FM BROADCAST SOLID STATE EXCITER


## INSTRUCTION MANUAL



## RECORD OF CHANGES - 802A

## CHANGE NO.

DATE

## EFFECTIVITY

1

2
3

14 November 1983
10 July 1984
27 May 1985

All Transmitters
SN 240 and Above
All Transmitters

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## SECTION 1 - GENERAL INFORMATION

1-1. GENERAL

The Continental Electronics Type 802A FM Exciter (Figure 1-1) is a solid state, synthesized phase locked FM Exciter which provides FM output over the 87 MHz to 109 MHz frequency range in 10 KHz increments. The output frequency is selectable in BCD code on DIP rocker switches. Power output is adjustable from 5 watts to 50 watts.

Designed primarily as a driver for higher power transmitters, the 802 A may also be used as a stand alone 50 watt transmitter.

The 802A is supplied with a balanced monophonic input, a balanced composite input and two balanced SCA inputs. The inputs may be driven from balanced or unbalanced sources.

The 802A is designed to mount in a standard 19 inch ( 483 mm ) rack. Equipment slides are furnished with the exciter.

Table 1-1 lists the technical characteristics of the Type 802A FM Exciter. Figure $1-2$ is a simplified block diagram of the exciter.


83-0655

Figure 1-1. Type 802A FM Exciter
1-2


1-2. EQUIPMENT REQUIRED OR SUGGESTED BUT NOT FURNISHED (OPTIONAL)
Recommended Semiconductor Spares Kit - 643-0055-002
100\% Semiconductor Spares Kit - 643-0055-001
Blank Panels per customer rack.

## TABLE 1-1. TECHNICAL CHARACTERISTICS

| ELECTRICAL DATA - |  |
| :---: | :---: |
| Input Power: | 115 V or $230 \mathrm{~V} \pm 10 \%$; $50 / 60 \mathrm{~Hz} \pm 5 \%$; single phase, 200 W . maximum |
| Power Output: | 5 to 50 W , continuously adjustable |
| RF Harmonic \& Spurious: | 60 dB or more below rated output |
| Frequency Range: | 87 to 109 MHz in 10 kHz steps |
| Frequency Control: | pLL Frequency Synthesis from high stability master oscillator |
| Frequency Stability: | $\pm 250 \mathrm{~Hz}, 0^{\circ}$ to $55^{\circ} \mathrm{C}$. |
| Modulation Type: | Direct carrier frequency modulation |
| Modulation Indication: | Peak reading LED display with overmodulation indicator |
| Asynchronous AM S/N: | 73 dB minimum, relative to carrier level |
| Synchronous AM S/N: | 60 dB minimum, relative to carrier level |
| WIDEBAND OPERATION - |  |
| Composite Inputs: | Balanced and Test |
| Composite Input Inpedance: | 5 k ohms, nominal |
| Composite Input Level: | 1.25 V RMS (3.54 volts peak to peak) for $\pm 75 \mathrm{kHz}$ deviation |
| Composite Amplitude Response: | $\pm 0.1 \mathrm{~dB}, 20 \mathrm{~Hz}$ to 100 kHz |
| Composite Phase Response: | $\pm 0.5^{\circ}, 20 \mathrm{~Hz}$ to 100 Hz |
| Composite Total Harmonic Distortion: | 0.08\% maximum |

TABLE 1-1. TECHNICAI CHARACTERISTICS - Cont.

WIDEBAND OPERATION - Cont.
Composite Intermodulation $0.08 \%$ maximum; $60 \mathrm{~Hz} / 7 \mathrm{kHz}$,
Distortion: ..... 4:1 ratio
Composite Transient IMD: $0.1 \%$ maximum
Composite $F M$ S/N RATIO: $\quad 75 \mathrm{~dB}$ minimum below $\pm 75 \mathrm{kHz}$deviation
SCA Inputs: Two, balanced
SCA Input Impedance: 50,000 ohms, nominal
SCA Input Level: $\pm 1.25 \mathrm{~V}$ RMS for $\pm 75 \mathrm{kHz}$ deviation
SCA Amplitude Response: ..... $\pm 0.3 \mathrm{~dB}, 40 \mathrm{kHz}$ to 100 kHz
MONAURAL OPERATION -
Audio Input Impedance: 600 ohms, balanced
Audio Input Return Loss: $30 d B$ or better
Audio Input Level: $\quad \pm 10 \mathrm{dBm}(6.93$ volts peak to peak@ 600 ohms) for $\pm 75 \mathrm{kHz}$ deviationAudio Frequency Response: $\pm 0.5 \mathrm{~dB}$; flat, 25,50 or $75 \mu \mathrm{sec}$pre-emphasis 20 Hz to 15 kHz
Total Harmonic Distortion: $0.08 \%$ maximum; 20 Hz to 15 kHz
Intermodulation Distortion: $0.08 \%$ maximum; $60 \mathrm{~Hz} / 7 \mathrm{kHz}$,4:1 ratio
Transient IMD: $0.1 \%$ maximum
FM S/N Ratio: 75 dB minimum below $\pm 75 \mathrm{kHz}$ deviation

TABLE 1-1. TECHNICAL CHARACTERISTICS - Cont. PHYSICAL DATA -

| Temperature Range: | $0^{\circ} \mathrm{C}$. to $55^{\circ} \mathrm{C}$. $\left(32^{\circ} \mathrm{F}\right.$. to $\left.131^{\circ} \mathrm{F}.\right)$ |
| :---: | :---: |
| Altitude Range: | 0 to 4600 M ( 0 to $15,100 \mathrm{ft}$. |
| Relative Humidity Range: | 0 to 95\% |
| Size: | 17-1/2" wide(444.5 mm) centered in |
|  | a 19 inch wide ( 483 mm ) rack- |
|  | mounting panel; 5-1/4" (133.35 mm) |
|  | high; 22" ( 558.8 mm ) deep |
| Weight: | approximately $31.5 \mathrm{lbs} .(14.3 \mathrm{~kg}$ ) |
|  | shipping: approx. $36 \mathrm{lbs} .(16.5 \mathrm{~kg}$ ) |

TABLE 1-2. RECOMMENDED SEMICONDUCTOR SPARES LIST

| REFERENCE DESIGNATOR | DESCRIPTION | PART NUMBER | QTY <br> USED | $\begin{gathered} \text { MIN. } \\ \text { RECOM } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| - | Recommended Spares Kit | 643-0055-002 |  | X |
| - | 100\% Spares Kit | 643-0055-001 | X |  |
| A5VR2 | Zener Diode, ln4753A | 353-6481-510 | 1 | 1 |
| A6DSl, 2 | Bar Graph Array HDSP-4840 | 262-5008-010 | 2 | 2 |
| ARIQ1 | Xstr, MJ3001 | 352-5016-010 | 1 | 1 |
| CR1 | Rectifier, MDA 2504 | 353-5017-010 | 1 | 1 |
| ARIAlQ3 | Xstr., MRF 315A | 352-5016-020 | 1 | 1 |
| ARIAlQ2 | Xstr., PT9732 | 352-4009-010 | 1 | 1. |
| ARIAlQl | Xstr., 2N3553 | 352-0632-010 | 1 | 1 |
| A7VRI | Diode, ln4728A | 353-6481-010 | 1 | 1 |
| A6U4 | I.C., LM555CN | 351-1140-010 | 1 | 1 |
| A6U2, 3 | I.C., LM3914N | 351-4709-010 | 2 | 1 |
| A2DSl, 2 | L.E.D. Grn. | 353-0293-010 | 6 | 2 |
| $\begin{array}{ll} \text { A3DS } 1, & 2 \\ \text { A6DS6, } & 7 \end{array}$ |  |  |  |  |
| A6DS3, 4, 5 | L.E.D. Red | 353-9293-040 | 3 | 1 |
| AlAlQ3, 4 | Xstr. 2N5l09 | 352-9863-920 | 2 | 1 |
| AlAlQ1, 2 | Xstr, U310 | 352-4005-000 | 2 | 1 |
| $\begin{aligned} & \text { AlAlCR7, } 8 \\ & \text { A6CRl-3 } \\ & \text { ARIAlCR1, } 2 \end{aligned}$ | Diode, 5082-2800 | 353-9448-020 | 7 | 4 |
| AlAlCRI-4 | Varactor, KV2801 | 922-8004-010 | 4 | 4 |
| A4U3 | I.C., UA 7805 KC | 351-1120-080 | 1 | 1 |
| $\begin{aligned} & \text { AlAlUl, } \\ & \text { A4U2 } \end{aligned}$ | I.C., LM317T | 351-1271-010 | 2 | 1 |
| A4Ul | I.C., LM377T | 351-1345-030 | 1 | 1 |

TABLE l-2. RECOMMENDED SEMICONDUCTORS SPARES LIST

| A5VR1 | Zener, 1N4752A | 353-6481-490 | 1 | 1 |
| :---: | :---: | :---: | :---: | :---: |
| A5U2 | I.C., UA723PC | 351-1035-060 | 1 | 1 |
| A 51 | Xstr., 2N6401 | 352-4008-010 | 1 | 1 |
| A 4CR5 | Diode, 3N256 | 352-5015-010 | 1 | 1 |
| A 3 VRl, 2 | Zener, 1N4739A | 353-6481-230 | 2 | 1 |
| A3U11 | I.C., UA 79150 C | 351-1124-160 | 1 | 1 |
| A 3010 | I.C., UA7815UC | 351-1120-050 | 1 | 1 |
| $\begin{aligned} & \text { A } 309, \\ & \text { A } 6 \mathrm{Ul} \end{aligned}$ | I.C., LF347N | 351-1370-020 | 2 | 1 |
| A308 | I.C., 4 N 28 | 351-0047-030 | 1 | 1 |
| A 3U6, |  |  |  |  |
| A5Ul, 3 | I.C., LM358N | 351-1211-040 | 3 | 1 |
| A3U3, 4 | I.C., CLM-51 | 352-4010-010 | 3 | 1 |
| A 3 U 2 | I.C., LF353N | 351-1370-040 | 1 | 1 |
| A 301 | I.C., MCl4568BCP | 351-8883-010 | 1 | 1 |
| $\begin{aligned} & \text { CR2,3 } \\ & \text { AlAlCR5, } 6 \\ & \text { A3CR3-6 } \\ & \text { A4CR1-4, } \\ & \end{aligned}$ | Diode, 1 N4005 | 353-6442-050 | 14 | 10 |
| $\begin{aligned} & \text { A2CR1, } 2 \\ & \text { A3CR1, } 2,7-11 \\ & \text { ASCR1-4 } \\ & \text { A6CR4-7 } \end{aligned}$ | Diode, 1N4148 | 353-3763-010 | 17 | 10 |
| A 2010 | I.C., SN74LS90N | 351-1711-650 | 1 | 1 |
| A2U9 | I.C., SN47LS93N | 351-1171-060 | 1 | 1 |
| A2U8 | I.C., SN74121N | 351-1187-010 | 1 | 1 |
| A 207 | I.C., SN7420N | 351-1548-090 | 1 | 1 |
| A 203-6 | I.C., SN74LS190N | 351-1171-010 | 4 | 2 |

TABLE 1-2. RECOMMENDED SEMICONDUCTORS SPARES LIST

| A2U2, | I.C., SN74LS74AN | $351-1710-020$ | 2 | 1 |
| :--- | :--- | :--- | :--- | :--- |
| A3U5 |  |  |  |  |
| A2U1 | I.C., MCl2011P | $351-4708-010$ | 1 | 1 |
| A12Q1-4, | XSTR., 2N2222A | $352-0661-020$ | 8 | 4 |
| A3Q1, 2 |  |  |  |  |
| A5Q1 |  |  |  |  |
| A6Q1 |  |  |  |  |

2-1. INSTALLATION PROCEDURE

1. Remove crating and packing material and inspect for shipping damage.
2. Remove top cover and inspect for shipping damage, loose connectors, etc.
3. The 802 A is shipped from the factory set for operation at 120 VAC unless directed otherwise by the customer. If operation at another line voltage is desired, pull the line voltage selector card (Figure 2-1) from the AC line connector and insert so that the desired voltage is visible on the card. If the line voltage is 220 or 240 VAC , replace the 3 ampere fuse in the AC line voltage connector with a 1.5 ampere fuse.
4. The 802 A is shipped from the factory set to the customer's operating frequency. If the operating frequency was not specified, the 802 A will be shipped set to 98.1 MHz . Refer to sections 5-2 and 5-3 for instructions when the frequency is to be changed.
5. The 802 A is shipped from the factory with $75 \mu \mathrm{sec}$ preemphasis on the monophonic input unless directed otherwise by the customer. Flat, $25 \mu \mathrm{sec}$ or $50 \mu \mathrm{sec}$ may also be selected. Refer to Section 5-3.
6. Mount detachable halves of the 802 A equipment slides in the equipment rack where the 802 A is to be located and insert 802A into the slides.
7. Connect RF output, modulating signal lines, etc. Refer to Figure 2-2.
8. Place the mono/composite toggle switch in the desired position.

## ON

## POWER

LINE VOLTAGE SELECTOR $120 / 240 \mathrm{~V}, 50 / 60 \mathrm{HZ}$ $3 \mathrm{~A} / 1.5 \mathrm{~A}$ S.B. FUSE

83.0571

```
Below 110 VAC
110 - 130 VAC
Below 220 VAC
220 - 250 VAC
```

100 V

100 V
120 V
220 V
240 V
9. Terminate the RF output in a 50 ohm load (50 watt rating) and set FOWER switch to ON. The POWER LED on the front panel will illuminate. After approximately 5 seconds, the AFC LED will illuminate and the forward power meter will indicate power output. Output power may be adjusted through the hole in the top cover. Verify the multimeter indications by checking against the factory test data sheets shipped with the 802A. Verify proper carrier frequency with the station frequency monitor.


Figure 2-2. Type 802A Connections

## SECTION 3 - OPERATION

3-1. CONTROLS AND INDICATORS
Table 3-1 describes the 802A operating features as shown in Figure 3-1. Figure 3-2 shows the location of the 802A major subassemblies.

3-2. OPERATING PROCEDURES

The 802A is placed in operation as follows:

1. Set Power switch to ON. The Power indicator LED will illuminate immediately. (The Power Switch may be left in the ON position and the exciter energized externally by filament auxiliary contacts or other means if desired.)
2. After a few seconds the AFC indicator LED will illuminate.
3. Verify programming by observing the modulation bar graph.
4. Verify Power output and proper load by noting Forward and Reflected power and the absence of VSWR indicator illumination.
5. Check meter readings.
a. The +22 V should read $22 \mathrm{~V} \pm 1.5 \mathrm{~V}$
b. The -22 V should read $22 \mathrm{~V} \pm 1.5 \mathrm{~V}$
c. The +5 V should read $5 \mathrm{~V} \pm 0.2 \mathrm{~V}$
d. AFC voltage is a function of operating frequency. Table 3-2 gives typical values. Refer to the factory test data for value applicable to a particular exciter. e. Amplifier voltage and current is a function of frequency and power output. Table 3-3 gives typical values. Refer to factory test data for values applicable to a particular exciter.
6. To turn the 802A OFF, simply place the Power Switch in the OFF position. There are no circuits (such as crystal ovens) in the 802 A that require standby power.

甘Z08
LW1-1(13)
Figure 3-1. Operating Controls \& Indicators

TABLE 3-1. OPERATING CONTROLS

| ITEM | DESCRIPTION |
| :---: | :---: |
| 1 | ANALOG METER |
| 2 | DIGITAL MULTIMETER |
| 3 | TOGGLE SWITCH |
| 4 | TOGGLE SWITCH |
| 5 | PUSH-PUSH SWITCH |
| 6 | PUSH-PUSH SWITCH |
| 7 | MULTIMETER SWITCH |
| 8 | PUSH-PUSH SWITCH |
| 9 | PUSH-PUSH SWITCH |
| 10 | BARGRAPH DISPLAY |
| 11 | GREEN LED |
| 12 | GREEN LED |

## FUNCTION

Monitors Forward or Reflected RF Power

Displays Voltage or Current selected
Turns on Power (Located on rear)
Enables Pre-emphasized Mono Input (Located on rear)

Selects Forward or Reflected (when depressed) for display on Item 1.

Mutes Power Output when depressed
Selects Power Amplifier Collector voltage, Power Amplifier Current, $+22 \mathrm{~V},-22 \mathrm{~V},+5 \mathrm{~V}$ or AFC voltage for display on Item 2. The switch positions are mechanically interlocked.

Selects bar or dot (when depressed) display mode on Item 10.

Selects 115\% (5\% increments) or $20 \%$ (1\% increments) scale for display on Item 10. The $20 \%$ scale (when switch is depressed) may be used to set SCA or pilot level.

20 segment display that monitors composite signal level to modulated oscillator. Calibrated in percent modulation.

Illuminates to indicate power is ON
Illuminates to indicate AFC loop is locked and exciter is on frequency

TABLE 3-1. OPERATING CONTROLS - Cont.

| 13 | RED LED | Illuminates to indicate high VSWR <br> condition at output. |
| :--- | :--- | :--- |
| 14 | RED LED | Illuminates to indicate over temper- <br> ature condition on Power Amplifier. |
| 16 | BNC JACK | Provides sample of RF output. May <br> be used to drive a frequency <br> counter, etc. |
| 17 | BNC JACK JACK | Composite input provided for test <br> convenience. |
| 18 | POTENTIOMETER | Provides sample of composite signal <br> to modulated oscillator for test <br> purposes. |



TABLE 3-2. TYPICAL AFC VOLTAGE vs FREQUENCY

| Fo MHz | AFC VOLTAGE |
| :---: | :---: |
| 87 | 3.5 |
| 88 | 4.0 |
| 89 | 4.4 |
| 90 | 4.9 |
| 91 | 5.4 |
| 92 | 5.9 |
| 93 | 6.4 |
| 94 | 6.9 |
| 95 | 7.4 |
| 9.6 | 8.0 |
| 97 | 8.7 |
| 98 | 9.7 |
| 99 | 11.0 |
| 100 | 5.7 |
| 101 | 6.1 |
| 102 | 6.5 |
| 103 | 6.9 |
| 104 | 7.3 |
| 105 | 7.7 |
| 106 | 8.1 |
| 107 | 8.7 |
| 108 | 9.2 |
| 109 | 10.0 |

TABLE 3-3. TYPICAL AMPLIFIER VOLTAGE AND CURRENT
FREQUENCY POWER OUTPUT COLLECTOR VOLTAGE COLLECTOR CURRENT (Amps)
88.1 MHz 5

10
15
20
25
30
35
40
45
50
98.1 MHz 5

10
15
20
25
30
35
40
45
50
107.9 MHz 5

10
15
20
25
30
35
40
45
50
8.6
1.03
10.9
1.54
12.7
1.95
14.4
2.31
15.9
2.62
17.4
2.92
18.8
3.20
20.1
3.44
21.5
3.71
22.7
3.94
8.4
.98
11.1
1.49
13.3
1.89
15.2
2.23
16.9
2.51
18.5
2.78
20.0
3.01
21.4
3.23
22.9
3.45
24.4
3.65
9.7
.90
13.4
1.37
16.1
1.73
18.5
2.03
20.6
2.30
22.6
2.54
24.5
2.75
26.4
2.94
28.5
3.12
30.4
3.27

3-7

## SECTION 4 - THEORY OF OPERATION

This section describes the theory of operation of the 802A FM Exciter. A description of each functional circuit is followed by a more detailed description of each subassembly.

## 4-1. FUNCTIONAL DESCRIPTION

The 802A is described in terms of five functional circuit blocks. These are the AFC, Audio, Amplifier and Power Output Control, Power Supply and Metering Circuits. The following paragraphs provide a brief description of each functional circuit along with simplified diagrams where applicable.

4-1.1 AFC CIRCUITS

The Automatic Frequency Control circuits are comprised of the Modulated Oscillator Assembly (A1), Frequency Divider Assembly (A2) and the AFC loop filter portion of the Audio/AFC Assembly (A3). Figure 4-1 is a simplified diagram of the AFC circuitry. Figure 4-2 shows the location of these assemblies in the 802A.

The heart of the AFC system is the Modulated Oscillator Assembly. This assembly is comprised of an FET operated as a Hartley oscillator. Two pairs of varactor diodes are utilized. One pair (CR1 \& CR2) is utilized for the AFC tuning voltage. The other pair (CR3 \& CR4) is used for modulation and biased with a DC voltage. The DC bias voltage is changed at 100 MHz to optimize the AFC tuning voltage range. The modulated oscillator board is mounted in a rigid box and shock mounted to minimize susceptibility to vibration. The modulated oscillator has two outputs, one is used to drive the Power Amplifier (approximately 20 MW ) and the other drives the Frequency Divider (approximately 10 MW ).

The Frequency Divider (A2) contains the frequency divider chain which divides the carrier frequency down to the phase comparison frequency of 625 Hz and the 10 MHz Reference Oscillator and its frequency divider chain. The carrier frequency is first applied to High Frequency Counter U1 which divides the carrier frequency by eight. The carrier frequency is further divided by two via flip-flop $U 2$ and applied to the $B C D$ programmable frequency counter comprised of decade counters U3, U4, U5 and U6 and NAND gate U7. The counter may be programmed in 10 KHz increments to any frequency in the 87 to 109 MHz frequency range (divided by 8700 to 10900 ) by means of DIP Rocker switches, located on the frequency divider assembly. The output of each counter
is applied to the clock input of the succeeding counter. The maximum/minimum count signal of each decade counter is sensed and applied to NAND gate U7. When all four counters reach maximum/ minimum count simultaneously, the output of $U 7$ will go low. This signal is used to load the programmed count into the decade counters and the count sequence will then start again. The signal is also applied to one shot $U 8$ which is used to stretch the very narrow pulse output of $U 7$ to an approximately $50 \%$ duty cycle 625 Hz signal. The signal is applied to the AFC loop phase comparator located on the Audio/AFC Assembly. The inverse of the $625 \mathrm{~Hz}(\overline{625} \mathrm{~Hz})$ is rectified and used to drive VCO activity monitor DS1 via Q1 and Q2. DS1 will go out should the modulated oscillator or divider chain fail. The $\overline{625} \mathrm{~Hz}$ is also routed to the Audio/AFC Assembly for use in the AFC loss of lock circuits. The 100 MHz command to the programmable counter is also routed to the Audio/AFC assembly and used to change the bias on one pair of the Modulated Oscillator varactor tuning diodes. The 10 MHz reference oscillator is divided by 16 by U9 and further divided by 10 via Ul0. The 62.5 KHz output is routed to the AFC phase comparator located on the Audio/AFC Assembly and is also rectified and used to drive the Reference Oscillator activity monitor DS2. DS2 will go out should the Reference Oscillator or its divider chain fail.

The Audio/AFC Assembly, in addition to the audio circuits, contains the AFC phase comparator, loop filter, lock detector and Modulated Oscillator bias circuits. Ul comprises the AFC phase comparator. The 62.5 KHz reference signal is further divided by one hundred by Ul and compared against the 625 Hz signal from the Modulated Oscillator divider chain. The output of $U 1$ will be high if the carrier frequency is higher than the reference frequency and low if the carrier frequency is lower than the reference frequency. If the carrier and reference frequency are the same, but different in phase, the output of Ul will be high for the time equal to the phase difference if the carrier leads the reference and low for the time equal to the phase difference if the carrier lags the reference frequency phase. If the carrier and reference frequency are the same frequency and in phase, the output of $U 1$ will be 2.5 volts. The output of the phase comparator is applied to the AFC loop active filter comprised of integrator $U 2 A$ and the 9.5 Hz Butterworth filter U2B. This high degree of filtering is necessary to remove the 625 Hz comparison frequency from the filter output. The loop filter output is then a DC voltage which will vary between 2.5 and 11.5 volts depending on frequency.



The AFC lock detection function is accomplished by flipflop U5. An output from phase comparator U1 and the 625 Hz signal are compared in U5. The output from U1 is high if the carrier and reference frequency are in phase. The $\bar{Q}$ output will be low. If the carrier and reference frequency are not in phase, the output from U1 will go low for a length of time equal to the phase difference. Since the inverted 625 Hz is applied to the lock detector U5, when the time that the U1 output is low exceeds $90^{\circ}$ the $\bar{Q}$ output of $U 5$ will go high. This high signal is applied through the fast charge/ slow discharge circuit formed by CR2, R17, R18 and C2 to lock driver U6. The output of U 6 is used to mute the power amplifier output and extinguish the front panel AFC LED (via Q1 and Q2). The output of U6 is also used to drive optically coupled variable resistors $U 3$ and U4. These resistors decrease in value when loss of lock is detected to speed up the loop filter response and decrease the amount of time required to achieve lock. Optically coupled variable resistor $U 5$, also driven by U6, is used to allow the AFC bias to charge C34 (audio coupling capacitor) rapidly rather than through high value resistor R28. The AFC bias is changed at 100 MHz by shunting resistor R27 with optically coupled transistor 48 below 100 MHz . The bias voltage is approximately 2.8 VDC below 100 MHz and 5.8 VDC at 100 MHz and above.

## 4-1.2 AUDIO CIRCUITS

The Audio Circuits include the monophonic input, SCA inputs and composite input signal paths to the Modulated Oscillator. Figure 4-3 is a simplified diagram of the Audio Circuits.

The audio inputs first pass through RFI filters and are then routed to the Audio/AFC Assembly (A3). The mono input is also routed through switch $S 2$. If $S 2$ is in the mono position, the mono input is connected to the Audio/AFC assembly. This is done to obtain maximum separation when operating in the composite mode.

The balanced audio inputs are summed at the inverting input ports of U9A and U9B. U9A, U9B and U9C comprise a balanced to unbalanced amplifier circuit. R43 is used to balance the gain of U9A and U9B and thereby maximize common mode (hum) rejection. R51 is used to set the output level of buffer amplifier U9D at 2.25 VRMs. Diode pre-distortion is used to linearize the modulation characteristics of the varactor diodes in the modulated oscillator. R59 is used to adjust the amount of pre-distortion utilized. R56 is used to adjust the audio level to the modulated oscillator. A sample of the composite signal at U9D output is routed to the front panel composite monitor jack. The front panel composite test input is applied directly through R7 to U9D.


The 802A may be driven to $200 \%$ modulation with very little increase in distortion and is usable to frequencies below 2 Hz input at full modulation capability without losing AFC lock. It is necessary to adjust R50 (predistortion) and R56 (mod level) at each carrier freuqency to optimize distortion characteristics.

## 4-1.3 AMPLIFIER AND POWER OUTPUT CONTROL CIRCUITS

The Power Amplifier (AR1) amplifies the approximately 20 MW signal from the Modulated Oscillator to the 50 watt output level. A Harmonic Filter (FL1) follows the Power Amplifier. The Amplifier Control Assembly (A5) provides output power adjustment and protective features controlling the amplifier collector voltage. Figure 4-4 shows the location of these circuits in the 802A. Figure $4-5$ is a simplified diagram of these circuits.

The Power Amplifier is a three stage solid state amplifier which operates broad band over the 87 to 109 MHz frequency range with no tuning. The amplifier PC board is mounted on a large heat sink for maximum cooling and transistor life. The first amplifier stage, a 2 N 3553 , is matched to the fifty ohm input by means of a lumped constant network. This stage amplifies the signal to approximately a two watt level. The output of the first stage is matched to the input of the second stage, a PT9732, by means of a lumped constant network and a short strip line. This stage amplifies the signal to approximately a ten watt level. The output of the second stage is matched to the input of the third stage by a combination strip line and lumped constant network. The third stage, a MRF315A, amplifies the signal to the 50 watt level. The output network matches the 50 ohm output utilizing a strip line technique. Capacitors C11 and C34 provide harmonic rejection. The amplifier contains a stripline directional coupler which is used to detect both forward and reflected power at the output. Power output level is adjusted by controlling the collector voltage to the second and third stages. The series pass transistor for the collector voltage regulator is mounted on the amplifier heat sink. A thermal switch is also mounted to the amplifier heat sink and used to cut power back should the heat sink temperature rise too high (in the event of a fan failure for instance) and also activate the cooling LED on the front panel.

The Power Amplifier is followed by a harmonic filter which provides additional harmonic rejection.


Figure 4－4．Amplifier \＆Power Control Circuit Location


The Amplifier Control Assembly (A5) contains the integrated circuit regulator which controls the Amplifier Collector voltage. The collector voltage regulator circuit may be operated in two modes; manual or automatic. In the manual mode, the collector voltage is adjusted for the desired power level using R21. Collector voltage is sensed via R29 and applied to the regulator via S1. Thus, the regulator serves to hold collector voltage constant. In the automatic (normal) mode, the directional coupler forward power signal is amplified by U1A and applied to the regulator via S1 and R6. Thus, the regulator serves to hold power output constant. Therefore, the power output will remain constant over temperature and slight load impedance changes. The directional coupler reflected power signal is amplified and used to protect the amplifier from damage when operating into a high VSWR. The reflected signal is coupled into the regulator via CRI and CR2 and acts to reduce power output to a safe level. At approximately a 2 to 1 VSWR the output of U3A will go high and light the front panel VSWR indicator. Under open or short circuit conditions, power output is limited to approximately 8 watts. Over voltage protection for the amplifier is provided by Crowbar Q1. If the collector voltage to the amplifier exceeds the threshold voltage of VR2, the crowbar will fire, shorting the collector voltage feed through R34 and blowing fuse F1. Over current protection for the amplifier is provided by foldback current limiting in the 723 regulator $U 2$. The voltage across low value resistors R30 and R31 is applied to the regulator via R27, R28 and R26. A positive bias voltage is also applied to the current limit input of the regulator via R23. This is to insure fast current limiting action in the event of a short circuit on the collector voltage feed to the amplifier.

The amplifier may be muted by depressing the mute switch on the front panel. This places a low on the regulator Frequency Compensation input, via CR4 and Q2, causing the regulator to take the collector voltage to approximately zero output. Loss of AFC lock is used to mute the amplifier in the same manner. An overtemperature condition will also mute the amplifier to approximately the 8 watt level (when operating at 50 watts output) via chassis components CR3 and A5R48. The front panel cooling LED indicator will illuminate when this occurs. The amplifier may be externally muted via TB1-6 and TB1-7 on the 802 A rear panel. +22 VDC is present via R7 at TBl-7. If applied to TB1-6 via relay contacts this will cause a hard mute of the amplifier output. A potentiometer ( 5 K to 100 K ) may be installed from TB1-7 to ground and the slider on the potentiometer applied to TBl-6 via relay contacts. The mute level may then be adjusted to the desired level by means of the potentiometer.

## 4-1.4 POWER SUPPLY CIRCUITS

Figure 4-6 is a simplified diagram of the 802A power supply circuits. Figure 4-7 shows the location of the major components of the Power Supply in the 802A.

The AC input is applied through the input connector to Tl. The line voltage selector card is a part of the AC input connector. The input connector also contains an RFI filter. The exciter cooling fan is operated from a 115 volt winding on the primary of T1. The center tapped secondary of $T 1$ is applied to full wave rectifier CR1 to obtain nominal +35 V and -35 V outputs. The +35 V output is routed to the Amplifier Control Assembly (A5) and the Power Supply Assembly (through voltage dropping resistors R8 and R9) after filtering by Cl. The -35 V output is routed directly to the Power Supply Assembly as is the 8.4 volt output from the remaining transformer secondary.

The +35 V input is passed through regulator U 2 to obtain +22 V output. This voltage is used to supply the first stage of the amplifier and other applications in the exciter where a very low noise voltage is not essential. This pre-regulated +22 V is farther regulated to +15 V in the modulated oscillator by $U 1$. This +15 V is used solely in the modulated oscillator to insure the outstanding noise characteristics of the 802 A . The preregulated +22 V and -22 V are also regulated to +15 V and -15 V on the Audio/AFC Assembly (A3) by regulators U10 and Ull. This is done to insure low noise and ripple on the supply voltage Proper operation of the regulators $U 10$ and $U 11$ is indicated by LEDs DS1 and DS2. These indicators will illuminate when the 15 V outputs are present. This $\pm 15 \mathrm{~V}$ is also used to supply the amplifier on the Modulation Display Assembly (A6).

The 8.4VAC is rectified on the Power Supply Assembly by full wave bridge CR5 and applied to regulator U3. The +5 V output from U3 is used to supply digital circuits throughout the 802A.

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4-1.5 METERING AND MONITORING CIRCUITS
Three Metering and Monitoring devices are utilized in the 802A. The forward and reflected power is monitored on analog meter M1. The directional coupler signals from the power amplifier are amplified on the Amplifier Control Assembly and routed to the Metering Network Assembly (A7) which selects either forward or reflected power on M1.

Power Supply voltages and current are monitored on digital multimeter M2. These metered items are routed to voltage dividers on the Metering Network Assembly and selected for display on multimeter M2. Figure 4-9 shows the location of the metering and monitoring circuits.

The composite modulating signal to the Modulated Oscillator is detected and displayed on the bar graph on the front panel (calibrated in percent modulation). Figure 4-8 is a simplified diagram of the Modulation Display circuits. The composite modulating signal is applied to buffer amplifier UlA. R2 serves to calibrate the $115 \%$ full scale range of the display. U1B and U1C form an absolute value detector. This circuit detects both positive and negative peaks of the modulating signal. The detector is flat well beyond 100 KHz in order to respond to fast peaks in program material. The output of U1C is applied to the fast charge/slow discharge circuit formed by CR3, C4 and R12. UlO provides gain and buffering of the detected signal. A small amount of bias is applied via R13 to improve accuracy at low modulation levels. The signal is then applied to bar graph drivers U2 and U3 via the $20 \%$ scale calibration potentiometer R17. Either a bar or dot display mode may be selected from the front panel. The $10 \%$ LED when in the $20 \%$ full scale mode and the $100 \%$ LED when in the $115 \%$ full scale mode outputs of the bar graph drivers are sensed and used to trigger one shot U4 which drives the over-modulation indicator LED DS3.

The POWER ON, VSWR, COOLING and AFC LED indicators are located on the Modulation Display Assembly. The POWER ON LED is activated by the +5 V supply. The COOLING, VSWR and AFC faults are summed and applied to 23 which drives the remote fault relay $K 1$.



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## 4-2. DETAILED CIRCUIT DESCRIPTION

The following paragraphs provide a more detailed description of the assemblies which comprise the functional groups described in Section 4-1.

## 4-2.1 MODULATED OSCILLATOR ASSEMBLY

Refer to schematic 643-0016-001 and assembly drawings 643-0015-001 and 643-0052-001.

The Modulated Oscillator Assembly is comprised of the Modulated Oscillator PC Board (A1Al) and associated RFI filtering components and connectors. Capacitors C1, C2, C3, C4 and C5 along with L1, L2, L3 and L4 (ferrite beads) provide RFI filtering.

Supply voltage for the modulated oscillator is derived from the $+22 V$ supply by voltage regulator Ul. R24 and R28 determine the output voltage of Ul (+15V). CR5 and CR6 provide transient protection. C18, C19 and C20 provide filtering to insure a very low noise, low ripple DC supply voltage for the oscillator.

The modulated oscillator is formed by JFET Ql operating as a Hartley oscillator. The resonant tank circuit is comprised of Ll , L2, CR1, CR2, CR3 and CR4. CR1-CR4 are varactor diodes used to modulate and tune the oscillator. Diode pair CR3 and CR4 are used for modulation and to bias the oscillator for the frequency ranges above or below 100 MHz . AFC tuning is accomplished by diode pair CR1 and CR2. An isolated return line is provided for the modulation and AFC inputs in order to minimize possible noise contributions from ground loops. Diodes CR7 and CR8 clamp the oscillator RF voltage and prevent rectification by the varactor diodes.

The output of oscillator $Q 1$ is capacitively coupled via C8 to source follower Q2. Q2 in turn drives emitter follower 03 through C10. These two high input impedance stages isolate the oscillator from the output load and prevent "pulling" of the oscillator due to output impedance changes. Q3 output drives amplifier Q4 via Cl2. Q4 is a conventional grounded emitter, Class A amplifier. C16, L5 and C17 provide harmonic rejection and impedance matching. The modulated oscillator has two outputs, one to drive the power amplifier and one to drive the frequency divider for the AFC circuits.

Refer to schematic 643-0004-001 and assembly drawing 643-0003-001.

The carrier frequency from the modulated oscillator is applied to ECL prescaler U1. Ul divides the carrier frequency by eight. Ul contains an ECL to TTL translator and the translator output is used to drive D flip-flop U2, half of which is used to further divide the carrier frequency by two. R1 provides a termination for the carrier signal input, R2 and C2 are required for $U 1$ operation and R3 insures U1 stability. U3-U7 comprise the BCD programmable counter $(\div 8700$ to 10900 ) as previously described. Frequency is programmed via the DIP switches Sl thru S4. Integrated circuit resistor networks R11 and R12 act as pull up resistors. The programming is BCD code. To change frequency set the the switches for the BCD code of the frequency desired. For instance 103.14 MHz is

| $10 \mathrm{MHz}(\mathrm{S} 4)$ |  |  |  |
| :---: | :---: | :---: | :---: |
| 1010 | $\frac{1 \mathrm{MHz}(\mathrm{S} 3)}{0011}$ | $\frac{100 \mathrm{MHz}(\mathrm{S} 2)}{0001}$ | $\frac{10 \mathrm{XHz} \text { (S1) }}{10}$ |
|  | 3 | .1 | 0100 |

One shot 48 stretches the pulse from the programmable counter. R4 and C6 determine the output pulse width of U8.

The 10 MHz crystal oscillator Y 1 is the reference oscillator for the AFC circuits. The AFC circuits phase lock the carrier frequency to the reference oscillator. The 10 MHz TTL output of Yl is divided by 16 via U9 and further divided by 10 via U10. The $\div 2$ and $\div 4$ frequency outputs of $U 9$ are applied to $J 3$ along with the 10 MHz signal. Thus Pl may be used to select $2.5 \mathrm{MHz}, 5 \mathrm{MHz}$ or 10 MHz for access on TPl to be used for frequency calibration.

The frequency divider operates from the +5 V supply which is RFI filtered by C13, C14, C15 and L1. Further decoupling of the digital circuits from the supply is provided by capacitors placed close to the chip $V_{C C}$ pins (C4, $\mathrm{C} 5, \mathrm{C} 9, \mathrm{C} 10$, etc.).

The Modulated Oscillator and Reference Oscillator and their respective divider chains are monitored for activity by identical circuits which drive LED indicators. The indicators are ON whenever activity is detected. Each activity monitor is coupled via a resistor capacitor network (R5, C7) to a diode detector (CR1) which drives an emitter follower stage (Q1) which in turn drives the LED driver (Q2). Should either oscillator or counter chain fail, the
activity monitor LED will extinguish and the AFC front panel LED will also extinguish.

## 4-2.3 AUDIO/AFC ASSEMBLY (A3)

Refer to schematic 643-0007-001 and assembly drawing 643-0006-001.

The Audio/AFC Assembly processes the audio inputs for application to the Modulated Oscillator and also contains the AFC phase comparator, loop filter and lock detector. The audio inputs (mono, composite and SCA) are applied to the balanced to unbalanced amplifier formed by U9A, U9B and U9C. Pre-emphasis is applied to the mono input by $\mathrm{C} 23, \mathrm{C} 24, \mathrm{C} 25$ and C 26 . By changing the jumpers on E1, E2, E3 and E4, E5, E6 flat, $25 \mu \mathrm{sec}, 50 \mu \mathrm{sec}$ or $75 \mu \mathrm{sec}$ preemphasis may be obtained. R43 is used to adjust the gain of U9A so that U9A and U9B have equal gain. This insures maximum common mode rejection (hum on the input lines for example). The output of U9A is inverted and summed with the output of U9B by U9C to provide the unbalanced signal required by the Modulated Oscillator. U9D acts as a buffer amplifier. The gain of U9D is adjusted by R51 to give 2.25 VRMS at U9D output. This level corresponds to $100 \%$ modulation. C30-C33 limit high frequency noise by reducing gain. The composite test input is applied to the inverting input of U9D. A sample of U9D output is routed to the Modulation Display Assembly and to the Composite Monitor jack on the front panel. Diode predistortion of the signal is used to compensate for the small non-linearity of the varactor diodes in the Modulated Oscillator. Diodes CR7, CR8, CR9 and CR10 are biased by their respective resistor networks and provide the predistortion. R59 is used to adjust the predistortion level for minimum distortion at the exciter output. R56 adjusts the signal level to achieve $100 \%$ modulation with 2.25 VRMS at TP9. R56 and R59 are adjusted at the carrier operating frequency and should be re-adjusted for optimum performance if the carrier frequency is changed. The modulating signal is coupled to the Modulated Oscillator through C34. The audio signal path is flat to beyond 100 KHz and usable to frequencies below 2 Hz .

To insure low noise power supplies for the operational amplifiers used in the audio and AFC circuits the pre-regulated +22 V and -22 V supplies are passed thru regulators UlO and Ull to obtain +15 V and -15 V . C15, C16, C19 and C20 provide filtering and CR3, CR4, CR5 and CR6 provide transient protection. The $\pm 15 \mathrm{~V}$ is also routed to the modulation display assembly. C17, C18, C21, C22, L2 and L3 provide decoupling for these outputs. The $\pm 15 \mathrm{~V}$ is monitored
by LEDs DS1 and DS2 through R29, R30 and zener diodes VR1 and VR2. Should the +15 V fail, DSl will extinguish and should the -15 V fail, DS2 will extinguish.

Phase comparison for the AFC phase locked loop is provided by U1. The 625 Hz from the carrier frequency divider chain and the 62.5 KHz from the reference frequency divider chain are applied to U1. Ul further divides the 62.5 KHz by one hundred to 625 Hz . These two 625 Hz signals are phase compared in Ul and the output of the phase comparator (Pin 13) is applied to active filter U2A. R4, R8 and R5 bias the phase comparator output to 2.5 VDC so that the output phase comparator pulses will go high or low around the 2.5 VDC point depending on whether the carrier phase leads or lags the reference phase. R7 provides a small amount of offset bias (dead band) to insure that the phase comparator does not "hunt" around the in phase point. U2A is an integrator with a break frequency of approximately. 05 Hz determined by C 8 and R7. The output of the integrator is applied to the Sallen-Key type active Butterworth filter formed by U2B, R13, R14, C10 and C35. The output of U2B is then a DC voltage used for AFC tuning. Since the frequency response of the active filters $U 2 A$ and $U 2 B$ is very low, the AFC loop would take quite a long time to achieve lock when first turning on or changing frequency. Optically coupled variable resistors U3 and U4 are used to speed up the AFC filter response until phase lock is achieved at which time the filter response is returned to its normal frequency response. Bias is applied to the modulator pair of varactor diodes to optimize the AFC tuning curve and is applied to the Modulated Oscillator via R28. R28 is required to be a high value resistor to insure good low frequency modulation characteristics. The bias voltage is developed by the resistance voltage divider network formed by R25, R26 and R27. The bias voltage is changed whenever a frequency 100 MHz or above is selected by optically coupled transistor 48 which shorts out R27. As the time constant of R28 and modulation coupling capacitor Cl 10 is long, optically coupled variable resistor U 7 is used to short R 28 with a low resistance value until lock is achieved.

The optically coupled variable resistors are driven by the output of buffer amplifier U6A. The lock detection function is performed by D flip-flop U5. An output from phase comparator U1 and the inverted 625 Hz carrier frequency signal are applied to U5. When the output from Ul goes low for a period of time equal to approximately $90^{\circ}$ or more the $\bar{Q}$ output of $U 5$ will go high. This high signal (indicating loss of lock) is applied to U6A via the fast charge/slow discharge circuit formed by R16, CR2, R18 and C13.

This causes the output of U6A to go high which energizes the optically coupled variable resistors to speed up the AFC filter response and extinguishes the AFC front panel $L E D$ via Q1 and Q2.

4-2.4 AMPLIFIER ASSEMBLY (AR1)
Refer to schematic 643-0028-001 and assembly drawings 643-0027-001 and 643-0054-001.

The Power Amplifier consists of the amplifier PC board, which is mounted on a large heatsink, and REI filtering. C1-C5 and L1-L4 (ferrite beads) perform RFI filtering. R1 provides +22 volts to the temperature switch $S 1$ which monitors the amplifier heatsink temperature and will mute the output to a safe level in the event of excessive heat sink temperature (caused by a fan failure for instance).

The Amplifier PC board(AR1A1) contains the three stage amplifier which accepts the approximately 20 milliwatt input from the Modulated Oscillator and amplifies it to the 50 watt output level. The first stage utilizes a 2 N 3553 operated with approximately 1.6 VDC bias developed by R1, R2 and emitter resistor R3. C1, C2, L1, C35 and C36 match Q1 input impedance to the 50 ohm input. C3 provides $R F$ ground for the emitter of Q1. The output of Q1 is matched to the input of Q2, a PT9732, by the matching network, comprised of L5, L15, C33, C9, L7E and a short strip line. C8 provides DC blocking while R4, RI3 and L7 prevent parasitic oscillation.

The second stage, Q2, is operated with zero bias with the emitter at $D C$ and $R F$ ground. The output of $Q 2$ is matched to the input of the third stage, a MRF315A, by the network comprised of C10, L8, C16, C17, C18, C19 and a short strip line. R15, R16, L11, L12 and R5 prevent parasitic oscillations and also prevent DC bias from developing at the base of Q3. C15 provides DC blocking. The output of $Q 3$ is matched to the 50 ohm output impedance by the output strip line. C11 and C34 provide harmonic rejection. C23 provides DC blocking.

A directional coupler follows the output strip line. Both forward and reflected power are detected by the directional coupler strip lines, which are backward wave coupled to the 50 ohm output strip line. Capacitors C39 (forward) and C27 (reflected) compensate the directional coupler over the 87 to 109 MHz frequency range. R8 is adjusted to provide maximum directivity on the reflected power coupler. Diodes CR1 and CR2 detect the coupler outputs to provide a DC analog of forward and reflected power.

The collector of each amplifier stage is isolated from the collector of the other stages by decoupling circuits such as that formed by R7, L13, L14, C20, C22 and C32 for Q3. The first stage operates from the +22 V supply. The second and third stages operate from the variable voltage provided by the Amplifier Control Assembly.

The series pass transistor for the collector voltage regulator is also mounted on the amplifier heatsink.

## 4-2.5 AMPLIFIER CONTROL ASSEMBLY (A5)

Refer to schematic 643-0013-001 and assembly drawing 643-0012-001.

The primary function of the Amplifier Control Assembly is to regulate and control the level of the collector voltage of the final two stages of the power amplifier.

Unregulated supply voltage is routed thru fuse $F 1$ and then applied to the collector of the series pass regulator Darlington transistor mounted on the amplifier heatsink. SCR Q1 provides overvoltage crowbar protection. Zener diode VR2 monitors the regulated voltage from the series pass transistor and will trigger Q1 should the collector voltage exceed 36 V . R34 provides current limiting. Fl will open in the event the crowbar triggers. The regulated voltage from the series pass transistors is routed through current limiting and monitoring resistors R30 and R31 and applied to the amplifier. The voltage developed across R30 and R31 is sensed and applied to the current sense and limit inputs of the 723 regulator via R27 and R28. R28 provides a bias voltage to insure fast foldback current limiting in the event of a short circuit. Operational amplifier U3B, operating with a non-inverting gain of 4 , is connected to differentially amplify the voltage drop across R30 and R31 by a factor of two. Potentiometer $R 40$ is used to adjust the output voltage of U3B to twice the voltage across the precision resistors R30 and R31. Thus, if the current to the amplifier is 4 amperes, the voltage across R30 and R31 will be . 4 V and the output of U3B will be . 8 V . The output voltage of U 3 B is routed to the Metering Network Assembly A7, adjusted and applied to the digital multimeter.

The internal reference voltage of the 723 regulator is applied to the non-inverting input of the regulator via R21. This voltage determines the output level of the regulator. In the manual mode, (AGC OFF) output voltage is applied to the inverting input of the regulator via R20 and the output voltage to the amplifier is maintained constant. In the automatic mode (AGC ON), the detected forward
power sample from the amplifier is amplified by U1A and applied to the inverting input of the regulator. Thus, the regulator acts to hold power output from the amplifier constant. VSWR protection is provided by UlB which amplifies the reflected power sample from the amplifier. This amplified voltage is routed through CR1 and summed with the forward power sample via $R 6, R 7$ and $R 8$ and acts to reduce power output as VSWR increases. In the manual mode this reflected power signal is summed with the regulator output voltage via CR2, R35, R36 and R18 and acts in a similar manner to reduce power output as VSWR increases. Thus, the amplifier is protected from excessive VSWR conditions by controlling the collector voltage.

The output of U1A (forward power analog) is routed thru R14 to the Metering Network Assembly (A7) for application to the power meter. The reflected power signal is routed in a similar manner and is also applied to VSWR detector U3A. When the reflected power signal at the non-inverting input to U3A exceeds the bias voltage at the inverting input established by R16 and R17, the output of U3A will go high and cause the front panel VSWR LED indicator to illuminate and actuate the remote fault indication relay.

The output of the 723 regulator (U2) is applied to the base of the Darlington series pass transistor via current limiting resistor R24. Zener diode VR2 clamps the output of the regulator to prevent application of excessive voltage to the amplifier.

The AFC and front panel mute signals are applied to the base of Q 2 , turning Q 2 ON and placing a low on the frequency compensation input to the regulator which causes the regulator to turn OFF. The external and cooling mute signals are applied to the inverting input of the regulator via R 48 and act to reduce power output.

4-2.6 MODULATION DISPLAY ASSEMBLY (A6)
Refer to schematic 643-0019-001 and assembly drawing 643-0018-001.

The Modulation Display Assembly provides a bar graph display of the composite signal to the modulated oscillator. The display is calibrated in per cent modulation. The assembly also contains the LED indicators for POWER ON, AFC, VSWR and COOLING.

The composite signal is applied to buffer amplifier U1A. For the bar graph $20 \%$ full scale range, the gain is established by R4 and R35 at eleven (11). For the $115 \%$ full scale range potentiometer, R2 is connected to ground via the Metering Network Assembly switch and the gain set for $115 \%$ full scale by R2. U1B acts as an absolute value detector with negative peaks detected by CRI and appearing at TP2 while positive peaks are deleted by $C R 2$ and appear at TP3. R9 limits the gain of U1B when the signal is too small to cause CR1 and CR2 to conduct. The peak detected positive and negative signals are summed in U1C to provide a positive signal at UlC output. This signal is applied to the fast charge/slow discharge network comprised of CR3, CR4 and R12 and amplified by U1D for application to * the bar graph drivers.

The bar graph drivers $U 2$ and $U 3$ each contain voltage comparators and linear voltage dividers which activate to drive 10 LEDs per driver. The comparators activate in sequence as the input signal is increased in level. The two bar graph drivers are connected in series to drive the two 10 element bar graph arrays DS1 and DS2. The detected composite signal from UlD is applied to the input of each driver at Pin 5. R17 adjusts the signal for $20 \%$ full scale. The reference voltage for the drivers is derived from the internal reference voltage of U3 via R20 and R21. The low end of U3 voltage divider network is applied to the high input end of the $U 2$ voltage divider. R20 and R19 set the output sink current of the drivers so that each LED in the bar graph array pulls approximately 10 ma from the +5 V supply. SIP resistor networks R24-R26 limit power dissipation in the bar graph arrays.

The bar graph driver may be placed in the dot or bar display mode. This is accomplished by switching the mode input of the drivers (Pin 9) via the switch on the Metering Network Assembly. Timer U4 is connected as a one shot to actuate the over-modulation LED indicator DS3. R23 and C9 determine the output pulse duration (approximately 2.5 seconds). The trigger input of $U 4$ is driven by the low signal which actuates the $100 \%$ or $10 \%$ LED in the bar graph array. The trigger input to $U 4$ is switched via the Metering Network Assembly to the appropriate LED.

The LED indicators for POWER ON, AFC LOSS OF LOCK, VSWR FAULT and COOLING FAULT are also located on the Modulation Display Assembly. The POWER ON LED is operated by the +5 V power supply. The fault LED inputs are summed via $C R 4, C R 7$ and $C R 5$ and used to turn on the remote fault relay via Q1. The collector of $Q 1$ will go low to actuate the relay whenever a fault is detected.

## 4-2.7 POWER SUPPLY ASSEMBLY (A4)

Refer to schematic 643-0010-001 and assembly drawing 643-0009-001.

The approximately 8.4 VAC from the power transformer is applied to full wave bridge rectifier CR5. C8 provides ripple filtering. U3 regulates the output of CR5 to +5 VDC . CR6 and CR7 provide transient protection while C 9 provides additional filtering.

The full wave rectified +35 volts from the chassis ripple filter C1 is applied to voltage regulator U 2 to provide +22 VDC output. R3 and R4 set the output of U3 to +22 V . CR3 and CR5 provide transient protection while C5, C6 and C7 provide additional filtering.

The full wave rectified -35 volts from chassis rectifier CR1 is filtered by C1 and C2 and applied to voltage regulator U1. R1 and R2 set the output of $U 1$ to -22 VDC. CR1 and CR2 provide transient protection while C3 and C4 provide additional ripple filtering.

## 4-2.8 METERING NETWORK ASSEMBLY

Refer to schematic 643-0025-001 and assembly drawing 643-0024-001.

The Metering Network Assembly comprises the front panel selector switch and associated metering resistor networks. Push-Push switch S1A selects forward or reflected power for display on M1. Mechanically interlocked S1C through SlH select either Amplifier Collector Voltage, Amplifier Collector Current, +22V, $-22 \mathrm{~V},+5 \mathrm{~V}$ or the AFC voltage for display on digital multimeter M2. R1 and R2 form the metering resistor network for Amplifier Voltage. R2 and R1, R3 and R1, R4 and R1 serve the same purpose for the $+22 \mathrm{~V},-22 \mathrm{~V}$ and +5 V input respectively. $\mathrm{R7}$ serves as the low end of the voltage divider network for the AFC voltage. R8 is used to calibrate the Amplifier Current.

Push-Push switch S1B (red button) provides front panel muting of the amplifier output. Push-push switch SII selects the bar or dot mode for the modulation bar graph display and push-push switch siJ changes the bar graph display from $115 \%$ to $20 \%$ full scale. SlJ also switches the trigger input of the over-modulation LED driver to the appropriate LED (i.e. $10 \%$ or $100 \%$ ).

## 4-2.9 HARMONIC FILTER ASSEMBLY (FL1)

Refer to schematic 643-0022-001 and assembly drawing 643-0053-001.

The harmonic filter provides sufficient harmonic rejection to allow the 802 A to be used as a stand-alone 50 watt transmitter. The filter is a five pole lumped constant filter. C2 and C4 are used to optimize filter input impedance and harmonic rejection. The voltage divider formed by R1 and R2 provides a sample of the RF output to the front panel monitor jack.

## SECTION 5 - MAINTENANCE AND ALIGNMENT

5-1. GENERAL

The following paragraphs describe maintenance and alignment procedures for the Type 802A FM Exciter. Logical and methodical trouble shooting procedures should be used, proceeding from front panel indicators and meter readings to circuit checks and measurements. The 802A utilizes sockets for integrated circuits to enable rapid replacement should a failure occur. A data sheet is shipped with each exciter which gives the voltage and current levels as measured at final factory test. Periodic readings should be taken and compared to the data sheet values. Refer to Figure 5-1 through Figure 5-3 for the location of adjustable components in the 802A.

The PC board assemblies in the 802A may be removed by unplugging the connectors to the board and removing the four screws that mount each board to the chassis. The Frequency Divider and Audio/AFC boards have covers which are held in place by four screws accessible from the bottom of the exciter.

The top cover of the amplifier may be removed for in-place trouble shooting. The amplifier is removed by removing the screws from the exciter rear panel and laying it back. The six screws mounting the amplifier are accessible from the bottom of the exciter. Once the rear panel is laid back, the six bottom amplifier screws removed and the amplifier plug disconnected, the amplifier may be tilted to the right and lifted out. If $Q 2$ or $Q 3$ is to be replaced, the transistor should be mounted to the heat sink prior to soldering to the PC board in order to avoid undue stress on the transistor leads.

The power transformer is accessible by removing the mounting screws from its cover. The mounting screws are accessible from the bottom of the exciter. Turn the power OFF and disconnect the AC line cord prior to removing the transformer cover.

CAUTION

115/230 VAC IS PRESENT ON THE POWER TRANSFORMER, POWER ON SWITCH AND AC LINE CONNECTOR WHEN THE EXCITER IS OPERATING.

The following maintenance equipment is required:

Flat blade screwdriver<br>Phillips screwdriver<br>FM Monitor<br>Audio Signal Generator<br>Distortion Analyzer<br>3-1/2 Digit DMM<br>Calibrated in line 50 ohm Wattmeter

5-2. POWER SUPPLIES

The power supplies in the 802A contain no operating adjustments. The integrated circuit voltage regulators contain internal current limiting and over temperature protection. Clearing an overload condition will in most cases restore the regulators to normal operation.

## 5-3. MODULATED OSCILLATOR AND FREQUENCY DIVIDER

The Modulated Oscillator has no operating adjustments. The outputs may be open or short circuited without damage to the oscillator. The frequency divider cover is removed by entending the 802A on the slides and removing four screws from the bottom of the exciter. The 802A output frequency may be calibrated by means of the reference oscillator (this adjustment is accessible without removing the cover). A sample of the reference oscillator is provided at TP1. The frequency at TP1 may be selected by P1 to be 2.5 , 5 or 10 MHz . A short wire may be inserted in TP1 and used with a standard receiver to calibrate output frequency. The operating frequency may be changed by programming the desired frequency, in BCD code, on the DIP switches. A DIP rocker switch in the OPEN position corresponds to a "1". For instance the BCD code for 88.37 MHz is:

| $\frac{10 \mathrm{MHz}}{1000}$ | $\frac{1 \mathrm{MHz}}{1000}$ | $\frac{100 \mathrm{KHz}}{0011}$ | $\frac{10 \mathrm{KHz}}{0111}$ |
| :--- | :--- | :--- | :--- |

Should either the reference oscillator or modulated oscillator fail, the appropriate on board LED indicator will extinguish. An oscilloscope probe may be used for trouble shooting the frequency divider chains. The pulses will be very narrow and will require a wide bandwidth oscilloscope.

## 5-4. AUDIO/AFC AND MODULATION DISPLAY

The Audio/AFC assembly contains two operating adjustments which are accessible without removing the cover. These are the modulation level and distortion null. These adjustments should be made to obtain best performance whenever the exciter operating frequency is changed. If the operating frequency is changed, only steps $C$ and $D$ in the following procedures need be performed. The cover may be removed from the audio/AFC assembly by extending the 802A on the slides and removing four screws from the bottom.
A. Balance Adjust

Apply a $400 \mathrm{~Hz},+10 \mathrm{dBm}$, signal from an audio signal generator to TB1-10. Connect a clip lead or jumper from TBl-10 to TB1-12. This applies the same signal to both mono inputs. Connect an oscilloscope probe to TP8 and adjust R43 for minimum signal on the oscilloscope. (Mono/Composite Switch in MONO position).
B. Audio Level Adjust

Apply a $400 \mathrm{~Hz}, 1.25$ VRMS, signal from an audio signal generator to the composite input. With a voltmeter or oscilloscope, adjust R51 for 2.25 VRMS ( 6.36 V peak to peak) at TP9. (Mono/Composite Switch in COMPOSITE position).
C. Modulation Adjust

Apply a $400 \mathrm{~Hz}, 1.25$ VRMS, signal from an audio signal generator to the composite input. Connect the output of the exciter through a 30 dB attenuator to an FM monitor. Adjust R57 for 75 KHz deviation.
D. Distortion Null (Predistortion)

Connect the signal generator output from an audio analyzer such as the Sound Technology 1710A to the composite input of the exciter. Connect the exciter output through a 30 dB attenuator to a good quality FM monitor. Connect the FM monitor output to the distortion analyzer input of the audio analyzer. Configure the audio analyzer for a 1:1 IM measurement. Set the signal generator output for 75 KHz deviation. Adjust R59 for minimum IM distortion as indicated on the analyzer (typically less than 2\%). Alternately, a 400 Hz tone may be used to modulate the 802 A and the output of the FM monitor displayed on an audio spectrum analyzer. The spectrum analyzer should have 80 dB dynamic range. R59 is then adjusted for minimum harmonic level of the 400 Hz
fundamental tone (each harmonic should be at least 75 dB below the fundamental 400 Hz tone).

The Modulation Display is calibrated following Steps A thru D. Step $E$ ( $20 \%$ cal) must be performed prior to Step $F(115 \%$ cal).
E. $20 \%$ Scale Adjust

Connect the output of the exciter through a 30 dB pad to an FM monitor. Apply a stereo pilot tone to the composite input and adjust the pilot tone level for 7.5 KHz deviation. Select the bar display mode and the $20 \%$ scale on the 802 A front panel switch. Adjust R17 until the $10 \%$ LED just starts to glow. Verify adjustment by varying the pilot tone level above and below 7.5 KHz deviation. Verify that the over modulation indicator illuminates when the $10 \%$ LED turns on.
F. 115\% Scale Adjust

Connect the exciter as in Step E and apply a stereo signal ( 400 Hz in the left channel) to the composite input. Adjust the signal level for 75 KHz deviation on the FM monitor. Select the bar display mode and the $115 \%$ scale on the 802A front panel switch. Adjust R2 until the $100 \%$ LED just starts to glow. The overmodulation indicator should illuminate when this occurs.

5-5. AMPLIFIER, AMPLIFIER CONTROL AND METERING
The output power adjustment is accessible through the top cover of the 802 A by extending the exciter on the slide.

The Amplifier Assembly contains one adjustment which is used to set the output directional coupler to maximum directivity. This must be done prior to calibrating the reflected power meter, but need not be done again unless the directional coupler has failed and been repaired (diode failure for instance).
A. Direction Coupler Directivity

Remove the top cover from the Amplifier. Connect the output of the exciter to a 50 watt, 50 ohm termination. Select reflected power on the front panel switch and adjust R8 for minimum indication on the power meter.
B. Forward Power Calibration

Connect the exciter output through a calibrated 50 ohm, in line wattmeter to a 50 ohm termination. Place the AGC switch in the OFF position (Manual mode). Select forward power on the 802A front switch. Adjust the power output control (R21) for 40 watts on the external power meter. Adjust the forward power calibration potentiometer, R5, for 40 watts indication on the 802A front panel meter.

## C. Reflected Power Calibration

Following calibration of the forward power meter, adjust the power level control for 5 watts output. Disconnect the 50 ohm termination from the exciter output. Select reflected power on the front panel switch and adjust R13 for 5 watts reflected power. Select forward power on the front panel switch and verify 5 watts forward. Repeat the process if necessary and adjust the power level control (R21) and reflected power calibration (R13) until 5 watts forward and reflected is obtained. Do not adjust the forward calibration (R5) during this process. The re-iteration of the reflected power calibration is necessary due to the fact that the VSWR protection is active at all times. Therefore, changing the gain of the reflected power amplifier will cause some change in power output. Connect the 50 ohm termination to the output of the exciter, set the AGC switch to the ON position (automatic mode) and adjust the power output control for the desired output level.

## D. Amplifier Current Meter Calibration

Using a digital voltmeter (a 3-1/2 digit hand held DMM is adequate), record the voltage drop across R30 and R31 on the Amplifier Control Assembly. Be very careful not to short R30 and R31 to ground with the voltmeter terminals. Connect the digital voltmeter from J2-14 or R6 to ground. Adjust R40 until a voltage exactly twice that recorded across R30 and R31 is obtained. Select Amplifier current on the front panel switch. Adjust R8 on the Metering Network Assembly until a current reading in amperes equal to the voltage drop recorded across R30 and R31 is obtained. (That is, if a voltage drop of .300 volts is recorded across $R 30$ and R31, adjust R8 for a current reading of 3.00 amperes.)

5-6. HARMONIC FILTER ALIGNMENT
The Harmonic Filter is aligned at the factory and will normally need no further adjustment. Connect the output of the exciter through a 50 watt, 30 dB attenuator to a spectrum analyzer with a frequency range extending to at least the tenth harmonic of the operating frequency. Adjust C2 and C5 for minimum reflected power and harmonic level. Several iterations of the adjustment may be necessary to achieve both minimum reflected power and optimum harmonic rejection. If operating frequency is changed, it may be necessary to adjust the Harmonic Filter for optimum harmonic rejection and minimum reflected power.



Figure 5-2. Alignment Location, Left Side, Top

AMPLIFIER
CURRENT CALIBRATION


Figure 5-3. Alignment Location, Top View


Figure 5-4. Modulated Oscillator P.C. Card



TABLE 5-1. LIST OF SCHEMATICS

| UNIT NO. | UNIT NAME | SCHEMATIC NO. |
| :--- | :--- | :--- |
| Al | TYpe 802A FM Exciter | $643-0040-001$ |
| AlAl | Modulated Oscillator Assy. | $643-0016-001$ |
| A2 | Modulated Oscillator Card | $643-0016-001$ |
| A3 | Frequency Divider | $643-0004-001$ |
| A4 | Powdio/AFC | $643-0007-001$ |
| A5 | Amplifier Control | $643-0010-001$ |
| A6 | Modulation Display | $643-0013-001$ |
| A7 | Metering Network | $643-0019-001$ |
| AR1 | Output Amplifier Assy. | $643-0025-001$ |
| ARlAl | Amplifier Card | $643-0028-001$ |
| FLl | Harmonic Filter Assy. | $643-0028-001$ |
| FLlAl | Harmonic Filter Card | $643-0022-001$ |















## 6-1 <br> GENERAL

This section contains a list of all repairable/replaceable electrical, and critical mechanical parts for the 802A Exciter.

6-2 REF DES

This column contains the electrical reference designators of all parts that have been assigned on schematics or wiring diagrams, and/or index numbers for all parts for which reference designators have not been assigned. When a reference designator, within a series of reference designators, has not been assigned a part number, the unassigned reference designator will be reflected as "NOT USED" in the DESCRIPTION column.

6-3 DESCRIPTION

This column contains the identifying noun or item name followed by a brief description. The description for electrical/ electronic parts includes the application ratings and tolerances. For consecutively listed identical parts within an assembly, "SAME AS---" is reflected in the description of subsequent listings, referencing to the first listing within the assembly.

6-4 CEMC PART NUMBER

The CEMC Radio Specification or drawing number, for each item in the parts list, is reflected in this column.

6-5 ILLUSTRATIONS

All parts listed in the REF DES column are located on corresponding illustrations. The illustration always precedes the parts list. When a replaceable electrical item is hidden from view by structural parts of wiring, a dotted leader line is used to show the locations of the item on the illustration.

Type 802A FM EXCITER - PARTS LIST 643-0001-001
Page 1 of 2

REF. DES.
Al
A2
A3
A4
A5
A6
A7
ARI
Bl
Cl
C2, C3
C4-C7
C8 thru Cl2
Cl3, Cl4
CP1
CR1
CR2, CR3
FI
Fl
FLl
Jl
J2
J3 thru J5

J6, J7
K1
L1, L2
L3, L4
M1
M2
Rl thru R4
R5
R6, R7
R8, R9
Sl
S2
Tl
TBl
W1

DESCRIPTION
Modulated Oscillator Assembly .
Frequency Divider Assembly
Audio/AFC Assembly
Power Supply Assembly
Amplifier Control Assembly
Modulation Display Assembly
Metering Network Assembly
Amplifier Assembly
Fan
Capacitor, $16,000 \mu \mathrm{f}, 50 \mathrm{~V}$
Capacitor, l00pf
Capacitor, 22pf
Capacitor, l000pf
Capacitor, 57 (ff
Adapter, BNC Bulkhead
Bridge Rectifier
Diode, lN4005
Fuse, 1.5A SB (240VAC)
Fuse, 3A SB (120VAC)
Harmonic Filter Assembly
AC Line Connector
BNC Bulkhead Jack
BNC Bulkhead Receptacle, Insulating
BNC Bulkhead Receptacle
Relay
RF Choke
RF Choke
Analog Meter
Digital Meter
Resistor, $4.99 \mathrm{~K}, 1 / 8 \mathrm{~W}$
Resistor, 620 ohms, $1 / 2$ Watt
Resistor, lK, l/2 Watt
Resistor, 68 ohms, 2 Watt
Toggle Switch
Toggle Switch
Transformer
Terminal Board
Power Cord

PART NUMBER
643-0052-001
643-0003-001
643-0006-001
643-0009-001
643-0012-001
643-0018-001
643-0024-001
643-0054-001
009-5007-001
183-5008-010
913-7007-010
912-2768-000
913-1186-000
913-5019-530
357-6000-010
353-5017-010
353-6442-050
264-0303-000
264-0306-000
643-0053-001
357-6601-010
357-6602-010
357-0076-010
357-9607-000
401-5011-010
240-2679-040
240-2715-530
458-5004-010
262-5007-010
705-3605-330
745-1343-000
745-0914-650
745-5602-000
266-9713-010
266-3712-010
667-4001-010
367-0020-000
424-3000-010

## TYPE 802A FM EXCITER - PARTS LIST 643-0001-000 <br> Page 2 of 2

REF. DES.

Pl thru P4
Plo, Pll, Pl4,
Pl5, Pl7, Pl8
P21, P22
P20
-
P16
-
P19
-
P13
-
P12
-
P23
-
-
-
-
-
-

DESCRIPTION
PART NUMBER

BNC Plug
357-7279-010

Connectors, 16 Pin
372-9604-010
Connector, 6 Pin 372-9604-160
Terminals for Above Plugs
372-9604-080
Connector, 6 Pin
372-9604-110
Terminal for Pl6
372-9604-050
Connector, 6 Pin
372-9604-090
Terminal for Pl9
Connector, 12 Pin
372-9604-010

Terminal for Pl3
Connector, 6 Pin
Terminal for Pl2
372-5909-790

Connector, DIP
Cover for P23
Slide
Vibration Isolator
015-9508-010

Clip-on Receptacle, l/4 T Fastener 0l2-0050-050
1/4 T Fastener 012-1507-000
Retainer, 1/4 T Fastener
012-2782-000


Figure 6-1. Modulator Oscillator Assembly, Al

Al MODULATED OSCILLATOR ASSEMBLY - PARTS LIST 643-0052-001


DESCRIPTION
PART NUMBER

Al
C1, C2, C4
C3
C5
El
J1, J2
J3
J3
Ll, L2, L3, L4

Card, Modulated Osc.
Feedthru Cap. 1000PF
Capacitor, 82PF
Capacitor, .56UF
Teflon Feedthru
Connector
Connector Terminals
Connector
RF Choke

Box, Modulated Osc.
Schematic
Spacer

643-0015-001
913-4064-000
912-3873-000
913-5019-530
306-3002-010
357-9670-000
372-9604-020
372-9604-090
240-2679-040

643-0041-001
-
-
643-0016-001
540-9209-003


Figure 6-2. Modulated Oscillator Bd, AlAI

## AlAl MODULATED OSCILLATOR - PARTS LIST 643-0015-001

REF. DES.
DESCRIPTION
Cl
C2, C3
C4, C5
C6
C7
C8
C9, Clo
Cll, Cl2
Cl3, C14
Cl5
Cl 6
Cl7
Cl8, Cl9
C20
C21, C22
C23
CRI, CR2
CR3
CR4
CR5, CR6
CR7, CR8
El
thru E7
Ll, L2
L3, L4
L5
Q1, Q2
Q3, Q4
R1
R2
R3
R4, R5
R6
R7
R8
R9
Rlo
Rll
R12
Rl3
R14
R15
R16

Capacitor, 470PF
Capacitor, 47PF
Capacitor, 390PF
Capacitor, 47UF
Capacitor, 470PF
Capacitor, 47PF
Capacitor, 470PF
Capacitor, 470PF
Capacitor, 470PF
Capacitor, 470PF
Capacitor, 27PF
Capacitor, 22PF
Capacitor, loUF
Capacitor, 47UF
Capacitor, 470 PF
Capacitor, 470PF
Varactor, KV2801
Varactor, KV2801
Varactor, KV2801
Diode, lN4005
Diode
'Terminal

RF Coil, .05lUH
RF Choke, l.OUH
RF Coil, .llUH
Transistor, U310
Transistor, 2N5109
Resistor, 2.2K, 1/4Watt
Resistor, $47 \mathrm{~K}, \mathrm{l} / 2$ Watt
Resistor, 100 Ohm, $1 / 4$ Watt
Resistor, 470 Ohm, $1 / 4$ Watt
Resistor, $120 \mathrm{~K}, 1 / 4$ Watt
Resistor, 560 Ohm, $1 / 4$ Watt
Resistor, 220 Ohm, 1/4 Watt
Resistor, 820K, $1 / 4$ Watt
Resistor, $390 \mathrm{~K}, 1 / 4$ Watt
Resistor, 820 Ohm, 1/4 Watt
Resistor, 120 Ohm, $1 / 4$ watt
Resistor, $1.5 \mathrm{~K}, 1 / 4$ Watt
Resistor, $3.3 \mathrm{~K}, 1 / 4$ Watt
Resistor, 180 Ohm, $1 / 4$ Watt
Resistor, 150 Ohm, 1/4 Watt

PART NUMBER
913-1189-000
912-3856-000
912-3921-000
183-5007-020
913-1189-000
912-3856-000
913-1189-000
913-1189-000
913-1189-000
913-1189-000
912-3844-000
912-3842-000
183-5007-060
183-5007-020
913-1189-000
913-1189-000
922-8004-010
922-8004-010
922-8004-010
353-6442-050
353-0448-020
306-1126-000
278-5042-040
240-1590-000
278-5042-010
352-4005-000
352-0863-020
745-0760-000
745-0808-000
745-0712-000
745-0736-000
745-0823-000
745-0739-000
745-0724-000
745-0853-000
745-0841-000
745-0745-000
745-0715-000 745-0754-000
745-0766-000
745-0721-000
745-0718-000

REF. DES.

RI 7
R18
R19
R20
R21
R22
R23
R24
R25
R26
U1
-

- Hex Nut, 6-32
- 
- 
- 
- 

I.C., LM317T

Pad

DESCRIPTION

Resistor, I. 5K, I/4 Watt
Resistor, $3.3 \mathrm{~K}, 1 / 4$ Watt
Resistor, 10 Ohm, $1 / 4$ Watt
Resistor, 150 Ohm, $1 / 4$ Watt
Resistor, $1 \mathrm{~K}, 1 / 4$ Watt
Resistor, 47 Ohm, 1/4 Watt
Resistor, 15 Ohm, 1/4 Watt
Resistor, 243 Ohm, 1/8 Watt
Resistor, $2.67 \mathrm{~K}, 1 / 8$ Watt
Resistor, 100 Ohm, $1 / 4$ Watt

352-9552-620
313-0045-000
310-0071-000
310-0046-000
343-0169-000
352-9552-120
643-0016-001
643-0014-001


DESCRIPTION

| REF. DES. | DESCRIPTION | PART NUMBER |
| :---: | :---: | :---: |
| Cl | Capacitor, 1000PF | 913-1186-000 |
| C2 | Capacitor, .lUF | 913-5019-320 |
| C3 | Capacitor, louF | 183-5007-060 |
| C4, C5 | Capacitor, .lUF | 913-5019-320 |
| C6, C7 | Capacitor, .lUF | 913-5019-320 |
| C8 | Capacitor, louF | 183-5007-060 |
| C9, Cl0 | Capacitor, .lUF | 913-5019-320 |
| Cll, Cl2 | Capacitor, .lUF | 913-5019-320 |
| Cl3 | Capacitor, 47UF | 183-5007-020 |
| Cl4, Cl5 | Capacitor, .lUF | 913-5019-320 |
| Cl6, Cl7 | Capacitor, .lUF | 913-5019-320 |
| Cl8, Cl9 | Capacitor, .lUF | 913-5019-320 |
| C20 | Capacitor, l0UF | 183-5007-060 |
| C21 | Capacitor, l000pF | 913-1186-000 |
| CR1, CR2 | Diode, , lN4148 | 353-3763-010 |
| DS1, DS2 | LED, Green | 353-0293-010 |
| Jl | Connector | 259-5205-010 |
| J2 | Connector | 372-9604-190 |
| J3 | Connector | 372-9604-180 |
| Ll | RF Choke, l.8UH | 240-1571-000 |
| Pl | Connector | 372-9604-150 |
| Q1, Q2 | Transistor, 2N2222A | 352-0661-020 |
| Q3, Q4 | Transistor, 2N2222A | 352-0661-020 |
| R1 | Resistor, 47 ohm, 1/4 Watt | 745-0700-000 |
| R2 | Resistor, 1000 ohm, 1/4 Watt | 745-0748-000 |
| R3 | Resistor, 10K, 1/4 Watt | 745-0784-000 |
| R4 | Resistor, 5.6K, 1/4 Watt | 745-0775-000 |
| R5 | Resistor, $6.8 \mathrm{~K}, \mathrm{l} / 4$ Watt | 745-0778-000 |
| R6 | Resistor, $220 \mathrm{~K}, \mathrm{l} / 4$ Watt | 745-0832-000 |
| R7 | Resistor, 100 ohm, 1/4 Watt | 745-0712-000 |
| R8 | Resistor, 680 ohm, 1/4 Watt | 745-0742-000 |
| R9 | Resistor, 220K, 1/4 Watt | 745-0832-000 |
| R10 | Resistor, 180 ohm, 1/4 Watt | 745-0721-000 |
| Rll, R12 | Resistor, Network, 10K | 350-4601-010 |
| R13 | Resistor, 6.8K, 1/4Watt | 745-0778-000 |
| R14 | Resistor, $220 \mathrm{~K}, \mathrm{l} / 4$ Watt | 745-0832-000 |
| R15 | Resistor, 100 ohm, 1/4 Watt | 745-0712-000 |
| R16 | Resistor, 680 ohm, 1/4 Watt | 745-0742-000 |
| R17 | Resistor, $220 \mathrm{~K}, \mathrm{l} / 4$ Watt | 745-0832-000 |
| R18 | Resistor, 180 ohm, 1/4 Watt | 745-0721-000 |
| R19 | Resistor, 470 ohm, 1/4 Watt | 745-0736-000 |
| R20, R21, R22 | Resistor, 2700 ohm, 1/4 Watt | 745-0763-000 |

A2 FREQUENCY DIVIDER - PARTS LIST 643-0003-001 (Continued)
REF. DES.
DESCRIPTION
PART NUMBER

Sl, S2
S3, S4
TPl
TP2, TP3
TP4, TP5
Ul
U2
U3, U4
U5, U6
U7
U8
U9
Ul0
xUl
XU2
XU3, XU4
XU5, XU6
XU7, XU8
XU9, XUl0
Yl
-
-

- Screw No. 2 Self-Tapping
- 
- 

Switch
Switch
Test Point
Test Point
Test Point
I.C., MCl2011P
I.C., SN74LS74AN
I.C., SN74LSI9ON
I.C., SN7420N
I.C., SN74121N
I.C., SN74LS93N

Socket, 14 Pin
Socket, 14 Pin
Crystal Oscillator

Trans-Pad

266-0243-010
266-0243-010
360-5003-010 306-1126-000
306-1126-000
351-4708-010
351-1710-020
351-1711-010
I.C., SN74LSI9ON 351-1711-010 351-1548-090 351-1187-010 351-1711-060
I.C., SN74LS90N 35l-l711-050

Socket, 16 Pin 220-0049-020
Socket, 14 Pin 220-0049-010
Socket, 16 Pin 220-0049-020
Socket, 16 Pin 220-0049-020
220-0049-010
220-0049-010
270-3003-010

LED Spacer 262-5006-010
352-9552-620
Screw No. 2 Self-Tapping MS5l861-2C
Circuit Board 643-0002-001
Schematic 643-0004-001

0
 DESNGNATIONS OR BCTH FOR COMPLETE DESIGNATION.
2. IIPCUIT BOARD FABRICATION SHALL MEET OR EXCEEO RERUIPEMENTS OF MIL-P-55IIOB ANO MIL-STD-Z7SC

REF. DES.
$\mathrm{Cl}, \mathrm{C} 2$
C3
C4
C5
C6
C7
C8
C9
Clo
Cl1, Cl2
Cl3
Cl4
Cl5
Cl6
Cl7, Cl8
Cl9
C20
C21, C22
C23
C24
C25
C26
C27, C28
C29
C30, C31
C32, C33
C34
C35
CR1, CR2
CR3, CR4
CR5, CR6
CR7, CR8
CR9, CRI0, CRIl
DS1, DS2
J1, J2
L1, L2, L3
Q1, Q2
R1, R2
R3
R4
R5

DESCRIPTION

Capacitor, .lUF
Capacitor, l00UF
Capacitor, 470UF
Capacitor, .lUF
Capacitor, 470UF
Capacitor, lUF
Capacitor, 33UF
Capacitor, l00PF
Capacitor, . 27UF
Capacitor, 47UF
Capacitor, l0UF
Capacitor, l00UF
Capacitor, l0UF
Capacitor, 47UF
Capacitor, .lUF
Capacitor, loUF
Capacitor, 47 UF
Capacitor, .lUF
Capacitor, l000PF
Capacitor, 500PF
Capacitor, l000PF
Capacitor, 500PF
Capacitor, 47UF
Capacitor, 220pf
Capacitor, 18PF
Capacitor, 6.8PF
Capacitor, lOUF
Capacitor, .lUF
Diode, lN4148
Diode, 1N4005
Diode, lN4005
Diode, lN4148
Diode, lN4148
LED
Connector
RF Choke, l.8UHY
Transistor, 2N2222A
Resistor, 10K, 1/4Watt
Resistor, 100 ohm, l/4 Watt
Resistor, l0K, l/8 Watt
Resistor, l00K, $1 / 8$ Watt

PART NUMBER

913-5019-320
183-5007-050
183-5007-010
913-5019-320
183-5007-010
913-5019-560
183-5007-030
913-7007-010
913-5019-490
183-5007-020
183-5007-060
183-5007-050
183-5007-060
183-5007-020
913-5019-320
183-5007-060
183-5007-020
913-5019-320
913-7006-010
913-7006-020
913-7006-010
913-7006-020
183-5007-020
913-7006-060
913-7006-050
913-7006-030
183-5007-060
913-5019-320
353-3763-010
353-6442-050
353-6442-050
353-3763-010
353-3763-010
353-0293-010
372-9604-190
240-1571-000
352-0661-020
745-0784-000
745-0712-000
705-1454-630
705-1092-000

REF. DES.
DESCRIPTION
Resistor, 470 ohm, $1 / 4$ Watt Resistor, l00K, $1 / 8$ Watt
Resistor, l0K, $1 / 8$ Watt
Resistor, l00K, $1 / 8$ Watt
Resistor, $2.2 \mathrm{~K}, 1 / 4$ Watt
Resistor, 15K, 1/4 Watt
Resistor, lK, 1/4 Watt
Resistor, l00K, l/4 Watt
Resistor, $8.2 \mathrm{~K}, 1 / 4$ Watt
Resistor, 470 ohm, 1/4 Watt
Resistor, $470 \mathrm{~K}, 1 / 4$ Watt
Resistor, lK, $1 / 4$ Watt
Resistor, $6.8 \mathrm{~K}, 1 / 4$ Watt
Resistor, $1 \mathrm{~K}, \mathrm{l} / 4$ Watt
Resistor, $12 \mathrm{~K}, 1 / 4$ Watt
Resistor, l. $8 \mathrm{~K}, 1 / 4$ Watt
Resistor, $6.8 \mathrm{~K}, 1 / 4$ Watt
Resistor, 180 ohm, $1 / 4$ Watt
Resistor, l0K, l/8 Watt
Resistor, 2.15K, 1/8 Watt
Resistor, $4.42 \mathrm{~K}, 1 / 8 \mathrm{Watt}$
Resistor, $560 \mathrm{~K}, 1 / 4$ Watt
Resistor, 180 ohm, $1 / 4$ Watt
Resistor, $6.8 \mathrm{~K}, 1 / 4$ Watt
Resistor, $49.9 \mathrm{~K}, 1 / 8$ Watt
Resistor, 3.9K, l/4 Watt
Resistor, $49.9 \mathrm{~K}, 1 / 8$ Watt
Resistor, 3.9K, $1 / 4$ Watt
Resistor, 4.99K, 1/8 Watt
Resistor, $24.9 \mathrm{~K}, 1 / 8$ Watt
Resistor, $4.99 \mathrm{~K}, 1 / 8$ Watt.
Resistor, $82.5 \mathrm{~K}, 1 / 8$ Watt
Resistor, $18 \mathrm{~K}, 1 / 4$ Watt
Resistor, lok, l/2 Watt, VAR
Resistor, $24.9 \mathrm{~K}, 1 / 8$ Watt
Resistor, $4.99 \mathrm{~K}, 1 / 8$ Watt
Resistor, $4.99 \mathrm{~K}, 1 / 8$ Watt
Resistor, 5K, l/2 Watt, VAR
Resistor, 4.7K, l/4 Watt
Resistor, l0K, $1 / 4$ Watt
Resistor, lK, 1/4 Watt
Resistor, 20K, l/2 Watt, VAR

PART NUMBER
745-0736-000
705-1092-000
705-1454-630
705-1092-000
745-0760-000
745-0790-000
745-0748-000
745-0820-000
745-0781-000
745-0736-000
745-0844-000
745-0748-000
745-0778-000
745-0748-000
745-0787-000
745-0757-000
745-0778-000
745-0721-000
705-1454-630
705-1012-000
705-1027-000
745-0847-000
745-0721-000
745-0778-000
705-3605-810
745-0769-000
705-3605-810
745-0769-000
705-3605-330
705-1063-000
705-3605-330
705-1088-000
745-0793-000
382-1405-070
705-1063-000
705-3605-330
705-3605-330
382-1405-060
745-0772-000
745-0784-000
745-0748-000
382-1405-080

REF. DES.
DESCRIPTION

Resistor, loK, l/4 Watt 745-0784-000
Resistor, 180 ohm, l/4 Watt 745-0721-000
Resistor, 500 ohm, 1/2 Watt,VAR 382-1405-030
Resistor, 39K, l/4 Watt 745-0805-000
Resistor, $100 \mathrm{ohm}, 1 / 4$ Watt 745-0712-000
Resistor, l00K, l/4 Watt 745-0820-000
Resistor, 39K, l/4 Watt 745-0805-000
Resistor, 100 ohm, 1/4 Watt 745-0712-000
Resistor, l00K, l/4 Watt 745-0820-000
Resistor, 150 ohm, 1/4 Watt 745-0718-000
Resistor, $100 \mathrm{ohm}, \mathrm{l} / 4$ Watt 745-0712-000
Resistor, $2.2 \mathrm{~K}, 1 / 4$ Watt 745-0760-000
Resistor, 4.7K, l/4 Watt 745-0772-000
Resistor, lK, 1/4 Watt 745-0748-000
Resistor, l00K, l/8 Watt 705-1092-000
Test Point 306-1126-000
thru
TPlo
Ul
U2
U3, U4
U5
U6
U7
U8
U9
Ul0
Ull
VRl, VR2
XUl
XU2
XU5
XU6
XU9
XU3, 4, 7, 8
I.C. MCl4568BCP

351-8883-010
I.C., LF353N

351-1370-040
I.C., CLM-51
I.C., SN74LS74AN

352-4010-010
I.C., LM358N

351-1710-020
I.C., CLM-51
I.C., 4N28
I.C., LF 347 N
I.C., UA7815UC
I.C., UA7915UC

351-1211-040
352-4010-010
351-0047-030
351-1370-020
351-1120-050
351-1124-160
Zener, lN4739A 353-6481-230
Socket, 16 Pin 220-0049-020
Socket, 8 Pin 220-0049-100
Socket, 14 Pin 220-0049-010
Socket, 8 Pin 220-0049-100
Socket, 14 Pin 220-0049-010
Socket, 6 Pin 220-6015-010
Spacer 262-5006-010
Mounting Pad 352-9552-620
Flat Washer, No. 6
310-0046-000
Lock Washer, No. 6
310-0071-000
Screw, 6-32×3/8 343-0169-000
Nut, 6-32 313-0045-000
Circuit Board 643-0005-001
Schematic
R57
58
R59
R60
R61
R62
R63
R64
R65
R66
R6 7
R68, R69
R70
R71
R72
Pl

U5

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

```
x
```

- 
- 

Lock Washer, No. 6
Nut, 6-32
Circuit Board
643-0007-001


NOTES:

1. PARTIAL RETERENCE DFSIGNATIONS ARE SHOWN. PREFIX WITH UNIT NUMBEP OR SUB-ASSEMBLY DESIGNATIONS OR BOTH FOR COMPLETE DESIGNATION.
2. CIRCUIT BOARD FABRICATION SHALL MEET OR EXCEED REQUIREMENTS OF MIL-P-55HOB AWD MIL-STD-ZTSC

Ref. 643-0009-001 Rev. -
Figure 6-5. Power Supply Assembly, A4



NOTES:
1 PARTIAL PEFERENCE DESIGNATIONS ARE SHOWN. PREFIX WITH UNIT NUMBER OR SUB-ASSEMBLY DESIGNATIONS OR BOTH FOR COSPLETE DESIGNATION.
2 CIRCUIT BOARD FABRICATION SHALL MEET OR EXCEED REQUIREMENTS OF MIL-P-55/10B AND MIL-STD-275C.

## REF DES.

Cl
C2
C3
C4
C5, C6
C7, C8, C9
CR1, CR2
CR3, CR4
Fl
Jl
J2
Q1
Q2
R1, R2
R3, R4
R5
R6
R7, R8
R9
R10
Rll
R12
Rl3
R14
R15
R16
R17
R18
R19
R20
R21
R22
R23
R24
R25
R26
R27
R28
R29
R30, R31
R32
R33

REF. DES.
R34
R35, R36
R37
R38
R39
R4 0
R41
R42, R43
R44
R45
R46
R4 7
R48
R49
Sl
Ul
U2
U3
VRI
VR2
XUl
XU2
XU3
-
-
-
-
-
-
-
-
-

## DESCRIPTION

Resistor, 2.2 ohm, 10 Watt
Resistor, $3.9 \mathrm{~K}, 1 / 4$ Watt
Resistor, $6.8 \mathrm{~K}, 1 / 4$ Watt
Resistor, l0K, l/4 Watt
Resistor, loK, l/8 Watt
Resistor, l0K, VAR
Resistor, 4.99K, 1/8 Watt
Resistor, l0K,'l/8 Watt
Resistor, $249 \mathrm{~K}, 1 / 8$ Watt
Resistor, l000K, l/8 Watt
Resistor, 10 ohm, l/4 Watt
Resistor, 680 ohm, 1/4 Watt
Resistor, $1 \mathrm{~K}, 1 / 4$ Watt
Resistor, 10 ohm, l/4 Watt
Switch, Slide, SPDT
I.C., LM358N
I.C., UA723PC
I.C., LM358N

Zener Diode, 1N4752A
Zener Diode, lN4753A
Socket, 8 Pin
Socket, 14 Pin
Socket, 8 Pin

Hex Nut, 6-32
Lock Washer, No. 6
Flat Washer, No. 6
Screw, 6-32×3/8 PPH
Fuse Clip
Mounting Pad
Schematic
Circuit Board

PART NUMBER

725-3002-010
745-0769-000
745-0778-000
745-0784-000
705-1454-630
382-5001-010
705-3605-330
705-1454-630
705-1111-000
705-1117-000
745-0676-000
745-0742-000
745-0748-000
745-0676-000
266-9714-010
351-1211-040
351-1035-060
351-1211-040
353-6481-490
353-6481-510
220-0049-100
220-0049-010
220-0049-100

313-0045-000
310-0071-000
310-0046-000
343-0169-000
265-9505-000
352-9552-620
643-0013-001
643-0011-001


## NOTES:

1. PARTIAL REFERENCE DESIGNATION ARE SHOWN, PREFIX WITH LINIT NUMBER OP SUB-ASSEMELY DESIGNATIONS OR BCTH FUR COMPLETE DESIGNATION.
2. CIPCUIT BOARD FABRICATIDN SHALL MEET OP EXCECED REQUIREMENTS OF MIL-P-SSIIOB AND MIL-STD-275C.

Ref. 643-0018-001 Rev. -

Figure 6-7. Modulation Display Assembly, A6

REF. DES.
Cl, C2, C3
C4
C5
C6, C7
C8

## C9

C10
CRI, CR2, CR3
CR4, CR5
CR6, CR7
DS1, DS2
DS3, DS4, DS5
DS6, DS7
Jl
J2
Q1
Rl
R2
R3, R4, R5
R6
R7, R8
R9
Rl0, R11
Rl2
R13
R14, R15
R16
R17
R18
R19
R20
R21
R22
R23
R24, R25, R26
R27
R28
R29
R30
R31
R32
R33

## DESCRIPTION

Capacitor, 6.8PF
Capacitor, .002UF
Capacitor, 6.8PF
Capacitor, 47UF
Capacitor, .lUF
Capacitor, louF
Capacitor, 47UF
Diode
Diode, lN4148
Diode, 1N4148
Bar Graph Array
L.E.D. Red
L.E.D., Green

Connector
Connector
XSTR, 2N2222A
Resistor, 100K, 1/4 Watt
Resistor, l0K, $1 / 2$ Watt, VAR
Resistor, l0K, $1 / 8$ Watt
Resistor, 4.99K, 1/8 Watt
Resistor, l0K, $1 / 8$ Watt
Resistor, $100 \mathrm{~K}, 1 / 8$ Watt
Resistor, 10K, 1/8 Watt
Resistor, $5600 \mathrm{~K}, 1 / 4$ Watt
Resistor, $470 \mathrm{~K}, 1 / 4$ Watt
Resistor, loK, 1/4 Watt
Resistor, l. $2 \mathrm{~K}, \mathrm{l} / 4$ Watt
Resistor, $5 \mathrm{~K}, 1 / 2$ Watt, VAR
Resistor, 10K, 1/4 Watt
Resistor, l. $2 \mathrm{~K}, \mathrm{l} / 4$ Watt
Resistor, l.8K, 1/4 Watt
Resistor, l0K, 1/4 Watt
Resistor, 120 ohm, l/4 Watt
Resistor, 220K, 1/4 Watt
Resistor, Network 180 ohm
Resistor, 820 ohm, 1/4 Watt
Resistor, 220 ohm, l/4 Watt
Resistor, 180 ohm, $1 / 4$ Watt
Resistor, $6.8 \mathrm{~K}, 1 / 4$ Watt
Resistor, 10K, $1 / 4$ Watt
Resistor, l. $5 \mathrm{~K}, 1 / 4$ Watt
Resistor, l.8K, l/4 Watt

PART NUMBER
913-7006-030
913-5019-240
913-7006-030
183-5007-020
913-5019-320
183-5007-060
183-5007-020
353-0448-020
353-3763-010
353-3763-010
262-5008-010
353-0293-040
353-0293-010
372-9604-190
372-9604-180
352-0661-020
745-0820-000
382-1405-220
705-1454-630
705-3605-330
705-1454-630
705-1092-000
705-1454-630
745-0883-000
745-0844-000
745-0784-000
745-0751-000
382-1405-210
745-0784-000
745-0751-000
745-0757-000
745-0784-000
745-0715-000
745-0832-000
350-4600-010
745-0745-000
745-0724-000
745-0721-000
745-0778-000
745-0784-000
745-0754-000
745-0757-000

A6 MODULATION DISPLAY ASSEMBLY - PARTS LIST 643-0018-001 (CONT.)

REF. DES.
R34
R35
R36
TPl
thru
TP5
Ul
U2, U3
U4
XDS1, XDS2
XU1
XU2, XU3
XU4
-
-
-
-

Resistor, $22 \mathrm{~K}, 1 / 4$ Watt
PART NUMBER
-745-0796-000
Resistor, $1 \mathrm{~K}, 1 / 8$ Watt Resistor, $3.01 \mathrm{~K}, 1 / 8$ Watt Terminal
I.C., LF 347 N

351-1370-020
I.C., LM3914N
I.C., LM555CN

351-4709-010
351-1140-010
Socket, 20 Pin
220-0049-090
Socket, 14 Pin
Socket, 18 Pin
220-0049-010

Socket, 8 Pin
220-0049-060
220-0049-100

XSTR Pad
352-9552-620
L.E.D. Spacer

262-5006-010
Schematic
643-0019-001
Circuit Board
643-0017-001

notes:

1. PARTIAL REFERENLE DESIGNATIONS ARE SHOWN. PREFIX WITH UNIT NUMBER OR SUB-ASSEMBLY DESIGNATIONS OR BOTH FOR COMPLETE DESIGNATION.
2. CIRCUIT BOARO FABRICATION SHALL MEET OR EXCEED REQUIREMENTS OF MIL-P-55IIOB AND MIL-STD-275C.

Ref. 643-0024-001 Rev. -

Figure 6-8. Metering Network Assembly, A7

REF. DES.
J1, J2
R1, R2, R3
R4
R5
R6
R7
R8
Sl
VRI

DESCRIPTION
PARTS NUMBER

| Connector | $372-9604-190$ |
| :--- | :--- |
| Resistor, $100 \mathrm{~K}, ~ 1 / 8$ Watt | $705-1092-000$ |
| Resistor, $9.09 \mathrm{~K}, ~ 1 / 8$ Watt | $705-1042-000$ |
| Resistor, $1.01 \mathrm{~K}, ~ 1 / 8$ Watt | $705-2502-010$ |
| Resistor, $499 \mathrm{~K}, 1 / 8$ Watt | $705-1118-000$ |
| Resistor, $1.01 \mathrm{~K}, 1 / 8$ Watt | $705-2502-010$ |
| Resistor, Variable, 1K | $382-1405-040$ |
| Switch, 10 Station | $266-9711-000$ |
| Diode, 1N4728A | $353-6481-010$ |

Schematic
643-0025-001
Circuit Board 643-0023-001

ARI, OUTPUT AMPLIFIER ASSEMBLY - PARTS LIST 643-0054-001

| REF. DES. | DESCRIPTION | PART NUMBER |
| :---: | :---: | :---: |
| Al | Card, Output Amplifier | 643-0027-001 |
| Cl, C2, C3, C4 | Capacitor, Feedthru, l000pF | 913-4064-000 |
| C5 | Capacitor, . $56 \mu \mathrm{~F}$ | 913-5019-530 |
| J1, J2 | Connector | 357-7093-000 |
| J3 | Connector | 372-5909-990 |
| L1, L2, L3, L4 | RF Choke | 288-0842-100 |
| Q1 | XSTR, MJ3001 | 352-5016-010 |
| Rl | Resistor, 2.7K, 1/4 watt | 745-0910-750 |
| Sl | Temp. Switch | 267-5001-000 |
| XQ1 | Socket, T0-3 | 220-0968-010 |
| - | Cable Clamp | 150-1540-000 |
| - | XSTR Insulator | 352-9655-040 |
| - | Terminal for J3 | 372-9604-050 |
| - | Spacer | 643-0043-001 |
| - | Output Amplifier Cover | 643-0039-001 |
| - | Front Heatsink Bracket | 643-0038-001 |
| - | Rear Heatsink Bracket | 643-0037-001 |
| - | Heatsink Support No. 2 | 643-0036-002 |
| - | Heatsink Support No. 1 | 643-0036-001 |
| - | Heatsink | 643-0035-001 |



0

ARIAl OUTPUT AMPLIFIER - PARTS LIST 643-0027-001

REF. DES.
Cl
C2
C3, C4, C5
C6
C7
C8
C9
Clo
Cll
Cl2
Cl3
Cl4
Cl5
Cl 6
Cl7
Cl8, Cl9
C20
C21
C22
C23
C24
C25, C26
C27
C28, C29
C30, C31, C32
C33
C34
C35
C36
CR1, CR2
El
thru
El2
L1
L2, L3
L4
L5
L6
L7
L8
L9
L10

L2, L3
L4
L5
L6
L7
L8

Llo

DESCRIPTION
Capacitor, 470PF
Capacitor, 47PF
Capacitor, 390PF
Capacitor, 470PF
Capacitor, 47UF
Capacitor, 390PF
Capacitor, 68PF
Capacitor, 12PF
Capacitor, 47PF
Capacitor, 390PF
Capacitor, 470PF
Capacitor, 47UF
Capacitor, 470PF
Capacitor, 47PF
Capacitor, 68PF
Capacitor, 220PF
Capacitor, 390PF
Capacitor, 470PF
Capacitor, 47UF
Capacitor, l000pF
Capacitor, 39PF
Capacitor, 330PF
Capacitor, 47PF
Capacitor, 330PF
Capacitor, .56UF
Capacitor, 6.8PF
Capacitor, 47PF
Capacitor, l0PF
Capacitor, 47PF
Diode
Terminal

RF Coil, .05lUH
RF Choke, 1.0UH
RF Choke, .56UH
RF Coil, .032UH
RF Coil, .023UH
RF Coil, .llUH
RF Coil, .051UH
RF Choke
RF Choke

PART NUMBER
913-1189-000
912-3856-000
912-3921-000
913-1189-000
183-5007-020
912-3921-000
912-3867-000
912-3922-000
912-7025-030
912-3921-000
913-1189-000
183-5007-020
912-7025-060
912-7025-030
912-7025-040
912-7025-050
912-3921-000
913-1189-000
183-5007-020
912-7025-070
912-3853-000
912-3915-000
912-3856-000
912-3915-000
913-5019-530
913-7006-030
912-7025-030
912-3837-000
912-3856-000
353-0448-020
306-1126-000

278-5042-040
240-1590-000
240-0874-050
278-5042-030
278-5042-020
278-5042-010
278-5042-040
240-2679-040
278-5041-000


motes:
4OTES: PARIIAL REFERENCE DESIGNuTIGNS
APE SNOWN FREFIX WITH UNIT
NLMBER OP SUB-ASSEMBLV
DEEIGNATIONS CR ACTH FUR
CEMPLETE DEELGNATIOA.
2 GRELIT BOAFD FABPKATION SWALL MEFT OP CKCLFD PRQUIREMFNTS CF
3. $50 L O E R Q Z$ QG TO EOARE

AFTEF MOUHTMS TCHEATSINK
Ref. 643-0027-001

Figure 6-10. Output Amplifier, ARIAl
0

ARIA1 OUTPUT AMPLIFIER - PARTS LIST 643-0027-001 (CONT.)

| REF. DES. | DESCRIPTION | PART NUMBER |
| :---: | :---: | :---: |
| Lll | RF Coil, . 051 UH | 278-5042-040 |
| L12 | RF Choke, 1.OUH | 240-1590-000 |
| Ll3 | RF Choke | 240-2679-040 |
| L14 | RF Choke | 278-5041-000 |
| L15 | RF Coil, .032UH | 278-5042-030 |
| Q1 | XSTR, 2N3553 | 352-0632-010 |
| Q2 | XSTR, PT9732 | 352-4909-010 4010 |
| Q3 | XSTR, MRF315A | 352-5016-020= |
| Rl | Resistor, 1.2K, 2 Watt | 745-5655-000 |
| R2 | Resistor, 100 ohm, 1/2 Watt | 745-1309-000 |
| R3 | Resistor, 15 ohm, 1/2 Watt | 745-1274-000 |
| R4 | Resistor, 22 ohm, 1/2 Watt | 745-1281-000 |
| R5 | Resistor, 10 ohm, 1/2 Watt | 745-1267-000 |
| R6, R7 | Resistor, 22 ohm, 2 Watt | 745-5581-000 |
| R8 | Resistor, 200 ohm, 1/2W, VAR | 382-1405-020 |
| R9 | Resistor, 1K, l/2 Watt | 745-1351-000 |
| Rl0 | Resistor, 100 ohm, 1/2 Watt | 745-1309-000 |
| Rl1, Rl2 | Resistor, 1K, 1/2 Watt | 745-1351-000 |
| Rl3 | Resistor, 22 ohm, 1/2 Watt | 745-1281-000 |
| R14 | Resistor, 2.2K, 2 Watt | 745-5665-000 |
| R15, R16 | Resistor, 150 ohm, 2 Watt | 745-5616-000 |
| - | Heatsink | 352-4007-010 |
| - | Schematic | 643-0028-001 |
| - | Circuit Board | 643-0026-001 |





Ref. 643-0053-001 Rev. -

Figure 6-11. Harmonic Filter, FLl

FLI HARMONIC FILTER - PARTS LIST 643-0053-001

| REF. DES. | DESCRIPTION | PART NUMBER |
| :---: | :---: | :---: |
| Al | Card, Harmonic Filter | 643-0021-001 |
| J1, J2, J3 | Connector | 357-9670-000 |
| - | GND Bracket | 643-0059-001 |
| - | Washer, Flat, No. 6 | 310-0046-000 |
| - | Washer, Lock, No. 6 | 310-0071-000 |
| - | Nut, Hex, 6-32 | 313-0045-000 |
| - | Screw, PPH, 6-32x3/4 | 343-0174-000 |
| - | Spacer, 3/8 Long | 541-6025-002 |
| - | Enclosure | 643-0050-001 |

## SECTION 7 - VENDOR DATA

## 7.-1. SOLID STATE COMPONENT LAYOUT

Table 7-1 contains connection layouts for the Solid State Components.

TABLE 7-1. SOLID STATE COMPONENT LAYOUTS


LM 317


FRONT VIEW LM 337



TABLE 7-1. SOLID STATE COMPONENT LAYOUTS - Cont.


TABLE 7-1. SOLID STATE COMPONENT LAYOUT - COnt.


0

FACTORY TEST DATA
TYPE 802A 50 WATT FM EXCITER

SERIAL NO.
363
FREQUENCY $\qquad$ STATION KJYK

TESTED BY $\qquad$ B. Loi

DATE $\qquad$

MONO PERFORMANCE DATA


| FM NOISE $-\quad 78$ |
| :--- |
| AM NOISE $-\quad$ dB |
| IM DISTORTION $(4: 1)$ |

COMPOSITE PERFORMANCE DATA

FREQUENCY
( Hz )
50
1,000
10,000
20,000
40,000
75,000
100,000

DISTORTION
(100\% MOD)
0.04
0.042
0.043
0.035
0.035
0.048
0.075

## FACTORY TEST DATA <br> TYPE 802A 50 WATT FM EXCITER

## METER READINGS

| +22 |  |
| :--- | :---: |
| -22 |  |
| +5 | C |
| AFC | 21.3 V |



