## TYPE 816R-3

II|
FM BROADCAST TRANSMITTER WITH SOLD STATE EXCiTER 802A ||
INSTRUCTION MAMMAL


83-0753

KO1-(6)
Continental Electronica mFG $C O$. 4212 S. BUCKNER BLVD.

## CHANGE NOTICE

CHANGE NO. 18

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816R-3

FM BROADCAST TRANSMITTER

INSTRUCTION MANUAL

This Change No. 18 for the 8l6R-3 FM Broadcast Transmitter Instruction Manual is effective for all transmitters. This Change Notice should be filed just after the Title Page.

| NEW PAGE | OLD PAGE |  |  |
| :--- | :--- | :--- | :--- |
| $6-11 / 6-12$ | Cl3/Cl8 | $6-11 / 6-12$ | $\mathrm{Cl3/Cl3}$ |
| $6-15 / 6-16$ | Cl8/- | $6-15 / 6-16$ | $\mathrm{C} 4 /-$ |
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30 August 1984

Continental Electronics Mfg. Co.
4212 South Buckner Blvd. Dallas, Texas 75227-4299

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## EFFECTIVITY

All Transmitters
All Transmitters
All Transmitters
SN 329 and Above
All Transmitters
All Transmitters
SN 344 and Above
All Transmitters
All Transmitters
All Transmitters
All Transmitters After Date
All Transmitters After Date
SN 360 \& Above \& All Transmitters with 802A Exciter

SN 360 \& Above \& All Transmitters with 802A Exciter

SN 365 \& above \& All Transmitters with 802A Exciter

SN 360 \& Above \& All Transmitters with 802A Exciter

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83-0754

1-1. INTRODUCTION
The transmitter operates in the FM broadcast range ( $88-108 \mathrm{MHz}$ ) with an RF output power of 25,000 watts. Reduced power is available by tap changes of the plate and screen transformer to meet customer requirements. The FM Transmitter, 816R, provides monaural programming or other optional programming as customer requires. When the exciter is inputed with optional stereo generator and SCA generator, the transmitter provides continuous monaural, stereophonic, and SCA (subsidiary cormunication authorization) frequency-modulated programs.

## 1-2. FUNCTIONAL DESCRIPTION

The transmitter consists of an exciter, a driver, and power amplifier. The output of the exciter is applied to the driver. The driver stage consists of two 4 CX 250 B tubes operated class $C$. The input to the driver is amplified to approximately 400 watts and applied to the power amplfiier that contains one 4CXI5000A tube operated class $C$. The input to the power amplifier is amplified and applied to a 50-ohm unbalanced load. Power control circuits monitor the rf output power level. When a change in output power is detected, these circuits change the plate voltage to compensate. Other control circuits within the transmitter monitor reflected power, forward power, operating voltage, air pressure and exhaust air temperature within the power amplifier section. They protect the transmitter by removing power when excessive currents, VSWR, loss of air pressure, or excessive air exhaust temperature occur.

## 1-3. PHYSICAL DESCRIPTION

The transmitter is housed in a basic unistrut cabinet that contains all transmitter components. (Refer to figure l-l.) The transmitter contains three sections. The section on the left in figure l-l contains the power amplifier and driver circuits. The center section houses the control panel, exciter, and control circuits. The section on the right contains the power supplies, the circuit breaker, and fuse panel.

## 1-4. TECHNICAL CHARACTERISTICS

## 1-4.1 MECHANICAL

Weight: $\quad 890 \mathrm{~kg}$ (1962 pounds)
Size:

| Height: | 1752.6 mm (69 inches) |
| :--- | :--- |
| Width: | $1816.1 \mathrm{~mm}(71-1 / 2$ inches) |

## general description

Depth
698.5 mm (27-1/2 inches)

Ventilation (2 Sources):
Squirrel-cage type blower mounted under the cavity
Axial fan that provides positive air pressure within the entire cabinet of the transmitter.

Ambient Temperature Range:
$+15^{\circ}$ to $+40^{\circ} \mathrm{C}$ operating
Relative Humidity Range:
0 to $95 \%$ relative humidity
Altitude:
Up to 7500 feet at $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$
Shock and Vibration:
Normal handling and transportation
Finish:
Front Panel: Tan
Cabinet: Brown

### 1.4.2 ELECTRICAL

Frequency Range:
88 to 108 MHz
Maximum Power Output:
25,000 watts into a 50 -ohm unbalanced line
Standing Wave Ratio:
Not to exceed 2:1 (Refer to Figure 5-6)

## Power Source:

200 to 250 volts, $60 \mathrm{~Hz}, 3-\mathrm{phase}$ (closed delta or 208 V wye)
Available voltage taps on transformer: 200, 210, 220, 230, 240, and 250 $50-\mathrm{Hz}$ operation available on special order

Power Line Variation:
$\pm 5 \%$ overall power line variations; in addition, the phase angle and voltage unbalance shall be within $5 \%$ of the average of all three phases

Harmonic and Spurious Radiation:
Any emission appearing on a frequency removed from the carrier by between 120 kHz and 240 kHz inclusive is attenuated at least 25 dB below the level of the unmodulated carrier.
Any emission appearing on a frequency removed from the carrier by more than 240 kHz and up to and including 600 kHz is attenuated at least 35 dB below the level of the unmodulated carrier.

Any emission appearing on a frequency removed from the carrier by more than 600 kHz is attenuated at least 80 dB below the level of the unmodulated carrier.

Modulation Characteristics:
Wideband direct fm; standard audio preemphasis is incorporated

## Input Power Requirements:

$40-\mathrm{kW}$ nominal for $25-\mathrm{kW}$ output ( 44.4 kVA at 0.90 power factor)
Excitation Source:
A CEMC 802A Exciter
Output Impedance:
50 ohms, unbalanced
Carrier Frequency Stability:
Frequency will not vary more than $\pm 500 \mathrm{~Hz}$ for an ambient temperature range of +15 to $+45^{\circ} \mathrm{C}\left(59^{\circ}\right.$ to $\left.113^{\circ} \mathrm{F}\right)$ and a line voltage variation of $\pm 5 \%$

Audio Input Impedance:
600 ohms, balanced
Audio Input Level: $+10 \mathrm{dBm} \pm 2 \mathrm{~dB}$

Audio Frequency Response: Complies with FCC standard 75-microsecond preemphasis curve (other available on request.)

Audio Frequency Distortion:
Stereo
Not more than $0.5 \%, 50 \mathrm{~Hz}$ to 15 kHz
Monaural
Not more than $0.25 \%, 50 \mathrm{~Hz}$ to 15 kHz
FM Noise Level
65 dB below $100 \%$ modulation ( $\pm 75 \mathrm{kHz}$ )
AM Noise Level:
55 dB below equivalent $100 \%$ am modulation

### 2.1 Unpacking and Inspecting

### 2.1.1 Domestic Shipments

a. The uncrated transmitter is shipped on a shipping skid. The transmitter is not attached to the skid. Inspect for loose screws and fasteners. Ensure that all controls operate freely. Examine the cabinet for dents or scratches. Ensure that cable and wiring connections are tight and situated clear of each other and the chassis.
b. If any received item is freight damaged, the customer should accept the equipment, note the damage on the shipping documents and immediately file a freight claim. All boxes and packing material should be retained for the freight inspector. Refusal to accept delivery of damaged equipment removes the evidence and makes freight-damage reimbursement complicated or impossible.

### 2.1.2 Foreign Shipments

a. The transmitter is shipped in a skid-type crate with unpacking instructions stenciled on the side. Heavy iron components are crated separately, bolted down to a 2 -inch solid base. Uncrate the transmitter carefully to avoid damage. Inspect for loose screws and fasteners. Ensure that all controls operate freely. Examine the cabinet for dents or scratches. Ensure that cable and wiring connections are tight and situated clear of each other and the chassis.
b. File any damage claims properly with the transportation company. Retain all packing material if a claim is filed.
2.2 Assembly
a. Plan the placement of the transmitter and its external wiring carefully before beginning installation. (refer to figure 2-1 and paragraph 2-4.) Four knockout holes are located on the top of the transmitter section that contains the power supplies. The holes accommodate cabling for 3-phase input voltage, audio input signal, and the remote control unit. A 2-inch conduit entry is also provided in the floor of the power supply section.
b. If optional modulation and frequency monitoring equipment is used, remove the center rear panel before positioning the transmitter. Determine the length of cable needed to connect the transmitter sample output to the monitoring equipment. Once the length is determined, connect the cable to the monitor jacks, and run the cable out of the transmitter through a previously unused knockout hole.
c. If the 802 A exciter was not factory installed, mount it in the area provided in the transmitter center section. Connect an rf cable from exciter output to the driver input. Attach the override voltage lead from A4TB1-16 to A19E6 and the mono/stereo leads from XA12-39 to A4TB1-14 and XA12-40 to A4TB1-13. Connect the 117-volt ac power cable from the exciter to connector J3 (figure 2-1). Refer to the 5l0R-1 exciter instruction book for installation of audio input cables. Replace the rear cover and place the transmitter in its permanent location.
d. Connect primary power according to instructions supplied in paragraph 2.3.1
e. Transformers T1 and T2, filters L1 and L2, and filter capacitor C3 may have been removed to facilitate shipping. Install these components if they were shipped separately.
f. Check the transformer taps for proper connection. Refer to paragraph 2,3,2 and table 2.1.
g. If output tube 4CX15000A was removed for shipping, install it using the procedure outlined in paragraph 5.7.1.
h. If a remote control panel is used, run the external wiring from the remote unit into the transmitter and connect it to TB4 (figure 2-1). Also install the appropriate optional remote control relay cards, A2A3 and A2A1.
i. Connect the customer-supplied 50 -ohm transmission line to the rf output connector mounted on top of the transmitter cabinet.

CAUTION
damage will result from an improper impedance match between the transmitter and the transmission line. Ensure that the transmission line and antenna PRESENT A 50-OHM IMPEDANCE AND A VSWR NOT GREATER THAN $2: 1$ TO THE TRANSMitter at the operating frequency.

### 2.3 Primary Power

### 2.3.1 General

The transmitter requires a 200 to 250 volt $\pm 5 \%$, 3 -phase, $60-\mathrm{Hz}$ ac power source (closed delta or 208 V wye). A 200 amp fused disconnect should be provided with

* 150 amp fuses and not morc than 100 feet of No. $1 / 0$ ANG wiring to the transmitter. AC line transient suppressors are suggested for the primary lines. For recommendation of installation, call Broadcast Products Field Service.


### 2.3.2 Transformer Connection

The broad range of allowable voltage sources ( 200 to 250 volts) is made possible by the availability of different tap connections of power transformers T1, T2, T3, and T4 and power supply transformers PSIT1 and PS2T1. Table 2-1 shows the detalls of the proper primary line connections for various line voltages.

NOTE
The inftial connections on transformers Tl and T 2 may be changed after tuning to reduce am noise and to maintain authorized station maximum power output. (See paragraph 5.6.7.6) Tl connections are selected to provide a power output approximately 10 percent above the authorized station rating. T3 connections are selected to give 1800 to 2000 volts of driver voltage at the authorized station output.

Two connections are made at transformer T4. One connection is made at Terminal No. 1 regardless of the source voltage. The second wire is connected to correspond with the power source voltage and is connected to instructions supplied in table 2-1.




802A EXCITER



Figure 2-1. FM Transmitter


Six connectins are made on power supply transformer PSlTl. Three of these connections (at Terminals 1,4 and 7) are made regardless of the source voltage. The other three connections are made to correspond with the power source voltage. These wires are connected according to instructions supplied in table 2-1.

Two connections are made at power supply transformer PS2T1. One connection is made at Terminal No. l regardless of the source voltage. The second wire is connected to correspond with the power source voltage and is connected according to instructions supplied in table 2-1.

### 2.4 Transmitter Cooling

Adequate cooling of the transmitter is imperative to reduce downtime, to extend component reliability, and to provide longer tube life. An adequate supply of cool clean uncontaminated ambient air (temperature must not exceed $+45^{\circ} \mathrm{C}$ ) is required. See Table 2-2 for nominal heat balance readings. Consult a qualified air-conditioning engineer for recommendations on ducting and cooling requirements. When designing the cooling system, observe the following rules:
a. If the exhaust air is ducted away from the transmitter, the duct work must not create any back pressure on the transmitter exhaust system. Use a fan or blower to compensate for duct losses when the exhaust is ducted outdoors or when back pressure is present (1200-cfm capacity).
b. If intake air is ducted in from the roof, raise the intake sufficiently high above the surface to prevent intake of air heated by sun reflection from the roof.
c. If both intake and exhaust ducts are used, locate the duct openings in a common area of the building to equalize wind pressure effects. However, do not allow the exhaust to recirculate into the intake causing heat build-up.

### 2.5 Initial Turn-on Procedure

a. Ensure that the transmitter has been properly assembled and connected according to instructions provided in paragraphs 2-2 through 2-4.
b. Open access panels to the control circuit cards and exciter circuit cards. Check the circuit cards for proper installation.
c. Replace all access panels and ensure that all doors and panels are properly closed.
d. Ensure that all transmitter circuit breakers are 0FF.
e. Apply primary power to transmitter.
f. Set the 28 VDC POWER SUPPLY and BLOWER circuit breaker to ON.

Check the phase loss/phase rotation indicator on A7 (top LED). If phase loss /phase rotation indicator is not on, interchange any two primary power input leads at A17TB3.


Table 2-2. 816R-3 25-kW FM Transmitter, Nominal Heat Balance
g. Press the FILAMENT ON pushbutton. The power amplifier blower will start.

## WARNING

DEADLY VOLTAGES ARE EXPOSED WHEN SIDE COVER IS REMOVED. USE EXTREME CAUTION TO PREVENT OPERATOR INJURY.
h. Loosen the two retaining bolts at the bottom of the left cabinet side panel. Grip the panel securely and lift it from place. Check the rotation of the blower. Rotation should be counterclockwise when viewed from the left side. Replace the side panel, reapply primary power and press the FILAMENT ON pushbutton.
i. Check the cabinet fan rotation by lifting the foam filter from the top right side of the cabinet. Rotation should be counter-clockwise when viewed from the top. Replace the filter, reapply primary power, and press the FILAMENT pushbutton.

## CAUTION

> DO NOT PERFORM THE REMAINDER OF THIS PROCEDURE IF THE TRANSMITTER IS NOT CONNECTED TO AN ANTENNA WITH A 50-OHM IMPEDANCE OR A DUNMY LOAD CAPABLE OF DISSIPATING AT LEAST THE RATED RF OUTPUT OF THE TRANSMITTER.
j. Set all circuit breakers to ON .
k . Set the test meter selector switch to 28 V SUPPLY ( 40 V scale). The test meter will indicate $28 \pm 2.0$ volts DC.

1. Set the AC Meter Panel selector switch to FIL. The test meter should indicate $6.0 \pm 0.1$ volts. Adjust Filament Voltage using procedures in Paragraph 5.6.2 and 5.6.3. These adjustments are required to be made at customer's normal line voltage.
m. Ascertain that the exciter POWER Switch is ON.

NOTE
The transmitter is adjusted and pretuned at the factory for specific customer power output and frequency requirements. In normal applications, the finetuning and adjustment procedures provided in steps $n$. through 7. are adequate to esnure proper transmitter operation. However, if the transmitter is to be operated at a frequency or power output different from the frequency or power output designated in the production test data supplied with the transmitter, perform the complete rf tuning and power adjustment procedures listed in Paragraph 5.6.7.
n. Set the POWER CONTROL switch to MANUAL.
o. Set the POWER switch to FORWARD.
p. Set the TRANSMITTER CONTROL switch to LOCAL.
q. Press the Plate switch. The PLATE ON switch will light.

CHANGE NO. 13

## installation

r. Slightly adjust the PA LOADING and PA TUNING controls until maximum power output is displayed on the RF WAITMETER.
s. RAISE or LONER the POWER ADJUST control until the RF WATIMEIER displays the station's authorized power level.
t. Compare meter readings with those listed in table 3-4 or 3-5. If additional tuning is required, refer to the adjustment procedures listed in section 5.
u. Set POWER CONTROL switch to AUTOMATIC. On the transmitter Power Control Adjust panel adjust A3R7 for $100 \%$ output power if necessary.

### 2.6 Remote Operation

To initiate remote operation, set the TRANSMITTER CONTROL switch to REMOTE. When operating with the control panel, this switch must be in the LOCAL position.

### 2.7 Frequency Change

The Transmitter operating frequency is changed by changing the Exciter operating frequency and performing the transmitter RF Tuning procedure as outlined in paragraph 5.6.7.

### 3.1 GENERAL

* The transmitter can be operated from the control panel or by Remote Control. Once the transmitter has been installed and properly tuned, it is only necessary to monitor meter indications and to make minor tuning and loading adjustments (figure 3-1). Instructions for the 802A exciter are found in the Exciter Instruction Manual.


### 3.2 Controls and Indicators

Refer to the following tables for a general description of the operating controls found on the front panels of the transmitter cabinets: table 3-1, left cabinet; table 3-2, center cabinet; and table 3-3, right cabinet.

### 3.3 Turn-on Procudure

a. Ensure that steps a. through m. in paragraph 2.5 have been performed.
b. Observe the control panel meters after plate voltage is applied and ensure that the transmitter readings agree with those in table 3-4, table 3-5, or manufacturer Data Sheet.

Table 3-1. Left Cabinet

| REF <br> DESIG | CONTROLS AND <br> INDICATORS | FUNCTION |
| :--- | :--- | :--- |
| C37 | DRIVER PLATE TUNING | A variable capacitor that adjusts <br> driver tuning. |

Table 3-2. Center Cabinet

| REF <br> DESIG | CONTROLS AND <br> INDICATORS | FUNCTION |
| :--- | :--- | :--- |
| AIMI | TEST METER | Displays 11 internal operational <br> voltage or current readings. |
| Rotary switch that selects one of <br> 11 readings to display on the <br> test meter. The value below each <br> switch position is the full-scale <br> reading for that position |  |  |



KO1-(2)
Figure 3-1. FM Transmitter, 816R, Controls \& Indicators

Table 3-2. Center Cabinet. (Cont)

| $\begin{aligned} & \text { REF } \\ & \text { DESIG } \end{aligned}$ | CONTROLS AND INDICATORS | FUNCTION |
| :---: | :---: | :---: |
| AlM2 | PLATE CURRENT | Displays power amplifier plate current. |
| Alm3 | PLATE VOLTAGE | Displays power amplifier plate voltage. |
| AlM4 | RF WATTMETER | Displays transmitter forward and reflected power. |
| AlS2 | POWER FORWARD/ REFLECTED | 2-position switch that selects forward or reflected power for display on the RF WATTMETER |
| AlS5 | POWER CONTROL AUTOMATIC/MANUAL | Spring-loaded momentary switch that selects automatic or manual power control. |
| AlS6 | POWER ADJUST LOWER/RAISE | Spring-loaded momentary switch that lowers or raises power when POWER CONTROL switch S5 is in MANUAL. |
| Als3 | PA TUNING RAISE/LOWER | Spring-loaded momentary switch that positions tuning capacitor C50. |
| AlS4 | PA LOADING RAISE/LOWER | Spring-loaded momentary switch that positions loading capacitor C51. |
| AlS7 | PLATE OFF | Pushbutton momentary indicator switch that removes all operating voltage from the transmitter. |
| A158 | PLATE ON | Pushbutton momentary indicator switch that applies operating voltage to the transmitter. |
| A1S9 | FILAMENT OFF | Pushbutton momentary indicator switch that removes filament voltage from the transmitter. |
| A1S10 | FILAMENT ON | Pushbutton momentary indicator switch that applies filament voltage to the transmitter. |
| A1S11 | FAULT RESET | Pushbutton momentary switch that resets the fault indicators. |

## operation

Table 3-2. Center Cabinet. (Cont)

| REF <br> DESIG | CONTROLS AND INDICATORS | FUNCTION |
| :---: | :---: | :---: |
| A20S10 | TRANSMITTER CONTROL LOCAL/REMOTE | 2-position switch that selects local or remote operation. |
| A7CR14 | PHASE LOSS | Phase Loss/Phase Sequence/Phase Unbalance Indicator. |
| A7CR15 | CARD CAGE INTLK | CARD CAGE interlock Indicator. |
| A7CR16 | AIR INTLK | PA Cooling Indicator |
| A7CR17 | TEMP INTLK | Exhaust Air Temp Indicator |
| A7CR18 | READY | Filament Time Delay Indicator |
| A7CR6 | PA SCREEN 0/L | PA Screen Fault Indicator |
| A7CR7 | PA PLATE 0/L | PA Plate Fault Indicator |
| A7CR8 | VSWR 0/L | VSWR Fault Indicator |
| A7CR9 | DR PLATE 0/L | Driver Plate Fault Indicator |
| A7S2 | AUTO RECYCLE | Automatic Recycle ON/OFF Switch |
| A7S1 | RECYCLE TEST | Automatic Recycle Circuit Test Switch |
| A7CR3 | RECYCLE LOCKOUT | Recycle Circuit Lockout Indicator |
| A7CR5 | RECYCLE PULSE | Recycle Circuit Pulse Indicator |
| A12CR5 | RMT PLT OFF INTLK | Remote Plate Off Relay Indicator |
| A12CR6 | PA GRID DOOR INTLK | PA Grid Door Interlock Indicator |
| A12CR7 | PA DOOR INTLK | PA Door Interlock Indicator |
| A12CR8 | L REAR PNL INTLK | Left Rear Panel Interlock Indicator |
| A12CR9 | C REAR PNL INTLK | Center Rear Panel Interlock Indicator |
| A12CR10 | R REAR PNL INTLK | Right Rear Panel Interlock Indicator |
| A12CR11 | C FR PNL INTLK | Center Front Panel Interlock Indicator |

Table 3-2. Center Cabinet. (Cont)

| $\begin{aligned} & \text { REF } \\ & \text { DESIG } \end{aligned}$ | CONTROLS AND INDICATORS | FUNCTION |
| :---: | :---: | :---: |
| A12CR12 | R FR PNL INTLK | Right Front Panel Interlock Indicator |
| A12CR13 | RMT INTL.K | Remote Interlock Indicator |
| Al2CR14 | FAILSAFE INTLK | Remote Fail Safe Relay Interlock Indicator |
| A12CR 15 | LOCAL CONTROL | AlSio Local Control Position Indicator |
| A12CR16 | REMOTE CONTROL | ATS10 Remote Control Position Indicator |
| A12CR17 | AUTO PWR CONTROL | A155 Automatic Power Control Position Indicator |
| Al2CR18 | MAN PWR CONTROL | AlS5 Manual Power Control Position Indicator |
| A12CR19 | STEREO | Stereo Mode Position Indicator |
| A12CR20 | MONO | Mono Mode Position Indicator |

Table 3-3. Right Cabinet.

| REF DESIG | CONTROLS AND INDICATORS | FUNCTION |
| :---: | :---: | :---: |
| A6CB1 | 28 VDC POWER SUPPLY | 1 ampere magnetic circuit breaker that protects the $28-V$ dc power supply. |
| A6CB2 | BLOWERS | 10-ampere magnetic circuit breaker that protects blower and fan. |
| A6CB3 | DRIVER POWER SUPPLY | 4.5-ampere magnetic circuit breaker that protects the driver power supply. |
| A6CB4 | PA SCREEN POWER SUPPLY | 15-ampere magnetic circuit breaker that protects the pa screen power supply. |

Table 3-3. Right Cabinet. (Cont)

| REF DESIG | CONTROLS AND INDICATORS | FUNCTION |
| :---: | :---: | :---: |
| A6CB5 | PA PLATE POWER SUPPLY | 70-ampere magnetic circuit break er with a series trip feature that allows the circuit breaker to be tripped from a remote location. |
| $\begin{aligned} & \text { A6F7/F9 } \\ & \text { F12 } \end{aligned}$ | FAN | 2-ampere fuse. |
| $\begin{aligned} & \text { A6F6/F8 } \\ & \text { F10 } \end{aligned}$ | CONTROLLER | 1-ampere fuse. |
| A6F4/F5 | PA BIAS POWER SUPPL.Y | 0.25-ampere fuse. |
| A6F1/F3 | FILAMENTS | 10-ampere fuse. |
| A6F2/F11 | EXCITER | 3 -ampere fuse. |
| A6F13/F14 | DRIVER FILAMENT | 2-ampere fuse. |

Table 3-4. Typical Indications, 25-Kilowatt Power Output.

| TYPICAL METER READINGS |  |
| :--- | :--- |
| Power output | 25.0 kilowatts |
| PA plate volts | 8500 to 8900 volts |
| PA plate current | 3.6 to 3.75 amperes |
| PA screen voltage | 640 to 670 volts |
| PA grid current | 90 to 120 mA |
| Left dvr. cath. 1 | 170 to 220 mA |
| Right dvr. cath. 1 | 170 to 220 mA |

## Table 3-4. Typical Indications, 25-Kilowatt Power Output. (Cont)

## TYPICAL METER READINGS

Dvr. screen 1
Dvr. grid 1
Dvr. plate volts
Dvr. screen volts
802A Output Power
PA plate efficiency
Control Voltage

$$
\begin{aligned}
& 30 \text { to } 40 \mathrm{~mA} \\
& 0 \text { to } 10 \mathrm{~mA} \\
& 1800 \text { to } 2000 \text { volts } \\
& 270 \text { to } 290 \text { volts } \\
& 5 \text { to } 10 \text { watts } \\
& 76 \text { to } 78 \% \\
& 26 \text { to } 28 \text { volts }
\end{aligned}
$$

### 3.4 Shutdown Procedures

### 3.4.1 Normal Turnoff

a. Press the PLATE OFF pushbutton and allow a few seconds for the voltage to decrease.
b. Press the FILAMENT OFF pushbutton.
c. Set AC LINE circuit breaker A25CB1 OFF.
d. Set 28 VDC POWER SUPPLY circuit breaker CBI OFF.
e. Open the primary disconnect switch. (Customer supplied wall disconnect switch)

### 3.4.2 Emergency Turnoff

In the event of an emergency, remove power in any of the following ways: turn $A C$ LINE Circuit Breaker A25CBI OFF, press the FILAMENT OFF pushbutton, turn 28 VDC POWER SUPPLY circuit breaker CBI OFF, or open the primary disconnect switch.

### 3.5 Power Readings

The transmitter control panel RF WATTMETER indicates percent of authorized station forward and reflected power. It does not indicate percent true power. To obtain percent true power using the wattmeter, subtract percent reflected power from percent forward power.

Table 3-5. Nominal Readings, Reduced Power Operation.

| POWER OUTPUT | PLATE VOLTAGE |  | PLATE CURRENT |  | SCREEN <br> vOLTAGE |  | SCREEN CURRENT |  | CONTROL GRID CURRENT |  | EFFICIENCY (\%) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Recorded | Nominal | Recorded | Nominal | Recorded | Nominal | Recorded | Nominal | Recorded | Nominal | Recorded | Nominal |
| 24,000 |  | 8650 |  | 3.6 |  | 610 |  | 475 |  | 100 |  | 77 |
| 22,000 |  | 8400 |  | 3.4 |  | 590 |  | 435 |  | 98 |  | 76.8 |
| 20,000 |  | 8150 |  | 3.25 |  | 575 |  | 395 |  | 96 |  | 76.3 |
| 18,000 |  | 7900 |  | 3.05 |  | 555 | . | 360 |  | 94 |  | 75.2 |
| 16,000 |  | 7650 |  | 2.9 |  | 540 |  | 320 |  | 90 |  | 73.2 |
| 14,000 |  | 7450 |  | 2.7 |  | 520 |  | 280 |  | 85 |  | 70.6 |
| 12.000 |  | 7200 |  | 2.5 |  | 500 |  | 240 |  | 80 |  | 69 |
| 10,000 |  | 6950 |  | 2.35 |  | 485 |  | 205 |  | 75 |  | 67.8 |
| Note: | The above are approximations. The individual transmitters will vary with source voltage and installation. |  |  |  |  |  |  |  |  |  |  |  |

### 3.6 Automatic Recycle Resetting

Automatic transmitter shutdown occurs when pa screen, pa plate, driver, or vswr is overloaded. An overload indicator A7CR6 through A7CR9 lights on Overload and $\mathrm{Pe}-$ cycle board A7. If the overload was of short duration, the automatic recycling circuits restart the transmitter. The indicator light remains on until the transmitter operator presses the FAULT RESET switch on the main control panel. The Fault Indicator lamp cannot be RESET from Remote Control location. Perform maintenance procedures if the automatic recycling circuits fail to restart the transmitter.

The fault recycling circuits may be disabled for tuning or maintenance by switching the AUTO RECYCLE switch A7S2 to OFF.

### 4.1 General

The FM Transmitter, 816 R , operates in the $88-$ to $108-\mathrm{MHz}$ range at a maximum rated RF output. A CEMC 802A solid-state fm wideband exciter provides excitation. The transmitter is equipped with monitoring circuits that check and correct changes in power output and overload conditions. A control panel provides complete transmitter metering and tuning controls. Refer to the overall schematic diagrams in Section 7 for detailed circuit information.

### 4.2 Block Diagram Discussion

Refer to figure 4-1. A 10-dBm input signal (monaural, stereo, or SCA) modulates the driver stage. The output of the driver is applied to the power amplifier. The power amplifier output is applied via a low-pass filter and directional coupler to a 50-ohm antenna.

A DC sample of the forward power from the directional coupler (Al6) is monitored bythe auto power control circuit. If a change in output power is detected, a signal is sent to the power control unit that increases or decreases the plate and screen power supply input voltage to compensate. A sample of the reflected power is also monitored by the power control circuits. If an excessive amount of reflected power is detected, the control circuits remove plate voltage from the mower amolifjer. The 28-volt power supply provides power for the control circuits.

### 4.3 RF Circuits

### 4.3.1 Exciter

* Refer to the 802 A instruction manual, principles of operation.


### 4.3.2 RF Driver

The exciter output is applied to the driver stage that consists of two 4CX250B tetrodes in parallel (AllV1 and AllV2). The stage operates class $C$ with adjustable cathode bias provided by R40 and R44 and grid leak bias by R50. The driver grid swamping resistor, R57, provides wide bandwidth and minimized plate-to-grid feedback.

The input circuit is a tuned transmission line with resistance loading. Neutralization Capacitor $\mathrm{C}_{\mathrm{N}}$ is a short piece of wire with a paddle on the end physically placed in
parallel with the anodes of V1 and V2. The location of the paddle provides sufficient capacitance to neutralize the stage. A sample of the screen current flows through a transformer winding connected across pins 9 and 12 inside Hall-effect probe A2225 for screen current monitoring. Using the principle of the Hall effect, the stationary magnetic field around the transformer produces a current through the
principles of operation


Figure 4-1. FM TRANSMITTER, 816R, Block Diagram.
control panel meter connected across pins 3 and 4 of A2225. A control current that is adjusted to calibrate the control panel meter flows through pins 1 and 2. A22z5 output (pins 1 and 2) is connected to Driver Screen meter calibration resistor A22R73.

### 4.3.3 RF Power Amplifier

* The driver output is coupled through C57A and C57B capacitors to the grid of the power amplifier tube V3. A tuned circuit composed of A21L7 and Al8C37 provides impedance matching. Loading of the driver amplifier is accomplished by adjusting A21L7 (tuning) and A21L8 (loading). Inductor A2lL8 is used to cancel a portion of the input capacity. Inductor Al8Ll4 and the distributed capacity of Al8R75 are strapped to the cavity wall, forming a suppressor that dampens the higher order cavity resonances that can occur near the third harmonic of the output frequency. Cathode tuning (or peaking) capacitor A21C39 improves the bypass action at the operating freouency. Resistors A21R76 and A21R77 broaden the frequency response and minimize symchronous amplitude modulation products. Inductors Allish and A2lL5 are the driver plate and the pa grid chokes and Al8LNl and Al8LN2 provide neutralization.

The power amplifier is a plate-tuned $4 C \times 15000$ A that is operated class $C$. The tube screen is grounded and the cathode is placed -750 volts below ground. A fixed bias from the pa bias power supply is applied to the control grid through A22TB8-19, A22R37, and A22TB8-20. When an input signal is present, grid current flows and develops grid leak bias across Al8R35, Al8R36 and Al8R80. The increased negative potential on the grid causes the diode in the pa bias supply to reverse bias, preventing grid current flow through the supply. Hall-effect probe A22Z4 monitors the amount of grid current for control panel metering.

The power amplifier plate circuit is coarse tuned from 88 to 108 MHz by resonating an adjustable coaxial resonator. (See figure 4-2.) The resonator is the area between the tube shelf and the sliding shorting plane. Two motor-driven capacitors permit more precise tuning (A18C51) and loading (A18C50). RAISE/LOWER switches S3 (PA TUNING) and S4 (PA LOADING) on control panel Al control capacitor drive motors.


4-3

## principles of operation

The DC blocking capacitor Al8C45 is located between the top of PA tube and input to air chimney. Figure 4-3 shows the electrical equivalence of the plate tuning circuit.

### 4.3.4 Low-Pass Filter Al8

Low-Pass filter Al3, (See Figure 6-1), consists of two coaxial filters in tandem. The first filter has a cutoff of 130 megahertz, while the second has a cutoff of 300 megahertz.

### 4.3.5 Directional Coupler Al6

The Directional Coupler (Al6) provides a DC voltage to both Forwand and Reflected circuit of A3 and the output is then routed and can be displayed on Forward/ Reflected Meter (M4). Also, a sample of Forward power is routed from A3 to A9 gating cards to control SCR's for PA Plate HV supply.

### 4.4 Power Supplies and Power Control Circuits

### 4.4.1 General

There are five separate power supplies in the transmitter. Three of the five, the plate, screen and bias power supplies, provide voltage to the power amplifier. The two remaining, the driver power supply, furnishes voltage to the driver stage and the 28 -volt dc power supply, provides power to the control circuits.

### 4.4.2 28-Volt DC Power Supply PSI

The 28 -volt dc supply receives its 3 -phase $60-\mathrm{Hz}$ input from the unregulated line voltage. The input is applied through circuit breaker A6CBl and stepdown transformer Tl to 3-phase bridge rectifier assembly CRI. The 28 -volt dc output of the bridge is filtered by the RC circuits and applied to the control circuits.


NOTE:
C45 is the capacitance between tube anode and the cavity center conductor
C50 is the capacitance between movable plate 1 and the tube anode
C51 is the capacitance between movable plate 2 and the tube anode
LR is the lumped constant equivalent of the shortened $1 / 4$ wave resonator
Figure 4-3. FM Transmitter, 816R, Schematic Diagram, Output Network.

WARNING: DISCONNECT PRIMARY POWER SOURCE BEFORE SERVICING.

### 4.4.3 PA Bias Power Supply PS2

The pa bias power supply provides the power amplifier with fixed grid bias that holds the tube near cutoff when no signal is present on the grid. Single-phase primary power is applied through contactor A19KI and step-up transformer $T 1$ to a bridge rectifier network. An L-section filter is formed by L1 and C2.

The power supply output is applied to the grid of the power amplifier through CR5.

* CR5 blocks grid current flow through the supply when the grid leak bias exceeds the fixed bias. A sample of the bias voltage is applied throuah R3 to front panel meter AlMl for monitoring.


### 4.4.4 PA Plate Power Supply

The pa plate power supply provides plate voltage to the power amplifier. Primary components of the supply are transformer T1, 3- phase bridge rectifier assembly ZI , filter choke L7, and filter capacitor C3. A meter multiplier board, Al5, samples plate voltage and allows constant monitoring. Input power to Tl is controlled by scr (silicon-controlled rectifier) power control unit A9. This unit, connected as a closed loop regulator, maintains constant power output to offset conditions of varying input power.

### 4.4.5 Power Control Unit A9

* Power control unit A9 regulates the 3-phase ac power input to the pa plate, the pa screen, and the driver power supplies through transformers T1, T2, and T3 respectively. Unit A9 consists of two major component assemblies-scr assembly A9Zl and firing control unit A9AR1. Scr assembly A9Z1 has three scr pairs; one pair in series with each primary winding of the 3 -phase power transformers. Each pair is connected within the delta circuit of the transformer primaries. Scr firing control unit AgARl consists of three control cards. Each control card controls the firing (turn-on) point of one scr pair.
* A cormon d.c. control signal from power control regulator A8 is fed simultaneously to each control card. This control signal governs the firing of the scr pairs that regulate the input power applied to the power supplies. Relay A9ARIKl deenergizes on PLATE OFF, disabling the three scr gate driving cards. (See figure 4-4).


### 4.4.6 Power Control Regulator A8

Power control regulator A8 provides the necessary control signals to operate power SCR control unit A9. A8 supplies a soft--start pa plate supply turn-on signal, a negative voltage for manual power control, and amplifier-mixer functions for automatic power control.

When the PLATE ON switch is pressed, +28 volts is supplied to XA8-27. The +28 volts activates transistor A8Q1 to turn on relay K12. Relay Al9Kl2 supplies 3-phase ac control power to AgAR1. An RC time delay circuit formed by A8R2 and A8C1 maintains Kl2 closed for a short interval after the PLATE OFF switch is pressed. Transistors A8Q2, Q3, and Q4, also energized by the +28 volts, provide the dc turn-on signal to unit A9AR1. On power control regulator A8, R8, R9, and C2 modify this signal to soft-start the high-voltage pa plate power supply. Zener regulator A8VR2 provides a -10-volt voltage to MANUAL power adjust resistor A20R43.


principles of operation

Transistors A8Q5 and A8Q4 amplify the automatic control signal from A3 and apply the signal to A9AR1TB2-1 when the MANUAL/AUTOMATIC switch is in AUTOMATIC. A8C5 and A8R5 phase-compensate the power control servo loop.

### 4.4.7 PA Screen Power Supply

The 3-phase regulated voltage from the power control unit is applied through transformer T2 to a silicon 3-phase full-wave bridge assembly, Z2, in the pa screen power supply. The output of $Z 2$ is filtered and applied to the cathode circuit of the power amplifier at the secondary center tap of filament transformer A18T5. The pa screen power supply also provides -28 volts, obtained from the junction of resistors Al7R4 and A17R18, for manual power control.

### 4.4.8 Driver Power Supply

The driver power supply provides plate and screen voltages for the driver stage. The 3-phase ac power for the primary of T3 is supplied by power control A9. The output of T3 is applied to a silicon 3-phase full-wave bridge assembly, 23 . The output of the rectifier bridge is filtered and applied to the driver plate circuit. The driver screen voltage, developed at the junction of A17R34 and A17R25 is applied through a metering resistor A22Rl to the driver screen circuit. Gaseous protector Al7E2B shorts excessive transient voltages to ground. Driver plate and screen metering samples are obtained from Al4R32 and Al7R3 respectively.

### 4.4.9 Filament Voltage Regulator A5

* When the Filament Regulator is in automatic mode, the filament voltage regulator detects and compensates for sustained fluctuations in the input ac voltage. The fluctuations are detected by a balanced bridge circuit, which in conjunction with a motor control circuit, adjusts the setting of variable transformer Al9A2Tl. The output voltage of the variable transformer ( Al 19 A 2 Tl ) is then applied to the primary of the Driver (AllT6) and PA (Al8T5) Filament Transformer.

The variable transformer output is also applied to the nrimary of detector circuit transfomer A20T8. Secondary (l) of this transformer is applied to a resistive bridge circuit consisting of lamps A5DS1, A5DS2, A5Rl and A5R2 and filament voltage adjust potentiometer A5R3. While observing PA filament meter, A5R3 can be adjusted. for the required filament voltage.

* When the input primary ac voltage increases, the voltage dropped across the bridge circuit increases, which causes more current to flow through the components located in the legs of the bridge circuit. The increased current flow causes the filament resistance of A5DS1 and A5DS2 to increase. The increased resistance of the filanents unbalances the bridge circuit and anplies an ac signal, in phase with the ac voltage dropped across the bridge circuit, to the junction of A5Cl and A5Rl7. From A5Cl and A5R17, the ac signal is coupled to the base of transistor A5Q1. Transistor A5Q1 amplifies and phase shifts the ac signal $180^{\circ}$. From A501, the inverted ac signal is routed through capacitor A5C3 to the gate circuits of controlled rectifiers A 5 Q 2 and A 5 Q 3 .
Another sample of the input ac voltage is applied from secondary (2) of A20T8 through diodes A5CR1 and A5CR2 to RAISE relay A5K1 and LOWER relay A5K2, respectively. Be-
cause of $A 5 C R 1$ and $A 5 C R 2$, only positive half cycles of the ac voltage are applied to $A 5 K 1$ and A5K2. As the input ac voltage increases, positive half cycles are connected through A5K2 to the cathode of A5Q3. The in-phase ac signal present at the gate of A5Q3 allows A5Q3 to conduct, energizing A5K2. Capacitor A5C6 discharges during negative half cycles keeping A5K2 energized. The ac signal present at the gate of A 5 Q 2 is out of phase with the half cycles connected through A5K1 to the cathode of A5Q2, preventing A5Q2 from conducting. This action prevents A5K1 from energizing.

Operation of the detector circuit under low input ac voltage condtions is similar to the operation during high-voltage conditions, with the following exceptions. The sample ac voltage dropped across the resistive bridge circuit is $180^{\circ}$ out of phase with the ac signal at the junction of $A 5 C 1$ and A5R17. The out-of-phase ac signal prevents A5Q3 from conducting, but allows A5Q2 to conduct. This action energizes $A 5 K 1$, but not A5K2.

If A5DS1 or A5DS2 burns out, a large ac signal will appear at the base of A5Q1. As a result, the drive motor would run to either end stop, trying to compensate for an erroneous indication of a very high or low ac filament voltage. To prevent this type of malfunction, a protective circuit is connected to the output of A5Q1. When a large ac signal is applied to the base of $A 5 Q 1$, the same ac signal is applied to the protective circuit which consists of voltage divider A5R17 and A5R16 and controlled rectifier A5Q4. From the junction of A5R17 and A5R16, the ac signal is connected to the gate of A5Q4 causing it to conduct. When A5Q4 conducts, the output of A5Q1 is shunted to ground preventing A5K1 or A5K2 from energizing. This action prevents the drive motor from operating.

The motor control circuits which operate to lower or raise the ac filament voltage are similiar; therefore, only the raise control circuit is discussed in detail. Under low ac filament conditions, raise relay A5Kl energizes, connecting +28 volts dc through contacts 8 and 9 to a time-delay circuit, consisting of resistor A5R19 capacitors $A 5 C 8$ and $A 5 C 9$. Relay $A 5 K 1$ must remain energized for 1.5 seconds before the time-delay circuit allows A5K3 to energize. The time delay assures that only sustained fluctuations of the ac filament voltage will allow the drive motor to operate. After 1.5 seconds, A5K3 energizes, applying 115 vac through contacts 11 and 12 and limit switches A9A2S1 to variac drive motor A19A2B1.

* The variac drive motor operates, driving the rotor on variable transformer Al9A2T1 until the input ac voltage is raised to a value to provide filament voltage determined by A5.


### 4.4.10 Filament Voltage Distribution

The filament voltage distribution is shown in figure 4-5. Filament voltage regulator A5 maintains a constant rms voltage on the filaments as discussed in paragraph 4.4.9.

### 4.5 Primary Power Distribution Control and Overload Circuits

### 4.5.1 Primary Power Distribution

The $60-\mathrm{Hz}, 3$-phase primary power is distributed to the various circuits of the transmitter via circuit breakers and fuses mounted on circuit breaker panel A6 (figure 4-6).
principles of operation

PA PLATE POWER SUPPLY circuit breaker A6CB5 is connected inside the delta of plate transformer Tl. It also serves to interrupt primary power to the PA screen transformer T 2 and driver plate transformer T 3 through additional associated circuit breakers, A6CB4 (PA SCREEN SUPPLY) and A6CB3 (DRIVER PONER SUPPLY).
$A C$ line voltage metering is provided by $A C$ meter panel A25. In addition to the

* three phase-to-phase voltages, a fourth position of A25Sl is used to monitor PA filament voltage.

BLOWERS circuit breaker, A6CB2, controls application of primary power to cavity blower Bl through filament-on relay Al9K2 and FAN fuses A6F7, F9, and F12. Relay Al9K2 is energized when the filaments switch (S10) is turned on.

Application of primary power to the filament circuits, the exciter, the pa bias power supply, and the pa tuning and loading motors is relay controlled. Filament-on relay A19K1 and blower-on relay A19K2 control application of power to the regulated filament circuit through auto-transformer A19A2T1. Relay Al9Kl also controls app* lication of power to E02A exciter A4, to pa bias power supply PS2, and to the pa tuning and loading motors (B2 and B3 respectively). Power to the exciter and the motors is through isolation transformer T4. Time-totalizing meter A6MI is placed across the load side of filament on relay Al9KI.

The filament, exciter, and pa bias supply input power circuits are protected by associated fuses.

### 4.5.2 Transmitter Turn-on

The transmitter is energized by pressing FILAMENT ON switch SlO in the Al control panel (figure 4-7). Relay Al9K2 is energized and power is applied to the blower motors. After sufficient air pressure is created in the power amplifier cabinet, air switch A18S1 is closed and relay A19K1 is energized.

After the 30 -second delay, relay A19K4 is energized. The PLATE ON switch is pressed and relay Al9K3 is energized and +28 volts is supplied to the base of transistor A8Q3. This turns on control amplifier A9AR1, which applies input voltage to the plate, screen, and driver power supplies.

* The transmitter may also be energized by pressing the PLATE ON switch which latches Al9K3 and energizes Al9K2 through contacts 8 and 5. By pressing a single switch (PLATE ON) will enable the transmitter to go through the above sequence of Blower Filament, Time Delay and Plate On.


### 4.5.3 Exciter Power Control Override

* An output override voltage is supplied to the 802 A exciter when the plate voltage is turned off. This mutes the output of the exciter while the pa plates are off (figure 4-7). The voltage is applied from the 28 -volt power supply through contacts 3 and 9 of relay Al9K4 to the 802A exciter power supply regulator.


Figure 4-5. Filament Voltage Distribution.


Figure 4-6. Primary Power Distribution.
principles of operation


Figure 4-7. Power ON-OFF Control Circuits

### 4.5.4 Fwd/Refl Calibrate and Auto Power Control Unit A3

The vswr calibrate and auto power control unit, A3, monitors the forward and reflected power received from directional coupler Al6. A forward power sample is applied through R1 to pin 3 of operational amplifier Ul. The output on pin 6 of Ul is applied to the control panel RF WATTMETER through FWD CAL potentiometer R14 and to Al7TB4-34 for remote monitoring.

Operational amplifier U3 is connected as an integrator. Feedback is supplied by the parallel combination of capacitor Cl and resistor R10. During automatic power operation, the output of U3 is connected to power control A9 through relay A12K1 and power control regulator A8. PWR CNTRL ADJ potentiometer R7 in the input of U3 increases or decreases the transmitter output power during automatic power operation by increasing or decreasing the output of U3.

A reflected power sample is applied to pin 3 of U 2 through R17. The output on pin 6 of U 2 is applied to the control panel RF WATTMETER through REFL CAL potentiometer R24 and to A17TB4-33 for remote monitoring. The output of U2 is also applied to the gate of $A 7 Q 8$. When excessive reflected power exists and switch A3S1 is closed, U2 produces an output that triggers scr A7Q8. Scr A7Q8 conducts and energizes relay A22K9 which removes power from the transmitter. (See paragraph 4.5.5)

FWD OFFSET potentiometer R25 and REFL OFFSET potentiometer R26 are adjusted for zero output at TP1 and TP2 respectively when no input exists at pin 3 of the related amplifier.

REFL ADJ potentiometer R27 and TEST switch S2 are used to test the VSWR protect circuit operation during maintenance operation. By pressing the push TEST switch S2, a simulated reflected power sample is applied to pin 3 of U2. With AlM4
calibrated for $10 \%$ of forward power output full scale in the REFIECTED position, R27 is adjusted to the desired reflected power trip level. Then VSWR PROT CAL potentiometer R20 is adjusted to trip at this level.

### 4.5.5 Overload Protection

Relays $122 \mathrm{~K} 6, \mathrm{~A} 22 \mathrm{~K} 7, \mathrm{~A} 22 \mathrm{~K} 8$, and A 22 K 9 are adjusted to energize and remove power from the transmitter when an overload occurs in the plate, screen, or driver supply or when the vswr exceeds a preset level. Screen current through A14R15 produces a voltage that is applied to relay A22K7 through A22R65. Plate current through A14R16 produces a voltage that is applied to relay A22K6 through A22R66. Driver current through Al7R33 produces a voltage that is applied to relay A22K8 through A22R60. When scr A7Q8 is gated on, a ground is applied and A22K9 is energized. Each relay is adjusted to trip at a factory preset current level. The relay contacts are in series with plate control relay A19K3. If an overload occurs, the corresponding relay trips and de-energizes Al9K3, removing plate power from the transmitter.
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### 4.5.6 Overload and Recycle Board A7

Overload and recycle board A7 contains circuits that provide overload indication and memory, automatic power on recycling and filament control circuit interlock status.

When an overload occurs in the pa plate pa screen, vswr, or driver plate, a 28volt pulse is supplied to the appropriate scr (Q4 through Q7). The scr latches and lights its associated LED indicator (CR6 through CR9) to indicate which overload has occurred. All indicators that have been lighted by an overload function remain lighted until FAULT RESET switch AISIl on the main control panel is pressed, Plate voltage is removed by overload relays A22K6, A22K7, A22K8 or A22K9. The 28-volt pulse that triggers the scr is simultaneously routed to the recycle circuit via diode CR10, CR11, CR12 or CR13 to be used to automatically restart the transmitter.

The automatic recycle circuit provides a timed, automatic restart pulse up to four times in a 30 -second period. The supplied card is connected so only two restart pulses will occur in a 30 -second period; but may be reconnected to allow four restart pulses in a 30 -second period. Conversion from the 2 -pulse to the 4 -pulse production may be accomplished by removing the jumper between terminals $A$ and $B$ on the card and replacing it between $A$ and $C$.

The auto recycle begins when the 28 -volt pulse is applied to the base of transistor Q1 causing it to conduct. The output of Q1 is fed to timers Ul and U4. Timer U1 provides a 0.5 -second delay, then triggers timer U2 which generates a 0.5 -second output pulse. This pulse is fed through gate U3A to inverter Q3 which causes Q9 to conduct and charge capacitor C16. The charging current of C 16 momentarily energizes $K 1$ which closes the PLATE ON circuit through S2. The charging current of Cl6 also flows through RECYCLE PULSE indicator CR5 giving an indication of the recycle circuit operation.

Gate U3D conducts the output pulse from timer U1 to counter U5. Counter U5 counts the number of recycle pulses and provides a logic 1 output at terminal $C$ when four pulses have been received. Depending on which terminal has been strapped to terminal A, two or four recycle attempts in a 30 -second period will close gates U3A, U3B, U3C, and U3D preventing any further attempts by the card to restart the transmitter. RECYCLE LOCKOUT indicator CR3 will light to indicate this condition. When the $30-s e c o n d$ period of time U4 has elapsed, a pulse is generated, inverted by Q2, and applied to U5 to reset it to zero. This clears the memory and allows another sequence to begin. If the maximum count of two or four pulses has not been received in the 30 -second period, the timer will also reset the counter automatically.

AUTORECYCLE switch S2 may be used to disable the auto recycle card when desired. This is usually done during tune-up or maintenance procedures. RECYCLE TEST switch S1 may be used to test the automatic recycle circuit during maintenance procedures by simulating an overload pulse at the input to the recycle circuit,

Filament control circuit interlock status indicators provide a visual indication of the condition of the filament protection circuit. The PHASE LOSS indicator Cl4 is lighted when phase monitor Al9K5 provides a 28 -volt signal indicating all three primary power phases are present, balanced, not too low and of the proper
principles of operation
sequence. CARD CAGE INTLK indicator CRI5 is lighted when the card cage cover is in place. AIR INTLK indicator CR16 is lighted when sufficient cooling air to the pa tube is flowing. TEMP INTLK indicator CR17 is lighted when the pa tube exhaust air temperature is below $240^{\circ} \mathrm{F} \pm 10^{\circ} \mathrm{F}$. The switch will reclose at $200^{\circ} \mathrm{F}$ temperature operating range of the PA tube. The READY indicator is lighted when the $30-$ second filament warm-up time has expired and the transmitter is ready for the application of plate voltage. These indicators are in series and in sequence from top to bottom as they are connected in the circuit. Therefore, an interlock must be satisfied before its status indicator will light or any indicator that follows it will light.

### 4.5.7 Power Failure Recycle Board A19A1

In the event of momentary loss of primary power, the power failure recycle circuit will restore the transmitter to operational status. Capacitor C3 maintains current flow through time delay relay Al9K4 keeping the time delay circuit active for short term power outages and a separate circuit provides a momentary ground at pin 10 when power is restored. The momentary ground is applied to A7C16 and the charging current of A7Cl6 pulls relay A7K4 in and initiates the power on command.

### 4.5.8 Latching Relay and Status Indicator Board A12

The latching relays permit local or remote selection of manual or automatic power control and local or remote selection of stereo or monaural excitation.

The latching relays are connected to the remote control panel through Al7TB4 (figure 4-8). A +28 -volt signal applied by local control switch AlS5 or through remote control interface terminal board Al7TB4 will latch relay Kl in one of two stable states. AUTO PWR CONTROL indicator CRI7 indicates automatic power control is selected and MAN PWR CONTROL indicator CR18 indicates manual power control is selected. A $+28-v o l t$ signal applied through remote control interface terminal board Al7TB4 will latch relay K2 in one of two stable states. STEREO indicator CR19 indicates the stereo mode and MONO indicator CR2O indicates selection of the mono mode.

Visual indication of TRANSMITTER CONTROL REMOTE/LOCAL switch A20S10 is given by status indicators CRT5 and CR16. CR15 lights when local control is selected and CR16 lights when remote control is selected.

Plate control circuit interlock status indicators are provided on the Al2 board. RMT PLT OFF INTLK indicator CR5 is lighted when optional remote relay A2A1K4 is de-energized. (If optional remote relays are not used, this relay will be jumpered and CR5 will always be lighted.) PA GRID DOOR INTLK indicator CR6 is lighted when the pa grid compartment door is closed. PA DOOR INTLK indicator CR7 is lighted when the pa plate compartment door is closed. L REAR PNL INTLK indicator CR8, C REAR PNL INTLK indicator CR9, R REAR PNL INTLK indicator CR10, C FR PNL INTLK indicator CRIl and R FR PNL INTLK indicator CR12 are panel interlock status indicators that are lighted when the respective panels are in place. Panel designations refer to the three bays of the transmitter cabinet (left, center and right) as viewed from the front of the transmitter. RMT INTLK indicator CR13 is lighted when continuity exists between remote control interface terminal board terminals 23 and 24.

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Figure 4-8. Latching Relays Al2, Simplified.
principles of operation

FAILSAFE INTLK indicator CR14 is lighted when optional remote relay A2AIKI is energized. (If optional remote relays are not used, LOCAL/REMOTE switch A2OS10 will bypass this interlock in the LOCAL position.) Indicators CR5 through CR14 are in series and in sequence from top to bottom as they are connected in the circuit. Therefore, an interlock must be satisfied before its status indicator will light or any that follow it will light.

### 4.5.9 Power Control Relays A2A3

Unit A2A3 provides remote manual power lower and raise control (figure 4-9). When power is decreased at the remote control panel, relay A2A3K2 is energized and closed contacts 7 and 9 provide 115 VAC to motor A20B5 which adjusts the resistance of A20R43 to decrease the transmitter power output. When the power is increased at the remote control panel, relay A2A3K3 is energized and closed contacts 7 and 9 provide 115 VAC to motor A2OB5 which adjusts the resistance of A20R43 to increase the transmitter power output.

### 4.5.10 Remote Relays A2AT

Remote relays unit A2Al parallels the front panel control operations. All relays and switches are momentary in operation. Failsafe relay A2Kl is energized only when +28 -volts is present in the control circuit. If $+28-v o l t s$ is lost, the relay deenergizes and removes power from the transmitter.

### 4.5.11 Remote connections

Typical remote interconnections to remote control terminal board TB4 are given in figure 4-10.


Figure 4-9. Power Control Relays A2A3 Simplified Schematic.


NOTE: As shown, the steering diodes (not supplied) ensure that the transmitter is placed in the AUTOMATIC power control mode when the PLATE ON control is energized and also that the transmitter is placed in MANUAL power control when either the MANUAL POWER RAISE or MANUAL POWER LOWER control is energized.

Figure 4-10. Typical Remote Interconnections to Remote Terminal Board Al7TB4

### 5.1 General

The transmitter is carefully inspected and adjusted at the factory to reduce maintenance to a minimum. To ensure peak performance, adhere to a regular schedule of periodic checks and maintenance procedures. Refer to the parts list, section 6, for component location in the transmitter.

## WARNING

high voltages are exposed when cabinet doors or access panels are opened. DEATH ON CONTACT MAY OCCUR IF YOU FAIL TO OBSERVE SAFETY PRECAUTIONS. WIEN WORKING INSIDE THE EQUIPMENT, BE SURE THAT ALL CIRCUIT BREAKERS ARE OFF AND that Primary power is disabled at the wall disconnect or circuit breaker unLESS OTHERWISE DIRECTED. ALWAYS SHORT ALL HIGH-VOLTAGE TERMINALS TO GROUND WITH THE GROUNDING STICK PROVIDED.

### 5.2 Cleaning

Clean the transmitter when dust accumulation occurs anywhere inside the equipment. A solvent composed of 25 percent methylene chloride, 5 percent perchloroethylene, and 70 percent dry cleaning fluid may be used as a cleaning material.

### 5.2.1 General Cleaning Procedures

a. Remove dust from chassis, panels, and components with a soft-bristled brush.
b. Remove foreign matter from flat surfaces and accessible areas with a lintless cloth moistened with solvent. Dry with a clean, dry, lintless cloth.
c. Wash switch and relay contacts with relay contact cleaner and less accessible areas with solvent lightly applied with a small soft-bristled brush.

### 5.2.2 Air Filter

The air filter, on the 816R-3 transmitter, should be cleaned whenever a perceptible quantity of dust and dirt accumulates on the filter element. Remove and clean the filter as follows:
a. Remove the cross-wire brace that holds the filter in place.
b. Remove the filter.
c. Use a vacuum cleaner to remove heavy dust accumulation from the filter.
d. Blow a stream of air through the filter in a direction opposite to normal airflow.
e. Wash the filter in a solution of hot water and detergent.
f. Replace the filter when dry.

### 5.2.3 Tube Cleaning

The power amplifier and driver tubes should be cleaned when a visable quantity of dust accumulates on the cooling fins of the tubes. Carefully remove the tubes from their sockets and clean each with a dry, oil-free jet of air.

### 5.3 Inspection

Inspect the transmitter at least once a week. Check all metal parts for corrosion and general deterioration. Examine wiring and components for signs of overheating. Ensure that all controls are operating smoothly. Inspect all connections and tighten any nuts, screws, or bolts found loose. Examine the blower and cabinet fans for normal operation.

### 5.4 Lubrication

The tuning and loading motor and the manual power increase/decrease motor are sealed and do not require lubrication. The cabinet inlet fan motor (B4) and the pa cavity blower motor (Bl) should be lubricated with SAE 10 oil as required.

### 5.5 Troubleshooting

If the transmitter fails to operate properly, check each circuit in the order that it is made operative. Use the simplified schematics in section 4 and the overall schematic in section 7 when needed. Normal control panel meter readings are provided in table 3-4 and an efficiency vs frequency graph is provided in figure 5-4.

### 5.5.1 Access Panel Interlock Switch

The access panel interlock switches must be blocked open to perform certain adjustment procedures. To block the panel switch open, push in on the plunger and insert two insulated blocks between the swith contactors. Remove the insulated blocks before replacing the panel.

### 5.5.2 Test Equipment

Table 5-1 lists the test equipment necessary to maintain the transmitter.

### 5.6 Adjustments

All transmitters are factory adjusted and pretuned to specific customer requirements, No adjustments are required by the customer unless a broken part is replaced, a specific assembly does not display meter readings within allowable tolerances, or the transmitter is operated at a frequency or power output different from the frequency or power output specified in the production test data supplied with the transmitter.

Table 5-1. Required Test Equipment.

| NAME | DESCRIPTION | MANUFACTURER AND MODEL. |
| :---: | :---: | :---: |
| Volt-ohm-milliammeter | Test Meter | Triplett 630-N |
| Ac Voltmeter | 0 to 10 volts, $1 \%$ tol (true Rms) | Weston 433 |
| Power supply | 0 to 28 volts dc, 5 amperes |  |
| Rf wattmeter | 2.5- and $25-\mathrm{kW}$ elements, 50 to 125 MHz | Bird 460 |
| Thruline wattmeter | 25 watts | Bird 43 |
| Dc Voltmeter | 0 to 10 kV |  |
| Dc ammeter | 0 to 5 amperes |  |

## WARNING

HIGH VOLTAGES ARE EXPOSED WHEN CABINET DOORS OR ACCESS PANELS ARE OPENED. DEATH ON CONTACT MAY OCCUR IF YOU ARE NOT EXTREMELY CAREFUL WHEN YOU PERFORM THE FOLLOWING PROCEDURES.

## NOTE

The 28 -volt power supply is on when both the filament and plate voltages are off.
Unless otherwise indicated, the POWER CONTROL switch is set to MANUAL, the POWER switch is set to FORWARD, the AUTO RECYCLE switch is set to OFF, and all circuit breakers are set to ON during adjustment procedures.

### 5.6.1 Switch Adjustments

### 5.6.1.1 Air Interlock Switch S1

a. Press the PLATE OFF and FILAMENT ON switches on control panel Al.
b. Remove the rear panel behind the plate cavity.
c. Adjust the tension bolt on switch Sl so that the green filament light goes out when the pa grid compartment door is opened approximately 1 inch.
5.6.1.2 Tuning Motor Limit Switches S11, S12, S13, and S14
a. Press the PLATE OFF and FILAMENT OFF switches on control panel A1.
b. Remove the rear panel behind the plate cavity, or the side panel next to the cavity.
c. Loosen the mounting screws on the limit switch.
d. Position the limit switches so that the peg mounted to the rack gear causes the switch to trip before the peg runs into either end-stop. The tuning and loading paddles must never be closer than $5 / 8$ inch from the blocking capacitor.

### 5.6.2 Filament Voltage Adjustment

a. Press the PLATE OFF and FILAMENT OFF switches on the control panel Al.
b. Open the pa grid compartment and connect a 0 - to 10 -volt true rms ac 1 percent meter to the pa filament rings on the tube socket.
c. Run the meter leads out the corner of the compartment and close the pa compartment door.
d. Remove the cover from the control circuits and pull the plunger on the card cage interlock all the way out.
e. Loosen motor coupling set screws on variable transformer end of coupling.

* f. With A5Sl in MANUAL position, run variable transformer drive motor until limit switch actuator arm is against the Upper (CW) limit switch.

WARNING
high voltages are exposed when cabinet doors or access panels are opened. THE SHAFT OF VARIABLE TRANSFORMER Al9T7 HAS HAZARDOUS VOLTAGE TO GROUND WHEN FILAMENT CONTACTOR IS ENERGIZED. DEATH ON CONTACT MAY OCCUR IF YOU are iot extremely careful when you perform the following procedures.
g. Press FIIAMENT ON switch on control panel Al.
h. Adjust variable transformer AlST7 with an insulated rod for an indication of 6.4 volts ac. Note the filament meter reading - if filament meter does not agree with calibration meter, then adjust A20AlRI until it does.

* i. Press FILAMENT OFF switch on control panel A1. Turn OFF Main circuit Brealeer (P25CBl).
j. Tighten set screws on variable transformer end of motor coupling.
* k. Turn Main Breaker ( A 25 CBl ) back on. Press FILAMENT ON switch on control panel Al .

1. Place A5S1 in AUTOMATIC position.
$m$. Adjust A5R3 for an indication of 6.0 volts ac.

### 5.6.3 Driver Filament Voltage Adjustment

NOTE

This procedure should be performed only after procedure in 5.6 .2 has been completed.
a. Press the PLATE OFF and FILAMENT OFF switches on control panel A1.
b. Remove the front panel beneath the grid compartment door.
c. Connect an ac voltmeter across terminals 3 and 4 of driver filament transformer AllT6 and adjust DVR FIL VOLTS ADJUST control AllR64 to produce an indication of $5.8 \pm 0.1$ volts on the ac voltmeter when PA Filament is at 6 volts AC.

### 5.6.4 DC Overload Adjustment -

a. Press the PLATE OFF and FILAMENT OFF switches on control panel A1. Turn DRIVER POWER SUPPLY, PA SCREEN POWER SUPPLY and PA PLATE POWER SUPPL.Y circuit breakers OFF.
b. Remove the front panel beneath the pa grid compartment door. DRIVER OVERTOAD ADUUSTMENT
c. Connect a milliammeter from the positive terminal of a 28 -volt dc power supply to TB8-6 on the transmitter.
d. Connect the negative terminal of the dc power supply to the transmitter chassis.
e. Raise the power supply current to 600 mA and note to see if overload occurs.
f. If overload does not trip then adjust DVR OVLD ADJ A22R60 to trip relay A22K8 at this current. (The DR PIATE O/L fault indicator on the overload/recycle board lights when the relay trips.)
g. Disconnect the milliammeter and remove the jumper from the dc power supply to the chassis.

## PA PLAITE OVERLOAD ADUUSTMENI

h. Connect an ammeter from the positive terminal of a 28 -volt dc power supply to Al4Rl5-1.
i. Connect the negative terminal of the dc power supply to Al4RI6-l.
j. Raise the dc power supply current to 4.5 amperes.
k. If overload does not occur, then adjust PA PLATE OVID ADJ A22R66 to trip relay A22K6 at this current. (The PA PLATE O/L fault indicator on the overload/ recycle board lights when the relay trips.)

1. Disconnect the ammeter and remove the jumper from the dc power supply to Al4Rl6-1.

## - PA SCREEN OVERLQAD ADTUSTMENT

m. Connect a milliammeter from the positive terminal of a 28 -volt power supply to TB8-5.
n. Connect the negative teminal of the dc power supply to TB8-4.
o. Raise the power supply current to 900 mA .
p. If overload does not occur, then adjust PA SCREEN OVLD ADU A22R65 to trip relay A22K7 at this curcent. (The PA SCRN O/L fault indicator on A7 lights when the relay trips.)
q. Disconnect the milliameter and remove the jumper from the dc power supply to TB8-4.
r. Press the FAUIT RESET switch on control panel Al.
5.6.5 PA Grid Current and Driver Screen Current Meter Calibration
a. Press PLATE OFF and FILAMENT OFF switches on control panel AT. Turn DRIVER POWER SUPPLY, PA SCREEN POWER SUPPLY and PA PLATE POWER SUPPLY circuit breakers OFF.
b. Remove the front panel beneath the pa grid compartment door.
c. Connect the negative terminal of a 28-volt dc power supply to Z4-9(E78) and the positive terminal to Z4-12(E77).
d. Adjust the dc power supply current to 400 mA .
e. Set the TEST METER selector switch to PA GRID 400 MA.
f. Adjust PA GRID MTRG CAL control A22R72 for a 400 mA reading on the test meter.
9. Remove the dc power supply test leads.
h. Attach the positive terminal of the $d c$ power supply to $E 76$ and the negative terminal to E75 and adjust the DC Power Supply currem to 80 milli amps.
i. Set the TEST METER selector switch to DVR SCREEN 80 MA.
j. Adjust the DVR SCREEN MTRG CAL control A22R73 for an $80-m A$ driver screen current reading on the TEST METER.
k. Remove the dc power supply test leads.
5.6.6 High-Voltage Power Supply Adjustments (Static Check - No Drive) WARNING

HIGH VOLTAGES ARE EXPOSED WHEN CABINET DOORS OR ACCESS PANELS ARE OPENED. DEATH ON CONTACT MAY OCCUR IF YOU ARE NOT EXTREMELY CAREFUL WHEN YOU PERFORM THE FOLLOWING PROCEDURES.
a. Remove the lower front panel below the exciter and block open the interlock switch.
b. Set the exciter POWER switch to OFF.
c. Press the FILAMENT $O N$ and PLATE $O N$ switches on control panel AI.
d. Raise or lower the POWER ADJUST control until approximately 8000 volts is indicated on the PLATE VOLTAGE meter.
e. Set TEST METER select switch to PA SCREEN 800 V . Observe that approximately 750 volts is indicated on the TEST METER.
f. Set TEST METER select switch to DVR SCREEN 400 V . Observe that $280 \pm 10$ volts is indicated on the TEST METER.

* g. Set TEST MEIER select switch to DVR PLATE 4000 V . Observe that 1800 to 2000 volts is indicated on the TEST METER.
h. Set the TEST METER selector switch to the LEFT DVR K 400 MA position.
i. Adjust the LEFT BIAS control on the driver box All until the TEST METER indicates 125 mA .
j. Set the TEST METER selector switch to the RIGHT DVR K 400 MA position.
k. Adjust the RIGHT BIAS control on driver box All until the TEST METER indicates 125 mA .
NOTE

The two bias controls interact and should be adjusted several times to acquire a constant 125 mA in both tubes.

1. Press the PLATE OFF and FILAMENT OFF switches on control panel A1.
m. Replace all panels and close all compartment doors.

### 5.6.7 RF Tuning Procedure

## NOTE

Major rf tuning is required only when components in the rf circuit are replaced or when the operating frequency is changed. Refer to the initial turn-on procedures (paragraph 2.5) for minor tuning instructions.

The following paragraphs provide procedures for major rf tuning of the transmitter. If the operating frequency is the same as the frequency specified in the production test data supplied with the transmitter, perform the procedures in paragraphs 5.6.7.3 through 5.6.7.6. If the operating frequency is different from the frequency specified in the production test data supplied with the transmitter, perform the procedures in paragraphs 5.6.7.1 through 5.6.7.6.
5.6.7.1 Shorting Plane, Driver Loading Slider, Driver Tuning Slider, Driver Grid Slider, and PA Neutralization Preliminary Adjustments

## NOTE

These adjustments are not necessary if the related components have not been replaced and the operating frequency is the same as the frequency specified in the production test data supplied with the transmitter.
a. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
b. Open the plate cavity and grid compartment doors.
c. Adjust the plate cavity shorting plane (figure 4-2) to the desired frequency in accordance with the graph in figure 5-1.
d. Adjust driver loading slider A21L8, driver tuning slider A21L7, and driver grid slider AllL9 to the desired frequency in accordance with the graph in figure 5-2.
e. Adjust the pa neutralization bar to the desired frequency in accordance with the graph in figure 5-3.
f. Remove the panel located beneath the exciter.

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HIGH VOLTAGES ARE EXPOSED WHEN CPBINET DOORG OR ACCESS PRNELS ARE OPENED. DEATH ON CONTACT MAY OCCUR IF YOI ARE NOT EXTREMELY CAPEFUL WIIEN YOU PERFORM THE FOLLOWING PROCEDURFR.
g. Discharge all large capacitors.
h. Remove the driver box access panel.
i. Adjust driver grid slider All山9 to the desired frequency in accordance with the graph in figure 5-2.
5.6.7.2 Driver Grid Tuning

NOTE
This procedure is not necessary if the related components have not been replaced and the operating frequency is the same as the frequency specified in the production test data supplied with the transmitter.
a. Perform the preliminary adjustments in paragraph 5.6.7.1 before proceeding.



Figure 5-1. PA Plate Tuning Cavity Slider Approximate Adjustment



DRIVER LOADING SLIDER



DRIVER TUNING
SLIDER
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INITIAL SETTINGS


Figure 5－2．Graph for Approximate Setting of Driver Loading， Driver Tuning，and Driver Grid Slider．
b. Tune the 802 A exciter to the desired operating frequency. Refer to the 802A exciter instruction book.


PA NEUTRALIZING ADJUSTMENT

NOTE: A NEUT. SETTING OF "L" BEING GREATER THAN INDICATED ON CHART RESULTS IN A MORE STABLE AMPLIFIER.


Figure 5-3. PA Neutralizing Adjustment
c. Block the interlock grounding switch open.
d. Set DRIVER, PA SCREEN, and PA PLATE POWER SUPPLY circuit breakers A6CB3, A6CB4, and A6CB5 to OFF.
e. Press the FILAMENT ON and PLATE ON switches.

WARNING

HIGH VOLTAGES ARE EXPOSED WHEN CABINET DOORS OR ACCESS PANELS ARE OPENED. DEATH ON CONTACT MAY OCCUR IF YOU ARE NOT EXTREMELY CAREFUL WHEN YOU PERFORM THE FOLLOWING PROCEDURES.
f. Adjust exciter POWER OUTPUT control until 15-watt forward power is indicated on exciter forward meter. Switch FWD/REFL switch of 802A exciter to read REFL POWER.
g. Adjust TUNE and COUPLE capacitors AllC33 and AllC34 on the driver box for minimum reflected power. Should be "0" or near "0".
h. Check that the TUNE and COUPLE capacitors are approximately onehalf mesh when they are adjusted for minimum reflected power.
i. If either control is not approximately midrange, remove power from the transmitter, adjust AllL9, and repeat steps e through h.
j. Turn transmitter OFF and replace all panels and close all compartment doors.

### 5.6.7.3. PA Tuning

a. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
b. If possible, connect the transmitter to an rf wattmeter/dummy load combination or a calorimeter capable of measuring and dissipating 25 kilowatts at 50 to 125 MHz . If these devices are unavailable, refer to the RF WATTMETER on the control panel for power output measurement.

CAUTION

DO NOT PERFORM THE REMAINDER OF THIS PROCEDURE IF THE TRANSMITTER IS NOT CONNECTED TO AN ANTENNA WITH A 50-OHM IMPEDANCE OR A DUMMY LOAD CAPABLE OF DISSIPATING AT LEAST 25 KILOWATTS.
c. Turn the DRIVER PLAIE IUNING control fully counterclocikise. Ihen turn the contro six turns clockwise ( 30 percent from maximm capacity).
d. Open the plate cavity access door and observe pa tuning and loading capacitors A18C51 and A18C50. (See figure 4-2.) Adjust the PA TUNING and PA LOADING controls on the control panel until the two capacitors are positioned approximately midrange. Close the plate cavity door.
e. Open the tube socket access door located beneath the DRIVER PLATE TUNING control.
f. Turn filament peaking capacitor A21C39 to near minimum capacity.
g. Set PA SCREEN circuit breaker to OFF. Ascertain that the exciter POWER switch is ON .

## CAUTION

DO NOT EXCEED THE FOLLOWING MAXIMUM RATINGS:
LEFT DRIVER CATHODE CURRENT: 250 mA
RIGHT DRIVER CATHODE CURRENT: 250 mA
PA SCREEN CURRENT: 600 mA
PA PLATE CURRENT: 4.0 AMPERES
h. Press the FILAMENT $O N$ and PLATE $O N$ switches on control panel A1.

## CAUTION

PROLONGED OPERATION WITH THE PLATE POORLY TUNED MAY DAMAGE THE POWER AMPLIFIER.
i. If an rf output from the transmitter is indicated when power is applied, quickly adjust the PA TUNING and PA LOADING controls for a maximum output power indication.
j. If an rf output is not present when power is applied, adjust the DRIVER PLATE TUNING control until an output is indicated.
k. Repeat steps $\mathbf{i}$. and $j$. until maximum output power is obtained. If the PA TUNING control encounters an end-stop while in the LOWER position, lower the shorting plane and retune. If an end-stop is encountered in the RAISE position, raise the shorting plane and retune.

* 1. Adjust the exciter output to produce 30 to 40 mA of Driver Screen current.
m. Check for pa neutralization. Refer to paragraph 5.6.7.5.
n. Check driver neutralization. Refer to paragraph 5.6.7.4.


## NOTE

Because of the relatively high output capacity of the 4CX15000A and the resulting low cavity inductance, no plate current dip will be noted at highter power levels. Tuning and loading should be adjusted in steps for maximum output power.
o. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
p. Open the pa cavity door and ensure that plate tuning capacitor A18C50 is approximately halfway between its limits.
q. If plate tuning capacitor A18C50 is not approximately halfway between its limits, adjust the pa plate cavity shorting plane (paragraph 5.6.7.1) and repeat steps c. through p. of this paragraph.
r. Remove the rear access panel behind the plate cavity.
s. Remove the access panel directly below the exciter. Block open the interlock switch.
t. Press the FILAMENT $O N$ and PLATE $O N$ switches on the control panel.

## WARNING

high voltages are exposed when cabinet doors or access panels are opened. DEATH ON CONTACT MAY OCCUR IF YOU ARE NOT EXTREMELY CAREFUL WHEN YOU PERFORM THE FOLLOWING PROCEDURES.
u. Using an insulated screwdriver, adjust PA BIAS ADJ resistor Al8R35 for proper output currents. The PA grid drive level determines the amount of bias required, and with higher drive levels an increase in bias results in greater amplifier efficiency. Compare the efficiency with the efficiency graphs, figure 5-4 and figure 5-5.

## NOTE

Efficiency is calculated using the following formula:
Efficiency $=\frac{\text { Power Output (watts) }}{\text { Plate Voltage } \times \text { Plate Current }}$
v. Adjust L DVR BIAS ADJ control AllR40, and R DVR BIAS ADJ control AllR44 until the pa is saturated. (LEFT DVR K 400 MA and RIGHT DVR K 400 MA test meter (MI) indications are not to exceed 250 mA .)
w. Adjust the power output as described in paragraph 5.6.7.6.

### 5.6.7.4 Driver Neutralization

a. Check for proper driver neutralization by adjusting the tuning of the transmitter and noting that the DVR SCREEN current peak is coincident with the peak of PA GRID current, and a dip of DVR K current. If neutralization is correct, do not perform the remiander of this procedure.
b. Press the PLATE OFF and FILAMENT OFF switches on control panel A1.
c. Open the tube socket access door directly beneath the DRIVER PLATE TUNING control.
d. Slightly adjust the paddle, $\mathrm{C}_{\mathrm{N}}$, attached to capacitor AllC35.
e. Close the access door and recheck the driver neutralization.
f. Repeat steps b. through e. until proper neutralization is obtained.

### 5.6.7.5 Neutralization

a. Check the transmitter for proper neutralization by tuning the transmitter for a pa screen current peak and observing that maximum output power occurs at the same time. If neutralization is correct, do not perform the remainder of this procedure.

NOTE

A minimum value of pa plate current also occurs when neutralization is correct.
b. Press the PLATE OFF and FILAMENT OFF switches on control panel A1.
c. Open the pa cavity door. Short all high voltage terminals with grounding stick.
d. Remove front half of tube air guide to gain access to screen sliders.
e. Refer to figure 5-3 and adjust the screen sliders, LN1 and LN2. The sliders should not require an adjustment greater than $\pm 1 / 4$ inch from the initial setting. (A setting on the plus side is preferred.)
f. Replace the tube air guide.
g. Close the cavity door and apply power to the transmitter.
h. Check for proper neutralization again. If incorrect, repeat steps b. through g.
5.6.7.6 Maximum Power Output Adjustment

## NOTE

This procedure is intended to maintain authorized station maximum power output with line voltage variations and should be performed using a $50-0 h m$ load capable of dissipating 25 kilowatts.

Do not make this adjustment until the pa tuning procedure in paragraph 5.6.7.3 is accomplished.
a. Set the POWER ADJUST control to RAISE until maximum power output is displayed on the RF WATTMETER.
b. If the maximum power output is not more than 10 percent above the authorized station maximum output, skip to step $h$. If the maximum power output is more than 10 percent of the authorized station maximum output, proceed to step $c$.
c. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
d. Turn off primary power to the transmitter.
e. Refer to table 2-1. Change wires to the transformer terminals for the next higher line voltage connection. (Example: If the wires are originally connected for a line voltage of 240 volts, reconnect the wires for a line voltage of 250 volts.) To change screen voltage only, refer to table 5-2.
f. Reapply primary power and press the FILAMENT $O N$ and PLATE $O N$ switches on control panel Al.
g. Repeat steps b. through f. until the maximum transmitter output is not more than 10 percent above the authorized station maximum output.
h. Compare the PLATE VOLTAGE reading with the plate voltage listed in table 3-5 for the authorized station maximum power output. (Linear interpolation of tabulatea values may be necessary.) If the compared voltages differ by more than 10 percent, proceed to step $i$. If the compared voltages differ by less than 10 percent, skip to step $m$.
i. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
j. Turn off primary power to the transmitter.
NOTE

In addition, the desired power setting may be achieved by changing the pa loading.
k. Refer to table 2-1. If the transmitter plate voltage exceeds the tabulated voltage, change wires on transformer T3 to the terminals listed for the next higher line voltage. If the tabulated voltage exceeds the transmitter plate voltage, change wires on transformer $T 3$ to the terminals listed for the next lower line voltage.

1. Repeat steps h. through $k$. until the transmitter and the tabulated plate voltages differ by less than 10 percent.
m. Adjust the POWER ADJUST control until the RF WATTMETER displays the authorized station maximum power output.
n. Refer to figure 5-6. Check the forward and reflected power levels and determine the vswr. If the vswr exceed 2:1, check the antenna impedance.

## NOTE

The vswr on a properly tuned antenna is 1.1:1, or less.
5.6.8 Board A3, Offset Zero Adjustment
a. Press the PLATE OFF and FILAMENT OFF switches on control panel AI.
b. Remove cover from the control circuits and pull the plunger on the card cage interlock all the way out.
c. Set the exciter POWER switch to off.
d. Place board A3 on a card extender.
e. Press the FILAMENT ON switch.
f. Connect a dc voltmeter from TP2 (red) and TP3 (orange). Set VSWR PROT switch to OFF.
g. Adjust REFL OFFSET control A3R26 until 0 volt is indicated on the dc voltmeter.
h. Remove the dc voltmeter from TP2 (red) and connect it to TP1 (brown).
i. Adjust FWD OFFSET control A3R25 until 0 volt is indicated on the dc voltmeter.
j. Press the FILAMENT OFF switch.
k. Replace board A3 in its proper place. Replace cover on the control circuits.
a. Set the POWER CONTROL switch to AUTOMATIC.
b. Remove the panel covering the control circuits and disable the interlock switch.
c. Press the FILAMENTS $O N$ and PLATE $O N$ switches on control panel A1.


Figure 5-6. Power to VSWR Conversion Graph.
d. Adjust POWER CONTROL ADJ A3R27 until the authorized station output is displayed on the RF WATTMETER. ( $100 \%$ )

## WARNING

hIGH VOLTAGES ARE EXPOSED WHEN CABINET DOORS OR aCCESS PANELS ARE OPENED. death on contact may occur if you are not extremely careful when you perFORM THE FOLLOWING PROCEDURES.
e. Adjust filament peaking capacitor A21C39 until minimum plate current is displayed on the PLATE CURRENT meter. (Power output should remain near maximum.)
f. Replace all panels and close all compartment doors.

## maintenance

### 5.6.10 VSWR Trip

a. Press the FILAMENT ON and PLATE ON switches on control panel AI.
b. Place the POWER CONTROL switch in the MANUAL position.
c. With the POWER ADJUST control, lower the maximum output power to 2500 watts ,
d. Press the PLATE OFF and FILAMENT OFF switches on control panel Al.
e. Carefully loosen the base clamps on directional coupler Al6 and reverse the assembly and re-tighten base clamps.
f. Remove cover from the control circuits and pull out the plunger on the card cage interlock.
g. Set the VSWR PROT switch on A3 to ON and the AUTO•RECYCLE switch on A7 to OFF,
h. Press the FILAMENT ON and PLATE ON switches on control panel AI.

1. Adjust VSWR PROT CAL A3R20 until vswr trip relay A22K9 is energized and plate voltage is removed. (The VSWR fault indicator on A7 will light.)
j. Set the VSWR PROT switch to OFF and press the PLATE ON switch.
k. Set the VSWR PROT switch to ON. If the transmitter fails to turn off, repeat steps a. through j .
2. Press the FILAMENT OFF switch and the FAULT RESET switch. Set AUTO RECYCLE switch to ON.
m. Replace the directional coupler in its normal position.
n. Adjust the transmitter power output to authorized station power output with the POWER ADJUST control.

### 5.6.11 VSWR Protect Test Circuit

a. Remove cover from the control circuits and pull out the plunger on the card cage interlock.
b. Press the FILAMENT ON switch on control panel Al.
c. Set control panel POWER switch to the REFLECTED position.
d. Press A3 Test switch S2 and adjust REFL ADJ potentiometer R27 for a reading of $100 \%$. Adjust VSWR PROT CAL to trip at this level. (Note $100 \%$ meter reading in the REFLECTED position is 2500 watts.)
e. Note: For greater VSWR trip sensivity, press A3 TEST switch S2 and adjust REFL ADJ potentiometer R27 for a reading less than 100\%. ( $50 \%$ reading corresponds to 1250 watts.) Then adjust A3R20 to trip at the new level. Caution: Nuisance tripping may occur if the sensitivity is increased too far.
5.6.12 Phase Monitor Adjustment

WARNING

HIGH VOLTAGES ARE EXPOSED WHEN CABINET DOORS OR ACCESS PANELS ARE OPENED. DEATH ON CONTACT MAY OCCUR IF YOU ARE NOT EXTREMELY CAREFUL WHEN YOU PERFORM THE FOLLOWING PROCEDURES.
a. Remove the right front bay access panel.
b. Block the interlock grounding switch open.
c. Set potentiomenter A19K5 to system operating voltage. (Voltage indicated on the dial is the normal operating phase-to-phase voltage of the three phase primary input power.)
d. For close protection, increase the adjustment until A19K5 drops out. (Red LED will go out.) Back adjustment down slightly until relay picks up.
e. Replace access panel.
5.7 Parts Replacement
5.7.1 4CX15000A PA TUBE
a. Remove air shields (tube chimney) between the PA blocker and the cabinet base. Loosen the two bands on PA blocking capacitor and slide the blocking capacitor down over the PA tube.
b. Remove the anode lead.
c. Carefully lift the tube and PA blocking capacitor out of its socket.
d. Reverse the procedure to replace the tube.

### 5.7.2 Control Panel Indicator Lamps

a. Pull the switch out and rotate it $90^{\circ} \mathrm{ccw}$; the lamp assembly should pop out.
b. Remove the defective lamp by pressing down on the bulb.
c. Reinsert new bulb and replace the assembly.
table 5-2. SCREEN VOLTAGE TRANSFORMER TAP SCHEDULE

|  | $\begin{array}{\|l} \hline \text { PRT } \\ \text { TAPS } \\ \hline \end{array}$ | LINE VOLTAGE. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 200 | 210 | 220 | 230 | 240 | 250 |
|  | 200 | 800 | 840 | 880 |  |  |  |
|  | 210 | 762 | 800 | 838 | 876 |  |  |
|  | 220 | 727 | 764 | 800 | 836 | 873 |  |
|  | 230 | 696 | 730 | 765 | 800 | 8.35 | 870 |
|  | 240 | 667 | 700 | 733 | 787 | 800 | 833 |
|  | 250 | 640 | 672 | 704 | 736 | 768 | 800 |
|  | 200 | 680 | 714 | 748 |  |  |  |
|  | 210 | 648 | 680 | 712 | 745 |  |  |
|  | 220 | 618 | 649 | 680 | 711 | 742 |  |
|  | 230 | 591 | 621 | 650 | 680 | 710 | 739 |
|  | 240 | 567 | 595 | 623 | 652 | 680 | 708 |
|  | 250 | 54.4 | 571 | 598 | 62.5 | 653 | 680 |
|  | 200 | 560 | 588 | 616 |  |  |  |
|  | 210 | 533 | 560 | 587 | 613 |  |  |
|  | 220 | 509 | 535 | 560 | 585 | 611 |  |
|  | 230 | 487 | 511 | 536 | 560 | 584 | 609 |
|  | 24.0 | 467 | 490 | 513 | 537 | 560 | 583 |
|  | 250 | 448 | 470 | 49.3 | 515 | 538 | 560 |
|  | 200 | 462 | 4.85 | 508 |  |  |  |
|  | 210 | 440 | 4.62 | 484 | 506 |  |  |
|  | 220 | 420 | 441 | 462 | 483 | 504 |  |
|  | 230 | 402 | 422 | 4.42 | 462 | 482 | 502 |
|  | 240 | 385 | 404 | 4.24 | 443 | 462 | 481 |
|  | 250 | 370 | 388 | 407 | 425 | 4.44 | 462 |

## maintenance



Figure 5-4. 816R-3 Amplifier Efficiency vs Frequency Graph


Figure 5-5. 816R-3 Amplifier Efficiency vs Output Level

### 6.1 General

This section contains a list of all repairable/replaceable electrical, and critical mechanical parts for the 816R FM Transmitter.

### 6.2 REF DES

This column contains the electrical reference designators of all parts that have been assigned on schematics or wiring diagrams, and/or index numbers for all parts for which reference designators have not been assigned. When a reference designator, within a series of reference designators, has not been assigned a part number, the unassigned reference designator will be reflected as "NOT USED" in the DESCRIPTION column.

### 6.3 Description

This column contains the identifying noun or item name followed by a brief dedescription. The description for electrical/electronic parts includes the application ratings and tolerances. For consecutively listed identical parts within an assembly, "SAME AS ---" is reflected in the description of subsequent listings, referencing to the first listing within the assembly.

### 6.4 CEMC Part Number

The CEMC Radio Specification or drawing number, for each item in the parts list, is reflected in this column.

### 6.5 Illustrations

All parts listed in the REF DES column are located on corresponding illustrations. The illustration always precedes the parts list. When a replacable electrical item is hidden from view by structural parts of wiring, a dotted leader line is used to show the locations of the item on the illustration.

## parts list

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KO1-(3)
Figure 6-1. 816R FM Transmitter (Sheet 1 of 3)


Figure 6-1. 816R FM Transmitter (Sheet 2 of 3 )


Figure 6-1. FM Transmitter (Sheet 3 of 3).
parts list

| REF DES | DESCRIPTION | CEMC PART NUMBER |
| :---: | :---: | :---: |
|  | 816R-3 25 kW FM TRANSMITTER | 640-3540-006 |
| AI | Control Panel | 786-3243-006 |
| A2 | Remote Control Assembly <br> - Optional equipment- | 786-3327-001 |
| A3 | Fwd/Refl Cal and Pwr Control Board | 648-8092-001 |
| A4 | 802A FM Exciter | 643-0001-001 |
| A5 | Filament Regulator | 648-8095-001 |
| A6 | Circuit Breaker Panel | 786-3416-005 |
| A7 | Overload \& Recycle Board | 640-5380-001 |
| A8 | Power Control Regulator | 627-6683-001 |
| A9 | Power Control Panel | 789-4342-002 |
| A10 | 2 KV Power Supply | 789-4358-001 |
| All | RF Driver Assembly | 786-3309-002 |
| Al2 | Latching Relay and Status Board | 648-8082-001 |
| Al3 | RF Output Low-Pass Filter | 786-3451-002 |
| A14 | Power Supply Filter | 786-3583-001 |
| A15 | Metering Multiplier board | 786-3168-001 |
| A16 | Directional Coupler | 786-3264-001 |
| A17 | Bleeder Resistor Panel | 786-3154-002 |
| A18 | Power Amplifier Cavity | 786-3335-003 |
| A19 | Component Panel | 648-8124-001 |
| A20 | Card Cage Assembly | 786-3301-002 |
| A21 | Power Amplifier Socket | 786-3686-001 |
| A22 | Overload and Meter Calibrate Panel | 786-3666-002 |
| $\begin{aligned} & \text { A23 } \\ & \text { A24 } \\ & \text { A25 } \end{aligned}$ | Extender Card Not Used AC Metering Pane? | $771-9168-001$ $636-7263-001$ |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| B1 | Fan, Centrifugal <br> Motor, Alternating Current 0.5 A , 208/220 VAC | $\begin{aligned} & 009-0167-010 \\ & 230-0593-010 \end{aligned}$ |
| C1 | Not Used |  |
| C2 | Not Used |  |
| C3 | Capacitor, Fxd, Paper $20 \mu \mathrm{~F}$, 10\% Tol, 10 KVDCW | 930-0781-040 |
| C4 |  |  |
| Through C36 | Not Used |  |
| C37 | Driver Tuning Capacitor, Vacuum Var. 3-30 pF, 7.5 KVP | 919-0301-010 |
| C38 |  |  |
| Through C44 | Not Used |  |
| C45 | Blocking Capacitor | 786-3597-001 |
| C46 | Not Used |  |
| C49 | Not Used |  |
| C50 | PA Loading Capacitor | 786-3048-001 |
| C51 | PA Tuning Capacitor | 786-3049-001 |
| C52 |  |  |
| Through C56 | Not Used |  |
| C57A | Capacitor, Fxd, Ceramic, $100 \mathrm{pF}, 10 \% \mathrm{Tol}$, 5 KVDCW | 913-0821-000 |
| C58B | Same as C57A |  |
| $J 1$ | Not Used |  |
| J2 | Not Used |  |
| J3 | Connector, Electrical, Receptacle Single Outlet, Grounding Type | 368-0139-010 |
| L1 | Plate Supply Filter Choke 4 H Inductance | 668-0199-010 |
| L2 | Screen Supply Filter Choke 1H Inductance | 668-0200-010 |
| L3 | Not Used |  |
| L4 | Not Used |  |
| L5 | PA Grid RFC <br> 4.7 UH, 10\% Tol | 240-1611-000 |
| PS1 | 28 Volt Power Supply | 786-3013-001 |
| PS2 | PA Bias Power Supply | 786-3081-001 |
| R1 |  |  |
| Through | Not Used |  |
| R35 | Resistor, Var, Wirewound, 1.0 Kilohm, 10\% Tol, 50 Watts | 749-1026-000 |
| R36 | Resistor, Fxd, Wirewound, 3.0 Kilohms, 5\% Tol, 80 Watts | 710-9294-000 |
| R37 | ```Resistor, Fxd, Wirewound, 10 ohms, 5% Tol, 3 Watts``` | 747-5320-000 |
| CHANGE 3 |  |  |

parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| S1 | Not Used |  |
| S2 | Not Used |  |
| S3 | Not Used |  |
| S4 | Switch, Sensitive | 260-0025-000 |
|  | SPDT Contact Arrangement |  |
|  | Includes |  |
| S5 | Actuator, Switch | 260-0026-000 |
| S6 | Same as S4 |  |
| S7 | Not Used |  |
| S8 | Not Used |  |
|  | Shorting Switch | 627-9743-004 |
|  | - Spring, Shorting Switch | 540-5342-002 |
|  | Strap, Grounding | 304-6000-000 |
|  | Strip, Shorting | 632-1149-001 |
|  | Contact, Shorting | 542-1773-002 |
|  | - Shaft, Flat, Straight | 627-9786-001 |
|  | Insulator, Standoff | 190-0026-000 |
| 59 | Same as S8 |  |
| 510 | Same as S4 |  |
| 511 | Same as S4 |  |
| S12 | Same as S4 |  |
| S13 | Shorting Switch (Same as S4 Except Shaft, Flat, Straight CPN 627-9786-007) | 627-9743-008 |
| 514 | Same as S13 |  |
| S15 | Same as Sl3 |  |
| 11 | Transformer, PWR, Step-Up | 664-0124-020 |
| T2 | Transformer, PWR, Step-Up | 664-0123-020 |
| T3 | Transformer, PWR, Step-Up | 664-0125-010 |
| T4 | Transformer, PWR, Step-Down | 662-0043-000 |
| 55 | Transformer, PWR, Step-Down | 662-0410-020 |
| VI | Not Used |  |
| $V 2$ | Not Used |  |
| $V 3$ | Electron Tube | 256-0157-000 |
| VR] | Suppressor, Plate Includes | 625-8349-002 |
|  | Absorber, Overvoltage | 353-0283-140 |
| VR2 | Suppressor, Screen | 625-8348-001 |
|  | Includes |  |
|  | Absorber, Overvoltage -CR6, CR7- | 353-0283-100 |
| 21 | Complete Rectifier |  |
|  | Includes |  |
|  | Rectifier Column | 353-6596-010 |
|  | -Qty 3- |  |
| 1 | Shorting Stick | 547-6572-002 |
|  | Includes |  |
|  | Rod, Shorting | 547-6574-002 |
|  | Spring, Compression | 547-6575-002 |
|  | Cord, Shorting Stick | 427-0004-000 |
| 2 | Clamp, Neutralizing -Qty 2- | 786-3236-001 |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| $\begin{aligned} & 3 \\ & \\ & 4 \\ & 5 \\ & 6 \\ & 7 \\ & 8 \\ & 9 \\ & 10 \\ & 11 \\ & 12 \\ & 13 \end{aligned}$ | ```Clamp, Neutralizing -Qty 2- Impeller, Fan Knob Bearing Assembly, Panel Joint, Universal Shaft Coupling, Insulator Filter Retainer, Upper Deflector Clamp``` | $\begin{aligned} & 786-3237-001 \\ & 009-3118-010 \\ & 757-0228-001 \\ & 015-3437-010 \\ & 233-0132-000 \\ & 789-4365-001 \\ & 015-3438-010 \\ & 786-3457-001 \\ & 786-3537-001 \\ & 786-5842-001 \\ & 013-1309-420 \end{aligned}$ |



Figure 6-2. Control Panel, A1 (Sheet 1 of 2)


Figure 6-2. Control Panel, A1 (Sheet 2 of 2)
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| CONTROL PANEL, A1 |  | 786-3243-006 |
| C1 | Capacitor, Fxd, Mica, 100 pF 5\% Tol, 500 VDCW | 912-2816-000 |
| C2 | Same as Cl |  |
| C3 | Same as Cl |  |
| C4 | Same as Cl |  |
| DSIA | Lamp, Incandescent, 0.04A, 28 volts | 262-0179-010 |
| DSIC | Same as DSIA |  |
| DS2A | Same as DSIA |  |
| DS2C | Same as DSIA |  |
| DS4A | Same as DSTA |  |
| DS4C | Same as DSIA |  |
| DS5A | Same as DSIA |  |
| DS5C | Same as DSIA |  |
| M1 | ```Meter, DC Test +1% O to 1 mA``` | 458-5005-060 |
| M2 | ```Meter, DC Plate Current }\pm1 O to 1 mA``` | 458-5005-050 |
| M3 | Meter, DC Plate Voltage $\pm 1 \%$ 0 to 2 mA | 458-5005-070 |
| M4 | ```Meter, DC Wattmeter +2% 0 to 100 \muA``` | 458-5005-100 |
| R1 | Resistor, Fxd, Composition, 180 Ohms, 10\% Tol, 1 Watt | 745-5621-000 |
| R2 |  |  |
| Through R4 | Same as Rl. |  |
| R6 | Not Used |  |
| R7 | ```Resistor, Fxd, Film, 1740 Ohms, 1% Tol, 1/4 Watt``` | 705-6758-000 |
| R8 | Resistor, Fxd, Composition, 39 Kilohms, 10\% Tol, 1 Watt | 745-3419-000 |
| R9 | ```Resistor, Fxd, Film, 301 Ohms, 1% Tol, 1/2 Watt``` | 705-7071-000 |
| S1 | Switch, Rotary <br> DP12T Contact Arrangement | 259-2219-010 |
| S2 | Switch, Rotary DPDT Contact Arrangement | 259-2759-010 |
| S3 | Switch, Rotary DP3T Contact Arrangement | 259-1980-000 |
| S4 |  |  |
| Through S6 | Sames as S3 |  |
| S7 | Switch, Push, Illuminated SPDT Contact Arrangement | 266-6806-100 |
| S8 <br> Through <br> Sl1 | Same as S7 |  |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| TB1 | Strip, Terminal 17 Termiaals -Qty 2- | 367-0025-000 |
| TB2 | Strip, Terminal 16 Terminals | 367-0024-000 |
| XDS 1 XDS2 | Switch, Push, Illuminated | 266-6806-010 |
| Through XDS5 | Sames as XDS 1 |  |
| 1 | Knob, Round, Skirted -Qty 6- | 757-0233-003 |
| 2 | ```Barrier, Vertical Mounting -Qty 8-``` | 266-6806-030 |
| 3 | Lens, Engraved Filament Off | 266-6806-270 |
| 4 | Lens, Engraved Filament On | 266-6806-280 |
| 5 | Lens, Engraved Fault/Reset | 266-6806-800 |
| 6 | Lens, Engraved Plate Off | 266-6806-740 |
| 7 | Lens, Engraved Plate On | 266-6806-790 |
| 8 | Boot, Bulb White -Qty 2- | 266-6268-000 |
| 9 | Boot, Bulb Green -Qty 4- | 266-6806-040 |
| 10 | Boot, Bulb Red -Qty 2- | 266-6806-060 |



Figure 6-3. Remote Control Assembly, A2.


## parts list



Figure 6-4. Fwd/Refl Cal and Pwr Control Board, A3.

parts list



Figure 6-5. Filament Regulator, A5.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
|  | FILAMENT REGULATOR BOARD, A5 | 648-8095-001 |
| C1 | Capacitor, Fxd, Solid Tantalum $33 \mu \mathrm{~F},+20 \%$, 25 VDC | 184-9102-260 |
| C2 | Capacitor, Fxd, Solid Tantalum $47 \mu \mathrm{~F},+20 \%$, 35 VDC | 184-9102-890 |
| C3 | Same as C1 .- |  |
| C4 | Same as C2 |  |
| C5 | Same as:C2 |  |
| C6 | Same as C2 |  |
| C7 | Capacitor, Fxd, Ceramic <br> $0.1 \mu \mathrm{~F}, 20 \%$ Tol, 50 VDC | 913-5019-720 |
| C8 | Capacitor, Fxd, Electolytic <br> $100 \mu \mathrm{~F}$, minus $10 \%$, plus $75 \%$, 50 VDC | 183-1281-080 |
| C9 | Same as C8 |  |
| C10 | Same as C8 |  |
| CR1 | Diode, IN4003 | 353-6442-030 |
| CR2 | Same as CR1 |  |
| CR3 | Same as CR1 |  |
| CR4 | Same as CR1 |  |
| CR5 | Diode, IN4748A, 22V 1 Watt ZENER | 353-6481-410 |
| CR6 | Diode, IN4106, 12V 1/4 Watt ZENER | 353-3591-080 |
| CR7 | Same as CR1 |  |
| DS1 | Lamp, Incand. | 262-3270-000 |
| DS2 | Same as DS1 |  |
| F1 | Fuse, . 25 Amp Cartridge, Slow Blow | 264-0291-000 |
| K1 | Relay, 4 C 800 Ohm, 24V | 970-2420-100 |
| K2 | Same as K1 |  |
| K3 | Same as K1 |  |
| , Q1 | Transistor, 2N2222A | 352-0661-020 |
| Q2 | SCR, 2N2323A, 50V, .22A | 353-3540-010 |
| Q3 | Same as Q2 |  |
| Q4 | Same as Q2 |  |
| Q5 | Same as Q1 |  |
| R1 | Resistor, Fxd, Wirewound 120 Ohms, $5 \%$ Tol, 6.5 Watt | 747-5442-000 |
| R2 | Resistor, Fxd, Composition 56 Ohm, 10\% Tol, 2 Watt | 745-5600-000 |
| R3 | Resistor, Var., Metal Film $1000 \mathrm{hm}, 20 \%$ Tol, 2 Watt | 382-0006-020 |
| R4 | Resistor, Fxd, Carbon Film <br> 5.6 Kilohms, 5\% Tol, $1 / 4$ Watt | 745-0910-830 |
| R5 | Resistor, Fxd, Carbon Film <br> 3.3 Kilohms, 5\% Tol, $1 / 2$ Watt | 745-0914-770 |
| R6 | Resistor, Fxd, Carbon Film 100 hhm, 5\% Tol, $1 / 4$ Watt | 745-0910-410 |
| R7 | Resistor, Var, 25 Turn 50 Kilohms, $10 \%$ Tol, $1 / 2$ Watt | 382-1405-100 |

parts list



## REAR VIEW

Figure 6-6. Circuit Breaker Panel, A6.

| REF DES | DESCRIPTION | CEMC PART NUMBER |
| :---: | :---: | :---: |
|  | CIRCUIT BREAKER PANEL, A6 | 786-3416-005 |
| CB1 | Circuit Breaker 1A 3 Pole | 260-4038-150 |
| CB2 | Circuit Breaker 10A 3 Pole | 260-0407-000 |
| CB3 | Circuit Breaker 4.5A 3 Pole | 260-4038-090 |
| CB4 | Circuit Breaker 15A 3 Pole | 260-0409-000 |
| CB5 | Circuit Breaker 70A 4 Pole | 260-0972-030 |
| F1 | Fuse, Cartridge 10A Current Rating | 264-1182-000 |
| F2 F3 | Fuse, Cartridge <br> 3A Current Rating, Slow Blow Same as Fl | 264-0009-000 |
| F4 | Fuse, Cartridge 0.25A Current Rating, Slow Blow | 264-0291-000 |
| $\begin{aligned} & \text { F5 } \\ & \text { F6 } \end{aligned}$ | Fuse, Cartridge 1A Current Rating | 264-4280-000 |
| F7 | Fuse, Cartridge <br> 2A Current Rating, Slow Blow | 264-0008-000 |
| F8 | $\begin{aligned} & \text { Same as F6 } \\ & \text { Same as F7 } \end{aligned}$ |  |
| F10 | Same as F6 |  |
| F11 | Same as F2 |  |
| F12 | Same as F7 |  |
| F13 | Same as F7 |  |
| F14 | Same as F7 |  |
| M1 | Meter, Time Totalizing | 458-0860-020 |
| XF1 | Fuseholder 20A Current Rating | 265-1241-090 |
| XF2 <br> Through <br> XF14 | Same as XF1 |  |



Figure 6-7. Overload \& Recycle Board, A7.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
|  | 0/L AND RECYCLE BOARD, A7 | 640-5380-001 |
| Cl | Capacitor, Fxd, Ceramic $0.01 \mu \mathrm{~F}, 20 \%$ Tol, 100 VDC | 913-5019-660 |
| C2 | Capacitor, Fxd, Ceramic $0.1 \mu \mathrm{~F}, 20 \%$ Tol, 50 VDC | 913-5019-720 |
| C3 | Same as Cl |  |
| C4 | Capacitor, Fxd, Ceramic <br> $1.0 \mu \mathrm{~F}, 20 \%$ Tol, 50 VDC | 913-5019-840 |
| C5 | Same as C2 |  |
| C6 | Same as Cl |  |
| C7 | Same as C4 |  |
| C8 | Same as C2 |  |
| C9 | Same as C2 |  |
| C10 | Same as C Same as |  |
| C11 C12 | Same as C 2 Same as Cl |  |
| C13 | Capacitor, Fxd, Solid Tantalum $10 \mu \mathrm{~F}, \because 20 \%$ Tol, 35 VDC | 184-9102-410 |
| C14 | Capacitor, Fxd, Solid Tantalum $2.2 \mu \mathrm{~F},+20 \% \mathrm{Tol}, 35 \mathrm{VDC}$ | 184-9102-370 |
| C15 | Same as C2 |  |
| C16 | Capacitor, Fxd, Electrolytic <br> $330 \mu \mathrm{~F}$, Minus $10 \%$ Plus $75 \%$, 50 VDC | 184-5102-040 |
| C17 | Same as C2 |  |
| C18 C19 | Same as C2 |  |
| C19 C20 | Same as C2 |  |
| C20 | Same as C2 Same as C2 |  |
| C22 | Same as C2 |  |
| C23 | Same as Cl. |  |
| C24 | Capacitor, Fxd, Solid Tantalum $4.7 \mu \mathrm{~F},+20 \% \mathrm{Tol}, 35 \mathrm{VDC}$ | 184-9102-390 |
| C25 | Same as Cl 3 |  |
| CR1 | Diode, IN914 | 353-2906-000 |
| CR2 | Same as CRI |  |
| CR3 | LED, Yellow | 353-0293-020 |
| CR4 | Diode, IN4004 | 353-6442-040 |
| CR5 | Same as CR3 |  |
| CR6 | LED, Red | 353-0293-040 |
| CR7 | Same as CR6 Same as CR6 |  |
| CR9 | Same as CR6 |  |
| CRIO | Diode, IN4003 | 353-6442-030 |
| CR11 | Same as CR10 |  |
| CRI2 | Same as CR10 |  |
| CR13 | Same as CR10 |  |
| CR14 | Same as CR3 |  |
| CR15 | Same as CR3 |  |
| CR16 | Same as CR3 |  |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| CR17 | Same as CR3 |  |
| CR18 | Same as CR3 |  |
| CR19 | Same as CR4 |  |
| CR20 | Same as CR1 |  |
| CR21 | Same as CR1 |  |
| CR22 | Same as CR1 |  |
| K1 | Relay, Reed, SPDT | 410-0572-010 |
| Q1 | Transistor, 2N2222A | 352-0661-020 |
| Q2 | Same as Q1 |  |
| Q3 | Same as Q1 |  |
| Q4 | SCR, GEC6F | 353-6468-010 |
| Q5 | Same as Q4 |  |
| Q6 | Same as Q4 |  |
| Q7 | Same as Q4 |  |
| Q8 | Same as Q4 |  |
| Q9 | Transistor, MJE243 | 352-1104-010 |
| R1 | Resistor, Fxd, Carbon Film 2.2 Kilohms, 5\% Tol, $1 / 4$ Watt | 745-0910-730 |
| R2 | Resistor, Fxd, Carbon Film 10 Kilohms, $5 \%$ Tol, $1 / 4$ Watt | 745-0910-890 |
| R3 | Resistor, Fxd, Carbon Film 1 Kilohm, 5\% Tol, 1/4 Watt | 745-0910-650 |
| R4 | Same as R1 |  |
| R5 | Resistor, Fxd, Carbon Film <br> 470 Kilohms, 5\% Tol, $1 / 4$ Watt | 745-0911-300 |
| R6 | Resistor, Fxd, Carbon Film <br> 4.7 Kilohms, $5 \%$ Tol, $1 / 4$ Watt | 745-0910-810 |
| R7 | Same as R5 |  |
| R8 | Resistor, Fxd, Carbon Film 470 Ohms, 5\% Tol, $1 / 4$ Watt | 745-0910-570 |
| R9 | Same as R3 |  |
| R10 | Resistor, Fxd, Composition 2.2 Megohms, $10 \%$ Tol, $1 / 4$ Watt | 745-0869-000 |
| R11 | Same as R3 |  |
| R12 | Resistor, Fxd, Wirewound 150 Ohms, 5\% Tol, 6.5 Watt | 747-5498-000 |
| R13 | Resistor, Fxd, Composition 2.7 Kilohms, $10 \%$ Tol, 1 Watt | 745-3370-000 |
| R14 | Same as R13 |  |
| R15 | Same as R13 |  |
| R16 | Same as R13 |  |
| R17 | Resistor, Fxd, Carbon Film 10 Ohms, 5\% Tol, 1/2 Watt | 745-0914-170 |
| R18 | Resistor, Fxd, Wirewound 560 Ohms, 5\% Tol, 6.5 Watt | 747-5455-000 |
| R19 | Same as R13 |  |
| R20 | Resistor, Fxd, Carbon Film 220 Ohms, 5\% Tol, 1/2 Watt | 745-0914-490 |
| R21 | Same as R20 |  |
| R22 | Same as R20 Same as R20 |  |

352-1104-010

Resistor, Fxd, Carbon Film 745-0910-730

745-0910-890
745-0910-650

745-0911-300
745-0910-810

745-0910-570

745-0869-000

747-5498-000
745-3370-000

745-0914-170
747-5455-000

745-0914-490



Figure 6-8. Power Control Regulator, A8.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| POWER CONTROL REGULATOR, A8 |  | 627-6683-001 |
| C1 | Capacitor, Fxd, Electrolytic, $100 \mu \mathrm{~F}$, Minus 10\%, Plus 75\%, 50 VDCW | 183-1281-080 |
| C2 | Capacitor, Fxd, Electrolytic, $180 \mu \mathrm{~F}$, $20 \%$ Tol, 25 VDCW | 184-8664-000 |
| C3 | Capacitor, Fxd, Ceramic, $0.1 \mu \mathrm{~F}$, Plus $80 \%$ minus $20 \%, 25$ VDCW | 913-3806-000 |
| C4 | Same as C3 |  |
| C5 | ```Capacitor, Fxd, Electrolytic, 47 \muF, 20% Tol, 20 VDCW``` | 184-9086-560 |
| CR1 | Diode, IN4003 | 353-6442-030 |
| CR2 | Same as CR1 |  |
| CR3 | Same as CR1 |  |
| CR4 | Same as CR1 |  |
| Q1 | Transistor, 2N3053 | 352-0613-010 |
| Q2 | Transistor, 2 2N222A Same as 01 | 352-0661-020 |
| Q4 | Same as Q2 |  |
| Q5 | Same as Q2 |  |
| R1 | Resistor, Fxd, Composition, 1000 Ohms, $10 \%$ Tol, $1 / 2$ Watt | 745-1352-000 |
| R2 | Resistor, Fxd, Composition, 15 Kilohms, $10 \%$ Tol, $1 / 2$ Watt | 745-1401-000 |
| R3 | $\text { Resistor, Fxd, Composition, } 22 \text { Kilohms, }$ $10 \% \text { Tol, } 1 / 2 \text { Watt }$ | 745-1408-000 |
| R4 | Same as R1 |  |
| R5 | Resistor, Fxd, Composition, 4700 Ohms, 10\% Tol, $1 / 2$ Watt | 745-1380-000 |
| R6 | Resistor, Fxd, Composition, 820 Ohms, 10\% Tol, 1 Watt | 745-3349-000 |
| R7 | Same as R3 |  |
| R8 | Resistor, Fxd, Composition, 47 Ohms, $10 \%$ Tol, $1 / 2$ Watt | 745-1296-000 |
| R9 | Same as R2 |  |
| R10 | Resistor, Fxd, Composition, 1500 Ohms, 10\% Tol, 1/2 Watt | 745-1359-000 |
| RII | Resistor, Fxd, Composition, 2700 Ohms, 10\% Tol, $1 / 2$ Watt | 745-1370-000 |
| R12 | Same as R8 |  |
| R13 | Resistor, Fxd, Composition, 1200 Ohms, 10\% Tol, 1 Watt | 745-3356-000 |
| R14 | Resistor, Fxd, Composition, 6800 Ohms 10\% Tol, $1 / 2$ Watt | 745-1387-000 |
| R15 TP1 | Same as Ril Jack, Tip |  |
| TP1 | $\underset{\text { Red }}{\substack{\text { Jack, Tip }}}$ | 360-0495-030 |
| TP2 | Jack, Tip Orange | 360-0495-040 |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :--- | :---: |
| TP3 | Jack, Tip <br> Black <br> VR1 <br> VR2 | Diode, IN4740 <br> Same as VR1 |



Figure 6-9. Power Control Panel, A9.
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| POWER CONTROL PANEL, A9 789-4342-002 |  |  |
| AR1 <br> Kl <br> XKI <br> CRI <br> CR2 <br> CR3 <br> Z1A <br> Z1B <br> ZlC | SCR Gate Drive Assembly Includes <br> Capacitor, Fxd, Ceramic $0.1 \mu \mathrm{~F}$, Plus $80 \%$ Minus 20\%, 25 VDCW -C1 Thru C3- <br> Connector, Electrical -Jl Thru J3- <br> Transformer -Tl Thru T3- <br> Terminal Board -TB1- <br> Terminal Board -TB2- <br> Card, Gate Drive <br> -Al Thru A3- <br> Relay <br> Relay Socket <br> Absorbor, Overvoltage <br> Same as CRI <br> Same as CRI <br> SCR Assembly <br> Same as 2lA <br> Same as ZlA | $\begin{aligned} & 627-5140-001 \\ & 913-3806-000 \\ & 372-5906-010 \\ & 270-0313-020 \\ & 367-0024-000 \\ & 367-0013-000 \\ & 270-0313-030 \\ & 974-0076-020 \\ & 220-1543-000 \\ & 353-0283-100 \\ & 353-6551-010 \end{aligned}$ |



Figure 6-10. Gate Drive Card, A9AR1A1-A3
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| GATE DRIVE CARD, A9ARIA1-A3 |  | 270-0313-030 |
| C1 | Capacitor, Fxd, Metallized Mylar $1.0 \mu \mathrm{~F}, 5 \%$ Tol, 200 VDC | 933-0258-250 |
| C2 | Capacitor, Fxd, Metallized Mylar $2.0 \mu \mathrm{~F}, 5 \%$ Tol, 200 VDC | 933-0258-290 |
| C3 | Capacitor, Fxd, Metallized Mylar $0.22 \mu \mathrm{~F}, 5 \% \mathrm{TO}, 200$ VDC | 933-0258-170 |
| C4 | Same as C3 |  |
| C5 | Capacitor, Fxd, Electrolytic <br> $10.0 \mu \mathrm{~F}$, Minus $10 \%$ Plus $75 \%$, 50 V | 183-1179-000 |
| C6 | Same as C5 |  |
| C7 | Capacitor, Fxd, Electrolytic <br> $2.7 \mu \mathrm{~F}, 10 \%$ Tol, 35 VDCW | 184-7690-000 |
| C8 | Same as C7 |  |
| C9 | Capacitor, Fxd, Electrolytic $220 \mu \mathrm{~F}$, Minus $10 \%$ Plus $75 \%$, 50 VDCW | 184-5102-030 |
| C10 | Same as C9 |  |
| D1 | Diode, IN4003 | 353-6442-030 |
| D2-D16 | Same as D1 |  |
| L1 | Reactor, Saturable | *C1-9028-315A |
| Q1 | Transistor, 2N2219A | 352-0661-010 |
| R1 | Resistor, Fxd, Metal Film $1000 \mathrm{hm}, 1 \%$ Tol, $1 / 2$ Watt | 705-7048-000 |
| R2 | Resistor, Fxd, Metal Film 2.21 Kilohm, 1\% Tol, 1/2 Watt | 705-7264-000 |
| R3 | Same as R2 |  |
| R4 | Resistor, Fxd, Carbon Film 3.3 Kilohm, 10\% Tol, 1/2 Watt | 745-0914-770 |
| R5 | Same as R4 |  |
| R6 | Resistor, Fxd, Composition 100 Ohm, 10\% Tol, 1 Watt | 745-3310-000 |
| R7 | Same as R6 |  |
| R8 | Resistor, Fxd, Composition 4.7 Ohm, 5\% Tol, 1 Watt | 745-3542-000 |
| R9 R10 | Same as R8 Resistor, Fxd, Wirewound | 747-8051-000 |
| R10 | 35 Ohm, 5\% Tol, 14 Watt | 747-8051-000 |
| R11 | Same as R10 |  |
| R12 | Resistor, Fxd, Composition 5.6 Kilohm, $10 \%$ Tol, $1 / 2$ Watt | 745-1384-000 |
| R13 | Same as R12 |  |
| R14 | Resistor, Fxd, Composition 120 Ohm, 5\% Tol, 1/2 Watt | 745-1314-000 |
| R15 | Resistor, Fxd, Metal Film 100 Kilohms, $1 \%$ Tol, $1 / 2$ Watt | 705-7192-000 |
| SCR1 | Silicon Controlled Rectifier 2N2323A | 353-3540-010 |
| SCR2 T1 | Same as SCRI Not Used |  |
| T2 | Transformer | *A31-9010-4 |
|  |  | *Vendor Part Number |



Figure 6-11. 2-kV Power Supply, A10.
parts list



Figure 6-12. RF Driver Assembly, All (Sheet 1 of 2).

WARNING: DISCONNECT PRIMARY POWER SOURCE BEFORE SERVICING.


Figure 6-12. RF Driver Assembly, All (Sheet 2 of 2).

parts list

| REF DES | DESCRIPTION | $\begin{aligned} & \text { CEMC } \\ & \text { PART NUMBER } \end{aligned}$ |
| :---: | :---: | :---: |
| R38 | Resistor, Fxd, Wirewound 5 Ohms, 1\% Tol, 2.5 Watts | 746-9447-000 |
| R39 | Resistor, Fxd, Wirewound 1 Ohm, $1 \%$ Tol, 36 Watts | 710-5076-010 |
| R40 | Resistor, Var, Wirewound, 500 Ohms, 10\% Tol, 50 Watts | 735-1013-410 |
| R41 | Not Used |  |
| R42 | Not Used |  |
| R43 | Not Used |  |
| R44 | Same as R40 |  |
| R45 | Same as R39 |  |
| R46 |  |  |
| Through $R 49$ | Not Used |  |
| R50 | Resistor, Fxd, Wirewound 820 Ohms, 5\% Tol, 11 Watts | 746-6158-000 |
| R51 | Resistor, Fxd, Wirewound 160 Ohms, 5\% Tol, 10 Watts | 710-2921-000 |
| R52 | Not Used |  |
| R53 | Resistor, Fxd, Composition 47 Ohms, 10\% Tol, 1 Watt | 745-3296-000 |
| R54 R55 | Same as R53 <br> Not used |  |
| R56 | Not Used |  |
| R57 | Resistor, Fxd, Composition, 50 Ohms, 10\% Tol, 16.5 Watts | 712-0129-000 |
| R58 |  |  |
| Through R60 | Not Used |  |
| R61 | Same as R51 |  |
| Tl |  |  |
| $\begin{aligned} & \text { Thr } \\ & \text { T5 } \end{aligned}$ | Not Used |  |
| T6 | Transformer, Pwr, Step-Down | 662-0394-010 |
| V1 | Electron Tube, 4CX250B | 256=0121-000 |
| V2 | Same as V1 |  |
| VR2 | Semiconductor Device, Set | 353-6015-000 |
| XV1 | Socket, Electron Tube 8 Pins | 220-1294-000 |
| XV2 | Same as XV1 |  |
| 1 | Rod, Extension -Qty 2- | 786-3312-001 |
| 2 | $\begin{aligned} & \text { Chimney, Air Socket } \\ & \text {-Qty 2- } \end{aligned}$ | 220-1466-000 |
| 3 | Knob, Plastic -Qty 2- | 281-0122-000 |



Figure 6-13. Latching Relay and Status Board, A12.
parts list



Figure 6-14. RF Output Low-Pass Filter, Al3.
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| RF OUTPUT LOW-PASS FILTER, A13 786-3451-001 |  |  |
| $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 4 \\ & 5 \\ & 6 \\ & 7 \\ & 7 \\ & 8 \\ & 9 \\ & 10 \end{aligned}$ | Coil Assy <br> Coil Assy <br> Coil Assy <br> Capacitor <br> Capacitor <br> Capacitor <br> Capacitor <br> Capacitor <br> Capacitor, Rod <br> Insulator, Disc | $\begin{aligned} & 786-3367-001 \\ & 786-3369-001 \\ & 786-3371-001 \\ & 786-3372-001 \\ & 786-3373-001 \\ & 786-3374-001 \\ & 786-3375-001 \\ & 786-3448-001 \\ & 786-3435-001 \\ & 786-3469-001 \end{aligned}$ |
| - | . | \% |



Figure 6-15. Power Supply Filter, Al4 (Sheet 1 of 2).


BOTTOM VIEW

Figure 6-15. Power Supply Filter, Al4 (Sheet 2 of 2).

| REF DES | DESCRIPTION | CEMC PART NUMBER |
| :---: | :---: | :---: |
|  | POWER SUPPLY FILTER, Al4 | 786-3583-001 |
| $\begin{aligned} & \mathrm{C} 1 \\ & \mathrm{C} 2 \end{aligned}$ | Not Used <br> Capacitor, Fxd, Paper, $0.03 \mu \mathrm{~F}$ 10\% Tol, 15,000 VDCW | 930-0614.000 |
| C3 | Not Used , |  |
| C4 | Capacitor, Fxd, Paper, $10 \mu \mathrm{~F}$, 10\% Tol, 2500 VDCW | 962-4204-000 |
| C5 | ```Capacitor, Fxd, Ceramic, 0.01 \muF, 20% Tol, 500 VDCW``` | 913-1188-000 |
| C6 | Capacitor, Fxd, Mica, $0.022 \mu \mathrm{~F}$, $2 \%$ Tol, 2000 VDCW | 938-2129-000 |
| C7 | Capacitor, Fxd, Paper, $12 \mu \mathrm{~F}$, 10\% Tol, 1500 VDCW | 962-4246-000 |
| C8 | Same as C7 |  |
| C9 | Not Used |  |
| C10 R1 | Same as C4 |  |
| Through | Not Used |  |
| R4 | Resistor, Fxd, Wirewound 330 Ohms, 5\% Tol, 26 Watts | 747-1790-000 |
| R6 | Not Used |  |
| R7 | Not Used |  |
| R8 | Not Used Fxd Wirewound, 0.250 hms |  |
| R9 | Resistor, Fxd, Wirewound, 0.25 Ohms, 1\% Tol, 10 Watts | 747-9451-000 |
| R10 | Resistor, Fxd, Wirewound, 4 Ohms, 10\% Tol. 100 Watts | 710-5076-060 |
| R11 | Resistor, Fxd, Composition, 1200 Ohms 5\% Tol, 1 Watt | 745-3355-000 |
| R12 | Resistor, Fxd, Composition, 3600 Ohms 5\% Tol, 1 Watt | 745-3375-000 |
| R13 | Same as R11 |  |
| R14 | ```Resistor, Fxd, Wirewound, 0.5 Ohms, 1% Tol, 36 Watts``` | 710-5076-030 |
| R15, R15A | Same as R10 |  |
| R16 | Resistor, Fxd, Wirewound, $10 h m$, 1\% Tol, 36 Watts | 710-5076-010 |
| $\mathrm{R17}$ | Not Used |  |
| R18 | Not Used |  |
| R19 | Not Used |  |
| R20 | Resistor, Fxd, Film <br> 200 Kilohms, $1 \%$ Tol, 2 Watts | 705-1493-050 |
| R21 | Same as R20 |  |
| R22 R23 | Same as R20 Same as R20 |  |

parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| R24 | Resistor, Fxd Composition, 47 Kilohms, 10\% Tol, 1 Watt | 745-3422-00 |
| R25 | Not Used |  |
| R26 | Not Used |  |
| R27 | Not Used |  |
| R28 | Resistor, Fxd, Film, 1.0 Megohm 1\% Tol, 2 Watts | 705-4254-000 |
| R29 | Same as R28 |  |
| R20 | Same as R28 |  |
| R31 | Same as R28 |  |
| R32 | Same as. R24 |  |
| R33 |  |  |
| Through | Not Used |  |
| R69 | Resistor, Fxd, Wirewound 310 Ohms, 5\% Tol, 14 Watts | 747-0754-000 |
| TB1 |  |  |
| Through | Not Used |  |
| TB6 |  | 786-3126-001 |
| VR1 | Not Used | 786-3126-001 |
| VR2 | Not Used |  |
| VR3 | Diode | 353-3121-000 |
| VR4 | Same as VR3 |  |
| Z1 | Not Used |  |
| Z2 | Rectifier | 353-0434-010 |
|  |  |  |
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Figure 6-16. Metering Multiplier Board, Al5

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
|  | METERING MULTIPLIER BOARD, Al5(A) | 643-7445-001 |
| Cl | Capacitor, Fxd, Ceramic, 0.CluF 20\% Tol, 500 VDCW | 913-1188-000 |
| C2 | Same as Cl |  |
| Rl | Resistor, Fxd, Film, 750 Kilohms, 1\% Tol, 2 Watts | 705-1493-020 |
| Through | Same as Rl |  |
| R25, R26 | Not Used |  |
| R27 | Resistor, Fxd, Composition, 180 kilohms 10\% Tol, 2 Watt | 745-5746-000 |
| R28 | Not Used |  |
| R29 | Resistor, Fxd, Film, 5110 Ohms, 1\% Tol, l/2 Watt | 705-7130-000 |
| R30, R31 | Resistor, Fxd, Film, l.0 Megohm, 1\% Tol, 2 Watts | 705-4254-000 |
| $\begin{aligned} & \text { VR1, VR3 } \\ & \text { VR2 } \end{aligned}$ | Diode <br> Not Used | 353-1339-000 |
| REMOTE | METERING MULTIPLIER BOARD, Al5 (B) | 643-7446-001 |
| Cl | Capacitor, Fxd, Ceramic, $0.01 \mu \mathrm{~F}$ 20\% Tol, 500 VDCW | 913-1188-000 |
| C2 | Same as Cl |  |
| Rl | Resistor, Fxd, Carbon, 180 Kilohms, | 745-5746-000 |
| Through | 5\% Tol, 2 Watts |  |
| R24 |  |  |
| R25, R26 | Not Used |  |
| R27 | Resistor, Fxd, Composition, 1800 ohms 10\% Tol, 2 Watt | 745-5662-000 |
| R28 |  |  |
| Through |  |  |
| R31 | Not Used |  |
| R32 | Resistor, Fxd, Composition, lok ohms, 1W | 745-3393-000 |
| VR1 | Zener Diode, 100V | 353-1339-000 |
| VR2 | Not Used |  |
| VR3 | 7ener, Diode, 6.8V | 745-3393-000 |



Figure 6-17. Directional Coupler, A16.
parts list



## REAR

Figure 6-18. Bleeder Resistor Panel, Al7.
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
|  | BLEEDER RESISTOR PANEL, A17 | 786-3154-002 |
| El | Not Used |  |
| E2 | Arrestor, Lightning | 013-1332-020 |
| R1 | Not Used |  |
| R2 | Resistor, Fxd, Film, 400 Kilohms, $1 \%$ Tol, 2 Watts | 705-1457-210 |
| R3 | Resistor, Fxd, Composition, 47 Kilohms, 10\% Tol, 1 Watt | 745-3422-000 |
| R4 | Resistor, Fxd, Wirewound, 330 Ohms, 5\% Tol, 26 Watts | 747-1790-000 |
| R5 | Not Used |  |
| R6 | Resistor Fxd, Wirewound 18 Ohms, 5\% Tol, 210 Watts | 746-6662-000 |
| R7 | Resistor, Fxd, Wirewound, 100 Kilohms, $5 \%$ Tol, 210 Watts | 746-6737-000 |
| R8 | Same as R7 |  |
| R9 |  |  |
| Through R17 | Not Used |  |
| R18 | Resistor, Fxd, Wirewound 5.1 Kilohms, 5\% Tol, 210 Watts | 746-6817-000 |
| R19 |  |  |
| Through R24 | Not Used |  |
| R25 | Resistor, Fxd, Wirewound, 20 Kilohms, 10\% Tol, 10 Watts | 710-9067-000 |
| R26 | Not Used |  |
| R27 | Resistor, Fxd, Wirewound, 82 Kilohms, 5\% Tol, 113 Watts. | 747-3834-000 |
| R28 |  |  |
| Through R32 | Not Used |  |
| R33 | Resistor, Fxd, Wirewound 10 Ohms; $1 \%$ Tol, 26 Watts | 747-1646-000 |
| R34 | Resistor, Fxd, Wirewound, 20 Kilohms, 5\% Tol, 210 Watts | 746-6723-000 |
| TB1 | Not Used |  |
| TB2 | Board, Terminal 18 Terminals | 367-4180-000 |
| TB3 | Board, Terminal 3 Terminals | 367-1188-000 |
| TB4 | Board, Terminal | 367-4180-000 |
| $\cdots$ | 18 Terminals -Qty 2- |  |
| XE1 XE2 | Not Used |  |
| XE2 | Arrestor, Lightning, Mtg | 013-1332-010 |


| REF DES | DESCRIPTION | CEMC |
| :---: | :---: | :---: |
| 1 | Standoff, Insulator <br> -Qty 12- <br> Standoff, Insulator <br> -Qty 2- <br> Plexiglass Cover | $190-0025-000$ |
| 3 |  | $190-1145-000$ |



Figure 6-19. Power Amplifier Cavity, Al8 (Sheet 1 of 3).


REAR VIEW

Figure 6-19. Power Amplifier Cavity, Al8 (Sheet 2 of 3).


Figure 6-19. Power Amplifier Cavity, Al8 (Sheet 3 of 3).

WARNING: DISCONNECT PRIMARY POWER SOURCE BEFORE SERVICING.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| POWER AMPLIFIER CAVITY, Al8 |  | 786-3335-003 |
| B1 | Not Used |  |
| B2 | Motor, $A C$ 115 VAC | 230-0581-010 |
| B3 | Same as B2 |  |
| C1 |  |  |
| Through | Not Used |  |
| C30 C31 | Capacitor, Fxd, Ceramic, 1000 pF 20\% Tol, 4000 VDCW | 913-3120-020 |
| C32 | Same as C31 |  |
| C33 |  |  |
| Through c 39 | Not Used |  |
| C40 | Capacitor, Fxd, Ceramic $310 \mathrm{pF}, 5 \%$ Tol, 2500 VDCW | 913-0845-000 |
| C41 | Capacitor, Fxd, Paper $0.47 \mu \mathrm{~F}, 20 \%$ Tol, 400 VDCW | 913-6849-000 |
| C42 | Same as C41 |  |
| C43 | Not Used |  |
| C44 | Not Used |  |
| C45 | Not Used |  |
| C46 | Capacitor, Fxd, Paper $10 \mu \mathrm{~F}, 10 \%$ Tol, 1 KVDCW | 930-0038-000 |
| C47 | Not Used |  |
| C48 | Capacitor, Fxd, Ceramic 500 pF, Plus 50\% Minus $20 \%, 20,000$ VDCW | 913-1101-000 |
| C49 | Same as C 48 |  |
| C50 | Not Used |  |
| C51 | Not Used |  |
| C52 | $\begin{aligned} & \text { Capacitor, Fxd, Ceramic } \\ & 100 \mathrm{pF}, 10 \% \text { Tol, } \\ & 15,000 \text { VDCW } \end{aligned}$ | 913-5113-050 |
| C53 | Not Used |  |
| C54 | Capacitor, Fxd, Ceramic 1000 pF, 20\% Tol, 2000 VDCW | 913-4843-000 |
| C55 | Capacitor, Fxd, Paper <br> $0.1 \mu \mathrm{~F}, 10 \%$ Tol, 600 VDCW | 214-0090-000 |
| $C 56$ $C 57$ | Same as C55 |  |
| Through C80 | Not Used |  |
| C81 | Capacitor, Fxd, Ceramic <br> $1000 \mathrm{pF}, 20 \%$ Tol, 5000 VDCW | 913-0101-000 |
| C82 | Capacitor, Fxd, Ceramic <br> $1000 \mathrm{pF}, 20 \%$ Tol, 500 VDC | 913-4064-000 |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| C83 | Same as C 82 |  |
| C84 | Same as C82 |  |
| C85 | Same as C82 |  |
| C86 | Capacitor, Fxd, Ceramic $0.1 \mu \mathrm{~F}$, Plus $80 \%$ Minus | 913-3152-000 |
|  | 20\%, 500 VDCW |  |
| C87 |  |  |
| Through | Same as C86 |  |
| C91 |  |  |
| C92 | Same as C82 |  |
| C93 | Same as C82 |  |
| $J 1$ | Not Used |  |
| J2 | Connector, Electrical 1 Contact | 357-9248-010 |
| J3 | Not Used |  |
| J4 | Connector, Electrical 1 Contact | 357-9670-000 |
| J5 | Same as $\mathrm{J4}$ |  |
| J6 | Same as J 2 |  |
| L1 |  |  |
| Through | Not Used |  |
| L5 |  |  |
| L6 | Choke, RF | 786-3548-001 |
| Lh 7 rough | Not Used |  |
| L71 | Not Used |  |
| L12 | Inductive Coupling Loop, 1" \#20 Buss | 421-2020-000 |
| L13 | Same as L12 |  |
| L14 | Choke, RF | 786-3673-001 |
| L15 | Choke, Static Drain | 640-3527-00 |
| P1 | Not Used |  |
| P2 | Not Used |  |
| P3 | Not Used |  |
| P4 | Connector, Electrical 1 Contact | 357-9292-000 |
| P5 | Same as P4 |  |
| R1 |  |  |
| Through | Not Used |  |
| R54 | Resistor, Fxd, Composition |  |
| R55 | Resistor, Fxd, Composition 22 Ohms, 10\% Tol, 2 Watts | 745-5582-000 |
| R56 | Not Used |  |
| R57 | Not Used |  |
| R58 | Resistor, Fxd, Composition 22 Ohms, 20\% Tol, 15 Watts | 712-0002-000 |
| R59 |  |  |
| Through R74 | Not Used |  |
| R75 | Resistor, Fxd, Composition 50 Ohms, $20 \%$ Tol, 60 Watts | 712-0070-000 |
| R80 | Resistor, Fxd, Wirewound 1.0 Kilohm, 5\% Tol, 26 Watts | 747-1686-000 |

WARNING: DISCONNECT PRIMARY POWER SOURCE BEFORE SERVICING.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| S1 | Switch, Pressure SPDT Contact Arrangement | 266-8384-090 |
| S2 | Switch, Sensitive SPDT Contact Arrangement Includes | 260-0025-000 |
| S3 | Actuator Same as S2 | 260-0026-000 |
| S4 | Not Used |  |
| S5 | Not Used |  |
| S6 | Shorting Switch Includes | 627-9743-004 |
|  | Spring, Shorting Switch | 540-5342-002 |
|  | Strap, Grounding | 304-6000-000 |
|  | Contact, Shorting | 542-1773-002 |
|  | Shaft, Flat, Straight | 627-9786-001 |
|  | Insulator, Standoff | 190-0026-000 |
| S7 | Same as S6 |  |
| S8 | Not Used |  |
| 59 | Not Used |  |
| S10 | Not Used |  |
| S11 | Switch, Sensitive <br> . SPDT Contact Arrangement | 266-3081-000 |
| S12 | Same as S11 |  |
| S13 | Same as S11 |  |
| S14 | Same as S11 |  |
| S15 | Switch, Thermostatic | 267-0243-100 |
| 1 | Conductor, Center, Cavity | 786-3124-001 |
| 2 | Duct, Blower | 786-3026-001 |
| 3 | Shield, RF | 786-3095-001 |
| 4 | Ceramic Post -Qty 2- | 190-1149-000 |
| 5 | Clamp ${ }_{\text {-Oty }}$ | 516-6730-001 |
| 6 | Tube Clip | 265-9020-000 |



Figure 6-20. Component Pane1, A19.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| COMPONENT PANEL, A19 |  | 648-8124-001 |
| A1 | Power Failure Recycle Board <br> See breakdown on page 6-65 | 640-3466-001 |
| A2 | Variac Drive Assembly <br> See breakdown on page 6-67 | 648-8104-001 |
| CR1 | Diode, IN645 | 353-2607-000 |
| CR2 | Same as CR1 |  |
| CR3 | Diode, IN5550 | 353-3718-040 |
| CR4 | Same as CR1 |  |
| CR5 CR6 | Same as CRI Not Used |  |
| CR7 | Not Used |  |
| CR8 | Not Used |  |
| CR9 | Same as CR1 |  |
| CR10 | Not Used |  |
| CR11 | Not Used |  |
| CR12 | Same as CR1 |  |
| K1 | Relay, Contactor, 28 V Coil <br> 3A 40 Amp Contacts <br> 1B 10 Amp Contact <br> - 1C 10 Amp Contact | 401-1607-000 |
| K2 | Relay, Contactor, 28 V Coil 5A 10 Amp Contacts <br> 1C 10 Amp Contact | 401-1614-000 |
| K3 | Relay, 24 VDC Coil 3C Low Level Contacts | 970-0007-180 |
| K4 | Relay, Time Delay, 30 sec . 24 V Coil, 2 C 10 Amp Contacts | 402-0489-190 |
| K5 | Relay, Phase Monitor 190-270V, SPDT 10A Contacts | 403-0038-010 |
| K6 |  |  |
| Through Kl1 | Not Used |  |
| K12 | Same as K3 |  |
| K13 | Same as K3 |  |
| R1 ${ }_{\text {Through }}$ | Not Used |  |
| R40 |  |  |
| R41 | Resistor, Fxd, Composition 820 Ohms, 10\% Tol, 2 Watt | 745-5649-000 |
| R42 | Same as R41 |  |
| Through | Not Used |  |
| R73 |  |  |
| R74 | Resistor, Fxd, Wirewound $0.5 \mathrm{Mm}, 10 \%$ Tol, 100 Watts | 710-5076-050 |
| XKI | Not Used |  |
| XK2 XK3 | Not Used Relay Socket | 220-0010-010 |
| XK3 | Relay Socket | 220-0010-010 |

WARNING: DISCONNECT PRIMARY POWER SOURCE BEFORE SERVICING.
parts list

| REF DES |  | DESCRIPTION |
| :--- | :--- | :--- |
| XK4 <br> XK5 <br> XK6 <br> Through <br> XK11 <br> XK12 <br> XK13 | Same as XK3 <br> Relay Socket, Octal <br> Not Used <br> Same as XK3 <br> Same as XK3 |  |

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Figure 6-21. Power Failure Recycle Board, A19A1
parts list

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| POWER FAILURE RECYCLE BOARD, A19A1 |  | 640-3466-001 |
| Cl | Capacitor, Fxd, Electrolytic $68 \mathrm{\mu F}, 20 \%$ Tol, 40 VDCW | 184-6330-360 |
| C2 | Capacitor, Fxd, Electrolytic $100 \mu \mathrm{~F}$, Minus 10\% Plus 75\%, 50 VDC | 183-1281-080 |
| C3 | Capacitor, Fxd, Electrolytic <br> $5500 \mu \mathrm{~F}$, Plus 100\% Minus 10\%, 40 VDCW | 183-1278-180 |
| CR1 | Diode, IN4003 | 353-6442-030 |
| Through CR6 | Same as CR1 |  |
| Kl | Relay, 24 V Coil 4C 3 Amp Contacts | 970-0002-030 |
| K2 | Same as Kl |  |
| Q1 | Transistor, MJE-243 | 352-1104-010 |
| Q2 | Same as Q1 |  |
| R1 | Resistor, Fxd, Carbon Film 220 Ohms, 5\% Tol, $1 / 2$ Watt | 745-0914-490 |
| R2 | Resistor, Fxd, Carbon Film 100 Kilohms, 5\% Tol, $1 / 2$ Watt | 745-0915-140 |
| R3 | Resistor, Fxd, Carbon Film 2.2 Kilohms, 5\% Tol, 1/2 Watt | 745-0914-730 |
| R4 | Same as R3 |  |
| R5 | Same as R3 |  |
| R6 | Resistor, Fxd, Carbon Film 10 Kilohms, $5 \%$ Tol, l/2 Watt | 745-0914-890 |
| R7 R8 | Same as R3 <br> Same as R3 |  |
| VR1 | Diode, IN4735,6.2V, 1W Zener | 353-6481-160 |
| VR2 | Diode, IN5646A, 36V, 1W Zener | 353-0221-360 |
| VR3 | Same as VR2 |  |
| XK1 XK2 | Relay Socket | 220-1582-010 |
| XK2 | Same as XK1 |  |



Figure 6-22. Variable Transformer Drive Assembly, A19A2.
parts list



Figure 6-23. Card Cage Assembly, A20.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| CARD CAGE ASSEMBLY, A20 |  | 786-3301-002 |
| B1 |  |  |
| Through | Not Used |  |
| B4 |  |  |
| B5 | Motor, Reversible, 115 VAC | 230-0641-010 |
| Cl | Capacitor, Fxd, Electrolytic <br> $100 \mu \mathrm{~F}$, Minus $10 \%$ Plus $75 \%$, 50 VDC | 183-1281-080 |
| C2 |  |  |
| Through Cl00 | Not Used |  |
| C101 | Capacitor, Fxd, Ceramic <br> $0.01 \mu \mathrm{~F}, 20 \%$ Tol, 500 VDCW | 913-1188-000 |
| C102 | Capacitor, Fxd, Paper $0.33 \mu \mathrm{~F}, 20 \% \mathrm{Tol}, 600$ VDCW | 951-1066-000 |
| C103 | Capacitor, Fxd, Electrolytic $100 \mu \mathrm{~F}$, Minus 10\% Plus 75\% 50 VDC | 183-1281-080 |
| CR1 | Diode, IN4003 | 353-6442-030 |
| CR2 | Same as CR1 |  |
| Through | Not Used |  |
| R18 |  |  |
| R19 | Resistor, Fxd, Composition 100 Ohms, $10 \%$ Tol, 1 Watt | 745-3310-000 |
| R20 |  |  |
| Through | Not Used |  |
| R43 | Resistor, Var, Wirewound, 10 Turn 5K Ohms, 3\% Tol, 2 Watts | 381-1648-020 |
| R44 |  |  |
| $\begin{aligned} & \text { Through } \\ & \text { R58 } \end{aligned}$ | Not Used |  |
| R59 | Resistor, Fxd, Composition 820 Ohms, $10 \%$ Tol, $1 / 2$ Watt | 745-1349-000 |
| R82 | Resistor, Fxd, Carbon Film 1800 Ohms, $5 \%$ Tol, $1 / 2$ Watt | 745-0914-710 |
| R83 S1 | Same as R82 |  |
| Through S9 | Not Used |  |
| S10 | Switch, Rotary DPDT Contact Arrangement | 259-2694-010 |
|  |  |  |
| Through S14 | Not Used |  |
| S15 | Switch, Interlock SPDT Contact Arrangement | 266-8000-000 |
| Through T7 | Not Used |  |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| T8 | ```Transformer, Pwr, Single Phase 50/60 Hz 166 VRMS Pri, 24 V RMS Sec (1) 56V RMS C.T.Sec (2)``` | 662-0898-010 |
| XA1 | Not Used |  |
| $X A 2$ $\times A 2 A$ | Connector, Consists of XA2A and XA2B |  |
| XA2A | ```Connector, Electrical 4 \text { Contacts} -Qty 10-``` | 372-2426-010 |
| XA2B | Connector, Electrical <br> 4 Contacts <br> -Qty 5- | 372-2426-010 |
| XA3 | Connector, Electrical <br> 4 Contacts <br> -Qty 11- | 372-2426-010 |
| XA4 | Not Used |  |
| XA5 | Same as XA3 |  |
| XA6 | Not Used |  |
| XA7 | Same as XA2A |  |
| XA8 | Same as XA2B |  |
| XA9 | Not Used |  |
| XA10 | Not Used |  |
| XA11 | Not Used |  |
| XA12 | Connector, Electrical 4 Contacts | 372-2426-010 |
| 1 | -Qty 13- Knob, Aluminum | 757-0233-003 |
| 2 | Plastic Fastener For Cover | 769-0532-003 |
| 3 | Pins for Cover | 311-0438-000 |



Figure 6-24. Power Amplifier Socket, A21.

parts list



Figure 6-25. Overload and Meter Calibrate Panel, A22.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
|  | OVERLOAD AND METER CALIBRATE PANEL, A22 | 786-3666-001 |
| C1 |  |  |
| Through | Not Used |  |
| C12 |  | 913-1186-000 |
| C12 | Capacitor, Fxd, Ceramic <br> $1000 \mathrm{pF}, 20 \% \mathrm{Tol}$, | 913-1186-000 |
|  | 1000 VDCW |  |
| C13 | Same as Cl 2 |  |
| C14 |  |  |
| Through | Not Used |  |
| C86 |  |  |
| C87 | Capacitor, Fxd, Ceramic <br> 0.1 uF, Plus $80 \%$ Minus 20\%, 200 VDCW | 913-3681-000 |
| C88 | Same as C87 |  |
| K1 |  |  |
| Through | Not Used |  |
|  |  |  |
| K6 | Relay, Armature IC Contact Arrangement | 408-1114-000 |
| K7 | Same as K6 |  |
| K8 | Same as K6 |  |
| K9 | Same as K6 |  |
| R1 | Resistor, Fxd, Composition 1000 Ohms, $10 \%$ Tol, $1 / 2$ Watt | 745-1352-000 |
| R2 |  |  |
| Through | Not Used |  |
| R59 |  |  |
| R60 | Resistor, Var, Wirewound 50 Ohms, 10\% Tol, 2 Watts | 377-0619-000 |
| R61 | Not Used |  |
| R62 | Resistor, Fxd, Wirewound 150 Ohms, 5\% Tol, 1 Watt | 746-6145-000 |
| R63 | Not Used |  |
| R64 | Resistor, Var, Wirewound 100 Ohms, $10 \%$ Tol, 12.5 Watts | 749-4512-000 |
| R65 | Same as R60 |  |
| R66 | Same as R60 |  |
| R67 | Not Used |  |
| R68 | Not Used |  |
| R69 | Not Used |  |
| R70 | Resistor, Fxd, Wirewound 60.4 Ohms, $1 \%$ Tol, 30 Watts | 747-0990-730 |
| R71 | Same as R70 |  |
| R72 | Resistor, Var, Wirewound 40 Ohms, 10\% Tol, 4 Watts | 377-0033-000 |
| R73 | Sames as R72 |  |


| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| TB] |  |  |
| Through | Not Used |  |
| TB7 |  |  |
| TB8 | Board, Terminal <br> 14 Terminals | 367-4140-000 |
| VR1 |  |  |
| Through | Not Used |  |
| VR6 |  |  |
| VR7 | Diode | 353-6230-000 |
| VR8 | Same as VR7 |  |
| Z1 | Not Used |  |
| 22 | Not Used |  |
| 23 | Not Used |  |
| 24 | Magnetic Circuit, Halltron | 270-0080-020 |
| Z5 | Same as $\mathrm{Z4}$ |  |

Z5 Same as $Z 4$


Figure 6-26. AC Metering Panel A25

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| * | AC METERING PANEL, A25 | $636-7263$-003 |
| A1 CB1 | Resistor Board Assy <br> See breakdown on page 6-80 <br> Circuit Breaker, 150 Amps, 3 Pole (OBSOLETE) <br> Circuit Breaker, 150 Amps, 3 Pole <br> (Requires new A25 Panel for replacing 260-4055-020) | $260-4055-020$ |
| M1 | Meter, Iron Vane <br> 1OmA. Movement, 2\% Accuracy <br> S1 | Switch, Rotary, Wafer, 2 Sections <br> 2 Pole, 5 Position |



Figure 6-27. Resistor Board Assembly, A25A1



Figure 6-28. 28-Volt Power Supply, PSI.



Figure 6-29. PA Bias Power Supply, PS2.

| REF DES | DESCRIPTION | CEMC <br> PART NUMBER |
| :---: | :---: | :---: |
| PA BIAS POWER SUPPLY, PS2 |  | 786-3081-001 |
| Cl | Capacitor, Fxd, Paper $0.047 \mu \mathrm{~F}, 20 \% \mathrm{Tol}$, 600 VDCW | 931-8592-000 |
| $\mathrm{C} 2$ | Capacitor, Fxd, Paper $10 \mu \mathrm{~F}$, $10 \% \mathrm{Tol}$, 1000 VDCW | 930-0038-000 |
| $\begin{aligned} & \text { CR1 } \\ & \text { CR2 } \end{aligned}$ | Diode, IN4586 | 353-6467-050 |
| Through CR5 | Same as CR1 |  |
| Ll | Reactor <br> 5H Inductance | 678-0584-000 |
| RI | Resistor, Fxd, Composition 330 Ohms, $10 \%$ Tol, 1 Watt | 745-3331-000 |
| R2 | Resistor, Fxd, Wirewound 10 Kilohms, $5 \%$ Tol, 14 Watts | 746-9131-000 |
| R3 | Resistor, Fxd, Film 1000 Ohms, $1 \%$ Tol, 2 Watts | 705-4254-000 |
| R4 | Resistor, Var, Composition 2500 Ohms, $10 \%$ Tol, 2 Watts | 380-2768-000 |
| $\begin{aligned} & \text { T1 } \\ & \text { TB1 } \end{aligned}$ | Transformer, Pwr, Step-Up Board, Terminal <br> 6 Terminals | $\begin{aligned} & 662-0218-010 \\ & 367-4060-000 \end{aligned}$ |
| TB2 | Terminal Board | 786-3139-001 |

Overall schematic diagram for the FM Transmitter, 816R, is contained in the pocket attached within the back cover of this instruction manual.

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# EXTENDING TRANSMITTERTUBE LIFE <br> By Robert Artigo 

> A carefully followed program of filament voltage management can substantially increase the life expectancy of transmitter power grid tubes. Whith today's rising operating costs, such a program makes good financial sense.

IN RECENT YEARS station managers have seen a substantial increase in replacement costs for power grid tubes. The blame can be placed on higher manufacturing costs due to inflation, volatile precious metal prices, and an uncertain supply of some exotic metals. The current outlook for the future holds little promise for a reversal in this trend toward higher prices.

One way to offset higher operating costs is to prolong tube life. For years station engineers have used various tricks to get longer operating life, with greater and lesser degrees of success. Success can be maximized, however, by understanding the various

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## Extending Transmitter Tuhe Life

factors that affect tube life and implementing a program of filament voltage management.

A number of factors can aid maximum tube life in your transmitter. For example, are the maximum ratings given on the tube manufacturer's data sheet being exceeded? Data sheets are available upon request from most companies. Most tube manufacturers have an application engineering department to assist in evaluating tube performance for a given application. Make use of these services!

## Headroom

Is the final power tube of the transmitter capable of delivering power in excess of the desired operating level? Or is the demand for performance so great that minimum output power levels can only be met at rated nominal filament voltage?

Figure 1 can be used as a basic guide to determine if a given transmitter and tube combination has a good probability of giving extended life service. Extended life service is defined as useful operating life beyond that normally achieved by operating at rated nominal filament voltage. The amperes/watt ratio is obtained by dividing average plate current by the product of filament voltage and filament current. If the amperes/ watt ratio falls in the "good" to "excellent" range, excess emission is sufficient to permit filament voltage derating. At a lower filament voltage, the filament temperature is lowered, thus extending life. A typical FM transmitter on the market today may have an amperes/watt filament ratio of 0.002 to 0.003 . This equipment would be considered an excellent choice to achieve extended tube life. On the other hand, if the amperes/watt ratio falls in the "poor"' range, it is unlikely that filament derating is possible due to limited
emission. Note that this guideline should be used for thoriated tungsten emitters only, and does not apply to oxide cathode-type tubes.

## Instrumentation

Are all tube elements metered in the transmitter? Elements should be metered for both voltage and current, and meters should be redlined to define operation within safe limits. More modern transmitters may incorporate a microprocessor-controlled circuit to monitor all pertinent parameters.

In addition, the following controls are necessary if an effective filament voltage management program is to be undertaken: power output metering for an FM transmitter or a distortion level meter for AM equipment; accurate filament voltage metering (an iron-vane instrument is preferred over the more common average responding RMS calibrated type; the filament voltage measurement must be made at the tube socket terminals); filament voltage control, capable of being adjusted to 0.1 V secondary voltage change; and a filament current meter-desirable but optional.

A means must be provided to hold filament voltage constant. If the filament voltage is permitted to vary in accordance with primary line voltage fluctuation, the effect on tube life can be devastating. An acceptable solution is the use of a ferroresonant transformer or line regulator. This accessory is offered by some transmitter manufacturers as an option and should be seriously considered if a tube life extension program is planned.

## Transmitter housekeeping

Once the transmitter has been place in operation, tube life is in the hands of the chief engineer. The first action to prolong tube life falls into the category of routine maintenance. Most transmitter manufac-

Fig. 1. Probabillty of extended Ilfe service can be determined from this graph. Divide the average p.a. plate current in amperes by the product of fllament voltage and current. The resulting amperes/watt ratlo ( $Y$-axis) is prolected horizontally to the appropriate curve. The vertical projection to the $X$-axis indicate the life extension probability.


# Extending Transmitter Tube Life 



Figure 3


Flgure 4


Figure 5
turers have a routine maintenance schedule established in the equipment manual. This procedure must be followed carefully if operating costs are to be held to a minimum. During routine maintenance it is very important to look for tube and socket discoloration, either of which can indicate overheating.

Look for discoloration around the top of the cooler near the anode core and at the bottom of the tube stem where the filament contacts are made. Review Figures 2 and 3 for examples of a tube operating with inadequate cooling. It is possible for discoloration to appear in the areas mentioned if the transmitter has to operate in a dirty environment. If this is the case, the tube should be removed and cleaned with a mild detergent. After cleaning, the tube should be rinsed thoroughly to remove any detergent residue and blown dry with compressed air. If the discoloration remains, this is an indication that the tube has operated at too high a temperature. Check inlet and outlet air ducting and filters for possible air restriction. It may also be necessary to verify that the air blower is large enough to do the job in the present environment and that it is operating at rated capacity.

With the tube removed, the socket should be blown or wiped clean and carefully inspected. Any discoloration in the socket finger stock caused by overheating could contribute to early tube failure. A finger stock that loses its temper through prolonged operation at high temperature will no longer make contact to the tube elements (Figure 4). A well-maintained socket will score the tube contacts when the tube is inserted. If all fingers are not making contact, more currect flows through fewer contacting fingers, causing additional overheating and possible burnout (Figure 5).

## Filament voltage management

The useful operating life of a thoriated tungsten emitter can vary widely with filament voltage. Figure 6 describes the relative life expectancy with various filament voltage levels. Obviously, a well-managed filament voltage program will result in longer life expectancy. Improper management, on the other hand, can be very costly.

For a better understanding of this sensitive aging mechanism, the filament itself must be understood. Most filaments in high-power, gridded tubes are a mixture of tungsten and thoria with a chemical com-

Fig. 2. Improper cooling means short tube life (left). Discoloration of metal around inner filament stem and anode fins indicates poor cooling or improper operation of tube. Properly cooled and operated tube (right) shows no discoloration after many hours of use. In both cases, good socketing is indicated by scoring on circular connector rings.
Fig. 3. Dirty and discolored cooler of amplifier tube at left indicates combination of discoloration due to heating and lack of cleaning. Tube has operated too hot and dust has collected in anode louvres.
Fig. 4. Minute scoring in base contact rings indicates that socket finger stock has made good, low-resistance contact to tube elements. Well-maintained socket will score the tube contacts when tube is inserted. If all fingers do not make contact, more current will flow through fewer contact fingers, causing additional overheating and burning, as shown in Fig. 5.
FIg. 5. High resistance socket contacts has caused severe burning of contact area in the base. Overheated base caused early demise of tube.

## Extending Transmitter Tube Life

position of $\mathrm{W}+\mathrm{THO}_{2}$. A filament made of this wire is not a suitable electron emitter for extended life applications until it is processed. Once the filament is formed into the desired shape and mounted, it is heated to approximately $2100^{\circ} \mathrm{C}$ in the presence of a hydrocarbon. The resulting thermochemical reaction forms di-tungsten carbide on the filament's surface. Life is proportional to the degree of carburization. If the filament is overcarburized, however, it will be brittle and easily broken during handling and transporting. Therefore, only approximately $25 \%$ of the cross-sectional area of the wire is converted to ditungsten carbide. Di-tungsten carbide has a higher resistance than tungsten; thus, the reaction can be carefully monitored by observing the reduction in filament current as the carburizing process proceeds.
As the tube is used the filament slowly decarburizes. At some point in life, all of the di-tungsten carbide layer is depleted and the reduction of thoria to free
thorium stops. The filament is now decarburized and is no longer an effective electron emitter.

The key to extending the life of a thoriated tungsten filament emitter is to control operating temperature. Emitter temperature is a function of the total RMS power applied to the filament. Thus, filament voltage control is temperature control. Temperature varies directly with voltage. As the emitter temperature rises the de-carburizing process is accelerated and tube life shortened. Figure 6 shows that useful tube life can vary significantly with only a $5 \%$ change in filament voltage. If the filament voltage cannot be regulated to within $\pm 3 \%$, the filament should always be operated at the rated nominal voltage. The danger of operating on the "cold" temperature side is that the emitter may be "poisoned." A cold filament acts as a getter; that is, it attracts contaminants. When a contaminant becomes attached to the surface of the emitter, that area is rendered inactive and loss of emission results. Operation of the filament at slightly below rated nominal voltage, however, can extend tube life if done properly.

## FILAMENT VOLTAGE MANAGEMENT (Figure 6)

Filament voltage management allows extended tube life when accompanied by a continuing housekeeping program. When fllament voltage is too high (dashes), power tube looses emission rapldly and normal operating life is not achleved. When fllament is operated at rated voltage (black curve) normal tube life is achleved In a majority of cases. With a filament voltage management program (bullets), extended tube life may be achieved. When the minimum required output power level is finally reached (right-hand portion of curve), the filament voltage may be raised to rated value, or above, to achieve addltional useful operating life. If filament is run "cool" (stars), extremely short life will result. Note that filament voltage management program does not take effect until about 200 hours of operating time have passed.
If voltage management program Is not undertaken, tube should be run at rated filament voltage.


## Extending Transmitter Tube Life

Of great importance to long tube life is the temperature of the elements and the ceramic-to-metal seals. Element temperature can be held within proper limits by observing the maximum dissipation ratings listed in the data sheet. Seal temperature should be limited to $200^{\circ} \mathrm{C}$ at the lower anode seal under worst-case conditions. As element temperature rises beyond $200^{\circ} \mathrm{C}$, the release of contaminants locked in the materials used in tube manufacturing increases rapidly. These contaminants cause a rapid depletion of the di-tungsten carbide layer of the filament.
When a new power tube is installed in a transmitter, it must be operated at rated nominal filament voltage for the first 200 hours. This procedure is very important for two reasons. First, operation at normal temperature allows the getter to be more effective during the early period of tube life when contaminants are more prevalent. This break-in period conditions the tube for operation at lower filament voltage to obtain longer filament life. Secondly, during the first 200 hours of operation filament emission increases. It is necessary for the life extension program to start at the peak emission point.
A chart recorder or other device should be used to monitor variations in primary line voltage for several days of transmitter operation. The history of line voltage variations during on-air time must be reviewed prior to derating filament voltage. Plan to establish the derated voltage during the time period of historically low line voltage, as this is the worst-case condition. If line variation is greater that $\pm 3 \%$, filament voltage must be regulated.

Record output power (FM) or distortion level (AM) with the tube operating at rated nominal filament voltage. Next, reduce filament voltage in increments of 0.1 V and record power or distortion levels at each increment. Allow one minute between each increment for the filament emission to stabilize.

When a noticeable change occurs in output power or the distortion level changes, the derating procedure must stop. Obviously, operation at this point is unwise since there is no margin for a drop in line voltage. It is safer to raise the voltage 0.2 V above the critical voltage at which changes are observed to occur. If this new filament voltage setting is more than $5 \%$ below the nominal rated level, filament voltage must be raised to the $95 \%$ level. Operation below this point is unpredictable and life expectancy is uncertain. Finally, recheck power output or distortion to see if they are acceptable at the chosen filament voltage level. Recheck again after 24 hours to determine if emission is stable and that the desired performance is maintained. If performance is not repeatable, the derating procedure must be repeated.

## Continuing the program

The filament voltage should be held at the properly derated level as long as minimum power or maximum distortion requirements are met. Filament voltage can
be raised to reestablish minimum requirements as necessary. This procedure will yield results similar to those shown in the illustration, to achieve as much as $10 \%$ to $15 \%$ additional life extension. When it becomes necessary to increase filament voltage, it is a good time to order a new tube. Filament voltage can be increased as long as the increase results in maintaining minimum level requirements.
When an increase fails to result in meeting a level requirement, filament emission must be considered inadequate and the tube should be replaced. Don't discard it or sell it for scrap! Put it on the shelf and save it. It will serve as a good emergency spare and may come in very handy some day. Also, in AM transmitters, a low-emission RF amplifier tube can be shifted to modulator use where the peak filament emission requirement is not as severe.
Start planning for longer tube life now! Review the following steps you can take:

- Investigate the manufacturer's ratings on the power tubes in your present equipment, or the transmitter you plan to buy.
- Check that your transmitter has sufficient headroom. Is there a margin of safety in tube operation?
- Look for important instrumentation in the next transmitter you buy. Are all tube elements monitored for voltage and current in the transmitter?
- Whether your transmitter is new or old, start a filament life extension program.
Remember that each time you replace a power tube, the recommended derating procedure must be rerun. Voltage levels required with one tube do not apply to a replacement tube.
When purchasing a tube, insist on a new tube that carries the full, original manufacturer's warranty. Only tubes manufactured by the company of origin have to perform to published data. This is the important reason that transmitter manufacturers buy new, warranted tubes from the original manufacturer. BM/E

Thanks to William Barkley, William Orr, William Sain, and Bob Tornoe, all of Varian EIMAC, for their help and suggestions in preparing this paper.

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The $7203 / 4 \mathrm{CX} 250 \mathrm{~B}$ and $8621 / 4 \mathrm{CX} 250 \mathrm{FG}$ are ceramic/metal forced-air cooled, external-anode radial-beam tetrodes with a maximum plate dissipation rating of 250 watts and a maximum input-power rating of 500 watts. The $7203 / 4 \mathrm{CX} 250 \mathrm{~B}$ is designed to operate with a heater voltage of 6.0 volts, while the $8621 / 4 \mathrm{CX} 250 \mathrm{FG}$ is designed for operation at a heater voltage of 26.5 volts. Otherwise, the two tube types have identical characteristics.

## GENERAL CHARACTERISTICS1

## ELECTRICAL

Cathode: Oxide Coated, Unipotential
Heater: Voltage (4CX250B)
$6.0 \pm 0.3 \mathrm{~V}$
Current, at 6.0 volts 2.6 A

Cathode-Heater Potential, maximum ........ $\pm 150$ V
Heater: Voltage (4CX250FG) . . . . . . . . . . . . . . . . . . . $26.5 \pm 1.3 \mathrm{~V}$
Current, at 26.5 volts
0.54 A

Cathode-Heater Potential , maximum. . . . . . . . $\quad \pm 150 \mathrm{~V}$

Amplification Factor (Average):
Grid to Screen ..... 5
Direct Interelectrode Capacitances (Grounded cathode) ${ }^{2}$
Input ..... 15.7 pF
Output ..... 4.5 pF
Feedback ..... 0.04 pF
Direct Interelectrode Capacitances (grounded grid and screen) ${ }^{2}$
Input ..... 13 pF
Output ..... 4.5 pF
Feedback ..... 0.01 pF
Frequency of Maximum Rating:
CW500 MHz1. Characteristics and operating values are based upon performance tests. These figures may change without noticeas the result of additional data or product refinement. EIMAC Division of Varian should be consulted before usingthis information for final equipment design.
2. In Shielded Fixture.
MECHANICAL
Maximum Overall Dimensions:
Length ..... $2.46 \mathrm{in} ; 62.5 \mathrm{~mm}$
Diameter ..... $1.64 \mathrm{in} ; 41.7 \mathrm{~mm}$
Net Weight ..... gm
Any
Operating PositionMaximum Operating Temperature:Ceramic/Metal Seals$250^{\circ} \mathrm{C}$
Anode Core ..... $250^{\circ} \mathrm{C}$
Cooling ..... Forced Air
Base Special 9-pin JEDEC-B8-236
Recommended Socket EIMAC SK-600 SeriesRecommended ChimneyEIMAC SK-600 Series

## RADIO FREQUENCY LINEAR AMPLIFIER GRID DRIVEN (SSB)

| Class $\mathrm{AB}_{1}$ |  |
| :---: | :---: |
| MAXIMUM RATINGS |  |
| DC PLATE VOLTAGE | 2000 VOLTS |
| dC SCREEN VOLTAGE | 400 VOLTS |
| DC GRID Voltage | -250 VOLTS |
| DC PLATE CURRENT | 0.25 AMPERE |
| PLATE DISSIPATION | 250 WATTS |
| SCREEN DISSIPATION | 12 WATTS |
| GRID DISSIPATION | 2 WATTS |

## RADIO FREQUENCY LINEAR AMPLIFIER <br> GRID DRIVEN, CARRIER CONDITIONS <br> Class $\mathrm{AB}_{1}$

MAXIMUM RATINGS

| DC PLATE VOLTAGE . . . . . . . . . . . . | 2000 VOLTS |
| :--- | :--- |
| DC SCREEN VOLTAGE . . . . . . . . | 400 VOLTS |
| DC GRID VOLTAGE . . . . . . . . . | -250 VOLTS |
| DC PLATE CURRENT . . . . . . . . . | 0.25 AMPERE |
| PLATE DISSIPATION . . . . . . . . | 250 WATTS |
| SCREEN DISSIPATION . . . . . . . . | 12 WATTS |
| GRID DISSIPATION . . . . . . . . . | 2 WATTS |

```
            2 WATTS
```

| Plate Voltage | 1000 | 1500 | 2000 | Vdc |
| :---: | :---: | :---: | :---: | :---: |
| Screen Voltage | 350 | 350 | 350 | Vdc |
| Grid Voltage 1. | -55 | -55 | -55 | Vdc |
| Zero-Signal Plate Current. | 100 | 100 | 100 | mAdc |
| Single Tone Plate Current | 250 | 250 | 250 | mAdc |
| Two-Tone Plate Current | 190 | 190 | 190 | mAdc |
| Single-Tone Screen Current ${ }^{2}$ | 10 | 8 | 5 | mAdc |
| Two-Tone Screen Current? | 2 | -1 | -2 | mAdc |
| Single-Tone Grid Current? | 0 | 0 | 0 | mAdc |
| Peak rf Grid Voltage2 | 50 | 50 | 50 | , |
| Plate Output Power | 120 | 215 | 300 | W |
| Resonant Load Impedance | 2000 | 3000 | 4000 | $\Omega$ |

1. Adjust to specified zero-signal dc plate current. 2. Approximate value.

## RADIO FREOUENCY POWER AMPLIFIER OR OSCILLATOR

Class C Telegraphy or FM Telephony
(Key-Down Conditions)

## MAXIMUM RATINGS

| dC plate voltage | 2000 VOLTS |
| :---: | :---: |
| dC Screen voltage | 300 VOLTS |
| DC GRID VOLTAGE | -250 VOLTS |
| dC PLATE CURRENT | 0.25 AMPERE |
| PLATE DISSIPATION | 250 WATTS |
| SCREEN DISSIPATION | 12 WATTS |
| GRID DISSIPATION | 2 watts |

TYPICAL OPERATION (Frequencies to 175 MHz ) Class $A B_{1}$, Grid Driven

| Plate Voltage . . . . . . . . . . . | 1000 | 1500 | 2000 | Vdc |
| :--- | :--- | ---: | ---: | ---: |
| Scr een Voltage. . . . . . . . | 350 | 350 | 350 | Vdc |
| Grid Voltage 1. . . . . . . . | -55 | -55 | -55 | Vdc |
| Zero-Signal Plate Current . . . | 100 | 100 | 100 | mAdc |
| Carrier Plate Current . . . . . | 150 | 150 | 150 mAdc |  |
| Carrier Screen Current . . . . . | -3 | -4 | -4 | mAdc |
| Peak rf Grid Voltage 2. . . . . | 25 | 25 | 25 | V |
| Plate Output Power . . . . . . | 30 | 50 | 65 | W |

1. Adjust to specified zero-signal dc plate current
2. Approximate value.

| PLATE MODULATED RADIO FREQUENCY POWER AMPLIFIER-GRID DRIVEN <br> Class C Telephony (Carrier Conditions) |  |
| :---: | :---: |
| maximum ratings |  |
| DC PLATE VOLTAGE | 1500 VOLTS |
| DC SCREEN VOLTAGE | 300 VOLTS |
| DC GRID VOLTAGE | -250 VOLTS |
| DC PLATE CURRENT | 0.20 AMPERE |
| PLATE DISSIPATION1. | 165 WATTS |
| SCREEN DISSIPATION2 | 12 WATTS |
| GRID DISSIPATION2 | WAT |

1. Corresponds to 250 watts at $100 \%$ sine-wave modulation.
2. Average, with or without modulation.

## TYPICAL OPERATION (Frequencies to 175 MHz )

| Plate Voltage | 500 | 1000 | 1500 Vdc |
| :---: | :---: | :---: | :---: |
| Screen Voltage | 250 | 250 | 250 Vdc |
| Grid Voltage | -100 | -100 | -100 'Vdc |
| Plate Current | 200 | 200 | 200 mAdc |
| Screen Current | 31 | 22 | 20 mAdc |
| Grid Current | 15 | 14 | 14 mAdc |
| Peak rf Grid Voltage | 118 | 117 | 117 v |
| Calculated Driving Power | 1.8 | 1.7 | 1.7 W |
| Plate Input Power | 100 | 200 | 300 W |
| Plate Output Power | 60 | 145 | 235 W |


| AUDIO FREQUENCY POWER AMPLIFIER |  |
| :---: | :---: |
| OR MODULATOR <br> Class AB , Grid Driven (Sinusoidal Wave) |  |
| MAXIMUM RATINGS (Per |  |
| DC PLATE VOLTAGE | 2000 VOLTS |
| DC SCREEN VOLT AGE | 400 VOLTS |
| DC GRID VOLTAGE | -250 VOLTS |
| DC PLATE CURRENT. | 0.25 Ampere |
| PLATE DISSIPATION | 250 WATTS |
| SCREEN DISSIPATION | 12 WATTS |
| GRID DISSIPATION | 2 WATTS |

1. Approximate value.
2. Per Tube.

## TYPICAL OPERATION (Two Tubes)

| Plate Voltage | 1000 | 1500 | 2000 | Vdc |
| :---: | :---: | :---: | :---: | :---: |
| Screen Voltage | 350 | 350 | 350 | Vdc |
| Grid Voltage 1/3 | -55 | -55 | -55 | Vdc |
| Zero-Signal Plate Current | 200 | 200 | 200 | mAdc |
| Max Signal Plate Current | 500 | 500 | 500 | mAdc |
| Max Signal Screen Current 1 | 20 | 16 | 10 | mAdc |
| Max Signal Grid Current1. | 0 | 0 | 0 | mAdc |
| Peak af Grid Voltage 2. | 50 | 50 | 50 | $\checkmark$ |
| Peak Driving Power | 0 | 0 | 0 | W |
| Plate Input Power | 500 | 750 | 1000 | W |
| Plate Output Power | 240 | 430 | 600 | w |
| Load Resistance (plate to plate) | 3500 | 6200 | 9500 | $\Omega$ |

3. Adjust to give stated zero-signal plate current.
RANGE VALUES FOR EQUIPMENT DESIGNHeater: 4CX250B Current at 6.0 volts
Heater: 4 CX 250 FG Current at 26.5 voltMin. Nom. Max.$\begin{array}{rrr}2.3 & -- & 2.9 \\ 0 & \text { A }\end{array}$Heater: 4CX250FG Current at 26.5 volts0.45 --- 0.62 A ..... $30 \quad 60$--- sec.
Cathode Warmup Time
Cathode Warmup Time
Interelectrode Capacitances ${ }^{1}$ (grounded cathode connection)
Input14.2--- 17.2 pF14.24.0$--\quad 5.0 \mathrm{pF}^{\mathrm{t}}$Output0.06 pF
Feedback--
Interelectrode Capacitances 1 (grounded grid and screen)--- 13.0
Input .
Output ..... 4.0

## MECHANICAL

mounting - The 4CX250B and 4CX250FG may be operated in any position. An EIMAC Air-System Socket, SK-600 series, or a socket having equivalent characteristics, is required. Sockets are available with or without built-in screen capacitors and may be obtained with either grounded or ungrounded cathode terminals.

COOLING - Sufficient forced-air cooling must be provided for the anode, base seals, and body seals to maintain operating temperatures below the rated maximum values. Air requirements to maintain anode core temperatures at $200^{\circ} \mathrm{C}$ with an inlet air temperature of $50^{\circ} \mathrm{C}$ are tabulated below. These requirements apply when a socket of the EIMAC SK-600 series and an EIMACSK-606 chimney are used with air flow in the base to anode direction.

| SEA LEVEL |  |  | 10,000 FEET |  |
| :---: | :---: | :---: | :---: | :---: |
| Plate <br> Dissipa- <br> tion(watts) | Air Flow <br> (CFM) | Pressure <br> Drop(In.of <br> water) | Air Flow <br> (CFM) | Pressure <br> (rop(In.of <br> water) |
| 200 | 5.0 | 0.52 | 7.3 | 0.76 |
| 250 | 6.4 | 0.82 | 9.3 | 120 |

The blower selected in a given application must be capable of supplying the desired airflow at a back pressure equal to the pressure drop shown above plus any drop encountered in ducts and filters. The blower must be designed to deliver the air at the desired altitude.

At 500 MHz or below, base cooling air requirements are satisfied automatically when the tube is operated in an EIMAC Air-System Socket and the recommended air flow rates are used. Experience has shown that if reliable long life operation is to be obtained, the cooling air flow must be maintained during standby periods when only the heater voltage is applied to the tube. The anode cooler should be inspected periodically and cleaned when necessary to remove any dirt which might interfere with effective cooling.

VIBRATION - These tubes are capable of satisfactorily withstanding ordinary shock and vibration, such as encountered in shipment and normal handling. The tubes will function well in automobile and truck mobile installations and similar environments. However, when shock and vibration more severe than this are expected, it is suggested that the EIMAC 4CX300A or 4 CX 250 R be employed.

ELECTRICAL
HEATER - The rated heater voltage for the 4 CX 250 B and 4 CX 250 FG is 6.0 volts and 26.5 volts, respectively, and the voltage should be maintained as closely as practicable. Short-time changes of $\pm 10 \%$ will not damage the tube, but variations in performance must be expected. The heater voltage must be maintained within $\pm 5 \%$ to minimize these variations and to obtain maximum tube life.

At frequencies above approximately 300 MHz transit-time effects begin to influence the cathode temperature. The amount of driving power diverted to heating the cathode by back-bombardment will depend upon frequency, plate current, and driving power. When the tube is driven to maximum input as a class-C amplifier, the heater voltage should be reduced according to the table below;

| Frequency MHz | $4 \mathrm{C} \times 250 \mathrm{~B}$ | $4 \mathrm{C} \times 250 \mathrm{FG}$ |
| :--- | :--- | :--- |
| 300 and lower | 6.00 volts | 26.5 volts |
| 301 to 400 | 5.75 volts | 25.3 volts |
| 401 to 500 | 5.50 volts | 24.3 volts |

CATHODE OPERATION - The oxide coated unipotential cathode must be protected against excessively high emission currents. The maximum rated dc input current is 200 mA for platemodulated operation and 250 mA for all other types of operation except pulse.

The cathode is internally connected to the four even-numbered base pins and all four of the corresponding socket terminals should be used to make connection to the external circuits. At radio frequencies it is important to keep the cathode leads short and direct and to use conductors with large areas to minimize the inductive reactances in series with the cathode leads.

It is recommended that rated heater voltage be applied for a minimum of 30 seconds before other operating voltages are applied. Where the circuit design requires the cathode and heater to be operated at different potentials, the rated maximum heater-to-cathode voltage is 150 volts regardiess of polarity.

GRID OPERATION - The maximum rated dc grid bias voltage is -250 volts and the ma ximum grid dissipation rating is 2.0 watts. In ordinary audio and radio-frequency amplifiers the grid dissipation usually will not approach the maximum rating. At operating frequencies above the 100 MHz region, driving-power requirements for
amplifiers increase noticeably. At 500 MHz as much as 20 watts of driving power may have to be supplied. However, most of the driving power is absorbed in circuit losses other than grid dissipation, so that grid dissipation is increased only slightly. Satisfactory 500 MHz operation of the tube in a stable amplifier is indicated by grid-current values below approximately 15 mA .

The grid voltage required by different tubes may vary between limits approximately $20 \%$ above and below the center value, and means should be provided in the equipment to accommodate such variation. It is especially important that variations between individual tubes be compensated when tubes are operated in parallel or push-pull circuits, to assure equal load sharing.

The maximum permissible grid-circuit resistance per tube is 100,000 ohms.

SCREEN OPERATION - The maximum rated power dissipation for the screen is 12 watts, and the screen input power should be kept below that level. The product of the peak screen voltage and the indicated dc screen current approximates the screen input power except when the screen current indication is near zero or negative.

In the usual tetrode amplifier, where no signal voltage appears between cathode and screen, the peak screen voltage is equal to the dc screen voltage.

When signal voltages appear between screen and cathode, as in the case of screen-modulated amplifiers or cathode-driven tetrode amplifiers, the peak screen-to-cathode voltage is the sum of the dc screen voltage and the peak ac or rf signal voltage applied to screen or cathode.

Protection for the screen should be provided by an over-current relay and by interlocking the screen supply so that plate voltage must be applied before screen voltage can be applied.

The screen current may reverse under certain conditions and produce negative current indications on the screen milliammeter. This is a normal characteristic of most tetrodes. The screen power supply should be designed with this characteristic in mind so that the correct operating voltage will be maintained on the screen under all conditions. A current path from screen to cathode must be provided by a bleeder resistor, gaseous voltage regulator tubes, or an electron
tube shunt regulator connected between screen and cathode and arranged to pass approximately 15 milliamperes per connected screen. An electron tube series regulator can be used only when an a equate bleeder resistor is provided.

Self-modulation of the screen in plate-modulated tetrode amplifiers using these tubes may not be satisfactory because of the screen-voltage screen-current characteristics. Screen modulation from a tertiary winding on the modulation transformer or by means of a small separate modulator tube will usually be more satisfactory. Screenvoltage modulation factors between 0.75 and 1.0 will result in $100 \%$ modulation for plate-modulated rf amplifiers using the 4 CX 250 B or 4 CX 250 FG .
PLATE OPERATION - The maximum rated plate dissipation power is 250 watts. In platemodulated applications the carrier plate dissipation power must be limited to 165 watts to avoid exceeding the plate dissipation rating with $100 \%$ sine wave modulation. The maximum dissipation rating may be exceeded for brief periods during circuit adjustment without damage to the tube.
MULTIPLE OPERATION - Tubes operating in parallel or push-pull must share the load equally. It is good engineering practice to provide individual metering and individual adjustment of bias or screen voltage to equalize the inputs.

Where overload protection is provided, it should be capable of protecting the surviving tube(s) in the event that one tube fails.
VHF OPERATION-The 4CX250B and 4CX250FG are suitable for use in the VHF region. Such operation should be conducted with heavy plate loading, minimum bias, and the lowest driving power consistent with satisfactory performance. It is often preferable to operate at a sacrifice in efficiency to obtain increased tube life.
HIGH VOLTAGE - The 7203/4CX250B and $8621 / 4 \mathrm{CX} 250 \mathrm{FG}$ operate at voltages which can be deadly, and the equipment must be designed properly and operating precautions must be followed. Equipment must be designed so that no one can come in contact with high voltages. All equipment must include safety enclosures for high-voltage circuits and terminals, with interlock switches to open the primary circuits of the power supplies and to discharge high-voltage condensers whenever access doors are opened. Interlock switches must not be bypassed or "cheated" to allow operation with access doors open. Always remember that HIGH VOLTAGE CAN KILL.
SPECIAL APPLICATIONS-If it is desired to operate these tubes under conditions widely different from those given here, write to Application Engineering Dept., EIMAC Division of Varian, San Carlos, Calif. 94070 for infomation and recommendations.



## PIN DESIGNATION



| DIMENSIONAL DATA |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| DIM. | INCHES |  | MILLIMETERS |  |
|  | MIN | MAX | MiN | MAX. |
| A | 2.342 | 2.464 | 59.03 | 62.59 |
| B | 1.610 | 1.640 | 40.89 | 41.66 |
| C | 1.810 | 1.910 | 45.97 | 48.51 |
| D | 0.750 | 0.810 | 19.05 | 20.57 |
| E | 0.710 | 0.790 | 18.03 | 20.07 |
| F | -- | 1.406 | -- | 35.71 |
| G | 0.187 | -- | 4.75 | -- |
| H | BASE: |  |  |  |
|  | B8-236 |  |  |  |
| J | 0.559 | 0.573 | 14.20 | 14.55 |
| K | 0.240 | -- | 6.10 | -- |



## techmical data

The EIMAC $8281 / 4 \mathrm{CX} 15,000 \mathrm{~A}$ is a ceramic/metal power tetrode intended for use in audio or radio frequency applications. It features a new type of internal mechanical structure which results in higher rf operating efficiency. Low rf losses in this mechanical structure permit operation of the $8281 / 4 \mathrm{CX15}, 000 \mathrm{~A}$ at full ratings up to 110 MHz , and at reduced ratings, to 225 MHz .

The $8281 / 4 \mathrm{CX15,000}$ is also recommended for radio-frequency linear power amplifier service, and for VHF television linear amplifier service.

## GENERAL CHARACTERISTICS 1

## electrical

Filament: Thoriated Tungsten
Voltage
$6.3 \pm 0.3 \mathrm{~V}$
Current, at 6.3 volts 160 A
Amplification Factor, average
Grid to Screen
4.5

Direct Interelectrode Capacitances (cathode grounded): ${ }^{2}$
Cin
160.0 pF

Cout 24.5 pF

Cgp 1.5 pF

Direct Interelectrode Capacitances (grid and screen grounded): ${ }^{2}$
Cin . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 67.0 pF
Cout 25.5 pF

Cpk 0.2 pF
Maximum Frequency Ratings
CW110 MHz

1. Characteristics and operating values are based on performance tests. These figures may change without notice as the result of additional data or product refinement. EIMAC Division of Varian should be consulted before using this information for final equipment design.
2. Capacitance values are for a cold tube as measured in a special shielded fixture in accordance with Electronic Industries Association Standard RS-191.

## MECHANICAL

## Maximum Overall Dimensions:

Length . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $9.375 \mathrm{in} ; 238.13 \mathrm{~mm}$

Diameter. $7.580 \mathrm{in} ; 192.53 \mathrm{~mm}$
Net Weight $12.8 \mathrm{lb} ; 5.81 \mathrm{~kg}$
Operating Position Axis vertical, base up or down

## Cooling

Forced air
Operating Temperature, maximum
Ceramic/Metal Seals and Anode Core . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $250^{\circ} \mathrm{C}$
Base Special, concentric
Recommended Air System Socket SK-300A
Recommended Air Chimney SK-316

## RADIO FREQUENCY LINEAR AMPLIFIER GRID DRIVEN, Class AB1

## ABSOLUTE MAXIMUM RATINGS

| DC PLATE VOLTAGE | 10,000 | VOLTS |
| :---: | :---: | :---: |
| DC SCREEN VOLTAGE | 2000 | VOLTS |
| DC PLATE CURRENT | 6.0 | AMPERES |
| PLATE DISSIPATION | 15,000 | WATTS |
| SCREEN DISSIPATION | 450 | WATTS |
| GRID DISSIPATION | 200 | WATTS |

1. Adjust for specified zero-signal plate current.
2. Approximate value.

TYPICAL OPERATION
Peak Envelope or Modulation Crest Conditions

| Plate Voltage | 7,500 | 10,000 | Vdc |
| :---: | :---: | :---: | :---: |
| Screen Voltage | 1.500 | 1,500 | Vdc |
| Grid Voltage 1 | -350 | -370 | Vdc |
| Zero-Signal Plate Current | 1.0 | 1.0 | Adc |
| Single-Tone Plate Current | 4.0 | 4.25 | Adc |
| Single-Tone Screen Current 2 | 170 | 150 | mAd |
| Peak rf Grid Voltage ? | 330 | 340 | $v$ |
| Plate Dissipation | 12.2 | 14.0 | kW |
| Single-Tone Plate Output Power | 20.8 | 28.5 | kW |
| Resonant Load Impedance | 865 | 1,260 | $\Omega$ |

RADIO FREOUENCY POWER AMPLIFIER OR

## OSCILLATOR

Class C Telegraphy or FM Telephony
(Key-Down Conditions)

## ABSOLUTE MAXIMUM RATINGS

| dC plate voltage | 10,000 | VOLTS |
| :---: | :---: | :---: |
| dC SCREEN VOLTAGE | 2000 | VOLTS |
| DC PLATE CURRENT | 5.0 | AMPERES |
| PLATE DISSIPATION | 15,000 | WATTS |
| SCREEN DISSIPATION | 450 | WATTS |
| GRID DISSIPATION | 200 | WATTS |

TYPICAL OPERATION

| Plate Voltage | 7,500 | 10,000 | Vdc |
| :---: | :---: | :---: | :---: |
| Screen Voltage | 750 | 750 | Vdc |
| Grid Voltage | -510 | -550 | $V \mathrm{dc}$ |
| Plate Current | 4.65 | 4.55 | Adc |
| Screen Current 1. | 0.59 | 0.54 | Adc |
| Grid Current ${ }^{1}$. | 0.30 | 0.27 | Adc |
| Peak of Grid Voltage ${ }^{\text {1 }}$ | 730 | 790 | $\checkmark$ |
| Calculated Driving Power | 220 | 220 | w |
| Plate Dissipation | 8.1 | 9.0 | kW |
| Plate Output Power | 26.7 | 36.5 | kW |
| 1. Approximate value. |  |  |  |

## PLATE MODULATED RADIO FREQUENCY POWER AMPLIFIER

GRID DRIVEN Class C Telephony
(Carrier Conditions)
ABSOLUTE MAXIMUM RATINGS

| DC PLATE VOLTAGE . . . . . . . . . . | 8000 VOLTS |
| :--- | :--- |
| DC SCREEN VOLTAGE . . . . . . . | 1500 VOLTS |
| DC PLATE CURRENT . . . . . . . | 4.0 AMPERES |
| PLATE DISSIPATION . . . . . . . . | 1000 WATTS |
| SCREEN DISSIPATION . . . . . . . | 450 WATTS |
| GRID DISSIPATION . . . . . . . . . | 200 WATTS |

TYPICAL OPERATION

| Plate Voltage | 6,000 | 8,000 | Vdc |
| :---: | :---: | :---: | :---: |
| Screen Voltage | 750 | 750 | Vdc |
| Grid Voltage | -600 | -640 | Vdc |
| Plate Current | 3.75 | 3.65 | Adc |
| Screen Current! | 0.45 | 0.43 | Adc |
| Grid Current ${ }^{1}$. | 0.18 | 0.18 | Adc |
| Peak af Screen Voltage 1 |  |  |  |
| Peak if Grid Voltage 1. | 800 | 840 | $v$ |
| Calculated Driving Power | 150 | 150 | W |
| Plate Dissipation | 5.1 | 5.8 | kW |
| Plate Output Power | 17.4 | 23.5 | kW |
| 1. Approximate value. |  |  |  |


| AUDIO FREQUENCY POWER AMPLIFIER OR MODULATOR | TYPICAL OPERATION (Two tubes) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| GRID DRIVEN, Class AB1 (Sinusoidal Wave) | Plate Voltage | 7,500 | 10,000 | Vdc |
|  | Screen Voltage | 1,500 | 1,500 | Vdc |
| ABSOLUTE MAXIMUM RATINGS (per tube) | Grid Voltage 1. | -350 | -370 | Vdc |
|  | Zero-Signal Plate Current ${ }^{3}$. | 1.00 | 1.00 | Adc |
| DC Plate voltage . . . . . . . . . 10.000 Volts | Maximum Signal Plate Current | 8.80 | 8.50 | Adc |
| dC Screen voltage . . . . . . . . . 2000 Volts | Maximum Signal Screen Current 2. | 0.34 | 0.30 | Adc |
| DC PLATE CURRENT . . . . . . . . . 6.0 AmPERES | Peak af Grid Voltage 2. . . . . . 3 | 330 | 340 | $v$ |
| PLATE DISSIPATION . . . . . . . . . 15,000 WATTS | Maximum Signal Plate Dissipation 3 Plate Output Power | 12.2 | 14.0 |  |
| SCREEN DISSIPATION . . . . . . . . 450 WATTS | Load Resistance |  |  |  |
| GRID DISSIPATION . . . . . . . . . 200 WATTS | (plate to plate) | 1,730 | 2,520 | $\Omega$ |
|  | 1. Adjust for specified zero-signal plate current. <br> 2. Approximate value. <br> 3. Per Tube. |  |  |  |

## TELEVISION LINEAR AMPLIFIER <br> Cathode Driven

ABSOLUTE MAXIMUM RATINGS

| 110 MHz to 225 MHz |  |  |
| :---: | :---: | :---: |
| DC Plate voltage | 6500 | VOLTS |
| DC SCREEN VOLTAGE | 1500 | VOLTS |
| DC PLATE CURRENT | 5.0 | AMPERES |
| PLATE DISSIPATION | 15,000 | WATTS |
| SCREEN DISSIPATION. | 450 | watts |
| GRID DISSIPATION | 200 | WATTS |


| TYPICAL OPERATION, Composite Signal Black Level Unless Otherwise Stated |  |  |  |
| :---: | :---: | :---: | :---: |
| Plate Voltage | 5000 | 6000 |  |
| Screen Voltage | 500 | 700 | Vd |
| Grid Voltage | -160 | -180 | Vd |
| Plate Current (zero sig.) | . 500 | . 650 | Ad |
| Plate Current | 2.800 | 3.335 | Ad |
| Grid Current | . 075 | . 035 | Ad |
| Screen Current | . 060 | . 040 | Ad |
| Peak Cath. Volt. (pk synch.) | 310 | 345 | $v$ |
| Cath. Driving Power (pk. synch.) | 975 | 1350 |  |
| Plate Output Power (pk. synch.) | 11.0 | 16.5 |  |
| Plate Load Resistance | 600 | 60 |  |

1. Approximate value.

TYPICAL OPERATION values are obtained by calculations from published characteristic curves. To obtain the specified plate current at the specified bias, screen, and plate voltages, adjustment of the rf grid voltage is assumed. If this procedure is followed, there will be little variation in output power when the tube is replaced, even though there may be some variation in grid and screen currents. The grid and screen currents which occur when the desired plate current is obtained are incidental and vary from tube to tube. These current variations cause no performance degradation providing the circuit maintains the correct voltage in the presence of the current variations. If grid bias is obtained principally by means of a grid resistor, the resistor must be adjustable to produce the required bias voltage when the correct rf grid voltage is applied.

## RANGE VALUES FOR EQUIPMENT DESIGN

Heater Current, at 6.3 volts
Min.
152 $\frac{\text { Max. }}{168 \mathrm{~A}}$

Interelectrode Capacitances, cathode grounded ${ }^{1}$
Cin
$154.0 \quad 167.0 \mathrm{pF}$
Cout $22.0 \quad 27.0 \mathrm{pF}$
Cgp
2.0 pF

Interelectrode Capacitances, grid and screen grounded 1
Cin
$62.0 \quad 72.0 \mathrm{pF}$
Cout $23.0 \quad 28.0 \mathrm{pF}$
Cpk 0.3 pF

1. Capacitance values are for a cold tube as measured in a special shielded fixture in accordance with Electronic Industries Association Standard RS-191.

## MECHANICAL

APPLICATION
MOUNTING - The 4CX15,000A must be operated with its axis vertical. The base of the tube may be down or up at the convenience of the circuit designer.
SOCKET - The EIMAC Air-System Socket Type SK-300A is designed especially for the concentric base terminals of the $4 \mathrm{CX} 15,000 \mathrm{~A}$. The use of recommended air-flow rates through this socket provides effective forced-air cooling of the tube. Air forced into the bottom of the socket passes over the tube terminals and through the SK-316 Air Chimney, into the anode cooling fins.
COOLING - The maximum temperature rating for the extemal surfaces of the 4CX15,000A is $250^{\circ} \mathrm{C}$. Sufficient forced-air circulation must be provided to keep the temperature of the anode at the base of the cooling fins and the temperature of the ceramic/metal seals below $250^{\circ} \mathrm{C}$. Air-flow requirements to maintain seal temperatures at $225^{\circ} \mathrm{C}$ in $50^{\circ} \mathrm{C}$ ambient air are tabulatted below (for operation below 30 megahertz). This data is for the tube mounted in an SK-300A socket with an SK-316 chimney.

| SEA LEVEL |  |  | 10.000' FEET |  |
| :---: | :---: | :---: | :---: | :---: |
| Plate <br> Dissipation <br> (Watts)Air Flow <br> (CFM) | Pressure <br> (ropl(Inches <br> of Water) | AII Flow <br> (CFM) | Pressure <br> (rop(Inches <br> of Water) |  |
| 7.500 | 230 | .7 | 336 | 1.0 |
| 12.500 | 490 | 2.7 | 710 | 4.1 |
| 15.000 | 645 | 4.6 | 945 | 7.0 |

*Since the power dissipated by the filament represents about 1000 watts and since grid-plus-screen dissipation can, under some conditions, represent another 600 watts, allowance has been made in preparing this tabulation for an additional 1600 watts dissipation.

The blower selected in a given application must be capable of supplying the desired air flow at a back pressure equal to the pressure drop shown above plus any drop encountered in ducts and filters.

At other altitudes and ambient temperatures the llow rate must be modified to obtain equivalent cooling. The flow rate and corresponding pressure differential must be determined individually in such cases, using rated maximum temperatures as the criteria for satisfactory cooling.

## ELECTRICAL

FILAMENT OPERATION - The rated filament voltage for the 4 CX15,000A is 6.3 volts. Filament voltage, as measured at the socket, should be maintained at this value to obtain maximum tube life. In no case should it be allowed to deviate by more than plus or minus five percent from the rated value.

ELECTRODE DISSIPATION RATINGS - The maximum dissipation ratings for the $4 \mathrm{CX} 15,000 \mathrm{~A}$ must be respected to avoid damage to the tube. An exception is the plate dissipation which may be permitted to rise above the rated maximum during brief periods, such as may occur during tuning.

GRID OPERATION - The 4CX15,000A control grid has a maximum dissipation rating of 200 watts. Precautions should be observed to avoid exceeding this rating. The grid bias and driving power should be kept near the values shown in the "Typical Operation" sections of the data sheet whenever possible. The maximum grid circuit resistance should not exceed 100,000 ohms per tube.

SCREEN OPERATION - The power dissipated by the screen of the $4 \mathrm{CX15,000A}$ must not exceed 450 watts.

Screen dissipation, in cases where there is no AC applied to the screen, is the simple product of the screen voltage and the screen current. If the screen voltage is modulated, the screen dissipation will depend upon loading, driving power, and carrier screen voltage.

Screen dissipation is likely to rise to excessive values when the plate voltage, bias voltage, or plate load are removed with filament and screen voltages applied. Suitable protective means must be provided to limit the screen dissipation to 450 watts in the event of circuit failure.

PLATE DISSIPATION - The plate-dissipation rating for the $4 \mathrm{CX} 15,000 \mathrm{~A}$ is 15,000 watts.

When the $4 \mathrm{CX} 15,000 \mathrm{~A}$ is operated as a platemodulated rf power amplifier, the input power is limited by conditions not connected with the plate efficiency, which is quite high. Therefore, except during tuning there is little possibility that the 10,000 watt maximum plate dissipation rating will be exceeded.

HIGH VOLTAGE - Normal operating voltages used with the $4 C X 15,000 A$ are deadly, and the equipment must be designed properly and operating precautions must be followed. Design all equipment so that no one can come in contact with high voltages. All equipment must include safety enclosures for high-voltage circuits and terminals, with interlock switches to open primary circuits of the power supply and to dis charge high-voltage condensers whenever access doors are opened. Interlock switches must not be bypassed or "cheated" to allow operation with access doors open. Always remember that HIGH VOLTAGE CAN KILL.

X-RADIATION - High-vacuum tubes operating at voltages higher than 10 kilovolts produce progressively more dangerous X -ray radiation as the voltage is increased. The $4 \mathrm{CX} 15,000 \mathrm{~A}$, operating at its rated voltages and currents, is a potential X-ray hazard. Only limited shielding is afforded by the tube envelope. Moreover, the X -ray radiation level can increase significantly with aging and gradual deterioration, due to leakage paths or emission characteristics as they are affected by the high voltage. X-ray shielding must be provided on all sides of tubes operating at these voltages to provide adequate protection throughout the tube's life. Periodic checks on the X-ray level should be made, and the tube should never be operated without adequate shielding in place when voltages above 10 kilovolts are in use. Lead glass, which attenuates X-rays, is available for viewing windows. If there is any doubt as to the requirement for or the adequacy of shielding, an expert in this field should be contacted to perform an X-ray survey of the equipment.

Operation of high-voltage equipment with interlock switches "cheated" and cabinet doors open in order to be better able to locate an equipment malfunction can result in serious X-ray exposure.

RADIO FREQUENCY RADIATION - Avoid exposure to strong if fields even at relatively low frequency. Absorption of rf energy by human tissue is dependent on frequency. Under 30 MHz , most of the energy will pass completely through the human body with little attenuation or heating effect. Public health agencies are concerned with the hazard, however, even at these frequencies, and it is worth noting that some commercial dielectric heating units actually operate at frequencies as low as the 13 and 27 MHz bands.

Many EIMAC power tubes, such as the 4CX $15,000 \mathrm{~A}$, are specifically designed to generate or amplify radio frequency power. There may be a relatively strong rf field in the general proximity of the power tube and its associated circuitry --. the more power involved, the stronger the rf field. Proper enclosure design and efficient coupling of rf energy to the load will minimize the rf field in the vicinity of the power amplifier unit itself.

INTERELECTRODE CAPACITANCE - The actual internal interelectrode capacitance of a tube is influenced by many variables in most applications, such as stray capacitance to the chassis, capacitance added by the socket used, stray capacitance between tube terminals, and wiring effects. To control the actual capacitance values within the tube, as the key component involved, the industry and the Military Services use a standard test procedure as described in Electronic Industries Association Standard RS-191. This requires the use of specially constructed test fixtures which effectively shield all external tube leads from each other and eliminates any capacitance reading to "ground".

The test is performed on a cold tube. Other factors being equal, controlling internal tube capacitance in this way normally assures good interchangeability of tubes over a period of time, even when the tube may be made by different manufacturers. The capacitance values shown in the manufacturer's technical data, or test specifications, normally are taken in accordance with Standard RS-191.

The equipment designer is therefore cautioned to make allowance for the actual capacitance values which will exist in any normal application. Measurements should be taken with the socket and mounting which represent approximate final layout if capacitance values are highly significant in the design.

SPECIAL APPLICATIONS - If it is desired to operate this tube under conditions widely different from those given here, write to the Application Engineering Dept., Power Grid Tube Division, EIMAC Division of Varian, 301 Industrial Way, San Carlos, Califomia, 94070 for information and recommendations.

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