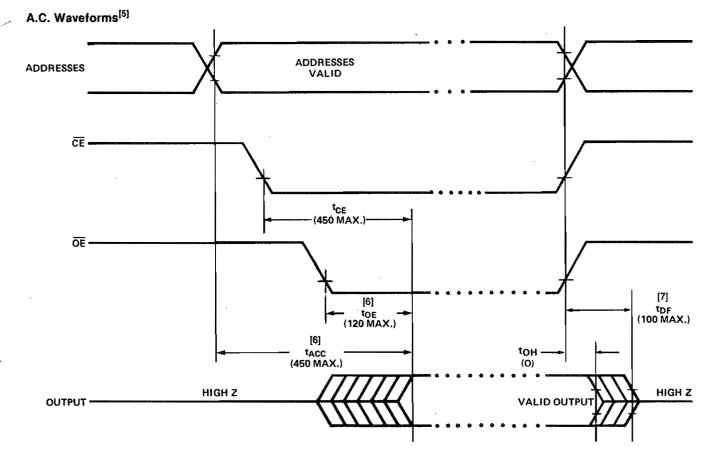
Capacitance^[4] $T_A = 25 \degree C$, f = 1 MHz

Symbol	Parameter	Тур.	Max.	Unit	Conditions
CIN	Input Capacitance	4	6	pF	V _{IN} = 0V
COUT	Output Capacitance	8	12	pF	V _{OUT} = 0V

NOTE: Please refer to page 2 for notes.

A.C. Test Conditions:

Output Load: 1 TTL gate and C_L = 100 pF Input Rise and Fall Times: ≤20 ns Input Pulse Levels: 0.8V to 2.2V Timing Measurement Reference Level: Inputs 1V and 2V Outputs 0.8V and 2V



NOTES: 1. V_{CC} must be applied simultaneously or before Vpp and removed simultaneously or after Vpp.

2. Vpp may be connected directly to VCC except during programming. The supply current would then be the sum of ICC and Ipp1.

3. Typical values are for $T_A = 25 \,^{\circ}$ C and nominal supply voltages.

4. This parameter is only sampled and is not 100% tested.

All times shown in parentheses are minimum times and are nsec unless otherwise specified.
 OE may be delayed up to 330 ns after the falling edge of CE without impact on t_{ACC}.

7. tDF is specified from OE or CE, whichever occurs first.

ERASURE CHARACTERISTICS

The erasure characteristics of the 2758 are such that erasure begins to occur when exposed to light with wavelengths shorter than approximately 4000 Angstroms (Å). It should be noted that sunlight and certain types of fluorescent lamps have wavelengths in the 3000-4000Å range. Data show that constant exposure to room level fluorescent lighting could erase the typical 2758 in approximately 3 years, while it would take approximately 1 week to cause erasure when exposed to direct sunlight. If the 2758 is to be exposed to these types of lighting conditions for extended periods of time, opaque labels are available from Intel which should be placed over the 2758 window to prevent unintentional erasure.

The recommended erasure procedure (see Data Catalog Programming Section) for the 2758 is exposure to shortwave ultraviolet light which has a wavelength of 2537 Angstroms (Å). The integrated does (i.e., UV intensity X exposure time) for erasure should be a minimum of 15 W-sec/cm². The erasure time with this dosage is approximately 15 to 20 minutes using an ultraviolet lamp with 12,000 μ W/cm² power rating. The 2758 should be placed within 1 inch of the lamp tubes during erasure. Some lamps have a filter on their tubes which should be removed before erasure,

DEVICE OPERATION

The five modes of operation of the 2758 are listed in Table 1. It should be noted that all inputs for the five modes are at TTL levels. The power supplied required are a +5V V_{CC} and a V_{PP} . The V_{PP} power supply must be at 25V during the two programming modes, and must be at 5V in the other three modes. In all operational modes, A_R must be at V_{IL} (except for the 2758 S1865 which has A_R at V_{IH}).

PINS	CE/PGM (18)	A _R (19)	OE (20)	V _{PP} (21)	V _{CC} (24)	OUTPUTS (9-11, 13-17)
Read	VIL	VIL	VIL	+5	+5	Dour
Standby	VIH	ViL	Don't Care	+5	+5	High Z
Program	Pulsed VIL to VIH	VIL	VIH	+25	+5	D _{IN}
Program Verify	VIL	VIL	VIL	+25	+5	DOUT
Program Inhibit	ViL	V _{IL}	ViH	+25	+5	High Z

READ MODE

The 2758 has two control functions, both of which must be logically satisfied in order to obtain data at the outputs. Chip Enable (\overline{CE}) is the power control and should be used for device selection. Output Enable (\overline{OE}) is the output control and should be used to gate data to the output pins, independent of device selection. Assuming that addresses are stable, address access time (t_{ACC}) is equal to the delay from \overline{CE} to output (t_{CE}). Data is available at

the outputs 120 ns (t_{OE}) after the falling edge of \overline{OE} , assuming that \overline{CE} has been low and addresses have been stable for at least $t_{ACC} - t_{OE}$.

STANDBY MODE

The 2758 has a standby mode which reduces the active power dissipation by 75%, from 525 mW to 132 mW. The 2758 is placed in the standby mode by applying a TTL high signal to \overline{CE} input. When in standby mode, the outputs are in a high impedence state, independent of the OE input.

OUTPUT OR-TIEING

Because EPROMs are usually used in larger memory arrays, Intel has provided a 2 line control function that accommodates this use of multiple memory connections. The two line control function allows for:

- a) the lowest possible memory Power dissipation, and
- b) complete assurance that output bus contention will not occur.

To most efficiently use these two control lines, it is recommended that \overline{CE} (pin 18) be decoded and used as the primary device selecting function, while \overline{OE} (pin 20) be made a common connection to all devices in the array and connected to the READ line from the system control bus. This assures that all deselected memory devices are in their low power standby mode and that the output pins are only active when data is desired from a particular memory device.

PROGRAMMING

Initially, and after each erasure, all bits of the 2758 are in the "1" state. Data is introduced by selectively programming "0's" into the desired bit locations. Although only "0's" will be programmed, both "1's" and "0's" can be presented in the data word. The only way to change a "0" to a "1" is by ultraviolet light erasure.

The 2758 is in the programming mode when the V_{PP} power supply is at 25V and \overline{OE} is at V_{IH} . The data to be programmed is applied 8 bits in parallel to the data output pins. The levels required for the address and data inputs are TTL.

When the address and data are stable, a 50 msec, active high, TTL program pulse is applied to the \overline{CE}/PGM input. A program pulse must be applied at each address location to be programmed. You can program any location at any time – either individually, sequentially, or at random. The program pulse has a maximum width of 55 msec.

The 2758 must be programmed with a DC signal applied to the \overline{CE}/PGM input.

Programming of multiple 2758s in parallel with the same data can be easily accomplished due to the simplicity of the programming requirements. Like inputs of the parallelled 2758s may be connected together when they are programmed with the same data. A high level TTL pulse applied to the \overline{CE}/PGM input programs the paralleled 2758s.

PROGRAM INHIBIT

Programming of multiple 2758s in parallel with different data is also easily accomplished. Except for \overline{CE}/PGM , all like inputs(including \overline{OE}) of the parallel 2758s may be common. A TTL level program pulse applied to a 2758's \overline{CE}/PGM input with V_{PP} at 25V will program that 2758. A low level \overline{CE}/PGM input inhibits the other 2758 from being programmed.

PROGRAM VERIFY

A verify should be performed on the programmed bits to determine that they were correctly programmed. The verify may be performed with V_{PP} at 25V. Except during programming and program verify, V_{PP} must be at 5V.

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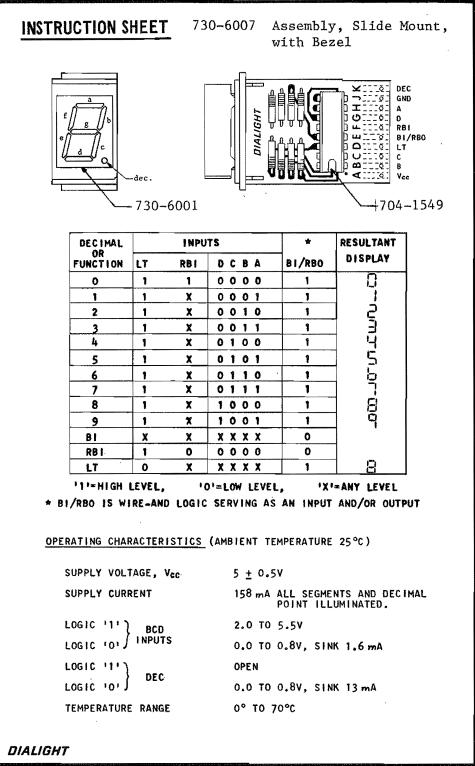
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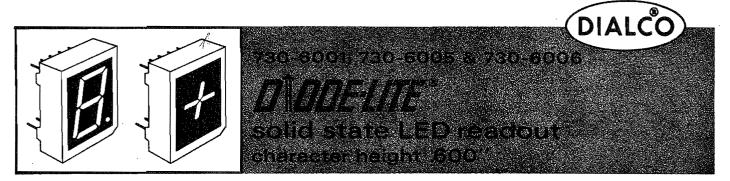
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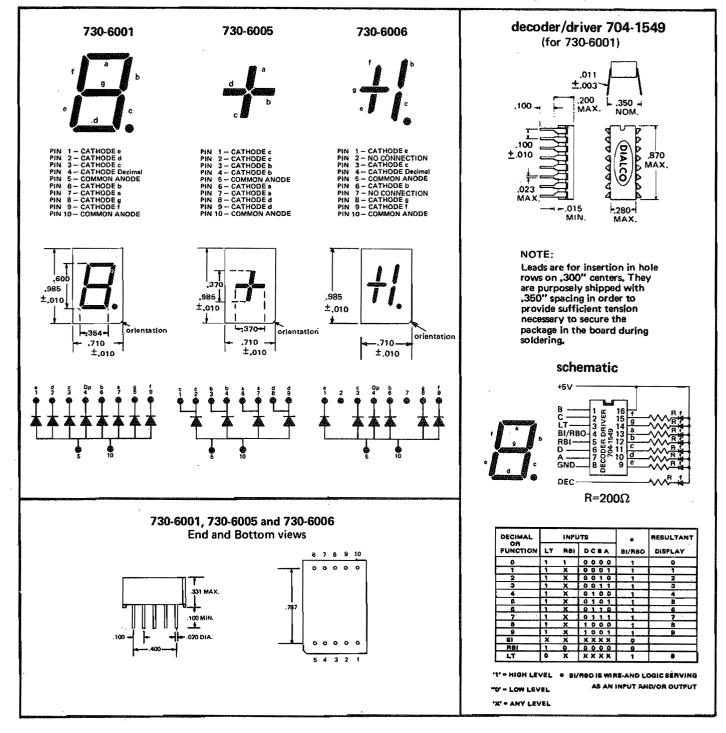
Fleid application location These representatives do not offer Intel Components, only boards and systems.





Features

- GaP Red LED
- Large Character .600"
- Common Anode Construction
- Seven Segment Format with Decimal Point
- Wide Viewing Angle, Single Plane Viewing
- Solid State Reliability
- Low Power Requirement, Typically 10mA per Segment
- Each Unit checked for uniformity of elements
- Package combines Filter for Contrast Enhancement
- Compact Package Design maximizes Package Density



operating specifications

Maximum ratings at 25°C ambient temperature

3 V
600 mW
450 mW
20°C to 75°C
260°C @ 0.1" from seating plane

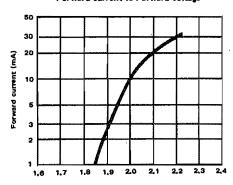
Note: Derate linearly to 75°C at the rate of 0.34 mA/°C,

Operating characteristics of each segment at 25°C ambient temperature

	PARAMETER	TEST CONDITIONS	ТҮР	MAX	UNIT
IV	Luminous Intensity		300		μcd
VF	Static Forward Voltage	1	2.0	2.8	v
λpeak	Peak Wavelength	IF=10mA	700		nm
ΒŴλ	Spectral Bandwidth between Half-Power Points		200		nm
С	Capacitance	V=0, F=1 MHz	100		pF
IR	Static Reverse Current	V _R =3V		10	μA

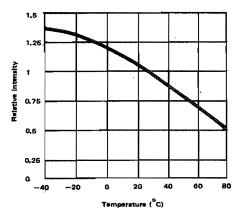
Recommended Cleaning Solution - Isopropanol





Forward voltage (V)

Relative intensity vs Temperature



Relative intensity vs Forward current

1

